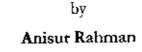
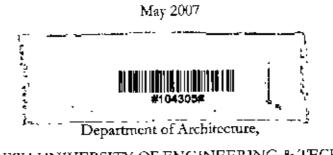
PERFORMANCE EVALUATION OF SHADING DEVICES USED IN TALL OFFICE BUILDINGS OF DHAKA CITY





A thesis submitted in partial fulfilment of the requirement for the degree of

MASTER OF ARCHITECTURE



BANGLADESH UNIVERSITY OF ENGINEERING & TECHNOLOGY,

Dhaka, Bangladesh

The thesis titled **"PERFORMANCE EVALUATION OF SHADING DEVICES USED IN TALL OFFICE BUILDINGS OF DHAKA CITY"** Submitted by Anisur Rahman, Roll No. 040301008[P], Session April 2003, has been accepted as satisfactory in partial fulfilment of the requirement for the degree of **MASTER OF ARCHITECTURE** on this day 9th May, 2007.

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ABSTRACT

One of the characteristics of tall office buildings in Dhaka city is the extensive use of glazing on the building facades. This increasing use of glass has caused considerable changes in the relationship between interior and ambient climate, where the problem of overheating has become a major concern. So facades of tall buildings need protection from solar heat gain to achieve desirable indoor environment and to reduce the energy consumption in the buildings by the air conditioning system. External shading devices can be utilised to block the solar radiation before it teaches the window surface and hence more effective than internal shading devices.

The problem was approached by performance evaluation of selected commonly used shading devices of tall office buildings through simulation study. Shadow simulation allows study of the effect of changes in one aspect, keeping other factors constant. The observations of simulated performance that occurs due to changing parameters allow the identification of elements, the reduction or introduction of which in the design contribute to solar heat gain. Through simulation study, it is possible to analyse the performance of shading devices for any period of the year. The simulation studies were conducted for the months from March to September representing hot-dry and warmhumid period, which is most significant in terms of climatic severity. The simulation studies were performed to evaluate performances of shading devices and identify the effects of different parameters and correlation among parameters in terms of reducing solar heat gain. This study also helped to understand the influence of window orientation on the performance of shading devices.

After all the investigations and critical evaluations, a parametric study to explore the strategies for optimum shading was pursued through a series of simulations as solar geometry is a predictable phenomenon and much of its impact is quantifiable. Parametric study allows study of various alternatives with reference to performance of the model and identifying the best one. Based on the parametric study, design recommendations and design guidelines were derived.

The findings of this thesis are concerned with the problem of solar heat gain in tall office buildings in tropical climate like Dhaka city. The results of the simulation studies and parametric studies have been expressed in terms of a number of climate responsive shading design guidelines. It is expected that the application of these guidelines will reduce solar heat gain in comparison to that of present practices.

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Dedicated to my parents

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I am very much grateful to my supervisor Dr. Khandaker Shabbir Ahmed, Associate Professor, Department of Architecture, Bangladesh University of Engineering & Technology, for his excellent supervision, wise guidance and inspiration throughout the thesis work. From him, I have learned the art and skills of conducting a research and more importantly the way of thought.

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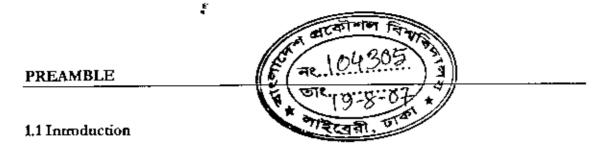
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CHAPTER: ONE PREAMBLE

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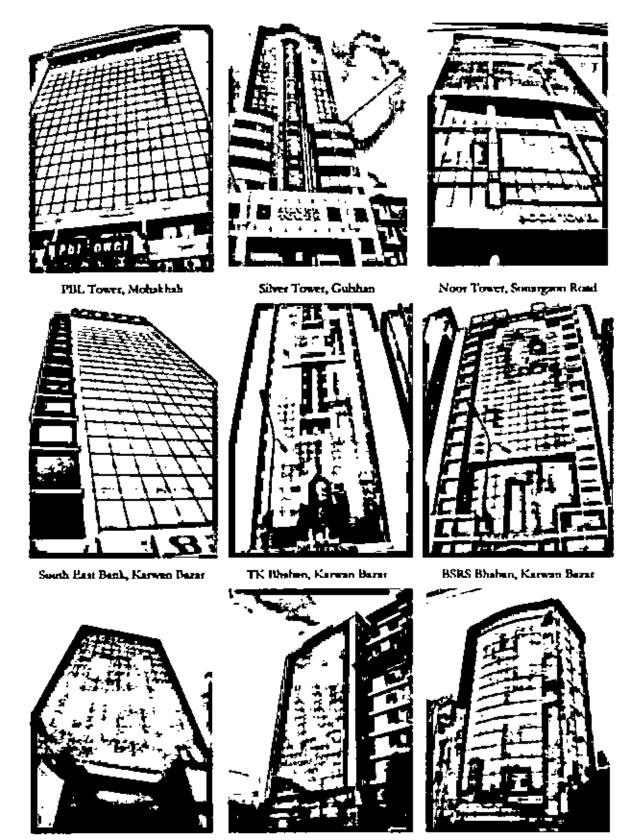
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The trend of recent development has shifted from low to high-rise buildings due to the pressure of population in much of the world, and Dhaka is no exception (Ahmed, 2003). Construction of tall office buildings in urban areas of Dhaka is characterized by extensive use of glass. These glass facades remain unprotected or bately protected from the scorehing solar radiation of the tropics. These often lead to green house like simanon (Givoni, 1969).

Along with the high out door air temperature, solar radiation is a major source of heat gain for building in tropics (Koenigsberger et al, 1973). Vast vertical surfaces of tall buildings are exposed to solar radiation and glass facades may act as heat trap for incoming solar radiation (Ahmed, 2003). So facades of tall buildings need protection in view of generating desirable indoor environment. Solar radiation transmitted through unprotected windows or transparent walls also cause a great increase in the cooling requirements of an air-conditioned building of high air temperatures in buildings without mechanical cooling systems (Stephenson et al, 1962; Goulding et al, 1992). This heat is particularly unwanted in summer and has to be expelled by the cooling system.

Solar radiation gain may be reduced by intercepting the radiation before it reaches the building surface. External solar shading can be beneficial in preventing unwanted solar heat gain thus reducing cooling load and thus can enhance thermal comfort. Moreover, the thermal effect of a glazed wall section depends on the shading provided and the spectral properties of glass (Givoni, 1969). Shading the glass affects the property of incident radiation and hence modifies both the heat flow to the intenor and the indoor temperature.

Limitation of energy resources and evet increasing energy prices and the global warming, the necessity to reduce the energy consumption in the buildings can be an important issue in a developing country like Bangladesh. In such a context the need to develop passive means of solar control is important and efficient design of shading devices may address this issue significantly.



UTC, Panthapeth

Haq Chumber, Penthapath

CADD Tower, Panthapath



1.2 Statement of the Problem

A good answer to overheating problems is controlling solar radiation incident on the buildings. Using solar-protective glazing is one simple solution which can be easily integrated into the building design (Olgyay and Olgyay 1957). One major drawback of solar-protective glass is that it reduces solar gains in the building even during winter-time. Therefore, in countries with dominant heating requirements, a moveable device is a hetter solution (Dubois 1999). But again manual control of movable shading devices is not reliable and may cause a constant disruption for the occupants and most of the people of our country can't afford the system of dynamic control of motorized shading devices. Shading provision should be considered as an integral part of fenestration system design, especially for facades with high solar gains. Shading devices may control solar gains, block direct sunlight and transmit diffuse daylight in the room, climinating glare and high contrast and creating a pleasant luminous environment (Haque, 2004). It is necessary, on the one hand, to classify the shading devices by their geometric characteristics; on the other hand, to analyse their energy and luminous performance through the definition of man made parameters and calculation methodology.

In the context of Dhaka, there is no tested rule for shading devices. According to construction act, 1952 (E.B. Act II of 1953) section 18, (Rajuk, 1996) which is enforced by RAJUK, it is said that maximum depth of shading device will not exceed 0.5 m over compulsory setback areas. But this rule may not have come from any investigation or analysis of shading performance nor any comparative study and evaluation for different climatic situations. Therefore, buildings are being constructed without proper attention to the performance of shading devices.

Due to our increased concern about energy efficient buildings and thermal comfort as well, experiments and analysis should be made for different types of shading devices. By thorough study of the relationship between depth and other parameters of shading device and amount of shade that cast on the windowpane, which is essential for thermal comfort and exclude heat gain (energy consumption) from solar radiation should be established and eventually incorporated in the design process.

1.3 Objectives of the Study

The study is an attempt to investigate the performance of commonly applied shading devices on facades of tall office buildings as a method of passive cooling with the following objectives:

- To evaluate the existing shading devices as solar control tool used in tall office buildings.
- To assess the impact of shading device on indoor environment as they relate to the solar heat.
- To propose a guideline for designing efficient shading device for control of solar radiation in tall office buildings.

1.4 Methodology

To achieve the above objectives the methodology that was followed for the entire work is stated below.

The problem was approached first by a survey of published information that provided the knowledge base for the research and information about the state of the art regarding solar shading systems. By theoretical studies the meaning and purpose of solar shading device was explored. Moreover, this study helped in analyzing factors influencing solar heat gain. The climatic characteristics of Dhaka City were studied to set the climatic imperatives with regard to solar heat gain in tall office buildings in Dhaka City.

A physical survey was conducted to record and to identify the characteristics and performance of commonly applied shading devices in reference to tall office buildings. It helped in forming the models for simulation study.

The simulation process was pursued in two phases. The first one was conducted to ascertain the performance of commonly used solar shading devices in reducing solar radiation gain. Simulation models with the external shading devices similar to the real ones in tall office buildings were simulated for different orientations. By the simulation study findings and results was analyzed to identify the effects of different parameters and correlation among parameters in terms of reducing solar heat gain. The second stage

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involved a parametric study pursued through series of simulations to explore possible climatically sensitive design guideline for solar shading device.

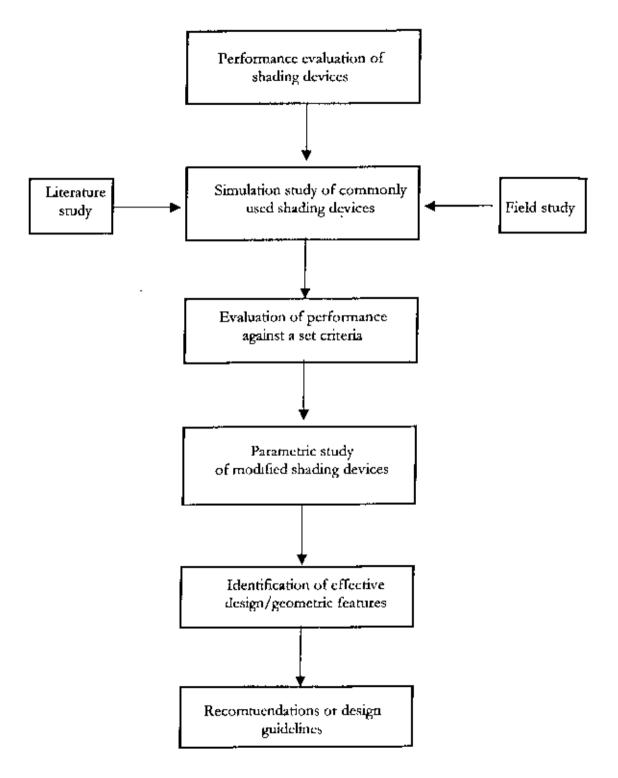


Figure 1.2: Structure of the work.

1.5 Scope and Limitations

The research work presented in this study concentrates on performance evaluation of various shading devices in reducing solar heat gain in the tall office buildings in Dhaka city. Although solar heat gain is a combined effect of direct radiation from the Sun and diffuse radiation reflected from surrounding environment, most of the solar heat gain to buildings is caused by direct radiation through windows. The study is limited to the role of geometry of the shading devices to cut off direct solar radiation hence reducing solar heat gain. Recommendations and design guidelines are made regarding geometry of shading devices. Other aspects like material of the devices, installation or construction systems are not considered in this research.

Besides, shading device has impact on daylight, ventilation and view through window. The performance of shading devices regarding daylight, ventilation and other aspects are beyond the scope of this research.

With these opportunities and constrains, research on performance of shading devices with special reference to Dhaka city was carried out and described in the following chapters.

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CHAPTER: TWO THE CLIMATIC CONTEXT: DHAKA CITY

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THE CLIMATIC CONTEXT: DHAKA CITY

Amongst the innumerable constraints that the Architect faces during the design of buildings, climate probably is considered as one of the major factors. The climate of a region presents a set of conditions, which need to be addressed adequately in order to produce climate-responsive buildings. Climate-responsiveness results in comfortable, energy-efficient, environmentally friendly buildings. Buildings constructed without regard to surrounding climate can, no doubt, operate given enough energy input to correct resulting problems, whether they concern over heating, or darkness. But access to such energy is beyond the reach of much of the population of developing countries.

The chosen location for this work is Dhaka, the capital city of Bangladesh. The country is surrounded by India on the west, north and north-east. The Bay of Bengal bounds it in the south and with Myanmar on its south-eastern part. The geographic location of Dhaka is, longitudes: 90° East- 90°30' East and latitudes: 23°40' North - 23° 55' North.

The following section is concerned with the analysis of climate of Dhaka city in terms of its challenges and potentials. This analysis will help to determine the climatic forces to be manipulated to provide satisfactory design solutions for tall structures in tropical situations from the view point of energy efficiency.

2.1 Climate of Bangladesh - General Overview

The climate of Bangladesh is categorized as warm-humid, based on the widely used classification of tropical climate by Atkinson (Koenigsberger *et al*, 1973). There are three distinctive seasons, the hot humid, the hot dry and the cool dry season (Reported in, Mallick, 1994). Generally, the winter is short and dry while the summer is long and wet. The hot dry period is between Match and May, the hot humid period covers June to September and the cold dry seasons starts from mid October to February.

Again, meteorologically the climate of Bangladesh is classified into four distinct seasons – winter, pre-monsoon, monsoon and post- monsoon (Reported in, Ahmed, 1995), where the winter is cool and dry, the pre-monsoon is hot and dry; monsoon and post-monsoon are hot and wet. The winter months, December to February, are characterized by infrequent rains, cold northerly winds, mean temperature 21°C and mean maximum below 26°C. The premonsoon period covers the months March, April and May and is characterized by occasional thunderstorms, and an average maximum temperature of 34°C. The monsoon is the longest season covering the months June to September, a period with torrential rains, with the average relative humidity above 80% and an average temperature of 31°C. The post-monsoon season ranges between the months October and November. It is also regarded as a transitional (to winter) period with infrequent rains and temperatures below 30°C.

2.2 Microclimate of Dhaka City

The climatic characteristics of Dhaka city differ from that of other cities of the country due to its dense physical developments and location. Again, within the same city these characteristics are further modified in different locations (Ahmed, 1995). It is due to the surface quality of the area – hard or soft, density of built environment, building type, building height and their orientations, proximity between buildings, material used for construction, dependence on electrical and mechanical appliances and other related factors.



Figure 2.1: Dhaka city: view of Dilkusha commercial area.

Clanatic period	Hot-Dry	Wat	m-Humid	Cool Dry
Months	March-May	June-Sept (Monsoon)	Oct-Nov (Port-Moesoon)	Dec-Feb (Winter)
Climatic Factors		(MIDELICOL)		(
1. Air Temperature (*c)				
a. Maximum	37.80	36.10	34.90	32.40
b. Minimum	13.80	20.90	13.30	6.80
c. Ävenge	28.02	28.8	25.42	19.43
d. Diurnal variation (average)	11.60	7.12	11	14
2. Relative Humidity % [average]	69.91	64.78	82.59	76.70
3. Rainfull (mm) (average)	156.70	317,50	125	23.33
4. Global Radiation (W/m²) [average]	495	373	412	431
5. Sunshine Hours (daily average)	7	4.5	7	8
6. Wind Speed (m/s) [average]	2.6	2.2	1.5	1.5
7. Wind Direction	5, S-H	S, S-E, S-W	S, S-E	N, N-W

Table 2.1: Climatic data of Dhaka.

(Seenc Khee, 2005)

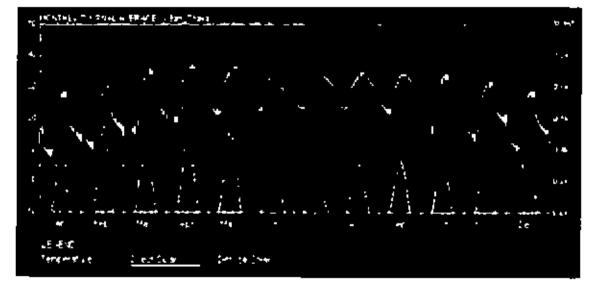


Figure 2.2: Yearly weather data showing temperature profile and solar radiation (Fiend Weather Tesl serger).

2.2.1 Temperature

On the basis of meteorological data, the temperature profile of Dhaka city shows similarity with that of the regional pattern. The highest temperature is recorded in the

month of March, April and May, which reaches to 37.8°C maximum in April. In the monsoon and post monsoon period, from June to October the temperature remains steady at an average of 28.8°C. In cool period it drops to 19.43°C on average (Fable 2.2).

	Jan	Feb	Mar	Apr	Ma	Jun]ոյ	Aug	Sep	Oct	Nov	Dec
Mean maximum air	26.2	27 9	32.3	342	33.0	31.8	31.2	31.1	31.7	313	28.8	26.4
temp (deg C)							ļ					-
Average air temp	19.0	21.2	260	29.0	29.0	28.8	28.7	28.6	28.8	27.5	23.5	19.8
(deg C)												
Mean minimum air	11.8	145	197	23.8	25.0	25.8	26.2	26.1	25.9	23.7	18 2	13.2
temp (d⊨g C)												

Table 2.2: Air temperature in Dhaka city.

(Source: Climate Division, Bangladesh Meteorological Department, Dhaka, 2005)

Overheating due to inexorable urban growth of Dhaka city is now a major environmental concern (Ahmed, 1995). Meteorological observation in pre-monsoon period records a maximum temperature of 37.8°C, indicating a possible trend towards the increase of temperature and overheating.

2.2.2 Solar Radiation

Solar radiation can be considered as a single most deciding factor for assessing the climate of an area, because it affects the temperature and density of air and thus affects the wind velocity, direction and humidity (Ahmed, 1994). Renewable Energy Research Center of Dhaka University collects radiation data for Dhaka city.

Figure 2.3 shows that in the hot dry period, particularly in the months of March, April and May solar radiation is high in comparison with that in the rest of the year and it is maximum in April (5.5 KWh/sqm/day). From July to November (monsoon to postmonsoon) the radiation remains fairly constant.

From Figure 2.4 it has been observed that, the horizontal surface (commonly the roof surface of a built form) receives the maximum amount of solar radiation round the year in comparison with other common external vertical facades. But this is true for low rise buildings only. For tall buildings, horizontal surface is very negligible in comparison to other four vertical surfaces and only the top floors of the tall buildings are affected by



incurring radiation on the roof of the buildings. This result depicts the importance of adopted strategy for vertical surfaces of the built forms in tropical architecture.

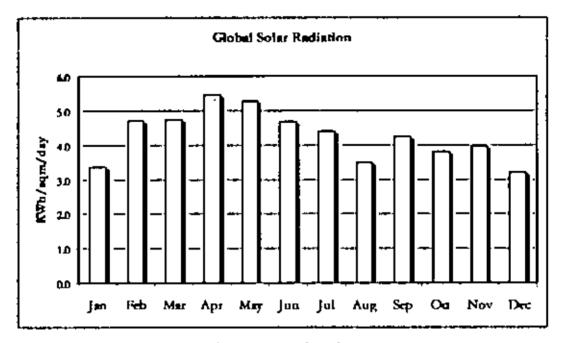


Figure 2.3: Monthly average daily solar radiations in Dhaka (Secure Records Europy Remote Grant, Dhaka (Jainesis), 2005).

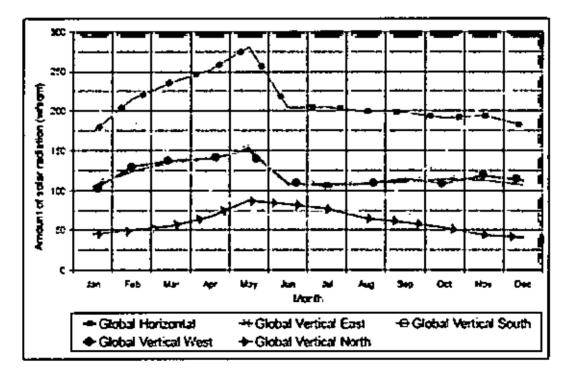


Figure 2,4: Amount of solar radiation on different surfaces (horizontal and vertical) for a year (Sume Klum, 2005).

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As overheating is one of the key problems for the given climate, the issue of heat gain from solar radiation is highly significant and the vertical surfaces are observed as more important than horizontal surfaces of the built forms (for tall buildings, specially when the suo is at a low angle).

2,2,3 Relative Humidity

The humidity of Dhaka city is high and the mean annual relative humidity is 77% (Table 2.4). If all conditions remain the same, then the relative humidity is inversely proportional to the temperature. So, higher temperature yields lower relative humidity levels. Since air temperature and radiation depend on the density of the built form, the humidity varies with the density of the surrounding built environment.

Table 2.4: Relative humidity in Dhaka city.

	Jan	Feb	Mar	Apr	Ma	Jun	ไฑ	Aug	Sep	Oct	Nov	Dec
Relative Humidity	69%	63%	61%	70%	79%	85%	86%	85%	86%	81%	75%	78%

(Source: Chmate Dunsion, Bangladesh Meteorological Department, Dhaka, 2005)

2.2.4 Cloud Coverage

The cloud cover is only 38% for the whole pre-monsoon and post-monsoon period (Table 2.5). This clear sky condition enhances the direct solar radiation to reach on building surfaces. The cloud coverage is very high in monsoon period and is almost 70%. The cloudy atmospheric condition during this period helps in decreasing the incoming solar radiation to the earth surface.

Table 2.5: Sky condition in respect to cloud cover for a year.

Type of Sky	Hot-Dry	Hot-	Cool-Dry	
	Pre-Monsoon	Monsoon	Post-Monsoon	(Dec-Feb)
	(March-May)	(June-Sept)	(Oct-Nov)	
Clear Sky	67%	31%	64%	85%
Overcast Sky	33%	69%	36%	15%

(Source: Climate Division, Bangladesh Meteorological Department, Dhaka, 2005)

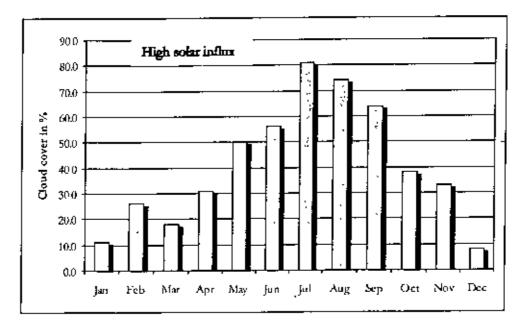


Figure 2.5: Monthly average cloud cover (Source: Chinate Division, Bangladesh Meteorological Department, Dhaka, 2005).

2.2.5 Sunshine Hours

The amount of solar radiation received by the surfaces also depends on the duration of sunshine (Reported in, Ahmed, 1994). The sunshine hour in pre-monsoon and postmonsoon is quite long than that of monsoon period (Figure 2.6).

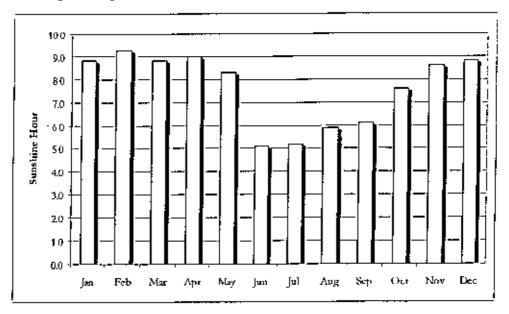


Figure 2.6: Monthly average sunshine hours (Source: Chemate Division, Bangladesh Meteorological Department, Diaka, 2005).

Wind speed in Dhaka in Hot period is relatively high and the direction is predominantly southerly and south-easterly (Table 2.5). For winter period the direction of wind was found mostly from north and north-west. According to the diurnal pattern of wind flow, in summer (except April) the wind speed is low between 42:00 and 15:00 hours (Reported in, Ahmed, 1995). During that period airflow may not be considered as reliable resource for cooling, rather depending on shading of surface from solar radiation would be more preferable.

Months and seasons	Wind speed in m/s	Wind direction		
January (Cool-Dry)	1.4	NW.		
February (Cool-Dry)	1.6	N		
March (Hot-Dry)	2.6	sw		
April (Hot-Dry)	3.7	SW		
May (Hot-Dry)	4.4	S		
June (Warm-Humid)	3.8	SE		
July (Warm-Humid)	3.9	SE		
August (Warm-Humid)	3.3	SE		
September (Warm-Humid)	34	SE		
October (Warm-Humid)	2 5	N		
November (Warm-Humid)	1.4	NW		
December (Cool-Dry)	1.5	NW		

Table 2.5: Monthly average wind speed and direction.

(Source, Chmate Division, Bangladesh Meteorological Department, Dhaka, 2005)

2.3 Problems in Designing in the Hot-Humid Climate

The hot-humid climatic zone is characterized by high ambient temperatures, high humidity, high and fairly evenly distributed rainfall, small diurnal and annual variations of temperature, little seasonal variation, light winds, and long periods of still air.

The physiological thermal requirements and hence the building characteristics are the same for the whole year, as the seasonal climatic variations are low (Yeang, 1990). The main cause of discomfort is the subjective feeling of skin we mass (Koenigsberger et al,

1973). Continuous ventilation is, therefore required to ensure a sweat evaporation rate sufficient to maintain thermal equilibrium and minimum sweat accumulation of the skin. Radiation solar heat gain should be prevented.

The hot-humid zones present two problems to designers:

- Avoidance of excessive solar radiation, and
- Provision for moisture evaporation by breezes.

To cope with these, the structures and settlements need to be built to allow free air movement. The roofs need to be insulated and provided with large overhangs to protect against sun and rain.

Under hot conditions, the thermal controls in the building should:

- Prevent heat gain.
- Maximise heat loss
- Remove any excess heat by mechanical or passive cooling.

2.4 Conclusion

Although for most of the period, overheaning is a major environmental concern for Dhaka, the nature of the problem is dictated by the combination of the environmental factors in the ambiance during those periods. From March to May there is high air temperature associated with high solar radiation, while from June to October, conditions with high humidity is associated with high air temperature. So from March to May, reducing the impact of solar tadiation can potentially moderate the overheated condition and optimizing shading can play a vital role towards moderation. For a tropical warm humid climate like Dhaka city the minimum solar heat gain with the help of adequate shading is the major considerations to achieve thermal comfort.

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CHAPTER: THREE TALL BUILDING AND SOLAR HEAT GAIN

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TALL BUILDING AND SOLAR HEAT GAIN

Increased land value, limited urban accessibility, expanding urban population, globalization of national economy and locational preferences of business make the tall building inevitable. In addition to accommodating living space for the purpose of habitation, tall buildings are now extensively used as working space. Although the principles of designing with climate are relatively advanced for low-rise and mid-nise buildings, adequate attention and research yet to be directed towards the tall building type (Yeang, 1990). A brief discussion on tall and high-rise buildings, with special reference to their climatic characteristics has been presented in the following sections.

3.1 Tall Building

3.1.1 Definition

The experts differ in defining the physical parameters of tall buildings. According to the Council for Tall Buildings and Urban Habitat (CTBUH), a tall building is not strictly defined by the number of stories or its height. It also depends upon the context in which it stands. CTBUH defines tall buildings as a building whose built form, by virtue of its height, requires its own special engineering systems (Yeang, 1997). The important criterion is whether or not the design, use or operation of the building is influenced by some aspects of tallness.

As stated by Eli Attia in his seminar paper in 'Fourth World Congress on Tall Building: 2000 and beyond' David Fisher defines the tall buildings as 'We build tall buildings of necessity; how we build them is a reflection of society. Tall buildings do not have to be beautiful, they simply must be functional; so it is the degree of our concern for their beauty that serves as a measure of our humanity' (Attia, 1990).

According to Ken Yeang (Yeang, 1997), a tall building can be characteristics by

- a) A small foot-print in comparison to its total built-up space
- b) Tall facades due to its height
- c) Small roof-area in comparison to external-wall area
- d) Special engineering systems, different from the low building type simply because of its height.

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According to Taranath, to define tall building from structural aspects, from structural design and construction point of view, it is simpler to consider a building tall when its structural analyses and design are in some way affected by the lateral loads (Taranath, 1998).

3.1.2 Justifications for Designing with Climate

Ken Yeang (Yeang, 1990) justifies the reasons for designing the tall buildings with climate very clearly. The most obvious justification must be the lowering of costs as a result of lowering the energy consumption in the operation of the building. This can be by as much as 40% of the overall life-cycle energy costs of the building. Significant savings in operational costs would justify incorporation of climatically-responsive design features despite a higher initial capital construction costs.

Another rationale is from the impact on the users of the tall building. The climateresponsive tall building would enhance its users' aesthetic well-being while enabling them to be aware of and to experience the external climate of the place. The climateresponsive design would provide the building's users with the opportunity to experience the external environment (and the diumal and seasonal changes where existent) and avett the blindness of spending their working hours over a significant part of their day in an artificial environment that remains constant throughout the year.

A further justification is the ecological one. Designing with climate would result in the reduction of the overall energy consumption of the building by the use of passive structural devices (i.e. non-mechanical). Cost savings in the operational costs means less use of electrical energy resources which is usually derived from the butning of non renewable fossil-fuels. The lowering of energy consumption would further reduce the overall emission of waste heat thereby lowering the overall heat-island effect on the locality.

3.1.3 Façade Design of Tall Buildings in Tropical Climates

In passive low-energy tall building design, attention should be given to the facade design. For low volume-to-surface ratio, tall buildings have more external surface than same volume of low rise building. In case of tall buildings, generally facades do not get mutual shading from its surrounding like low rise buildings. That's why; external surfaces of tall buildings should be designed as an environmentally-responsive filter.

The façade should be multi-functional in its design. For instance, it can provide for reducing solar heat gain to the space through external shading devices, fresh air ventilation, acoustic barrier, maintenance access and a contribution to the building's aesthetic.

Tall buildings are exposed more directly than others to the full impact of external temperatures and direct sunlight. The greatest source of heat gain in the tropical climate can be the solar radiation entering through the window. This solar heat gain can be reduced by using shading devices. These shading devices cut the huge solar heat gains directly through window. This enables the designer to use clear-glass, to give better daylight entering the internal spaces, which then reduces the lighting energy-load (Yeang, 1997).

3.2 Solar Radiation

Solar radiation influences the indoor thermal climate by direct heating on penetrating the windows, and indirectly by heating the external envelope of the building. Heat flow through the wall and roof then determines the indoor surface and air temperatures. The effect of solar radiation on internal temperatures, as mentioned at the beginning, may be divided into two parts: 1) the effect on the temperatures of the external surfaces and roof and the resulting heat flow and indoor heating, 2) heating caused by penetration of radiation through glazed or open areas (Givoni, 1969).

Solar radiation is an electromagnetic radiation emitted from Sun (McMullan, 1992). The Spectrum is broadly divided into two regions i.e. the visible radiation and non-visible radiation. Solar radiation teaching the earth's surface consists of about 47 percent visible, 48 percent short-wave infra-red (heat), and about 5 percent ultra violet radiation (Lechner, 2001).

Sunlight contains no heat, both in the visible region and in the non-visible region (mainly infra-red with some ultra-violet) in about equal proportions. It is only when radiation falls on surfaces that it is converted into heat. The non-visible part of the spectrum often

referred to as 'thermal radiation', implying that only this part is the cause of heating. But the visible part still carries half the energy that potentially can become heat (Steemers et al, 2002).

3.2.1 Visible Radiation

The wavelengths of electromagnetic radiation that are visible to the eye range from approximately 380 nm to 760 nm [1 nanometre (nm) is 10⁻⁹ meter]. If all the wavelengths of light are seen at the same time the eye cannot distinguish the individual wavelengths and the brain has the sensation of white light (McMullan, 1992).

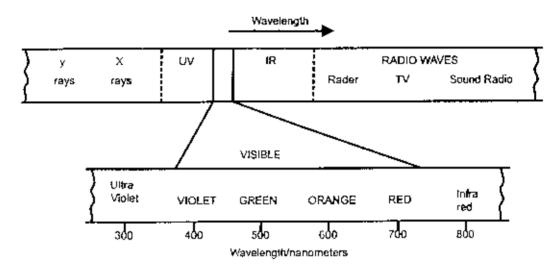


Figure 3.1: Electromagnetic spectrum (Source: McMullan, 1992).

White light is the effect on sight of combining all the visible wavelengths of light. White light can be separated into its component wavelengths. One method is to use the different refractions of light that occur in a glass prism. The result is a spectrum of light, which is traditionally described in the seven colours of the rainbow although, in fact, there is a continuous range of hues (colours) whose different wavelengths cause different sensanons in the brain. Monochromatic light is light of one particular wavelength and colour 1f the colours of the spectrum are recombined then white light is again produced. Varying the proportions of the individual colours can produce different qualities of 'white' light.

3.2.2 Non-Visible Radiation

Electromagnetic radiations with wavelengths outside the range of visible wavelengths cannot, by definition, be detected by the human eye. However, those radiations immediately adjacent to the visible range of wave lengths are emitted by the Sun, along with light, and are often relevant to lighting processes (McMullan, 1992).

Infra-Red

Wavelength range of infra-red is from 760 nm to above. Infra-red (IR) radiation has wavelengths slightly greater than those of red light and can be felt as heat radiation from the Sun and from other heated bodies. Infra-red radiation is made use of in radiant heating devices, for detecting patterns of heat emissions, for 'seeing' in the dark, and for communication links.

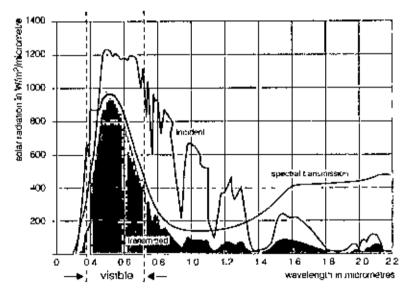


Figure 3.2: Solar spectrum (Source: Stemeers et al, 2002).

Ultra-Violet

Wavelength range of ultra-violet is below 380 nm. Ultra-violet (UV) radiation has wavelengths slightly less than those of violet light. It is emitted by the Sun and also by other objects at high temperature. Ultra-violet radiation helps keep the body healthy but excessive amounts can damage the skin and the eyes. The composition of the Earth's atmosphere normally protects the planet from excessive UV radiation emitted by the Sun. Ultra-violet radiation can be used to kill harmful bacteria in kitchens and in hospitals. Certain chemicals can convert UV energy to visible light and the effect is made use of in fluorescent lamps.

3.2.3 Direct, Indirect Solar Radiation

Solar radiation is a dominating influence on all climatic phenomena. Of the total energy radiated by the sun towards the earth, part is reflected off clouds outwards, part is absorbed by water vapour, pollutants, dust particles and other atmospheric conditions, being re-emitted as diffuse radiation, and the rest of it is directly transmitted to the earth's surface.

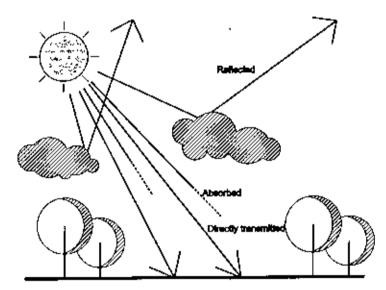


Figure 3.3: Direct, indirect solar radiation (After Abred, 1987)

Whereas direct radiation is dependent only on the altitude of the sun, and is independent of geographical position, diffuse radiation varies with the time of the day, the weather, the cloud cover and the portion of the sky from which it is received. According to Jones, no specific direction can be assigned to diffuse radiation and therefore there is no directional shadow associated with it. Diffuse radiation also varies with solar almude, as direct intensities reach their highest values at midday, and there is much more radiation available for scattering than when the sun is low in the sky (Reported in, Ahmed, 1987).

3.3 Solar Heat Gain

The heat gain in a building by radiation from the Sun depends upon the following factors (McMullan, 1992):

- The geographical latitude of the site, which determines the height of the Sun in the sky.
- The orientation of the building on the site, such as whether rooms are facing south or north.
- The season of the year, which also affects the height of the Sun in the sky.
- The local cloud conditions, which can block solar radiation.
- The angles between the Sun and the building surfaces, because maximum gain occurs when surfaces are at right angles to the rays from the Sun.
- The nature of the window glass and whether it absorbs or reflects any radianon.
- The nature of the toof and walls, because heavyweight materials behave differently to hghtweight materials.

Solar radiation falls on a surface varies throughout the day and the year. Most solar heat gain to buildings is by direct radiation through windows. The maximum gains through south-facing windows tend to occur in pre-monsoon and post-monsoon period when the lower angle of the Sun causes radiation to fall more directly onto vertical surfaces. The solar heat gains for a particular building at a specific time are relatively complicated to calculate, although it is important to do so when predicting summer heat gains in commercial buildings.

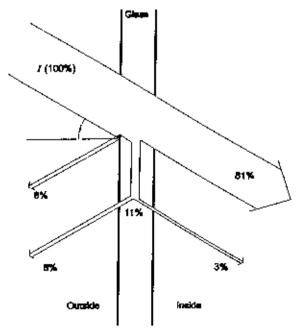


Figure 3.4: Typical proportions of incident solar radiation, reflected, absorbed, transmitted and retransmitted by glass (Source: Smith et al, 1982).

The solar radiation falling upon a clear glass surface is reflected, absorbed and transmitted in proportions similar to those indicated in Figure 3.4. These quantities depend upon the angle of incidence (i) and the proportion of direct and diffuse radiation. The angle of incidence (i) is the angle measured between the incident light beam and the normal to the plane of the glass (Smith *et al*, 1982).

The absorbed radiation heats the glass and part of this heat reaches the room surfaces by convection and radiation from the inside surface of the glass. The solar heat gain is obtained by adding this inwards released heat to the directly transmitted component of the incident solar radiation. Absorption of this solar heat gain by the internal surfaces raises their temperature. These heated surfaces behave as low temperature, long wave radiators. Since glass transmits shortwave radiation in the range 0.3 to 2.8 µm but is opaque to long wave radiation from low temperature surfaces, the solar heat gained is trapped within the enclosure causing an internal temperature rise. This phenomenon, frequently referred to as the greenhouse effect, may give rise to solar overheating. Heat gain is directly proportional to the area of glass exposed to solar radiation and therefore large glazed areas will permit a large and rapid heat gain.

3.4 Conclusion

The extensive use of glazing in the building façades is one of the charactenstics of modern architecture. This, and the increasing use of lightweight structures has caused considerable changes in the relationship between interior and ambient climates and the problem of overheating has become a major concern. To face this problem, in most of the cases mechanically cooling system is the solution. But this becomes a hurden on total energy load of the country. The idea of a climate-responsive tall building may change the preference to one away from the present fully arnficial working environment. Tall buildings designing with climate are evidently justified on the ground of recurring savings in cost and energy use in the operation of the building.

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CHAPTER: FOUR SOLAR CONTROL AND SHADING DEVICES

SOLAR CONTROL AND SHADING DEVICES

Tall buildings are exposed to the full impact of direct solar radiation, which is the greatest source of heat gain in the tropical climate. Heat gain through window is directly proportional to the area of glass exposed to solar radiation and therefore large glazed areas permit a large and rapid heat gain. Shading is a key strategy to reduce solar heat gain in overheated periods. The most efficient solar control is provided by external shading devices. This chapter presents a brief discussion on methods and principles of solar control emphasising on external shading devices. It helps to develop a clear understanding of the issues involved for the further development of design strategies of shading devices in the later sections of this work.

4.1 Solar Control

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Direct solar radiation can be prevented from reaching all or part of the walls, toof or windows of a building by the use of shading. Shading can be provided by natural vegetation, neighbouring buildings or the surrounding landscape. Shading devices on the building (fixed or movable, the latter being manually or automatically controlled) can prevent direct radiation reaching critical parts, such as windows, doors and even roofs. Indirect solar gain from the sky, or reflected from the surrounding buildings or the ground and air heated by irradiated surfaces also enhance significantly to the cooling load.

4.2 Method of Solar Control

The greatest source of heat gain can be the solar radiation entering through a window. This could, in fact, increase the indoor temperature far above the out-door air temperature, even in moderate climates, which is known as the 'greenhouse effect' (Koenigsberger *et al*, 1973). Window glasses are practically transparent for short-wave infra-red radiation emitted by the sun, but almost opaque for long-wave radiation emitted by objects in the room. The consequence of this is that the radiant heat, once it has entered through a window, is trapped inside the building.

There are four methods available for the reduction of solar heat gain through windows:

- 1. Window Orientation
- 2. Internal blinds, curtains
- 3. Heat absorbing/reflecting glasses
- 4. External shading devices

4.2.1 Window Orientation

Building orientation affects the indoor climate in two respects, by its regulation of the influence of two distinct climate factors (Givoni, 1969):

- a. Solar radiation and its heating effect on walls and rooms facing different directions.
- b. Venulation problems associated with the relation between the direction of the prevailing winds and the orientation of the building.

The effect of window orientation on the indoor temperatures is largely determined by the ventilation conditions and the degree and efficiency of the window shading. When shading is not effective, solar radiation enters through the windows and directly heats the building interior, the temperatures of which will obviously be influenced by the orientation of the windows. The heating effect of solar energy penetrating a glazed wall or closed unshaded windows is magnified, as the energy is transformed in the exterior or by longwave radiation, to which the glass is opaque.

In the equatorial location, if solar heat gain is to be avoided, the main windows should face north or south (Koenigsberger *et al*, 1973). At higher latitude, an orientation away from the equator would receive the least sunshine, but here it may be desirable to have some solar heat gain in the winter, when the sun is low — so an orientation towards the equator may be preferable. In both locations only minor openings of unimportant rooms should be placed on the east and west side. Solar heat gain on the west side can be particularly troublesome as its maximum intensity coincides with the hottest part of the day.

4.2.2 Internal Blinds and Currains

From an energy-rejection point of view, the external shading devices are the most effective. But for a number of practical reasons, the interior devices, such as curtains, roller shades, venetian blinds, and shutters, are also vety important. Interior devices are often less expensive than external shading devices, since they do not have to resist the elements. They are also very adjustable and movable, which enables them to easily respond to changing requirements. Besides shading, these devices provide numerous other benefits, such as privacy, glare control, insulation, and interior aesthetics (Lechner, 2001).

Since internal devices are usually included whether or not external devices are supplied, we should use them to our advantage. They should be used to stop the sun when it out flanks the exterior shading devices. They are also useful for those exceptionally hot days during the transition or under heated periods of the year, when exterior shading is not designed to work. In the form of venetian blinds or light shelves, they can also produce fine day lighting.

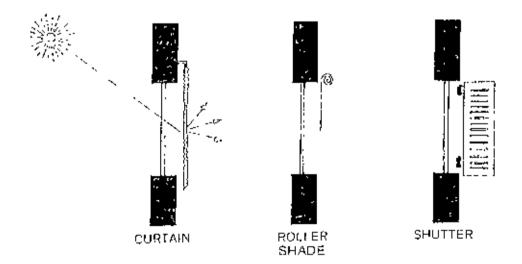


Figure 4.1: Interior shading devices for solar control (Source: Lochner, 2001).

One of the main drawbacks of interior shading devices is that they are not always discerning. They cannot block the sun while admitting the view, something that can be effectively done with an external overhang. Since they block the solar radiation on the inside of the glazing, much of the heat remains indoors.

It is true that they stop the passage of radiation, but they themselves absorb the solar heat and can reach a very high temperature (Koenigsberger *et al*, 1973). The absorbed heat will be partly convected to the indoor air and partly reradiated. Significant portion of this reradiation is outwards, but as it is of a long wavelength, it is stopped by the window glass. The usual narrow space between the window and the blind will thus be quite substantially overheated. The hot surface of the blind causes the indoor MRT to rise far above the air temperature.

As a broad generalization the daily average solar gain factor of a single glazed window will be:

 $\theta = 72\%$ without any solar control device, and

 $\theta = 55\%$ with an internal venetian blind [i.e. the reduction is only 1.7%]

4.2.3 Heat Absorbing/ Reflecting Glasses

Even the clearest and thinnest glass does not transmit 100 percent of the incident solar radiation. The radiation that is not transmitted is either absorbed or reflected off the surface. The amount that is absorbed depends on the type and thickness of the glazing. The amount that is reflected depends on the nature of the surface and the angle of incidence of the radiation (Lechner, 2001).

One type of tinted glazing is called heat absorbing because it absorbs the shortwave infra-red part of solat radiation much more than the visible part. But even this type of glazing reduces the solar heat gain by only a small amount. Although tinted glazing reduces the light transmission, it usually does not decrease the heat gain by much because the absorbed radiation is then reradiated indoors (Givoni, 1998).

Glazing also blocks solar radiation by reflection. The amount of solar radiation that is reflected from glazing can be increased significantly by adding a reflective coating. One surface of the glazing is covered with a metallic coating thin enough that some solar radiation still penetrates. The percentage reflectance depends on the thickness of this coating, and a mirror is nothing more than a coating that is thick enough so that no light is transmitted. Reflective glazing can be extremely effective in blocking solar radiation while still allowing a view.

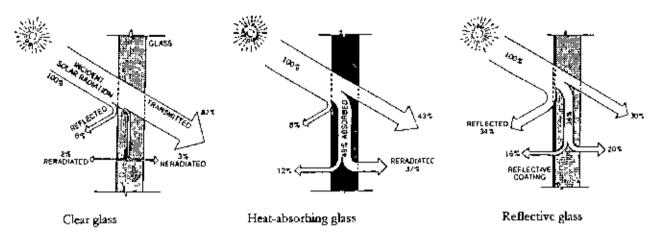


Figure 4.2: Heat gain through different types of glazing (Source: Larbner, 2001).

When reflective glazing became available in the 1970s, it quickly became popular for several reasons. It blocked solar radiation better than heat-absorbing glass, and did so with out any color distortion.

Although tinted and reflective glazing systems can be effective shading devices, they are very undiscerning. They do not differentiate between light from the sun and light from the view. They filter out light whether daylight is desired or not. And they block the desirable winter sun as much as the undesirable summer sun. Thus, tinted or reflective glazing is not appropriate where either day lighting or solar hearing is desired. It is also not appropriate when only the sun should be excluded, but not the view. When glazing is expected to do all the shading, it has to be of a very low transnuttance type. The view through this kind of glazing makes even the sunniest day look dark and gloomy. Thus, external overhangs, fins, etc. which are more discerning, are usually still the best shading devices. Tinted or reflective glazing is excellent, however, for blocking diffuse sky radiation in very humid regions, and for glaze control (Lechner, 2001).

When daylighting is desired and solar heating is not, having the visible component of solar radiation pass through while heat radiation is blocked would he advantageous. Certain "specially selective" glazing systems can do that to a limited extent. Specially selective low-e-glazing transmits cooler daylight than other glazing materials, because it transmits a much higher ratio of visible-to-infrared radiation (Givoni, 1998).

In the near future, there might be even better glazing system than the "selective" types mentioned above. These are known as responsive glazing systems because they change in response to light, heat, and electricity.

Responsive glazing can be either the passive or the active kind. Passive glazing responds directly to environmental conditions, such as light level or temperature (photochromics or thermochromics, respectively). The active system can be controlled as needed and can include such devices as hquid crystal, dispersed particle, and electrochromics.

Photochromics: These materials change their transparency in response to light intensity. They are ideal for automatically controlling the quantity of daylight allowed into a building. The goal is to let in just enough light to eliminate the need for electric lighting, but not so much that the cooling load would increase.

Thermochromics: These materials change transparency in response to temperature. They are transparent when cold and reflective, white when hot. They can be used in skylights, where the loss of transparency on a hot day is not a problem as it would be in a view window. These materials could also be used to prevent passive systems from overheating in the summer

Liquid-Crystal Glazing: When electric power is applied, the transparent liquid crystals align and become translucent. Thus, liquid-crystal glazing has some application for shading, but its teal potential is in privacy control.

Dispersed-Particle Glazing: Although similar to liquid-crystal glazing, this material is more promising for solar control because the applied power can change the transmittance of the material in a range between clear and dark states, thereby preserving the view.

Electrochromic Glazing: This is the most promising material because it can change transparency-not translucency-continuously over a wide range (about 10 percent to 70 percent) and can be easily controlled. Consequently, either a computer, a photocell, a thermostat, or the occupant can adjust the transparency as the local conditions require.

4.2.4 External Shading Devices

Blocking the sun before it reaches the building, particularly the glazed, but also the opaque surfaces (including the roof) and reflecting the solar radiation, is fundamental to the prevention of heat gain (Goulding, 1992). The appropriate choice from a wide range of fixed and movable shading systems will depend on location, orientation, building type

and the overall cooling, heating and daylighting strategies adopted in the design phase of the building.

While shading systems must provide good solar protection in summer, they should not reduce solar gains in winter, obstruct natural lighting or impede natural ventilation. Well designed shading systems can actually enhance natural ventilation and daylighting. Shading systems can block the direct component of solar radiation but are usually not as effective in reducing the diffuse and reflected components.

4.3 Shading Devices

Once the window size has been established the most effective method of reducing solar heat gain is to prevent the transmission of shortwave radiation through the glass by external shading.

The effectiveness of a typical glazing and shading system may be measured in terms of the solar gain factor. This is the proportion of incident solar radiation transmitted by the window and shading device to the interiot of an enclosure. The solar gain factor for an unglazed unshaded aperture is unit. This factor decreases as the shading system becomes mote effective in reducing solar heat gain (Smith *et al*, 1982).

The requirements for daylight and ventilation may well conflict with the need to provide shading devices to control solar heat gain, reduce glare and prevent direct radiation falling upon the occupants of an enclosure. Traditional heavyweight building with small windows is unlikely to experience the solar overheating problems, which may occur in the excessively glazed lightweight modern office block.

4.3.1 Objective of Shading

Shading the glass affects the quantity of incident radiation and hence modifies both the heat flow to the interior and the indoor temperatures. It is useful to set out the purpose of shading in some detail (Steemers *et al*, 2002). They are mentioned as follows.

 To minimise the total solar energy entering a room and thereby reduce the average temperature of the room

- To prevent sunlight from falling directly onto occupants, resulting in an effective increase of temperature of between 3°c and 7°c
- To reduce the local illumination of surfaces that may present glare sources to the occupants
- To prevent the view of brightly linoutside surfaces, or clouds, or the sun itself

4.3.2 Types of Shading Devices

Shading devices are broadly classified into three categories based on its integration with the window (Goulding, 1992; Steemers *et al*, 2002; Lechner, 2001). They are classified , again within these categories by their morphological characteristics and physical forms. The broad categories of shading devices are:

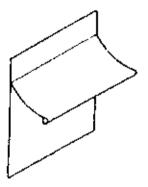
- Retractable or removable shading device
- Movable or adjustable shading device
- Fixed shading device

Retractable Shading Device:

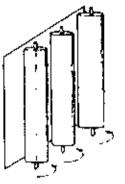
Retractable means that these elements can be completely or pattially removable from the window aperture (Steemers *et al*, 2002). It is important to note that shading devices of this type do not influence the availability of daylight in the room. That is, they will not influence switch-on time, because at times of low light availability they can be removed from the aperture. Clearly this property reconciles the conflict between allowing useful light in and keeping unwanted radiation out. If correctly operated, devices of this type will not lead to an increase in artificial lighting energy.

Movable Sbading Devices

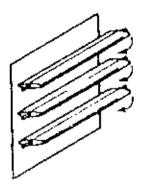
Movable shading is used externally or internally. Control can be either manual or power assisted and may be automated to respond to changing conditions, such as current radiation levels and daylighting or thermal requirements (Goulding, 1992). The configuration of operable shading devices can be changed, and therefore their performance can be much betret than that of fixed devices. However, their position has to be adjusted, daily or seasonally, to the changing patterns of the sun's relative motion and the shading needs (Givoni, 1998). They usually need maintenance to keep them in good condition.



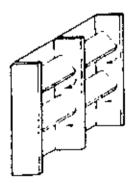
Overhang, Awning



Fin Rotating fins



Overhang: Rotating horizontal louvers



Eggerate: Rotating Horizontal louvers

Figure 4.3: Some of movable shading devices (Source, Lechner, 2001).

The movement of shading devices can be very simple or very complex. An adjustment twice a year can be quite effective and yet simple. Late in spring, at the beginning of the overheated period, the shading devices would be manually extended. At the end of the overheated period in late fall, the device would be retracted for full solar exposure (Lechner, 2001).

There is a general conviction that since a building should be as low maintenance as possible, movable shading devices are unacceptable. The use of existing technology and careful detailing can produce trouble-free, low-maintenance movable shading devices.

Fixed Shading Devices

Fixed shading systems include structural elements, such as halconies and projecting fins or shelves and non-structural elements, such as canopies, blinds, louvers and screens. The orientation and shape of the opening to be shaded, relative to the position of the sun at different times of day and year, is critical to the design of fixed systems (Goulding, 1992). Each orientation will need to be examined separately, taking account of direct and diffuse or reflected components of the overall solar radiation throughout the day and year. Typically horizontal shading is used for south facades, whereas vertical or diagonal fins or louvers are often more efficient on the east or west facades in northern hemisphere.

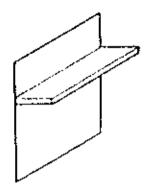
Fixed shading systems are most commonly used on the external facades where they can prevent direct radiation from reaching glazing or other openings and where heat absorbed by the shading system can be dissipated to the outside air. An obvious advantage of fixed shading is that it needs no handling by the occupants and is often maintenance free.

Fixed shading devices are of three types based on their physical forms (Koenigsberger et al, 1973; Givoni, 1998). They are horizontal shading device, vertical shading device and combination of the two (eggerate). A brief discussion of these three types of fixed shading devices are presented below:

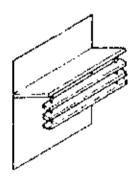
Vertical Shading Devices

Vertical devices consist of louver blades or projecting fins in a vertical position. Narrow blades with close spacing may give the same shadow angle as broader blades with wider spacing (Koenigsberger *et al*, 1973). Vertical fins are often presented as the shading devices of choice for east and west.

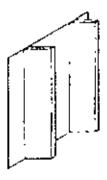
Vertical fins can be appropriate either when there is a desire to control the direction of view or when the view is not important. This type of device is most effective when the sun is at one side of the elevation, such as an eastern or western elevation. A vertical device to be effective when the sun is opposite to the wall considered, would have to give almost complete cover of the whole window.



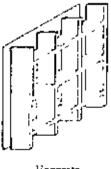
Overhang Horizontal panel



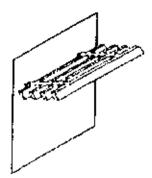
Overhang: Louvers in vertical plan



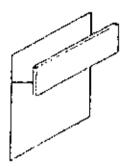
Vertical fin



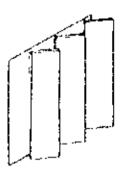




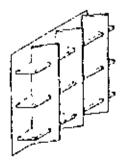
Overhang: Louvers in horizontal plan



Overhang: Vertical panel



Vertical fin slanted



Eggerate with slanted fins

Figure 4.4: Some of fixed shading devices (Source: Lachner, 2001).

Horizontal Shading Devices

The horizontal overhangs and its variations are the best choice for south facade. Because they are directionally selective, they can allow the low winter sun to enter while fully shading the high summer sun with minimum obstruction of the view.

Horizontal louvers have a number of advantages over solid overhangs. Horizontal louvers in a horizontal plane reduce structural loads by allowing wind to pass right through (Lechner, 2001). In the summer, they also minimize the collection of hot air next to the windows under the overhang, Horizontal louvers in a vertical plane are appropriate when the projecting distance from the wall must be limited. This could be important if a building is on or near the property line. Louvers can also be useful when the architecture calls for small-scale elements and a rich texture.

When designing an overhang for the south facade, one must remember that the sun comes from the southcast before noon and from the southwest after noon. Therefore, ' the sun will outflank an overhang the same width as a window. Narrow windows need either a very wide overhang or vertical fins in addinon to the overhang. Wide strip windows are affected less by this problem.

Horizontal devices will be the most effective when the sun is opposite to the building face considered and at a high angle, such as for north and south facing walls (koenigsberger *et al*, 1973). In summer they can block the rays of the sun and in winter they can admit radiation from the sun's lower position. To exclude a low angle sun, this type of device would have to cover the window completely, permitting a view downwards only.

Egg-crate

Eggerate shading devices are mainly for east and west windows in hot climates and for the additional southeast and southwest orientations in very hot climates (Lechner, 2001). An eggerate is a combination of horizontal Overhangs (louvers) and vertical fins. By controlling sun penetration by both the altitude and azimuth angle of the sun, very effective shading of windows can be achieved. The Designer should first decide on the general appearance of the eggerate system. As far as sun penetration is concerned, the scale of the eggerate can be changed at any time as long as the ratio of height/depth and width/depth are kept constant.

4.4 Conclusion

Shading is a key strategy of achieving thermal comfort in the summer. Although shading of the whole building is beneficial, shading of the glazed areas is crucial. Heat gain is directly proportional to the area of glass exposed to solar radiation and therefore large glazed areas will permit a large and rapid heat gain. Existing heat-absorbing glasses can protect only 20% of the total incident radiation and reflective glazing prevents solar radiation up to 50%. Hence external shading devices can be a good answer to control the solar radiation. The most efficient solar control is provided by external shading devices, the design of which can only come from understanding the solar geometry. Direct radiation is dependent only on the altitude of the sun and geographical position. That's why; direct radiation can be controlled effectively by proper external shading devices.

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CHAPTER: FIVE PERFORMANCE EVALUATION OF SHADING DEVICES

PERFORMANCE EVALUATION OF SHADING DEVICES

The performance of shading devices and its impact on solar heat gain through windows can precisely be evaluated by simulation study. Because in reality, due to the simultaneous influence of many different conditions, it is difficult to isolate the exclusive effect of one single aspect or the changes of it. Shadow simulation allows study of the effect of changes in one aspect, keeping other factors constant. The observations of simulated behaviour that occurs due to changing parameters allow the identification of elements, the reduction or introduction of which in the design contribute to solar heat gain. Another significant achievement of simulation study is that, it is possible to analyse the performance of shading devices for any period of the year simply by assigning simulation parameters (e.g. temperature, radiation, wind speed and direction, relative humidity and cloud cover).

In this chapter, nine tall office buildings from different commercial areas in the Dhaka city have been considered to evaluate performance of their shading devices, in terms of reducing solar heat gain through simulation study on the basis of set criteria. A dynamic computer simulation program named 'Ecorect' (version 5.20) has been used for this simulation study.

5.1 Selection of Shading Devices for Evaluation

Before making selection of shading devices, tall office buildings are identified nn the basis of certain considerations to be discussed in the following section. These tall office buildings are located in different commercial areas in the Dhaka city, such as Motijheel, Dilkusha, Karwan bazaar, Panthapath, Banani, Mohakhali etc. After that, buildings were categorised considering the typology (based on geometry) of shading devices installed on their front façade. Sketches of window sections with shading device of these buildings were prepared with detail construction features, installation technique and geometric features. After analysing the sketches, nine shading devices were selected to evaluate performance in terms of reducing solar heat gain considering shading device typology and similarities in geometric features.

Tall Building Criteria

There is no fixed parameter of height to denote rall and high-rise building. According to the Council for Tall Buildings and Urban Habitat (CTBUH), the number of stories or its height does not strictly define a tall building. It also depends upon the context in which it stands. The Council for Tall Buildings and Urban Habitat (CTBUH) considers for instance, tall buildings as being buildings of ten storeys or more.

- a) Walk up limit / provision for lift:
 - According to Building construction rules (2006), buildings of seven storied and above in height shall have provision for lift.
 - According to Bangladesh National Building Codes (1993), lifts shall be provided in buildings more than six storied or 20m in height.
- b) Fire escape provision:
 - According to Fire Service and Civil Defence rules, buildings of seven storied and above in height shall have provision for Fire escape/ alternative staircase.
- c) Structural analysis and design:
 - According to Wolfgang Shueller, buildings with height-to-width ratio above 5-7 are considered as high-rise structure.

In view of the above considerations, in the present context of Dhaka city, buildings above six storeys may be considered as tall buildings.

Selection of Shading Devices

Following the above criteria, eighty-four tall office buildings of Dhaka city were identified for investigation. Among them, forty buildings are situated at Motijheel and Dilkusha area; twenty-four buildings at Mohakhali, Gulshan Avenue and Banani Kemal Ataturk Avenue; fourteen buildings at Karwan Bazaar area and six buildings at Panthapath.

Among these buildings, twenty two buildings have horizontal shading devices, eleven buildings have vertical shading devices, twenty buildings have composite type (combination of horizontal and vertical) shading devices and thirty one buildings do not have shading devices on their front façade. Among these eighty-four tall office buildings, nine buildings were selected to evaluate performance of their shading devices. The list of buildings with location, height, orientation and type of shading device installed is presented below:

2 K	Identification Number	Location	Storey	Orlensation	Shading Device
ŧ	R01	Janata Bank Bhaban, Motijheel	23	East	Horizontal
z	1102	Global Insurance Ltd. Dillusha	11	South	Horizontal
3	H03	Brac Center, Mohakhali	20	North	Horizootal
4	V01	Rupah Bank Ltd, Dilkusha	10	South	Vertical
5	V02	Ispahani Bhahan, Dilkusha	9	West	Vertical
6	V03	Bangladesh Samobye Bhaban, Motijheel	9	East	Venical
7	CD1	Krishi Bhaban, Dilkusha	11	South	Composite
8	C02	BCIC Bhahan, Dilkusha	22	South	Composite
9	C03	Meghna Life Insurance, Dilkusha	10	East	Composite

Table 5.1: List of the selected buildings and shading devices.

View of front facades of the selected building and sketches of window sections with shading devices of these buildings are presented below.



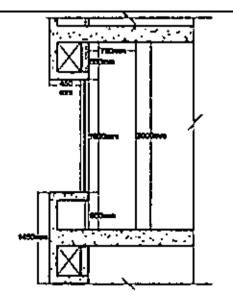




Figure 5.1(b): Window section of H01.

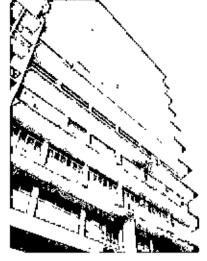


Figure 5.2(a): View of building H02.



Figure 5.3(a): View of building H03.

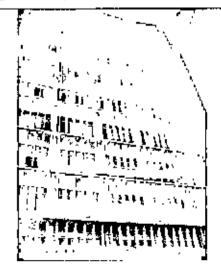


Figure 5.4(a): View of building V01.

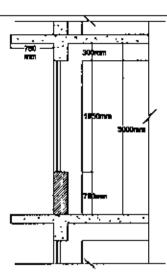


Figure 5.2(b): Window section of H02.

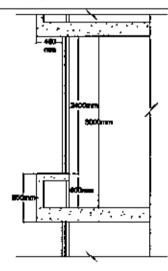


Figure 5.3(b): Window section of H03.

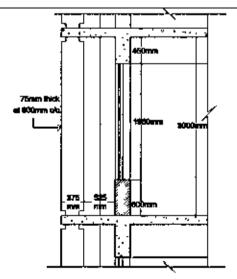


Figure 5.4(b): Window section of V01.

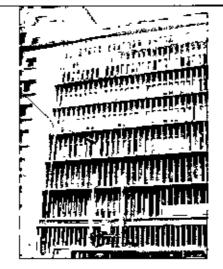


Figure 5.5(a): View of building V02.

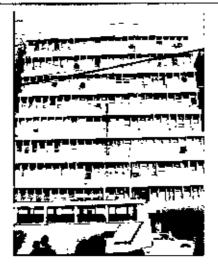


Figure 5.6(a): View of building V03.

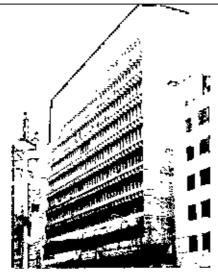


Figure 5.7(a): View of building C01.

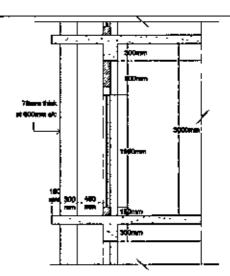


Figure 5.5(b): Window section of V02.

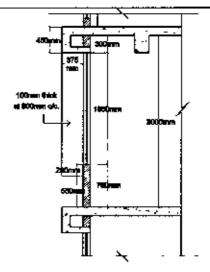


Figure 5.6(b): Window section of V03.

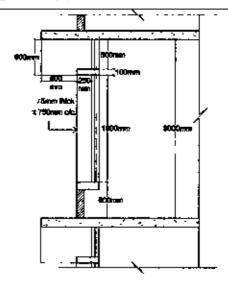


Figure 5.7(b): Window section of C01.



Figure 5.8(a): View of building C02.

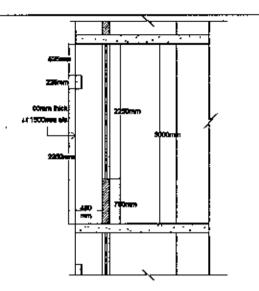
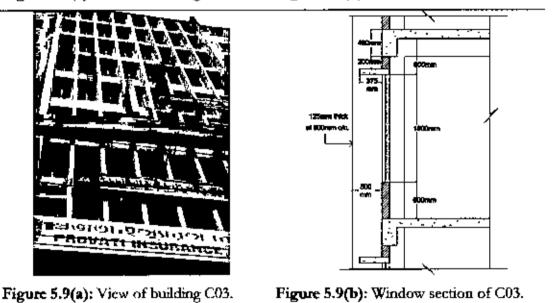


Figure 5.8(b): Window section of C02.



5.2 Performance Evaluation Process

Performance of the selected shading devices will be evaluated in terms of reducing solar heat gain through simulation study on the basis of set criteria to be discussed in the following section. Simulation is a powerful technique for solving a variety of problems. To simulate is to copy the behaviour of the phenomenon under study. It refers to some representation or model of a system that can be studied in order to understand the behaviour of the actual system itself and to make predictions about the future. It involves developing a model of a system and carrying out experiments on it. It helps analyzing the effect of phenomenon and their interaction on one another (Suri, 2005). Evaluation process comprises the following steps:

- Setting criteria for performance evaluation
- Preparing climate database
- Setting simulation parameters
- Developing simulation model
- Analysing results of simulation

In order to evaluate the performance of shading devices in reducing solar heat gain, a base-case situation is established by studying the unshaded window (without shading device) during the critical shading period of the year at different orientations.

5.2.1 Criteria for Performance Evaluation

- The percentage of the shade area, given by vanous types of fixed shading devices (Givoni, 1969; Steemers *et al*, 2002). The percentage of the shade areas refers to portion of the window area, which is not exposed to the direct solar radiation. This also reflects the ability of a fixed shading device to protect the window area at critical time.
- Computation of the shading coefficient, which is the ratio of the heat entering the window-shading combination to that entering an unshaded window. Shading coefficient (C_{sb})can be expressed as below.

Heat entering through the window with shading device $C_{ab} = -----$

Heat entering through the window without shading device

Shading coefficients basically refer to the fraction of solar heat gain that passes through a transparent solar aperture compared to the amount of solar radiation incident upon it. The shading coefficient is expressed as a dimensionless number from 0 to 1. A high shading coefficient means high solar gain, while a low shading coefficient means high solar gain, while a low shading coefficient means low solar gain (Givoni, 1969; Givoni, 1998; Steemers *et al*, 2002; Lechner, 2001).

5.2.2 Simulation Program

Simulations regarding solar performance analysis are carried out using building analysis software 'ECOTECT v5.20'. It features a user-friendly 3D modelling interface fully

integrated with a wide range of performance analysis and simulation functions. The visual nature of calculation feedback makes 'ECOTECT' unique. The process can be started with a detailed climatic analysis to calculate the potential effectiveness of various passive design techniques or to optimise the use of available solar, light and wind resources.

The original 'ECOTECT' software was written as a demonstration of some of the ideas presented in PhD thesis by Dr. Andrew Marsh at the School of Architecture and Fine Arts at The University of Western Australia. The software has undergone some major changes since then. Version 5.2 builds significantly on the functionality of previous versions introducing a range of new analysis functions and real-time hidden line and sketch visualization. It also refines some of the major algorithms, such as the thermal and daylight factor calculations.

ECOTECT provides a range of thermal and solar performance analysis options. At its core, is the Chartered Institute of Building Services Engineers (CIBSE) Admittance Method used to determine heat loads. The Admittance Method is widely used around the world and has been shown to be an extremely useful design-tool. This thermal algorithm is very flexible and has no restrictions on building geometry or the number of thermal zones that can be simultaneously analyzed. Most importantly, with only a few pre-calculations for shading and overshadowing, it is very quick method to calculate and can be used to display a wide range of very useful information.

Whilst in summary it is a simplified method, the Admittance Method encapsulates the effects of conductive heat flow through building fabric, infiltration and ventilation through openings, direct solar gains through mansparent materials, indirect solar gains through opaque elements, internal heat gains from equipment, lights and people and the effects of inter-zonal heat flow.

Nicki Taylor validated ECOTECT as part of his research work for the degree of Bachelor of Engineering (Hons.) from Department of Environmental Engineering at University of Western Australia in 2002. He showed in his research that the mean error of the estimated results is less than 2%, indicating a reasonable degree of accuracy (Taylor, 2002).

5.2.3 Climate Database

The climate database stores files containing hourly weather data. The weather files supplied with Ecotect cover different regions of the world and each represents a typical year's weather for a particular region. The weather file is not provided with the software. But facilities are provided to allow creating own weather files and can be added to the climate database.

The weather file Ban_Dhaka.wea' has been prepared for the research purpose by using the Weather Tool, associated software of Ecotect. The Weather Tool is a visualization and analysis program for hourly climate data. The weather file consists of a group of parameters relating to the weather site and hourly values of seven weather variables (drybulb temperature, relative humidiry, direct radiation, diffuse radiation, wind speed and direction and cloud cover). Hourly radiation data has been collected from Renewable Energy Research Centre of Dhaka University. Three hourly weather data regarding drybulb temperature, relative humidity, wind speed and direction and cloud cover has been collected from Climate Division, Bangladesh Meteorological Department Agargaon, Dhaka. Due to the simulation requirements, all three hourly data have been converted to hourly data by interpolation method. Hourly weather variables for Dhaka have been collected for the year 2005.

The site parameters of Dhaka for weather file are as follows:

Parameters	Details	
Latitude (degrees North)	23°50' North	
Longitude (degrees East)	90°20' East	
Time Zone (hours ahead of GMT)	GMT +06.00	

The combination of site parameters and hourly weather variables forms the weather file, with which the simulation program Ecotect is capable to analyse any climatic characteristics of the selected site.

5.2.4 Simulation Parameters

Before starting the simulations a set of parameters are set. These are described below. To investigate the results of the aimulations, a specific day has been selected (from the weather database for a year) on the basis of some specific attributes to observe the results.

Considerations for Identifying the Simulation Day

For individual daily profile analysis, a day of the year has been selected in consideration of the typical characteristics of the given climate.

The test day is 21st of March (Day: 80). Outdoor air temperature range of this day is 24.5°C -35.4°C and sky condition is clear. From 0900-1700 hours the cloud cover is 1.1 out of 8.0 (13.8% coverage). This is a day with considerable high outdoor air temperature but not the extreme one and beats a common chatacter regarding the climatic features specially of the hot-dry season. The average temperature of this day (29°C) is very close to the average temperature of the scason (28.02°C). It has been observed that the sky condition in the given climate is clear for 67 percent of the whole pre-monsoon period (earlier shown in table 2.3) and the 'clear sky' condition prevail for the chosen day. This 'clear sky' condition of the chosen day is also important to investigate the impacts of solar radiation and this clear sky condition impedes direct radiation to reach on building surfaces. Fixed shading device are effective to reduce heat gain from direct solar radiation. These are the reasons behind choosing a day with clear sky condition.

For a fixed shading device, the shading period is symmetrical about June 21 (Lechner, 2001). This is because the position of the sun cycles through the sky on a seasonal basis. Thus, the Sun will pass through the same path twice every year, the first time when going from winter to summer and the second time when traveling back to winter. Thus, any shading device will always shade between two dates. In the northern hemisphere, an optimized shading device for the 21st of March will actually shade from the 21st of March, right through June until the 21st of September. Thus the whole overheated period (hot-dry and warm-humid) is taken into account for simulation.

Considerations for Identifying the Time Period for Simulation

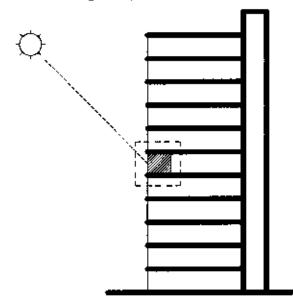
For simulation to investigate the performance of the shading devices, the time period is considered when the space is only considered to be used during office hours. In general, the office time is from 0900 to 1700 and this time period is taken as a critical time period for shading requirement.

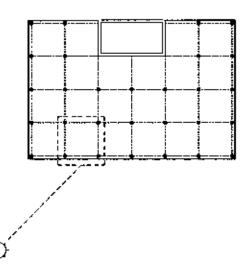
5.2.5 Simulation Model

Following models have been developed for simulation that represent the selected shading devices. These models refer to the high-rise buildings selected with identical facades with a similar treated floor area with the shading device with single glazed clear glass. The room size for simulation model is 6000mm x 6000mm which is considered as located in an intermediate floor of a high-rise building. The room size is taken from the typical high-rise column grid. A fixed window width 5400mm has been considered with single glazed glass, as the window covers the whole span between two columns. Different shading devices are attached with it for simulation study. For the ease of calculation, a study plane at the level of the exterior surface of the window wall is considered.

In terms of shading analysis and solar heat gain, the simulations are done for the following options of models:

- 'The 'without shading' option which refer to the high-rise models with identical facades with a similar treated floor area without the shading device but with clear glass;
- The 'with shading' option which refer to the high-rise models with shading as designed by the architect.

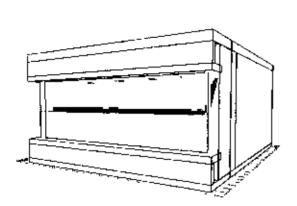




Section of typical high rise building

Typical floor plan of high rise building

Figure 5.10: Schematic drawings showing generation of simulation model from typical high rise building.



The simulations are done for the following models generated by 'Ecotect':

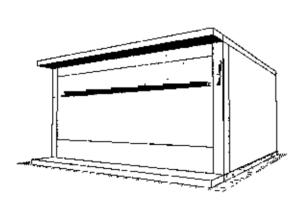
Parameters:

- Office room dimension: 6000mm x 6000mm
- Floor height: 3000mm
- Window: Sill: 600mm,

Width: 5400mm, Height: 1800mm

• Overhang depth: 450mm

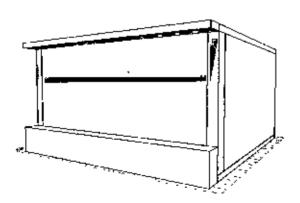
Figure 5.11: Simulation model of Shade H01.



Parameters:

- Office mom dimension: 6000mm x 6000mm
- Floor height: 3000mm
- Window: Sill: 600mm,
- Width: 5400mm, Height: 2100mm
- Overhang depth: 750mm

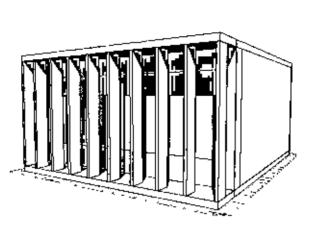
Figure 5.12: Simulation model of Shade H02.



Parameters:

- Office room dimension: 6000mm x 6000mm
- Floor height: 3000mm
- Window: Sill: 750mm,
 - Width: 5400mm, Height: 2400mm
- Overhang depth: 450mm

Figure 5.13: Simulation model of Shade H03.



Parameters:

- Office room dimension: 6000mm x 6000mm
- Floor height: 3000mm
- Window: Sill: 600mm,
- Width: 5400mm, Height: 1950mm
- Vertical Fin: Depth: 375mm, Spacing: 600mm

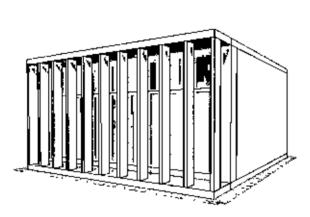
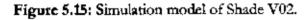
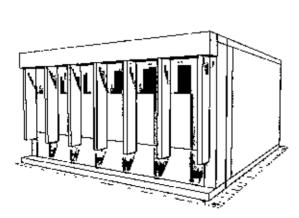


Figure 5.14: Simulation model of Shade V01.

Parameters:

- Office room dimension: 6000mm x 6000mm
- Floor height: 3000mm
- Window: Sill: 600mm,
- Width: 5400mm, Height: 1950mm
- Vertical Fin: Depth: 300mm, Spacing: 600mm

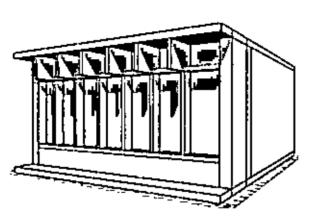




Parameters:

- Office room dimension:
 6000mm x 6000mm
- Floor height: 3000mm
- Window: Sill: 600mm, Width: 5400mm, Height: 1950mm
- Vertical Fin: Depth: 450mm, Spacing: 600mm

Figure 5.16: Simulation model of Shade V03.



Parameters:

- Office room dimension:
 6000mm x 6000mm
- Floor height: 3000mm
- Window: Sill: 600mm,

Width: 5400mm, Height: 2400mm

- Vertical Fin: Depth: 300mm& 900mm, Spacing: 750mm
- Overhang depth: 300mm & 900mm

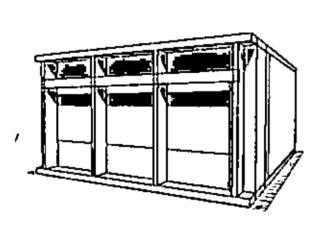


Figure 5.18: Simulation model of Shade C02.

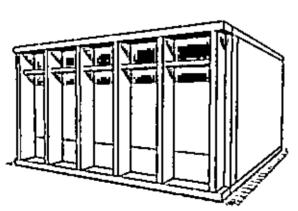


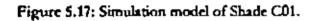
Figure 5.19: Simulation model of Shade C03.

Parameters:

- Office room dimension: 6000mm x 6000mm
- Floor height: 3000mm
- Window: Sill: 750mm,
- Width: 5400mm, Height: 2250mm
- Vertical Fin: Depth: 450mm, Spacing: 1500mm
- Overhang depth: 225mm

Parameters:

- Office room dimension:
 6000mm x 6000mm
- Floor height: 3000mm
- Window: Sill: 600mm,
 - Width: 5400mm, Height: 1800mm
- Vertical Fin: Depth: 500mm,
 Spacing: 1050mm
- Overhang depth: 375mm



5.3 Simulation Study for Performance Evaluation

Two studies about the performance of shading devices on solar radiation protection are carried out as under. The first study investigated the impact of orientation on the performance of shading devices while the second study compared the performance among the selected shading devices in different orientations on the basis of previously set criteria.

This study will help in identifying the effect of different parameters and internelation among parameters in terms of solar shading aspect. This study will also assist to understand the influence of window orientation on the shading performance of shading devices.

5.3.1 Effect of Orientation on Shading Performance

The efficiency of the window shading is largely determined by the orientation of the window. When shading is not effective, solar radiation enters through the windows and heats up the building interior directly. Hence the indoor temperature will obviously be influenced by the orientation of the windows.

The quantitative effect of window orientation has been studied by simulation technique under different shading condition, which also reveal whether shading devices used are effective or not, according to orientation in order to cut direct sunlight penetration at critical times of the day. The results of the study are summansed in the following section.

5.3.1.1 Performance of Horizontal Shading Devices

The three models with selected horizontal shading devices were oriented in the three cardinal directions (East, West & South) and two oblique directions south-east and south-west. The results are given below with respect to individual cases.

Table 5.2 shows percentage of shaded area with respect to whole window area of Shade H01 at every 30-minute interval from sunrise to sunset. In the field investigation it was found that this shading device was attached mostly with an east-facing window. But through simulation, it is found that this shading device is not efficient at east orientation. It is capable to shade below 50% of the window area at east but up to 60% window area at south orientation. The performance at south is more consistent than that of other orientations. Figure 5.20 shows the shading performance of Shade H01 in different orientations and it expresses a consistent performance only in south orientation.

Orientation	0340	04-10	1040	10-10	(L) (L)	05-11	ώ ε η	01210	0041	071	43341	0(1)	WHAT	15:00	(077)	14.30	17.00
	- 14	34	1.	,	26	- 74	- 96	••	*	- 94	•	- 55	\$ 1		- 16	•	4
Bart	22	73	33	51	•	•	٠	•	•	•	٠	•	•	•	٠	•	٠
Southeast	21	Z7	31	34	45	59	•	•	•	•	•	•	•	*		•	•
South	52	ж	ស	8	×	55	60	ទ	×	57	54	55	ц Ц	50	45	42	8
Southwest	*	•	*	•	•	•	•	63	50	41	34	28	22	19	15	12	10
West	•	•	•	•	•	•	•	•	•	e	41	30	Ā	26	13	11	1

Table 5.2: Percentage of shaded area by Shade H01 for 21" March.

* Percentage of shaded area is not taken into account as the sun does not see the window.

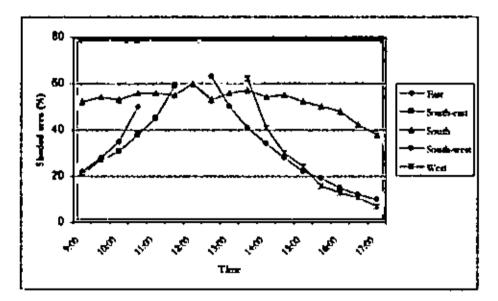


Figure 5.20: Percentage of shaded area by Shade H01 for 21" March at different orientations."

In case of Shade H02, simulation results show that the device shades more window area at south orientation. In the field investigation it was found that this shading device was attached with a south facing window. As per simulation it is capable to shade up to 53% of window area at south orientation. The performance at south is more consistent than

¹ Corresponding values of percentage of abaded area prior to bours shown are not indicated as the sundoes not see the window prior to the time range shown period.

that of other orientations. At south-west orientation it shades up to 56% of window area but the performance is not consistent. Table 5.3 and Figure 5.21 show the performance of Shade H02 at different orientations and it indicates a consistent performance only in south orientation.

Otintation	ch0)	01-00	(unaț	10.00	11:00	ot:te	1210	0C¢I	0041	91	00¥1	14.30	0)61	11.10	1400	16.30	17:00
•	۰.	- 24		*	1		**	5				34		- 94	-	.	2
Fac	11	20	27	*	٠	•	٠	•	٠	•	•	٠	•	•	•	•	•
Southeast	12	15	20	25	37	52	•	٠	•	•	•	٠	4	•	•	•	•
South	45	*	47	55	50	50	53	43	32	47	46	45	42	41	36	27	25
Southwest	•	•	•	٠	٠	•	٠	56	41	33	Z 3	17	13	R	4	0	e
West	•	•	•	•	•	•	•	•	•	54	n	21	32	•	3	°_	0

Table 5.3: Percentage of shaded area by Shade H02 for 21^e March.

* Percentage of shaded area is not taken into account as the sun does not see the window.

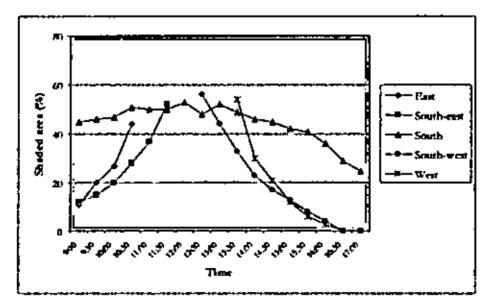


Figure 5.21: Percentage of shaded area by Shade H02 for 21[#] March at different orientations.¹⁶⁻³⁹

Table 5.4 and Figure 5.22 show the performance of Shade H03 at different orientations and it expresses a comparatively better performance at south orientation than that for other orientations. It shades maximum 46% window area at south and more or less consistent for the whole day.

Orientation	86	(C4)	N:01	0,01	(11.11)	60H		0(21	ant	001	1ero	0641	0)-51	15.10	16-00	0(791	0×1
	-	*	- S.	4	*	76	÷.	74		- 54	- 15	1	*	- 16	*	1	٩.
East	11	20	33	34	•	•	•	•	•	•	•	•	•	•	•	•	•
Southcast	17	22	21	n	34	4	•	•	•	•	•	•	•	٠	•	•	•
South	39	41	45	42	41	44	*	40	44	39	.%	43	59	78	33	30	2
Southwest	•	•	•	•	•	•	•	45	3a	30	24	Żì	17	13	12	7	•
West	•	•	•	•	•	•	•	•	+	47	31	23	19	19	-	7	,

Table 5.4: Percentage of shaded area by Shade H03 for 21" March.

* Percentage of shaded area is not taken into account as the sun does not see the window.

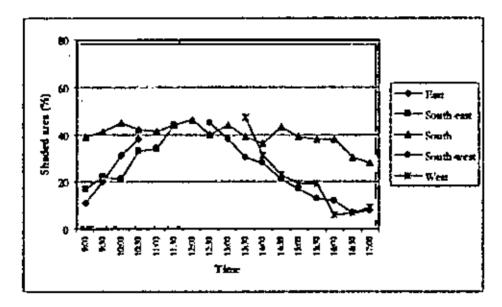


Figure 5.22: Percentage of shaded area by Shade H03 for 21st March at different orientations.^{1 (p. 35)}

Findings

It has been observed from the results of the simulations that the performance of horizontal shading devices remains quite consistent at south orientation only. It works better when the sun is opposite to the window pane at a high altitude. This performance drops when the sun is in a lower altitude and oblique to the window pane. The horizontal overhang is not capable to protect the window when the sun azimuth and altitude are low. So from these analyses, need for modification is evident when the sun is at low azimuth and altitude.

5.3.1.2 Performance of Vertical Shading Devices

The three selected vertical shading devices were oriented in the three cardinal directions (East, West and South) and two oblique directions south-east and south-west to evaluate their performance at different orientations. The results are given below with respect to individual cases.

Orientation	(1146)	66.99	tees	10,00	8011	0011	1200	12.0	140	1110	1400	14.30	19-00	15.30	uși	16.10	60721
	*		*	-5							*		1	*	••		
East	47	53	71	ព	•	٠	•	•	٠	•	•	•	•	•	•	•	•
Southeast	46	50	50	53	75	91	•	٠	٠	٠	•	•	٠	٠	*	٠	•
South	=1	87	8	91	91	8)	B 1	55	M	17	88	ស	ß	78	67	ភា	36
Southwest	╞╼╴	•	•	٠	٠	٠	•	*	π	58	55	*	#	45	45	++	51
West	•	•	•	•	•	•	•	•	•	49	7 0	66	52	40	ת	.16	n

Table 5.5: Percentage of shaded area by Shade V01 for 21^a March.

* Percentage of shaded area is not taken into account as the sun does not see the window.

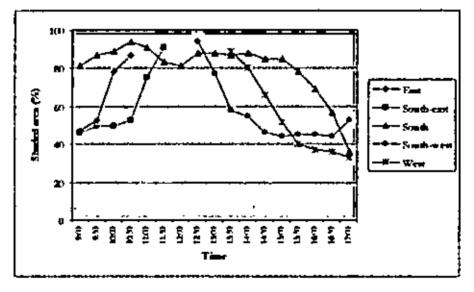


Figure 5.23: Percentage of shaded area by Shade V01 for 21" March at different orientations. ¹⁽⁶⁻⁵³⁾

Table 5.5 shows percentage of shaded area with respect to whole window area of Shade V01 at every 30 minute interval from sunrise to sunset. In the field investigation it was found that this shading device was attached with a south facing window. But through simulation, it is found that this shading device is not only efficient at south orientation, it also works well at east and west. This shading device is capable to shade 60% of the window area on an average at east and west and up to 94% window area at south orientation. But one thing is clear that the large overhang that holds the vertical fins makes the whole shading device effective at south. Actually vertical fins do not have significant role in protection of window at south.

Orientation	060	04.90	10-00	10.00	tt:	0011	(12()	12.00	(JHC)	UXN	(1)++1	14,30	ωvi	(3)	t0:01	té, X	ωź1
	*	×			1	2	*		- 14	5	4	*	*	*	1	**	*
Last	4)	41	8	82	٠	•	•	٠	*	•	•	•	•	•	•	٠	•
Southcast	#	36	43	46	*	٩0	•	•	+	•	•	•	•	•	•	•	•
South	76	R 3	स्त ।	R)	71	75	66	65	72	71	74	86	43	73	4	55	21
Southwest	•	•	٠	•	•	•	•	м	57	42	<u>,</u> ¥	39	35	39	ж.	48	51
West	•	•	*	•	•	•	•	٠	•	- în	**	50	45	*	41	x	26

Table 5.6: Percentage of shaded area by Shade V02 for 21" March.

* Percentage of shaded area is not taken into account as the sun does not see the window

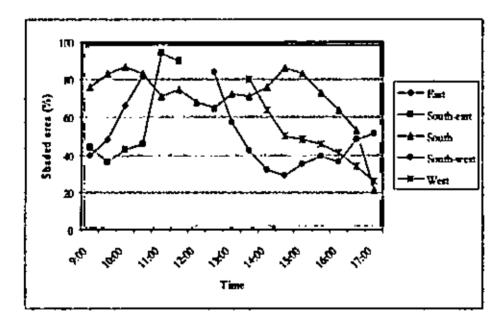


Figure 5.24: Percentage of shaded area by Shade V02 for 21" March at different orientations. 14-53

Io case of Shade V02, simulation results show that the device shades more window area at south orientation only when the sun is at an angle with the windowpane. That is when the sun is in southwest and southeast, this shading device is effective and capable to shade up to 87% of window area. In the field investigation it was found that this shading device was attached with a west-facing window. Through aimulation it is found that this shading device is effective at west orientation and it also shades well at east and west. This shading device is capable to shade 52% of the window area on an average at east and west.

Table 5.7 shows percentage of shaded area with respect to whole window area of Shade V03. In the field investigation it was found that this shading device was attached with an east facing window. Through simulation, it is found that this shading device is efficient at south orientation; it also works well at south-cast and south-west. This shading device is capable to shade 50% of the window area on an average at cast and west. This shading device is effective in south façade only when the sum is at an angle with the window.

Orientation	ra;co	0 . 40	1040	10.00	ÚU 11	00:11	0721	orti	1400	DC:FC	03+T	0011	0061	4C'51	14400	264.MP	1700)
	1		₹.	ĩ	54	*	•	54	۶.	ţ,	*	%	*	~	%	¥.	*
East	м	42	55	8	•	+	•	*	٠	٠	٠	•	•	٠	٠	٠	•
Southeast	43	.12	30	ж	47	£ 1	•	•	•	•	•	•	•	•	•	+	•
South	100	×	4 2	8	75	54	51	63	66	73	72	92	jon	101	ţΩ	L(2)	100
Southwest	•	•	•	•	•	•	•	54	51	50	45	35	ж	39	37	,12	41
West	•	•	٠	•	•	•	•	•	•	76	64	45	38	36	ы	25	3

Table 5.7: Percentage of shaded area by Shade V03 for 21" March.

* Percentage of shaded area is not taken into account as the sun does not see the window.

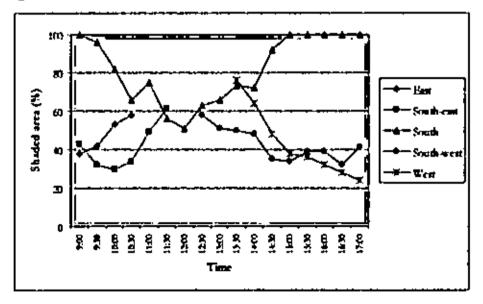


Figure 5.25: Percentage of shaded area by Shade V03 for 21" March at different orientations.¹⁶⁻³⁹

Findings

The investigation shows that vertical shading devices are effective on west and cast façade. The simulation results show that all these three vertical shading devices are capable to shade above 50% of the window area on an average at east and west. Vertical shading devices are also capable to shade up to 94% window area at south orientation. But one thing has to be noticed that the large overhangs that holds the vertical fins makes the whole shading device effective at south. Actually vertical fins do not have significant role in shading of window at south. They work efficiently when the sun is at an angular position with the window. They are not effective when the sun's altitude is low and perpendicular with the façade. It has also to be noticed that vertical fins are not efficient at east and west orientation when the sun is just in front of the window. This phenomenon needs further investigation.

5.3.1.3 Performance of Composite Shading Devices

The three selected composite shading devices (combination of vertical lin and horizontal overhang) were oriented in the five directions - East, West, South, South-cast and South-west and then simulated to investigate the influence of orientation on their shading performance. The results are given below with respect to individual cases.

Orientation	840	9760	(JFCD	07401	11500	0(11	1200	12.0	[01]	0.CL	1+W	u:st	ωs	11.10	iem	14.30	1700
	*	•	••	*	*	**	%	*	•	-	2	1	*	14	- 54	- 94	×
East	5	*	74	87	٠	٠	٠	•	•	•	•	•	٠	•	•	•	•
Southeast	56	36	56	62	75	25	•	•	•	•	٠	•	•	•	•	·	•
South	100	-	<u>3</u> 3	91	9)	90	65	М	10)	ท	9 U	M	10)	1(1)	10)	1(1)	107
Southwest	•	•	•	•	•	-	•	*	ы	69	24	59	Я	33	57	65	37
West	•	•	•	•	•	•	•	•	•	94	#2	76	1 0	35	48	40	25

Table 5.8: Percentage of shaded area by Shade C01 for 21" March.

* Percentage of shaded area is not taken into account as the run does not see the window.

Table 5.8 shows percentage of shaded area with respect to whole window area of Shade C01 at every 30 minute interval from sunrise to sunset. In the field survey it was found that this shading device was attached with a south facing window. Through simulation, it is found that this shading device is not only efficient at south orientation; it also works well at south-east and south-west. This shading is capable to shade 60% of the window area on an average at south-east and south-west and up to 100% window area at south orientation.

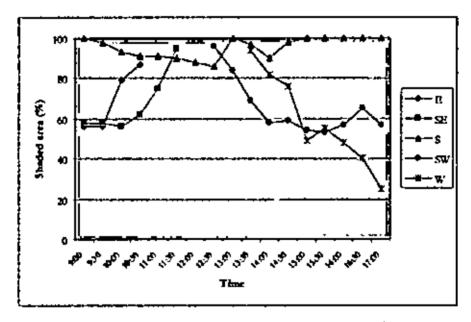


Figure 5.26: Percentage of shaded area by Shade C01 for 21" March at different orientations.^{1(p-30)}

In case of Shade C02, simulation results show that the device works better at south orientation specially when the sun is in an angle with the window pane. That is when the sun is in south-west and south-east, this shading device is effective and capable to shade up to 100% window area. In the field survey it was found that this shading device was attached with a south facing window. But through simulation it is found that this shading device is also effective in east, south-east and south-west orientation.

Orientation	(U-40	0740	IFCO	0-01	1100	0,11	17-L	12.10	ùн(t	911	(L) M	QC+1	th th	D751	1613	16.M	1703
	- 55	**	2	•	*	96	*			94		1		1	*	- 54	4
Rest	50	ъ Б	56	76	•	٠	·	•	•	•	•	•	•	*	•	•	•
Southeast	*	41	43	52	54	75	•		•	+		-	•	•	•	•	•
South	M	6 4	R2	76	74	71	67	67	67	73	BC)	15	R1	95	100	300	100
Southwest	٠	•	•	•	•	•	•	83	6	56	43	40	*	48	41	41	49
West	·	•	•	•	•	•	•		•	(0)	62	50	47	43	39	נל	21

Table 5.9: Percentage of shaded area by Shade C02 for 21" March.

* Percentage of shaded area is not taken into account as the sun does not see the window.

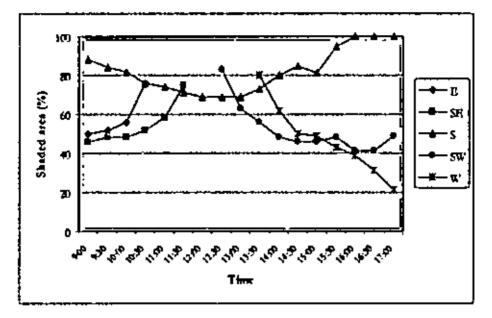


Figure 5.27: Percentage of shaded area by Shade C02 for 21" March at different orientations. 14: 37

Table 5.10 shows percentage of shaded area with respect to whole window area by Shade C03. In the field survey it was found that this shading device was attached with an east facing window. Through simulation, it is found that this shading device is effective at east and west orientation, but not consistent. The shading performance at south-east and south-west is more consistent than other orientations.

														1			
Orientation	8	9749	terro	10.10	e a	11:50	5	12.10	e S	0.41	£.	14,30	ê și	0451	ŝ	14.20	0741
	•4	*	И		%	•	*	•1	- 24	95	×	÷ %			*	24	•
East	35	+	54	π	•		•	•	•	•	•	•	•	•	•	*	•
Southcast	37	n) 7	38	45	"	·	•	•	•	•	•	•	•	•	•	•
South	100	:00	93	8 1	•7	57	\$1	50	67	69	ФÓ.	- 14	-100	100	10	100	100
Southwen	•	•	•	•	•	•	•	67	51	43	35	6٤	37	47	51	41	50
West	•	•	•	•	•	·	•	•	•	76	52	42	52	37	33	31	21

Table 5.10: Percentage of shaded area by Shade C03 for 21* March.

* Percentage of shaded area is not taken into account as the sun does not see the window.

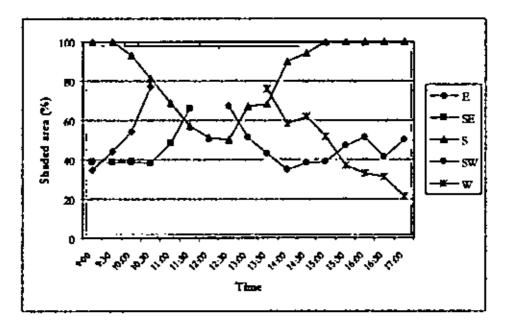


Figure 5.28: Percentage of shaded area by Shade C03 for 21" March at different orientations, ^{1 (s. 35)}

Findings

The analysis shows that composite shading devices are effective in south, south-east and south-west orientation. They are effective both when sun is in perpendicular and angular position with the window pane. Horizontal overhangs of the composite shading are effective to protect the sun when it is at perpendicular position to the window. And vertical fins of the composite shading are effective to protect the sun when it is at an angular position to the window. But their performance in cast and west orientation is not consistent.

5.3.2 Comparative Analysis of Shading Performance

To evaluate the shading performance on the basis of set criteria discussed earlier a comparative analysis among the selected shading devices has been summarised in the following section. This study will help in identifying the effect of different parameters and correlation among parameters.

5.3.2.1 Comparison among Horizontal Shading Devices

From above investigation on influence of orientation, it was observed that horizontal shading devices were effective on windows at south orientation than other orientations. At south orientation, all three shading devices were capable to shade maximum area of window pane at mid day. Simulation results show that among the three horizontal shading devices, Shade H01 can shade maximum 60% of the whole windowpane, Shade H02 can shade maximum 53% and Shade H03 can shade maximum 46% of the whole windowpane.

Table 5.11: Percentage of shaded area at different orientations by horizontal shading devices for 21" March.

Odentation	Shuding	0 -6 0	Q.60	10(1)	8.4	0)1	11:30	요리	97 <u>1</u>	0A(I	150	(u+)	(474)	0,461	1930	16-M)	160 1	17M
2	2	7.	7	••	÷4	*		1	~	94	¥	56	Υ.	۴.	*	-	*-	*
	HD1	2	7	.35	50	•	•	•	•	•		•	*	*	*	•	•	•
East	1102	11	30	77	*	٠	1	•	•	•	•	•	•	•	•	•	·	•
Ī	1103	11	Ð	31	R	•	•	•	•	•	•	· · ·	+	•	•	٠	•	•
South	1601	א	77	31	50	45	50	•	·	٠	•	•	•	•	•	•	•	•
	1102	12	15	20	28	37	52	ŀ	•	٠	*	•	*	٠	٠	*	•	•
	1103	17	22	71	33	ж	+	•		•	•	•	•	•	•	•	•	•
	1101	22	54	53	56	56	55	60	53	56	57	54	55	52	50	48	42	ĸ
South	1102	45	*	-	51	50	50	51	41	52	*		-6	42	0	.96	29	25
	H03	3	41	45	42	-41	+4	*6	40	44	39	36	43	39	39	х,	30	28
South	H01	•	•	•	•	*	•	•	65	50	41	м	75	2	19	15	12	10
west	1102	*	٠	•	•	•	•	•	×	**	33	23	17	13	8	4	٥	0
···· -	1103	•	•	•	•	•	+	•	45	35	30	28	21	17	13	12	7	8
	H01	•	•	•	•	•	•	•	•	•	62	-11	30	ĸ	16	13	11	7
Wei	HOÇ	•	4	•	*	•	•	•	•	•	я	30	21	12	4	3	0	0
f	FIO3	•	•	•	•	•	•	•	•	•	47	31	23	19	19	•	7	•

* Percentage of shaded area is not taken into account as the run does not see the window.

From table 5.11 it is observed that at cast, south-east, west and south-west orientations all three shading devices are oot effective. Sometimes these three shading devices can shade up to 63% of the window area but the efficiency drops frequently. Considering all these limitations, in comparison among these three horizontal shading devices, Shade H01 is capable to shade better than other two shading devices at all five orientations. Shade H01 performs better in protecting solar radiation in comparison to other two shading devices.

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Table 5.12 shows that at south orientation, Shade H01 can block 3411 watt solar radiation which is 54% of the total incident radiation (6314 watt). If it is compared with other two horizontal shading devices, it is found that Shade H02 can block 46% of the incident radiation and Shade H03 can block 41% of the incident radiation.

Table 5.12: Amount of direct solar radiation incident on windowpane at different orientations.

ŀ	Shad	e 1401	Shad	k 1102	Shad	e H03
Orientation	Shaded	Unshaded	Shaded	Unshaded	Shaded	Unshaded
	in Watt	în Watt	in Watt	in Watt	in Wett	in Watt
Past	1685	3761	2153	3764	2126	3761
South	2903	6314	3439	6319	3766	6326
South-east	2420	5020	2759	5005	2856	5013
South-west	1693	3983	1960	3981	2085	3980
Wrst	1138	2553	1318	2554	1421	2558

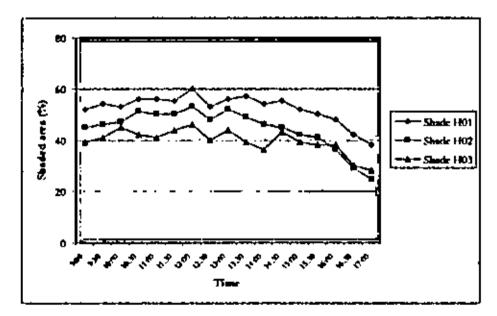


Figure 5.29: Comparison of percentage of shaded area at south orientation by horizontal shading devices for 21^e March.

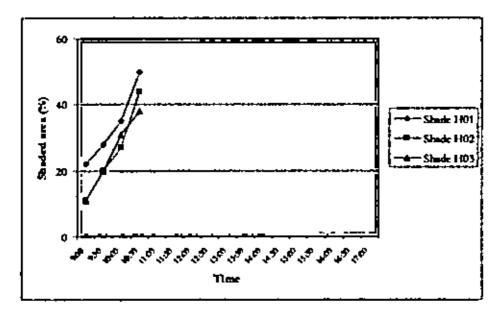


Figure 5.30: Comparison of percentage of shaded area at east orientation by horizontal shading devices for 21st March.^{14, 59}

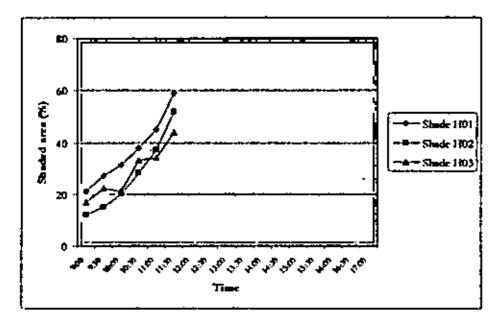


Figure 5.31: Comparison of percentage of shaded area at south-east orientation by horizontal shading devices for 21" March.^{14, 19}

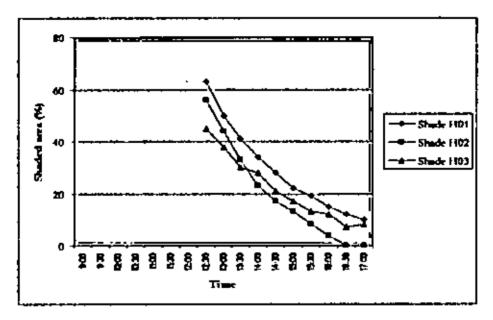


Figure 5.32: Comparison of percentage of shaded area at south-west orientation by horizontal shading devices for 21" March.^{1 (p. 35)}

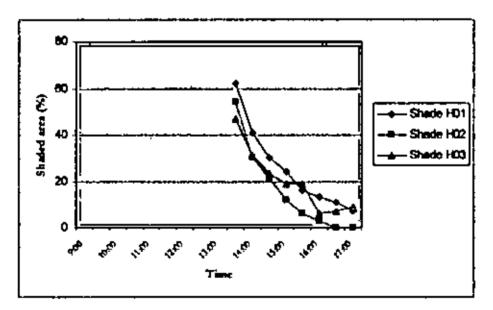


Figure 5.33: Comparison of percentage of shaded area at west orientation by horizontal shading devices for 21" March.¹⁶⁻⁵⁹

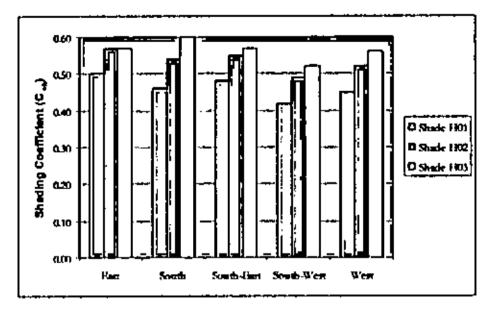


Figure 5.34: Comparison of shading coefficient of three horizontal shading devices at different orientations.

Although Shade H01 is more effective in comparison to Shade H02 and H03, the shading performance of Shade H01 is not up to the mark. It can not block almost 50% of the total incident radiation. This huge radiation enters through the unshaded part of the window pane into the space. So, horizontal projection of this Shade H01 is not enough to protect the window from the solar radiation properly.

Findings

The investigation shows that the horizontal shading device with larger overhang with respect to window height, shades more window area and reduces heat gain than other types. It indicates that projection depth of horizontal shading devices is the main determining factor for shading the window from direct solar radiation.

5.3.2.2 Comparison among Vertical Shading Devices

From aforesaid investigation on influence of orientation, it was also observed that Vertical shading devices were effective on windows at south-east and south-west orientation. So firstly, the performances of the vertical shading devices are evaluated with reference to their performance at these two orientations. At south-east and south-west orientation, almost same character of performance of these vertical shading devices has been observed. All three shading devices are capable to shade maximum area of window pane at the time when the sun is just tilted to east or west from south. Simulation results show that among the three vertical shading devices, Shade H01 can shade 53% of the whole windowpane, Shade H02 can shade 45% and Shade H03 can shade 42% of the whole windowpane on an average.

From table 5.13 it is observed that at east, south, west orientations all three shading devices are not consistent in their performance. Sometimes these three shading devices can protect almost 90% of the window area but the efficiency drops frequently to 15%. Considering all these limitations, in comparison with these three vertical shading devices, Shade V01 is capable to shade better than other two shading devices at all five orientations. So Shade V01 gives better protection from solar radiation in comparison to other two shading devices.

Table 5.13: Percentage of shaded area at different orientations by vertical	shading
devices for 21" March.	

Orientation	Shading	ŝ	(K.40	EM1	a di	tt.m	0011	(UST	12.0	1900	600	9 4 0	64.41	ещ Ц	15.10	0.41	<u>8</u> 3	1700
ő	8	5	•		*	۴.	*	14	*_	74	*	%	*	36	*	44	%	74
	Voi	47	51	71	•7	15	•	•	•	•	1	•	•	•	1	•	1	•
East	V02	40	48	6		*	1 .	!		•	•	•	•	٠	•	•	•	· ·
	V03	78	42	53	54	m	1		•	•	•	•	•	٠	•	٠	*	·
South	V01	*	50	50	53	75	1 1	ŀ	i •	•	•	•	•	•	•	•	•	•
cast.	V02	41	м	47	*6	*	91	·	i •	•	•	•	•	•	1	•	•	İ
	VDS	0	32	30	×	•	41	•	•	•	1	•	•	٠	•	•	•	•
	Vai	81	87	67	*	9 1	Ð	81	10	10	87	10	15	85	78	G	57	.8
South	V02	76	w	17	63	71	ন	1	65	72	71	к		63	ъ	64	53	21
İ	103	100	96	•	66	75	×	31	ø	60	73	72	92	109	100	100	100	100
South	VOI	•	٠	•	•	•	·	i ·	*	Π	58	55	*	#	45	45	44	55
weit	V02	1	•	٠	•	•	•	·	м	57	42	¥	27	35	37	56	41	\$1
	V03	•	•	•		•		ŀ	58	51	50	45	35	ж	39	33	32	41
	VOI		•	17	•	•	•	·	•	•	•	PC)	"	42	40	27	26	13
West	V@2	l ·	÷	۱ ۰		•	•	ŀ	•	•	e 0	*	50	40	×	31	7	36
	V03	•	•	·	†		•	1.	•	٠	76	44	43	.58	×	72	t:A	34

* Percentage of shaded area is not taken into account as the sun does not see the window.

	Stad	e V01	Sud	k V02	Shade V03			
Orientation	Shaded	Unshaded	Shaded	Unshaded	Shaded	Unshaded		
	èn Wett	en Watt	en Wett	in Watt	in Watt	in Watt		
East	1248	3766	1461	3766	1443	3763		
South	1102	6319	1783	6326	1336	6318		
South-cart	1490	5015	1962	5010	1998	5013		
South-west	1022	3984	1465	4364	1492	4364		
West	701	2556	906	2556	848	2556		

Table 5.14: Amount of direct solar radiation incident on window pane at different orientations.

Table 5.14 shows that at south-cast and south-west orientation, Shade V01 can prevent almost 70% of the total incident radiation. If it is compared with the other two vertical shading devices, it is found that Shade V02 can resist 60-65% of the incident radiation and Shade V03 can prevent 60-65% of the incident radiation.

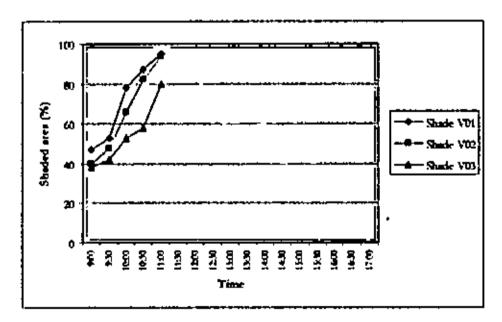


Figure 5.35: Comparison of percentage of shaded area at east orientation by vertical shading devices for 21" March.^{14, 50}

I.

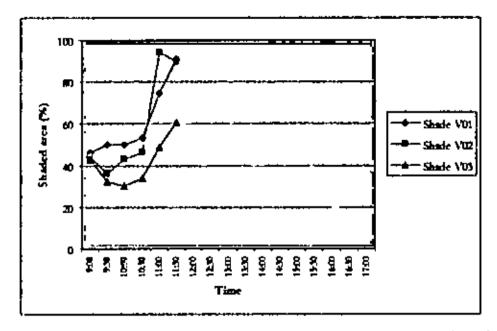


Figure 5.36: Comparison of percentage of shaded area at south-east orientation by vertical shading devices for 21⁸ March.¹⁰⁻⁵⁹

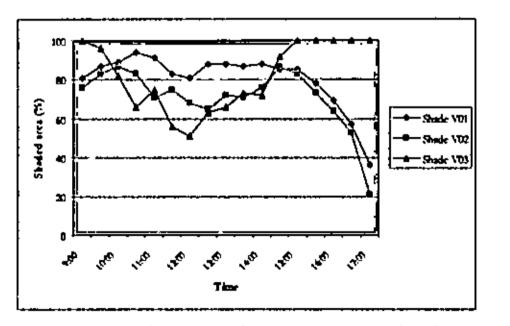


Figure 5.37: Comparison of percentage of shaded area at south orientation by venical shading devices for 21" March.

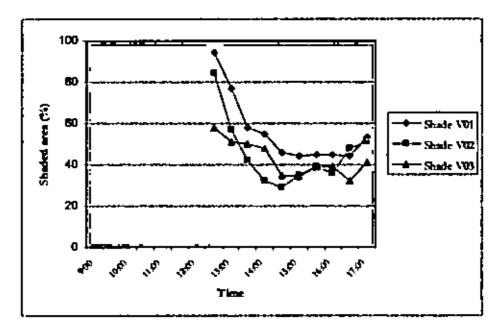


Figure 5.38: Comparison of percentage of shaded area at south-west orientation by vertical shading devices for 21" March.¹⁰⁻³⁰

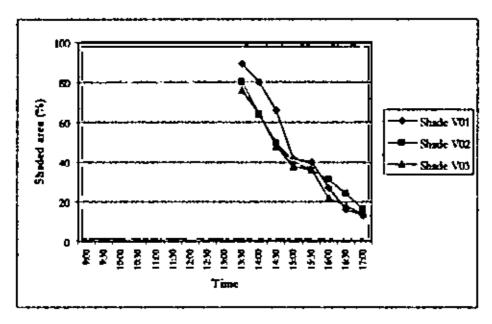


Figure 5.39: Comparison of percentage of shaded area at west orientation by vertical shading devices for 21^e March.^{1 (p 33)}

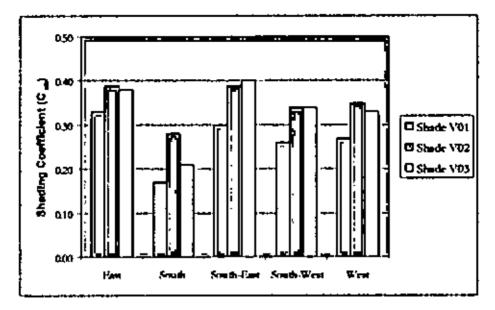


Figure 5.40: Comparison of shading coefficient of three vertical shading devices at different orientations.

Although Shade V01 is more effective in comparison to Shade V02 and V03, the performance of Shade V01 is not up to the mark. Actually it can not block 30% of the total incident radiation. This radiation enters through the unshaded part of the window pane into the space. So the depth, spacing and angle of the vertical fins of this Shade V01 are not enough to protect the window from the solar radiation properly.

Findings

The investigation shows that the vertical shading device with larger fin depth shades more than other selected vertical devices. It indicates the role of effective depth of shading devices (distance from window face to outer face of fins) including the gap between them on shading performance.

5.3.2.3 Comparison among Composite Shading Devices

From earlier investigation on influence of orientation, it was observed that composite shading devices were effective on windows at south, south-east and south-west orientation. So the performance of the composite shading devices is evaluated with reference to their performance at these three orientations. At south-east and south-west orientation, the same character of performance of these composite shading devices has been observed. Simulation results show that among the three composite shading devices, Shade C01 can shade maximum 96% of the whole windowpane, Shade C02 can shade maximum 83% and Shade C03 can shade maximum 67% of the whole windowpane. The percentage of shaded window area decreases when sun moves to east or west from south. Table 5.16 shows that at south-east and south-west orientation, Shade C01 can block almost 80% of the total incident radiation. If it is compared with the other two composite shading devices, it is found that Shade C02 can block 65-70% of the incident radiation and Shade C03 can also block 60-65% of the incident radiation.

Table 5.15: Percentage of shaded area at different orientations by composite shading devices for 21^a March.

						_												_
Otimotikon	Shade	00-00	(6-10	0.4û1	10-30	85	153	0147	1230	13-02	11.00	1409	271	1500	15.10	(14/10)	0771	מאלנ
ð	5	*	4	*	۶.	5	×.	*	1 4	*	۴.	%	*.	н	*	14	%	
	C01	R	54	77	67	•	•	•	•	•	•	•	•	•	•	•	•	•
East	C702	\$0	52	54	76	·	•	•	•	•	•	•	•	•	•	•	•	•
	COS	35	44	54	n	•	•	•	•	•	•	•	٠	•	•	•	•	•
South	C01	8	51	56	42	75	*	•	•	1	•	•	1	•	•	•	•	•
cati	C02	46	48	43	52	۶A	75	•	•	4	•	•	*	•	•	•	•	•
	C03	39	37	37	38	4	66	•	•	•	+	•	4	•	•	•	•	•
	C01	100	ų	93	91	91	9 0	m.	86	1(17)	17	90	ų	າຫ	ហោ	າຫ	101	100
South	C02	8	м	12	75	74	71	67	67	67	73	80	e e	F 1	45	100	100	100
	C03	100	100	91	8 1	61	57	51	50	67	68	90	1	. ioi	100	100	10)	100
South	CM	•	•	*	•	•	•	•	*		69	8	51	54	5)	57	65	n
west	002	•	•	•	+	•	•	•	8)	65	×	4	*	46	41	41	31	47
	<u> 005</u>	•	•	•	•	•	•	•	67	51	45	35	38	3	47	51	41	50
	C01	+	•	•	•	•	•	•	•	•	£	R	76	3	55	47	40	ъ
W'est	002	•	•	•	+	•	•	•	•	•	10	2	50	4	43	39	31	21
	(303	•	•	•	*	•	•	*	•	•	ĸ	Şa	4	52	37	33	31	2 1

* Percentage of shaded area is not taken into account as the sun does not ace the window.

	Shac	k C01	Shac	le C02	Shade C03			
Orientation	Shaded	Unstaded	Shaded	Unshaded	Shaded	Unshaded in Watt		
	in Watt	in Watt	in Watt	in Wett	in Watt			
East	960	3764	1255	3762	1342	3767		
South	364	6324	1211	5843	1180	6319		
South-east	1461	5015	1697	5008	1669	5025		
South west	788	3986	1159	3985	1388	4089		
West	531	2556	780	2558	801	2558		

Table 5.16: Amount of direct solar radiation incident on window pane at different orientations.

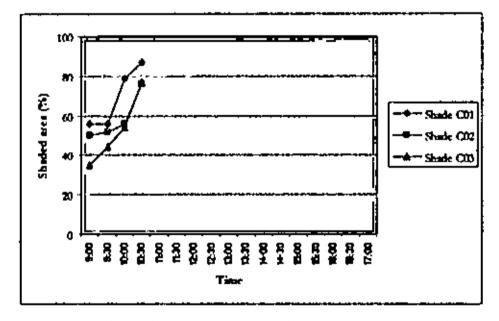


Figure 5.41: Comparison of percentage of shaded area at east orientation by composite shading devices for 21* March.^{1 (6, 53)}

The performance of composite shading devices is quite satisfactory at south orientation. They can shade up to 100% of window area. Although all three shading devices can shade up to 100% of window area, only Shade C01 is consistent in its performance throughout the day. It is clearly evident from figure 5.43. At south orientation, Shade C01 can block 5960 Wan, which is almost 95% of the incident radiation (6324 Wan).

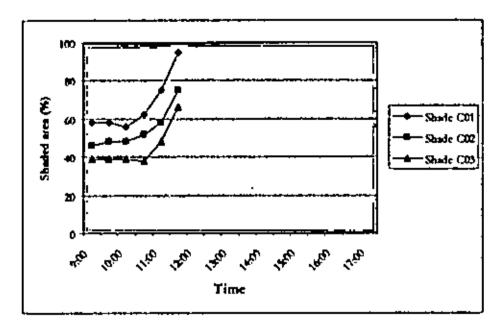


Figure 5.42: Comparison of percentage of shaded area at south-east orientation by composite shading devices for 21" March.^{1 (+ 35)}

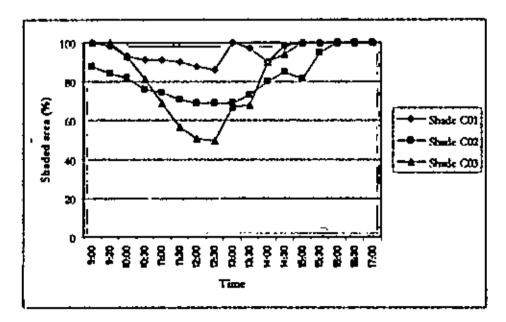


Figure 5.43: Comparison of percentage of shaded area at south orientation by composite shading devices for 21" March.

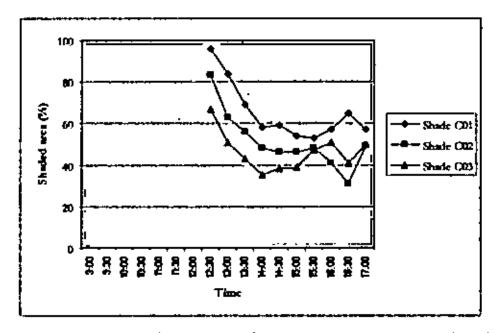


Figure 5.44: Comparison of percentage of shaded area at south-west orientation by composite shading devices for 21* March.^{34, 39}

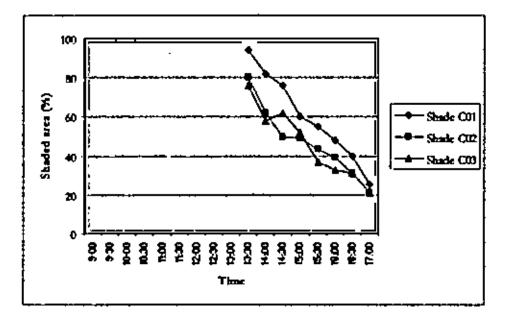


Figure 5.45: Comparison of percentage of shaded area at west orientation by composite shading devices for 21" March.^{14, 39}

From table 5.15 it is observed that at cast and west orientations all three shading devices are not consistent in their performance. Sometimes these three shading devices can protect almost 90% of the window area but the efficiency drops frequently to 15%. Considering all these limitations, in comparison among these three composite shading

devices Shade C01 is able to shade better than other two shading devices at all five orientations. So Shade C01 performs better in protecting solar radiation with compared to other two shading devices.

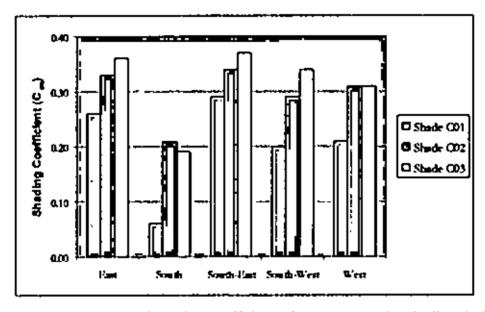


Figure 5.46: Comparison of shading coefficient of three composite shading devices at different orientations.

Although Shade C01 is more effective in comparison to shade C02 and C03, the performance of C01 is not up to the mark at south-east and south-west. It can not block almost 20%-30% of the total incident radiation. This radiation enters through the unshaded part of the window pane into the space. So the depth, spacing or angle of the vertical fins and horizontal overhang of this shade C01 can be modified to protect the window from the solar radiation properly.

Findings

The investigation shows that the composite shading devices are significantly efficient at south orientations. The shading device with larger overhang and fin-depth and smaller spacing between fins performs better than the others. It indicates the role of depth and spacing of fins and overhang on shading performance. With same depth and spacing of fins and overhang, shading devices are not as effective at south-cast and south-west like south orientation. Here angle of fins may help to cut off the direct radiation at south-east and south-west.

5.4 Conclusion

The influences of orientations on performance of various shading devices are now clearly evident. It is also evident that horizontal overhangs are effective on facades facing south, vertical fins on windows at cast and west orientation and composite shading devices are effective on windows at south-cast and south-west. It has been also observed that vertical fins are not effective at east and west orientation when the sun is in east or west side.

After investigating the performance of commonly used shading devices it could be stated that the design of the shading devices are need to be explored for desired performance. The results of both the studies indicate that depth and spacing of overhangs and depth, spacing and angle of vertical fins has significant effect on shading performance. Modification of these parameters may make the shading devices effective in different orientations at the critical periods.

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PARAMETRIC STUDY FOR OPTIMUM SHADING

CHAPTER: SIX

PARAMETRIC STUDY FOR OPTIMUM SHADING

After investigating the selected commonly used shading devices, it is found that the performances of these selected shading devices are not consistent through out the critical period of the day. Heat gain is directly proportional to the area of glass exposed to solar radiation and, therefore, unshaded glazed areas permit a large and rapid heat gain. Solar heat gain can be controlled effectively by optimising shading. To achieve optimum shading, the design strategy of shading devices is needed to explore further.

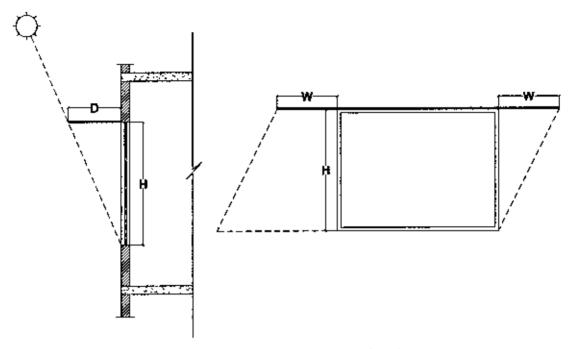
An investigation through parametric study to explore the strategies for optimum shading is presented in this chapter. Parametric study allows study of various specific alternatives with reference to performance of the model and choosing the best one. Series of parametric studies are performed where different parameters of shading devices are subjected to adjustment. Only one parameter is changed at a time in order to determine the relative influence of each. On the basis of the investigation and analysis that has been carried out in the previous chapter, some parameters have been chosen as variables to investigate through computer simulation for optimum shading. The simulation program 'Ecotect' (version 5.20) has been used for this parametric study.

6.1 Parameters for Optimum Shading Analysis

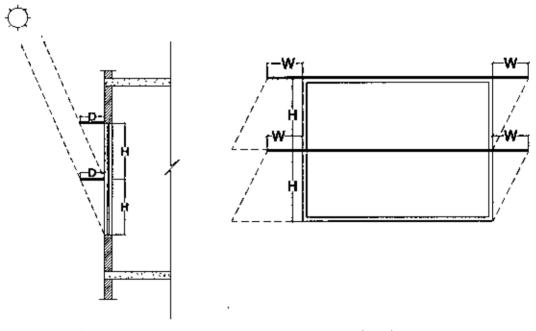
Before starting the parametric study, a set of parameters are considered as variables and some parameters are considered as constant. Variables and constants are considered separately for horizontal, vertical and composite shading devices. Variables that have been taken into consideration as different alternatives for simulations are given below:

A. Cases with horizontal shading devices:

- Depth (D) of horizontal overhangs
- Side offset (W) of horizontal overhangs
- Minimizing the effective height (H)



Section Elevation Figure 6.1: Schematic diagrams showing parameters of horizontal shading device.



Section Elevation Figure 6.2: Schematic diagrams showing parameters of horizontal shading device.

B. Cases with vertical shading devices:

- Depth (D) and spacing (S) of vertical fins
- Horizontal angle of vertical fins (0)
- Extension (X) of vertical fins above window

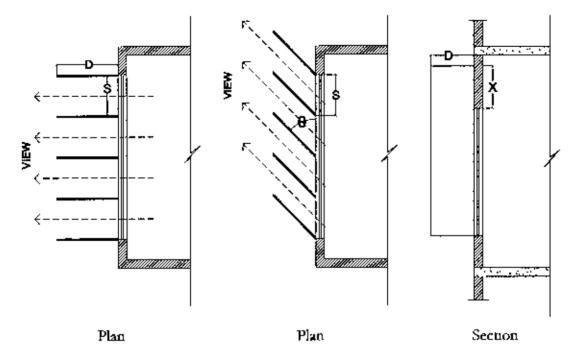


Figure 6.3: Schematic diagrams showing different parameters of vertical shading device.

C. Cases with composite shading devices:

- Depth (d) and spacing (h) of horizontal overhangs
- Depth (d') and spacing (w) of vertical fins
- Horizontal angle of vertical fins (Ø)

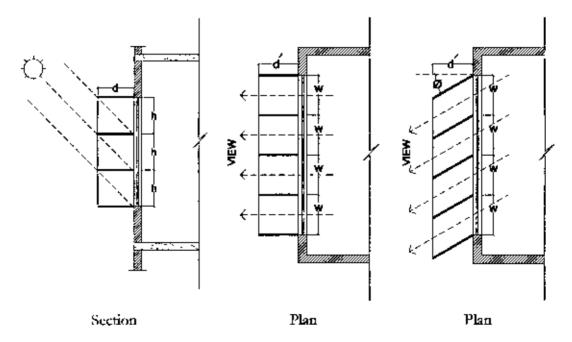


Figure 6.4: Schematic diagrams showing different parameters of composite shading device.

6.2 Simulation Day and Time for the Parametric Study

The considered day for simulation is 21st of March (Day: 80). The time period is considered from 0900 to 1700. The considerations behind selecting the day and time period were mentioned earlier.

6.3 Parametric Modelling

Models have been developed for the parametric study by 'Ecotect'. The following aspects have been considered for the parametric models:

- The room size for simulation model is 6000mm x 6000mm, which is considered as located in an intermediate floor of a high-rise building. The room size is taken from the typical high-rise column grid.
- A fixed window size (5400mm x 2400mm) has been considered with single glazed clear glass for the parametric study. The window width is determined by the column span as it is assumed that the window covers the whole span between two columns. The maximum window height found in the field survey is taken as the height of the window for the parametric study. Different shading devices are attached with it for simulation study.
- For case of calculation, thickness of the shade has not been taken into account and a study plane at the level of the exterior surface of the window wall has been considered.

In order to evaluate the shading performance of shading devices in reducing solar heat gain a base case situation is established by studying the unshaded window (without shading device) during the critical shading period of the year at different orientations.

6.4 Parametric Studies for Horizontal Shading Devices

From case studies and literature reviews it has been observed that horizontal shading devices are effective at south orientation. Through parametric study an attempt has been made to find out the size of the horizontal overhang for optimum shading at south orientation only. Three parameters (overhang depth, side offset of horizontal overhangs and minimizing the effective height) are considered as variables for this parametric study. Only one parameter is changed at a time in order to determine the effect of each parameter on the shading performance. The parametric study is started with a cettain value of parameters and then an increase in value of parameters has been considered to assess the impact of parameter on the shading performance. In all the cases, the shading performance is increased to a certain level with the increase in value of parameters. After that, the shading performance is not increased any more with the increase in value of parameters. This value of parameter is considered as optimum value for maximum shading. The results of this study are summarised in the following sections.

6.4.1 Effect of Depth of Horizontal Overhange

The parametric study is started for horizontal shading devices of varying depth, started from 750mm up to 1350mm from the exterior surface of the wall, over the window (model shown in figure 6.5). In each step impact of 150mm increment has been studied.

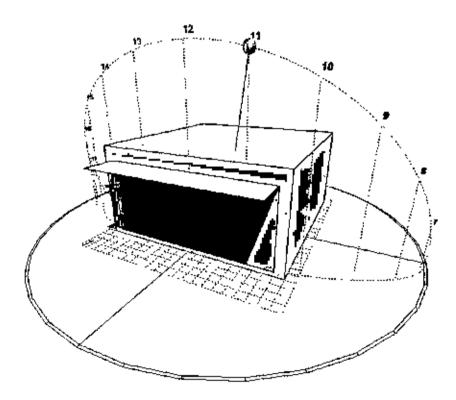


Figure 6.5: View of the model with horizontal overhang (1050mm depth) used for parametric study for 21st March (Ecotect output).

The percentage of shaded area of the window varies for different depths of overhang. Table 6.1 shows percentage of shaded areas for different overhang depth. The percentage of shaded area is increased with the increase of shading depth up to some extent. For 750mm depth, it shades maximum 74% of the window area and for 900mm depth it can shade maximum 88% of the window area. For 1050mm depth, it shades inaximum 100% of the window area and after that the percentage of shaded area is not increased with the increase of shaded area is not increased with the increase of shaded area is not increased with the increase of shading depth. But although for 1050mm depth, it shades maximum 100% of the window area, the percentage of shaded area is decreased along as time passes before and after mid day (shown in figure 6.6).

Table 6.1: Percentage of shaded area by horizontal overhangs with different depth for 21st March.

Depeb	COPACIL COPACIL	0 . 0	10-01	10.10	turut.	11.19	thái	12.30	13-00	13:40	14-(0)	14:50	9) 1 1()	15.10	(unde	14.30	er.t
In mm		*.	÷.	.		•	16		5	**	96	56	26	5	••	26	**
750	57	*	63	45	67	67	74	67	68	66	63	41	60	53	50	40	31
900	66	4	ĸ	77	79	83	54	(B)	83	79	74	69	*	10	54	43	27
1050	73	78	<u>81</u>	87	72	*	im	¥	94	91	м	79	75	66	59	4)	31
1200	74	80	ю	90	12	55	97	96	94	7 2	17	KZ :	Π	67	60	45	79
1350	74	81	#	89	*2	*	99	97	9	71	85	42	74	70	60	42	29

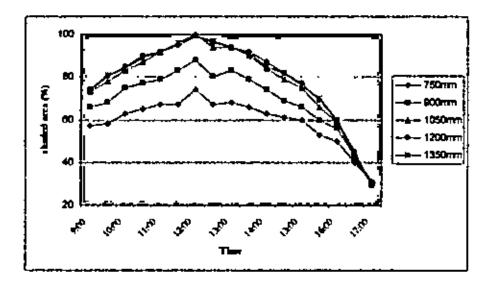


Figure 6.6: Percentage of shaded area by horizontal overhangs with different depth for 21" March.

From table 6.2, it is evident that more energy is saved with the increase of shading depth, which is not always applicable e.g. energy saving performance of 1050mm device is same to 1200mm and 1350mm device. Highest percentage (81%) of energy is saved by the devices having 1050mm to 1350mm depth, while the lowest was presented by 30inches device, which was only 61%.

Table 6.2: Shading coefficient by horizontal overhangs with different depth for 21" March.

	Shading depth	With shade	Without shade	
No.	in mm	in Watt	in Watt	Shading Coefficient
1	750	2463	6327	0.39
2	900	1673	63Z7	0.26
3	1050	1202	6327	0.19
4	1200	1185	6327	0.19
5	1350	1179	63Z7	0.19

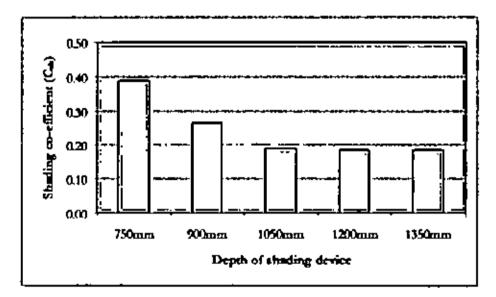


Figure 6.7: Shading coefficient by horizontal overhangs with different depth for 21* March.

From figure 6.7, it has been observed that the ratio of total energy received between shaded and unshaded situation is lowest for 1050mm to 1350mm depth of shading device, while it is highest for 750mm depth. The 1050mm device shows lowest shading coefficient 0.19, which is equal to that of 1200mm and 1350mm device. For 1050mm depth the shading device reaches the lowest shading coefficient and after that it goes same for 1050mm and 1350mm depth. The lower the shading coefficient is better against solar radiation gain.

Findings:

For 1050mm depth, horizontal overhang shades maximum window area and shows lowest shading coefficient. So, for 2400mm window height, optimum depth of overhang for maximum shading is 1050mm which is 7/16 of window height.

6.4.2 Effect of Side Offset of Horizontal Overhange

From the above investigation, it has been observed that honzontal shading device with 1050mm depth can provide maximum shading. After that, further increase in depth has no significant improvement to increase shading area. To improve the performance of 1050mm depth device at morning and afternoon, the effect of side offset of horizontal overhangs from window edge is studied. The parametric study is statted for horizontal shading devices with varying side offset, started from 300mm up to 1200mm (model shown in figure 6.8). In each step 300mm increment has been considered.

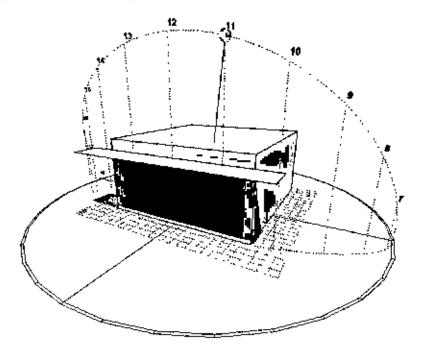


Figure 6.8: View of the model with horizontal overhang (1050mm depth) with 1200mm side offset used for parametric study for 21st March (Ecotect output).

The percentage of shaded area of the window varies for different side offset of overhang. Table 6.3 below shows percentage of shaded areas for different side offset. The percentage of shaded area is increased with the increase of side offset. I'or 1200mm depth, it shades 91% of the window area at 9 am, which is 18% higher than that of without side offset of 1050mm device. I'or 1050mm depth, it shades 84% of the window area and after that, the percentage of shaded area is decreased as time passes (shown in figure 6.9). At 5pm it can shade 44% of the window area, which is 13% higher than that of without side offset of 1050mm device.

Table 6.3: Percentage of shaded area by horizontal overhangs (1050mm depth) with different side offset from window edge for 21" March.

Side Offset	0-0	04:40	1040	10.10	1150	01:10	1100	97	1700	5	61¥1	1 C	15(0)	15.0	16(1)	ik,W	eri.
in mm	-			*		34	*	•				5			••		
0	73	72	61	87	•2	96	100	*	#	10	м	79	75	66,	59	43	31
300	71	83	. 177	93	9 4	101	100	*	1 77	*	<i>і</i> л.	M	Ð	73	ы	45	73
600	82	87	93	47		*7	'n	*	100	9 8	92		ц.	π	70	53	×
900	629	w	%	74	9H	ю	97	30	10)	1(1)	"	34	52	63	73	56	+1
1200	91	† 2	*	92	98	100	100	[f2)	urt -	1(1)	*5	95	92	H	ж	2	+

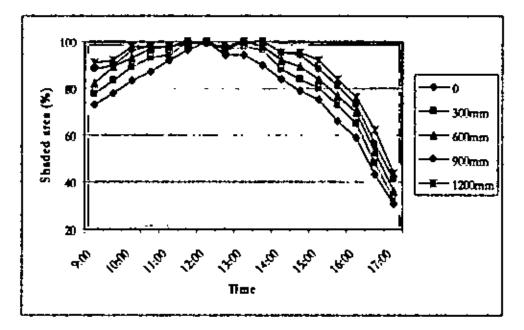


Figure 6.9: Percentage of shaded area by horizontal overhangs with different aide offset from window edge for 21" March.

Findings:

For 1200mm side offset from window edge, horizontal overhang shades maximum window area. So, for 2400mm window height, optimum side offset of overhang for maximum shading is 1200mm which is 1/2 of window height. 900mm side offset may also be used.

6.4.2 Effect of Minimizing the Effective Height of the Window

From the above investigation it has been observed that horizontal shading device with 1050mm depth with 1200mm side offset from window edge can provide maximum shading.

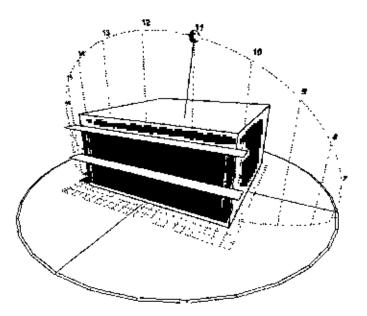


Figure 6.10: View of the model with horizontal overhangs (525mm depth) with 600mm side offset used for parametric study for 21" March (Ecotect output).

After that, to investigate the impact of the effective height of the window on the shading performance of the devices, two options have been studied. At first option, two overhangs are considered, one at lintel level and another at mid pane of the window. The depth of both of the overhangs is 525tnm, which is half of the previous depth (1050mm) with 600mm side offset from window edge (model shown in figure 6.10). At second option, four overhangs are considered, one at lintel level and the other three are distributed evenly at 600mm intervals. The depth of both the overhangs is 262mm

inches, which is half of the previous depth (525mm) with 300mm side offset from window edge (model shown in figure 6.11).

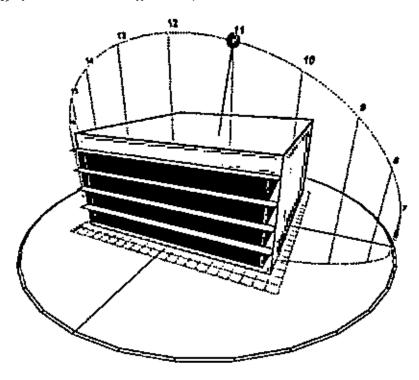


Figure 6.11: View of the model with horizontal overhangs (262mm depth) with 300mm side offset used for parametric study for 21" March (Reotect output).

Table 6.4: Percentage of shaded area by horizontal overhangs with different effective heights of the window for 21^e March.

Depth	(JAKI)	9740	0401	10-30	11:00	11,10	1200	12.0	00¥1	0141	14-00	14,30	19-00	0.41	14/13	IA, D	621
in mm	÷.		16	1 4	14	3 •	1 5	16	1 5	34	*		7		14	*	7
1050	9 L	92	747	9 .0	-	10)	100	97	100	100	ň	5	\$ 2	64	74	2	4
525	"	96	77	*7	99	\$ 7	100	*7	1(0)	# \$	#	97	7 3	19	ы	מ	តា
262	*	48	**	\$(*)	101	77	1(=>	10)	1(1)	1(+)	'n	99	16	96	*1	8	82

The percentage of shaded area of the window increases with minimizing the effective height of the window. Table 6.4 shows percentage of shaded areas for different options. For first option, it shades 95% of the window area at 9 am and 67% of the window area at 5 pm while for second option, it shades 98% of the window area at 9 am and 82% of the window area at 5 pm. At 5pm the percentage of shaded area for second option is 15% higher than that of for first option.

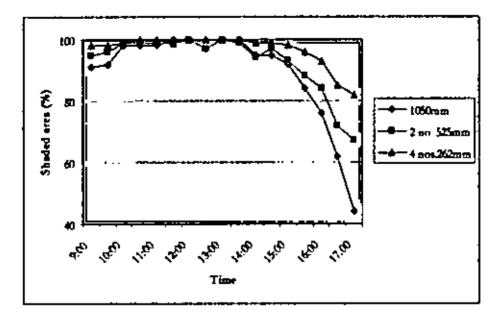


Figure 6.12: Percentage of shaded area by horizontal overhang with different effective heights of window for 21" March.

From table 6.5 it is evident that more energy is saved with minimizing the effective height of the window. Highest percentage (95%) of energy is saved by second option which is 4% higher than that of first option. The ratio total energy received between shaded and unshaded situation is lowest for second option. In the second option the lowest shading co-efficient is 0.05. The lower the shading co-efficient is better against solar radiation gain.

 Table 6.5: Shading coefficient by horizontal overhangs with different depth at different

 height for 21" March.

No	Effective height of the window in mm	With shade in Warr	Without shade in Watt	Shading Coefficient
1	2400	714	6327	0.11
2	1200	582	6327	0.09
3	600	339	6327	0.05

Findings:

Minimizing effective height of window is beneficial to improve the performance of shading device further. This could be done by using several overhangs on the window pane instead of one large overhang.

6.5 Parametric Studies for Vertical Shading Devices

From case studies and literature reviews it has been observed that vertical shading devices are effective at west and east orientation. Through parametric study an attempt has been made to find out the size and geometry of the vertical fins for optimum shading at cast and west orientation only. Parametric study is done for optimum shading at west orientation. As sun path is symmetrical about 12 pm, same solution will be applicable for east orientation. Three parameters (depth and spacing of vertical fins and angle of vertical fins) are considered as variables for this parametric study. The results of this study are summarised in the following sections.

6.5.1 Effect of Depth and Spacing of Vertical Fins

The parametric study has been started for vertical shading devices of varying depth, from 600mm to 1200mm from the exterior surface of the wall, over the window (model shown in figure 6.13) while the spacing between the first is considered as constant. In each step impact of 300mm increment has been observed.

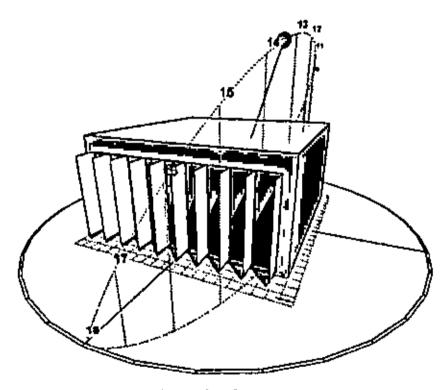


Figure 6.13: View of the model with vertical fins (600mm depth at 600mm interval) used for parametric study for 21^a March (Ecotect output).

Depth	8	01760	turco	10,30	11-00	11.10	00¢1	1210	t) U	0471	13+1	340X0	t\$411	0.Ft	16-(1)	14:39	17(0
ia 10400	14	N		1			14		1 +	4	4	÷	1	¥.			14
600	[•	•	•	•	•	•	i •	•	70	6)	#	37	л	22	ZL	7
900	.	•	•	•	•	·	•	ŀ	•	70	72		51	4	75	27	14
1200	·	•	•	•	•	•	•		•	71	72	8	6 3	57	43	X	×

Table 6.6: Percentage of shaded area by vertical fins with different depth for 21" Match

* Percentage of shaded area is not taken into account as the sun does not see the window.

The percentage of shaded area of the window varies for different depths of fins. Table 6.6 shows percentage of shaded areas for different fin-depth. The percentage of shaded area is increased with the increase of shading depth but not very significantly. For 600mm depth, the device shades maximum 70% of the window area and for 900mm depth it can also shade maximum 70% of the window area and for 1200mm depth it can shade maximum 71% of the window area. For 600mm, 900mm, and 1200mm depth, the minimum percentage of shaded area is 9%, 14% and 24% respectively. So, only increasing of depth of fins is not effective to shade the window from solar radiation.

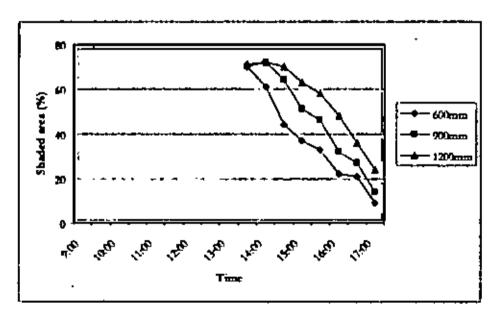


Figure 6.14 Percentage of shaded area by vertical fins with different depth for 21" March.¹

¹ Corresponding values of percentage of shaded area prior to hours abown are not indicated as the sun does not see the window prior to the time range abown period.

Findings:

The percentage of shaded area is increased with the increase of shading depth but not very significantly. So, only increasing of depth of lins is not effective to shade the window from solar radiation.

6.5.2 Effect of Angle of Vertical Fins

From the above investigation it has been observed that for vertical shading only increasing of depth of fins is not effective to protect the window from solar radiation. After that the increase in depth of fins is not further effective to increase shading area. To improve the performance of vertical devices, the effect of different angle of vertical fins with window surface is studied. The parametric study is done for 600mm, 900mm and 1200mm deep vertical fins with 30° and 45° angles with the line perpendicular to the window surface (model shown in figure 6.15, 6.16).

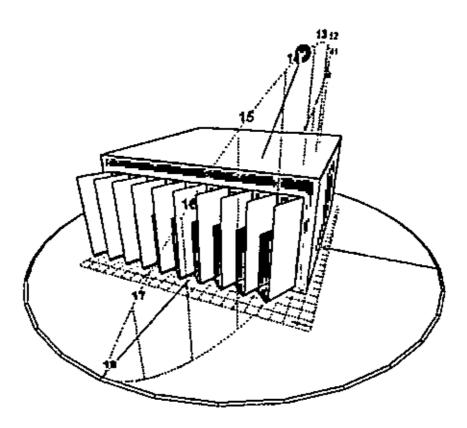


Figure 6.15: View of the model with vertical fins (900mm depth 30° slanted) used for parametric study for 21" March (Ecotect output).

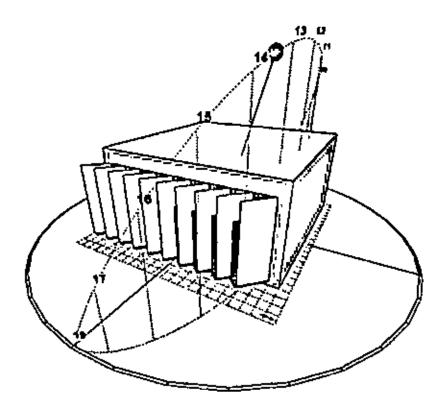


Figure 6.16: View of the model with vertical fins (900mm depth 45° slanted) used for parametric study for 21" March (Ecotect output).

Table 6.7: Percentage of shaded area by vertical shading devices with different depth and angle for 21st March.

Depth in mm	Angle	сни Сни	07-40	£uµi‡	10 X	0711	0¢-11	1200	1230	(UHCI	671	(J)+1	Q ¥1	ω π ι	15.21	1600	14,10	17.00
<u>۾</u> ک	₹	*	-	•	1.24	24	**	36	**	*	••	7	÷.	*	7-	İ *	74	
600	30"	ŀ	•	ŀ	•	ŀ	ŀ	•	•	ŀ	m	63	M	π	n	70	4	56
600	45*		•	•	•	•	·	•	•	1	8.	67	87	71	N	6	R2	73
900	30*	ŀ	•	*	•	•	•	•	•	•	85	n	F5	n	5 75	9 1	•1	67
200	45*		·	1	·	·	•	•	•	•	84	80	•0	93	92		97	97
1200	30°	·	•	•	•	•	•	•	٠	•	80	83	65	87	88	91	91	95
1200	45*	ŀ	·	·	•	•	•	٠	•	-	M	87	89	91	90) 1	*	73	×

* Percentage of shaded area is not taken into account as the sun does not see the window,

The percentage of shaded area of the window varies for different depths of fins with different angle. With changing the angle from perpendicular to the window surface the percentage of shaded area of the window is increased significantly. Table 6.7 shows percentage of shaded areas for different fin-depth with different angles. The highest performance is seen by vertical fins, 900mm depth with 45° angle. For 900mm depth with 45° angle vertical fins, it shades maximum 97% of the window area and after that the percentage of shaded area is not increased with the increase of shading depth. The performance of 900mm depth with 30° angle vertical fins is very close to that of 900mm depth with 45° angle vertical fins.

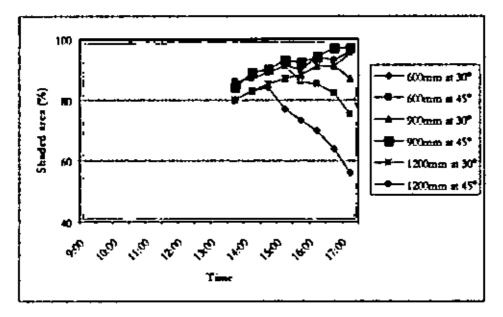


Figure 6.17: Percentage of shaded area by vertical shading devices with different depth and angle for 21st March.¹⁴⁽⁴⁾

Table 6.8: Shading coefficient by vertical shading devices with different depth and angle for 21^a March.

	Depth		With shade	Without shade	
Na	inam	۸agte	in Witt	in Warı	Shading coefficient
1	600	30°	564	2558	0.22
2	600	45*	384	2558	0.15
3	900	30°	444	2558	0.17
4	900	45*	346	2558	0.14
5	1200	30*	439	2558	0.17
6	1200	45*	347	2558	0,14

From table 6.8, it is evident that more energy is saved with the increase of shading depth, which is not always applicable e.g. energy saving performance of 900mm depth with 45°

angle vertical fins is same to that of 1200mm depth with 45° angle vertical fins. Highest percentage (86%) of energy is saved by the devices having 900mm depth with 45° angle vertical fins, while the lowest is presented by 600mm depth with 30° angle vertical fins, which is only 78%.

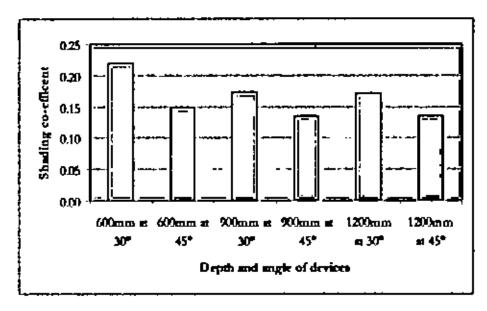


Figure 6.18 Shading coefficient by vertical shading devices with different depth and angle for 21^e March.

Findings:

For 900mm depth, vertical fin at 45° angle with the line perpendicular to the window surface, shades maximum window area and shows lowest shading coefficient. So, for 600mm spacing, optimum depth of fins for maximum shading is 900mm which is 3/2 of spacing between fins.

6.5.3 Effect of Extending of Vertical Fins above Window

From the above investigation it has been observed that for vertical shading increasing of depth and angle of fins is effective to protect the window from solar radiation. After that the increase in depth and angle of fins is not further effective to increase shaded area. To improve further the performance of vertical devices, the effect of extending of vertical fins above window is studied for 900mm depth with 45° angle vertical fins. The parametric study is started for vertical shading devices with varying extension of vertical fins above window, started from 150mm to 600mm (model shown in figure 6.19). In each step 150mm increment has been considered.

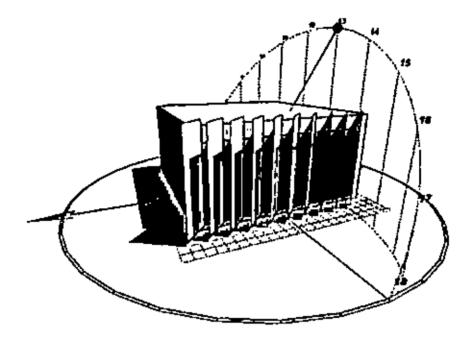


Figure 6.19: View of the model with vertical fins with 600mm extension above window used for parametric study for 21" March (Ecotect output).

The percentage of shaded area of the window varies for different extension of vertical fins above window. Table 6.9 shows percentage of shaded areas for different extension of vertical fins above window. The highest performance is seen by vertical fins with 600mm extension above window, which shades constantly 100% of the window area.

Table 6.9: Percentage of shaded area by vertical fins with varying extension of vertical fins above window for 21^{er} March.

Depth	£D-€D	06'60	torfo	05-01	to tt	11:10	1200	011	1300	04%t	140)	00141	(041	15.30	(U-91	16.30	1701
त्य का	ł.	26	5		4	1		1 4	14	1	1			3	1	55	ř.
150	•	•	•	•	•		•	•	•	90	93	*	*	97	9	77	101
300	•	•	•	•	•	•	•	•	•	35	95	я.	47	100	1(1)	1(=)	100
450	•	ŀ	·	•	٠		·	·	1	94	1(*)	100	10)	10)	1(*)	1(•)	109
600	·	•	·	•	•	-	·	·	-	100	100	2(2)	10)	1(1)	100	tin)	100

* Percentage of shaded area is not taken into account as the sun does not see the window.

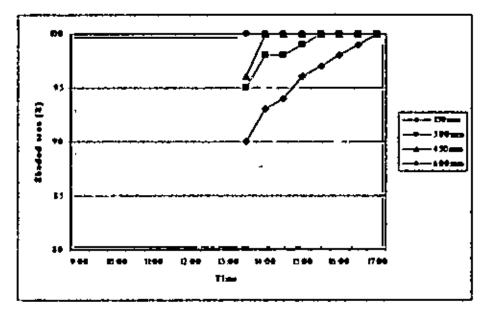


Figure 6.20: Percentage of shaded area by vertical fins with varying extension of vertical fins above window for 21st March.^{16,99}

From table 6.10 below, it is evident that more energy is saved with different extension of vertical fins above window. Highest percentage (99%) of energy is saved by the devices having 900mm depth and 45° angle vertical fins with 600mm extension above window.

Table 6.10: Shading coefficient by vertical fins with varying extension of vertical fins above window for 21st March.

No.	Extension	With shade	Without shade	Shuding Coefficient
	in mm	in Watt	in Watt	
1	150	218	2558	0.09
2	300	132	2558	0.05
3	450	67	2558	0.03
4	600	32	2558	0.01

Findings:

For 600mm extension above window, vertical fin shades maximum window area and shows lowest shading coefficient. So, for 600mm spacing, optimum extension of vertical fin above window for maximum shading is 600mm, which is equal to the spacing between fins.

6.6 Parametric Studies for Composite Shading Devices

Case studies and literature reviews so far done, reveal that composite shading devices are effective at south-east and south-west orientation. Through this parametric study an attempt has been made to find out the size and geometry of the horizontal overhangs and the vertical fins for optimum shading at south-east and south-west orientation only. Parametric study is done for optimum shading at south-west orientation. As sun path is symmetrical about 12 pm, the same solution will be applicable for south-east orientation also. Two parameters (depth and spacing of horizontal overhang and vertical fins and angle of vertical fins) are considered as variables for this parametric study. The results of this study are summarised in the following sections.

6.6.1 Effect of Depth and Spacing of Horizontal Overhange & Vertical Fins

The parametric study has been done for composite shading devices of varying spacing of horizontal overhangs and vertical fins, while the depth of the fins and overhangs is considered as constant. As composite shading devices are combination of horizontal overhangs and vertical fins, spacings of both devices have impact on the shading performance of composite shading devices.

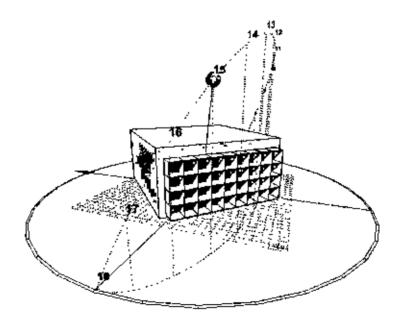


Figure 6.21: View of the model with composite shading device used for parametric study for 21^a March (Ecotect output).

Two options have been studied. At first option, spacing of vertical fins is considered as constant along with the depth of horizontal overhangs and vertical fins; only spacing of horizontal overhangs is a variable. The parametric study is done for 600mm and 1200mm spacing of horizontal overhangs. At second option, spacing of horizontal overhangs is considered as constant along with the depth of horizontal overhangs and vertical fins, only spacing of vertical fins is a variable. The parametric study is done for 600mm and vertical fins, only spacing of vertical fins is a variable. The parametric study is done for 600mm and 1200mm spacing of vertical fins is a variable. The parametric study is done for 600mm and 1200mm spacing of vertical fins is a variable. The parametric study is done for 600mm and 1200mm spacing of vertical fins is a variable. The parametric study is done for 600mm and 1200mm spacing of vertical fins is a variable.

Table 6.11: Percentage of shaded area by composite shading devices with different spacing for 21" March.

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1200 x 1200	•	•	•	·	•	*	•	im	10)	E2 .	*7	61	56	я	50	•	n

* Percentage of shaded area is not taken into account as the sun does not see the window.

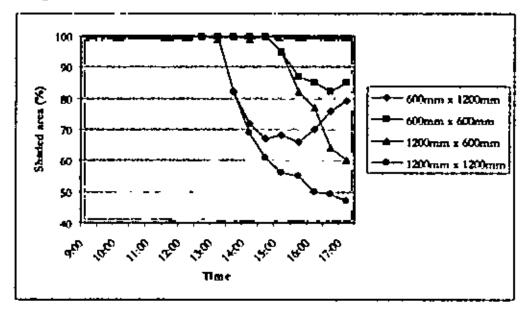


Figure 6.22: Percentage of shaded area by composite shading devices with different spacing for 21" March.^{1(p9)}

The percentage of shaded area of the window varies for different spacing of fins and overhangs. Table 6.11 shows percentage of shaded areas for different spacing of fins and overhangs. The percentage of shaded area is increased with the decrease of spating of fins and overhangs. The highest performance is seen by 600mm spacing vertical fins with 600mm spacing horizontal overhangs. For 600mm spacing vertical fins with 600mm spacing horizontal overhangs, it shades from 79 to 100% of the window area at different time of the day. The performance of other alternatives is not consistent (shown in figure 6.22).

Findings:

For 600mm depth of fins and overhangs at 600mm interval, composite shading devices shade maximum window area and shows lowest shading coefficient. So, at 600mm interval, optimum depth of vertical fins and overhangs for maximum shading is 600mm, which is equal to the spacing between fins and overhangs respectively.

6.6.2 Effect of Angle of Vertical Fins

From the above investigation it has been observed that for composite shading only increasing of spacing of fins and overhangs is not effective to protect the window from solar radiation throughout the day. To improve the performance of composite shading devices, the effect of different angle of vertical fins with window surface is studied in the following section. The parametric study is done for 600mm spacing horizontal overhang and 600mm spacing vertical fins with 30° and 45° angles with the line perpendicular to the window surface (model shown in figure 6.23).

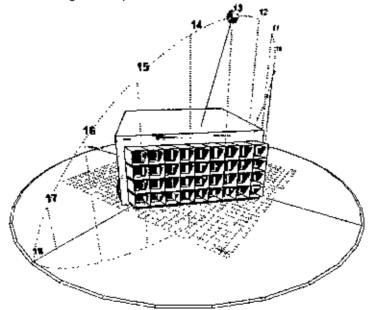


Figure 6.23: View of the model with composite shading device with slanted fins used for parametric study for 21st March.

The percentage of shaded area of the window varies for vertical fins of composite shading device with different angle. With changing the angle from perpendicular to the window surface the percentage of shaded areas of the window is increased significantly. Table 6.12 shows percentage of shaded areas for vertical fins with different angles. For 600mm spacing horizontal overhangs with 600mm spacing vertical fins with 30° angle, it shades maximum 100% of the window area. The performance of 600mm spacing horizontal overhangs with 600mm spacing vertical fins with 45° angle is almost same to that of 600mm spacing horizontal overhangs with 600mm spacing vertical fins with 30° angle (shown in figure 6.24).

Table 6.12: Percentage of shaded area by composite shading devices with different angle for 21^a March.

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45*	•	•	•	•	•	٠	•	180	ιn	**	*7	*	*7	47	100	101	52

* Percentage of shaded area is not taken into account as the sun does not see the window.

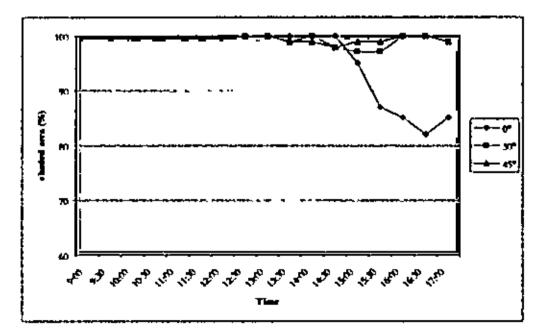


Figure 6.24: Percentage of shaded area by composite shading devices with different angle for 21st March.^{14,59}

Following Table 6.13 shows that, energy saving performance of 600mm spacing horizontal overhangs with 600mm spacing vertical fins with 30° angle is very close to that of 600mm spacing horizontal overhangs with 600mm spacing vertical fins with 45° angle. Highest percentage (99%) of energy is saved by the devices having 600mm spacing horizontal overhangs with 600mm spacing vertical fins with 45° angle.

 Table 6.13: Shading coefficient by composite shading devices with different angle for

 21* March.

		With shade	Without shade	
No.	Angle	in Wett	in watt	Shading Coefficient
t	0*	84	4015	0.02
2	30*	36	4015	0.01
3	45*	27	4015	t0.0

Findings:

For 600mm depth of fins and overhangs at 600mm interval, composite shading device at 45° angle with the line perpendicular to the window surface shades maximum window area and shows lowest shading coefficient.

6.7 Conclusion

Based on the observation made in the parametric studies, it can be stated that with the help of some simple strategies and modifications of shading devices, the optimum solution concerning solar heat gain issues within tall office buildings can be achieved for considerable period of office hours at five critical orientations for periods requiring shading. By providing a better protection against solar heat gain, the energy consumption to dissipate that heat could be reduced.

CHAPTER: SEVEN GUIDELINES FOR DESIGN OPTIMIZATION OF SHADING DEVICES

GUIDELINES FOR DESIGN OPTIMIZATION OF SHADING DEVICES

Shading is the major consideration to reduce solar heat gain in overheated periods. Shading of a window offers the first line of defence against heat gains from solar radiation. External shading device is the most efficient solar control as it cuts off solar radiation before reaching the window. The design of shading devices can primarily come from understanding the solar geometry. The efficiency of the window shading devices is largely determined by the orientation of the window. Every orientation of the window requires appropriate shading strategy.

In the previous sections, the theoretical basis and the results of the simulation studies were discussed. Based on the set criteria nine selected shading devices were evaluated through simulation. The evaluation of these selected shading devices in terms of solar control helped in identifying the factors that affect in reducing solar heat gain. To explore the strategies for optimum shading, a parametric study was pursued through series of simulations. The observations of the simulated behaviour that occurs due to changing parameters allow the identification of geometric elements, the reduction or introduction of which in the design contribute to reduce solar heat gain. The following sections present recommendations and guidelines.

7.1 Proposed Guidelines for Efficient Shading System

In view of all the investigations and on the basis of findings outlined above, a set of guidelines has been drawn for efficient shading to reduce solar heat gain. Investigations showed that different types of shading devices were appropriate for different orientations. The following recommendations are made for different orientations and for different types of shading devices. The recommendations and guidelines are particularly applicable for tall office buildings of Dhaka cny (longitudes: 90°23' East and latitudes: 23°46' North).

7.1.1 Guidelines for Horizontal Shading Device

• It has been found from the investigation that horizontal shading devices were efficient at south orientation only. Hence honzontal shading devices are appropriate

to protect the windows from solar heat gain at south orientation. It works efficiently from 10 am to 2 pm when the sun is opposite to the window pane and at a high altitude.

- The depth of the overhang depends on the window height and is independent of the window width. The performance of horizontal shading device increases with the increase of depth of the overhang. After a certain depth, the performance does not increase significantly with the increase of shading depth. The important factor is the ratio between depth of the overhang and height of the window.
- For optimum shading, the ratio between depth of overhang and height of the window is

D=7/16 x H

Where, D= depth of overhang

H= Height of window

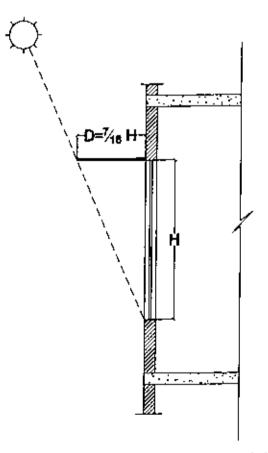


Figure 7.1: Schematic diagram showing parameters of horizontal shading device.

- When designing an overhang for the south facade, one must remember that the sun travels from the southeast before noon and to the southwest after noon. Therefore, the sun will outflank an overhang with the same width as window-width. Windows need wider overhang offset from the window edge (figure 7.2). The side offset from window edge also depends on the height of the window.
- The ratio between the side offset from window edge of overhang and height of the window is

W= H/2

Where, W= side offset from window edge

H= Height of window

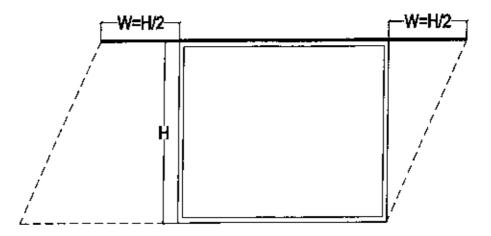


Figure 7.2: Schematic diagram showing parameters of horizontal shading device.

 Fot large height of windows, minimizing effective height of window is beneficial to improve the performance of shading device further. This could be done by using several overhangs on the window pane instead of one large overhang (figure 7.3). Installing several overhangs on the window pane is also appropriate when the projecting distance from the wall is limited for structural or other reasons. This could be important if a building is on or near the property line or there are certain restrictions by building regulations. As far as sun penetration is concerned, the scale of the overhangs can be changed at any time as long as the ratio of D/H and W/H ate kept constant.

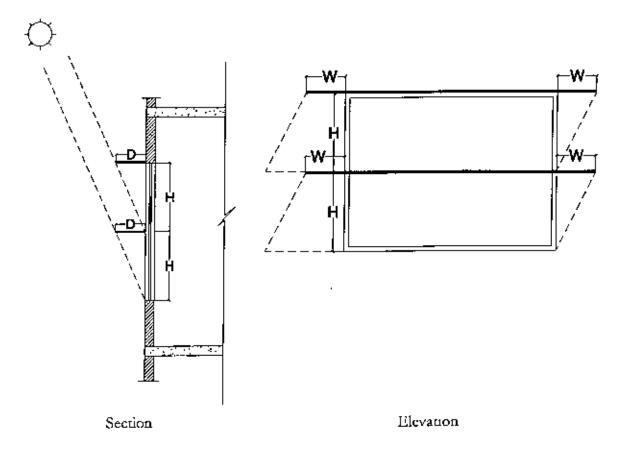


Figure 7.3: Schematic diagrams showing parameters of horizontal shading device.

7.1.2 Guidelines for Vertical Shading Device

- It has been found from the investigation that vertical shading devices were efficient at east and west orientation only. Hence vertical shading devices are appropriate to protect the windows from solar heat gain at east and west orientation. It works efficiently with the sun at a low alrivade.
- The depth and spacing of vertical fins is independent of window height and width. The performance of vertical shading devices increases with the increase of depth of vertical fins and with the decrease of spacing between vertical fins. After achieving certain depth, the performance does not increase with the increase of shading depth. The depth of vertical fin depends on the spacing between vertical fins and vice versa. The important factor is the tatio between the depth of vertical fin and the spacing between vertical fin and the spacing between vertical fin and the spacing between vertical fins.

 For optimum shading, the ratio between the depth and the spacing of vertical fin is D=1.5x S

Where, D= depth of vertical fin

S= spacing of the vertical fin

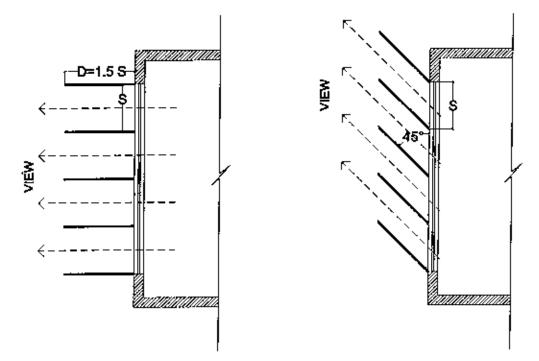


Figure 7.4: Schematic diagrams showing different parameters of vertical shading device.

- This type of device is most effective when the sun is at one side of the elevation. A vertical device to be effective when the sun is opposite to the window considered would have to give almost complete cover of the whole window. With changing the angle from perpendicular to the window surface to clock-wise direction, the performance of vertical fin increases significantly. Vertical fins at 45° angle with the line perpendicular to the window surface are most effective. This type of vertical slanted fin can be appropriate either when there is a desire to control the direction of view or when the view is not important.
- When designing a vertical fin for west facade, one must remember that the sun travels relative to earth from the southwest. Therefore, the sun will outflank a vertical fin with the same height as a window-height. Windows need higher vertical fin extending over the window edge. The extension over the top edge of window depends on spacing between vertical fins.

The ratio between extension of fins over the window edge and the spacing between vertical fins is

x=s

Where, X= extension of fin over the window edge

S= spacing between vertical fins

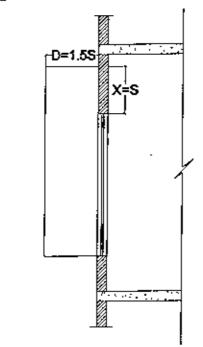


Figure 7.5: Schematic diagram showing different parameters of vertical shading device.

7.1.3 Guidelines for Composite Shading Device

- The investigation showed that the composite shading devices were efficient at southcast and south-west orientation. By controlling sun penetration by both the altitude and azimuth angle of the sun, very effective shading of windows can be achieved.
- The depth and spacing of vertical fins and horizontal overhang of composite shading device is independent of the window height and width. The performance of composite shading devices increase with the increase of depth and with the decrease of spacing between vertical fins and horizontal overhangs of composite shading device. The depth of vertical fin and horizontal overhang depend respectively on the spacing between vertical fins and horizontal overhangs and vice versa. The important factor is the ratio between the depth and the spacing between vertical fins and horizontal overhangs.

For optimum shading, the ratio between the depth and the spacing of the vertical fins
of composite shading device is

w=d

Where, d = depth of vertical fin

w= spacing between vertical fins

And the ratio between depth and spacing of horizontal overhangs of composite shading device is

h=d

Where, d= depth of horizontal overhang

h= spacing between horizontal overhangs

It means that depth of vertical fins and depth of horizontal overhangs has to be equal.

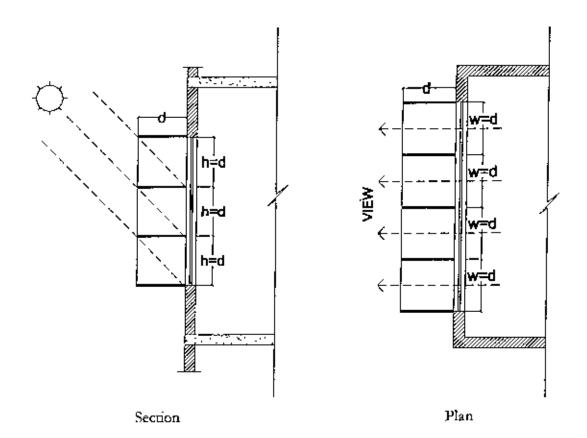


Figure 7.6: Schematic diagrams showing different parameters of composite shading device.

 With changing angle of vertical fin from perpendicular to the window surface to anticlock-wise direction, the performance of composite shading device increases. Vertical fin at 30° angles with the line perpendicular to the window surface are most effective.

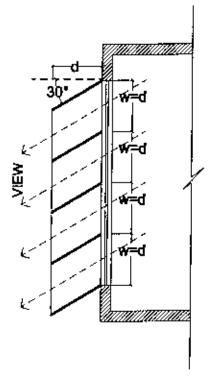


Figure 7.7: Schematic diagram showing different parameters of composite shading device.

 The Designer should first decide on the general appearance of the composite system. As far as sun penetration is concerned, the scale of the composite shading device can be changed at any time as long as the ratio of h/d and w/d are kept constant.

7.2 Conclusion

This work was an attempt to explore design strategies of efficient shading devices in tropical urban climatic context with a focus to teduce solar heat gain in overheated periods. To achieve the objectives, through investigations a set of strategies has been drawn that could help to design an efficient shading device in place of commonly practised ones in Dhaka. This work may also instigate designers design efficient shading devices with a reference to climate issues. At present the necessity to reduce the energy consumption in the buildings is an important issue in Bangladesh. The design strategics of efficient shading devices that have emerged as a direct outcome of this study are important in producing energy efficient design solutions. It may be extremely useful to have such strategies in mind during the pre-design and design stages of buildings, as passive solutions allow buildings to responsive with environment, thereby reducing energy consumption.

7.3 Suggestions for Future Research

Some of the most important ateas that need to be explored further are summarized below:

- More research needed to assess the impact of shading devices on daylight and ventilation through the window.
- Performance of shading devices can be evaluated in reducing heat gain for diffused solar radiation.
- Performance evaluation can be done with various thickness of shading devices with different types of materials. The use of shading materials and methods of installation with regards to their thermal properties need to be investigated for detailed recommendation for their uses.
- Possibility of mechanized movable shading device can be explored. The cost effectiveness of fixed shading device with comparison to movable shading device can be done considering maintenance and construction cost.
- Combination of shading devices (interior and exterior), movable shading devices and shading devices combined with special (solar-protective, low-e) glazing should be studied.
- 'Dhaka Metropolis Building Construction Rule 2006' can be examined considering solar shading in buildings.
- Impact of shading optimization on building energy consumption may be studied in view of energy saving potentials.

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APPENDICES

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APPENDIX A: Hourly Dry Bulb Temperature (°C)

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Hourly Dry Bulb Temperature (*C) Source Bangladeth Meteorological Department, Limate Division, Agargaon, Dhala Year 2005 Month: January

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ត	T	1	Ξ	: :-	Ē	2	80	- 17	61%	309	8) (R	20.2	19.61	100	18.3	17.7	÷	16.9	16.7	16.6	166	16.5	16.5	12.6	18.8
22	ſ	20	2	Ξ	12	3	ŝ	194	2()2	en <u>s</u>	217	21.7	107	187	174	11791	ΥŦ	344	13.9	13.5	144	151	16.2	17.8	194
51	ſ	12.3	1	15.8	17.6	5	30.5	30 27	2711	22.0	9 20 20	20.6	19.2	17.8	17 4	16.9	16.5	16.2	15.9	156	14.7	13.9	13.1	16.6	202
ᇟ		14 6	155	ş	17.2	12	195	9 (K	21.5	52.3	2,12	22.3	21.3	20.4	19.2	17.9	16.7	16.5	164	16.2	15.5	4 1	14.01	16.7	19.5
51	Γ	÷.	6	2	Ē	14.7	21.5	23.0	23.3	23.7	24 1)	234	22 K	22.2	21.5	20.7	100	194	18.81	1K 2	163	14.5	12.6	16.3	391
1.R		14 9	10,1	174	18.6	20.3	22.1	23.8	21.0	23.9	24.0	232	22.4	21.6	211.9	20.2	195	19.2	18.8	18.5	17.6	16.7	15.8	18.7	21.5
71		12, X	14 6	16.4	1H 2	21.3	+ L2	24.5	2541	23.6	26.1	342	22.3	ਸ਼ੋ	19.5	18.5	17.6	1.1	165	IF.	16.5	17.1	17.6	19.6	217
16		1141	941	16.2	N.71	11(12)	223	245	247	25.0	22.2	21 K	22.4	21.14	19.8	18 G	÷:	167	101	154	: 154	t5.4	154	H CE	20.1
		14.2	15.1	14,1	t7.0	É HI	211.3	ដ	225	211	362	<u>७</u>		ž	1 U U	140	1.5	11.4	Ę	16.8	15.9	14.9	14.0	ŝ	18.4
14		14.2	° ₽	5	16.4	1K.3	21.2	21	ដ	22.7	23.0	ដ	21.1	ន័	19.6	19,1	1% 5 1	17.5	16.0	15.6	35.6	15.5	15.5	17.5	19,6
5		1, H. K.	14.5	15.2	15.0	17.5	ر قا	ā	21.1	21.6	ы П	5	141	19.61	191	LR 3	177	175	172	Ē	16.3	15.7	151	3	18.7
12		13.6	147	15 1	17.0	18.5	20.1	11.0	ลี	ទ	232	3	215	ž	191	19.3	18.6	1K.1	5	17.2	14.6	1 L L L	154	ý	-
=		159	14.5	17.2	17 8	181	18.4	ξ	ŝ	2	1	5	1	15 ×	15,4	t57	5	155	11	15.2	15.3	155	15.6	ź	165
2		13.8	151	164	17.7	19.5	11 +	212	33	21	5	¥ เ	Ē	112	18	+	59	1 165	145	16.5	15.0	152	140	15.9	2
•		15.2	154	15.7	15.9	6-1	2111	5	5	6 1	÷.	22.3	21.1	211.0	12	7	176	5	t 1/1 5	53	16.0	5	12	_	2
•		16.1	16.9	17.5	1	19.8	21.5	231	5	57	572 57	ត	5	212	31.5	8 19.9	19:2	5 18.8	184	180	6	9 2 9	13.4		0 16.5
~		16.6	17.4	18.1	14.0	20.6	23	₽. #	7 245	е. Л	÷ Si	593 1	212	13	13.4	9 <u>2</u> 0.8	2151	195	191	8- 8- 7- 8-	5 179	17.5	110	11	7.17.0
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ا ت		1 154	0 16.7	7 18.41	5 10.3	5 21.3	7 232	-+	52	_	0 268	_	6 217	-	1 21 6	2 21.0	4 211.4	0 215	-	_	_	2 17.9	4 tú 6		821 0
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-	_	51.5	Ŧ	5	18.2	R	577	5 2 5	5	255	ວ ໃ	-+-	+	+	+	14	-+	+	+	+	╈	13.3	2	+-	164
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Hourly	Dry	Bulb	Temperature ((°C))
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Sources Bangladesh Meteorological Department, Climate Division, Agargion, Dhaka

Year 2005 Month: February

Day	1	2	3	_4	5	6	7	8	9	10	11	12	13	14	٤5	16	17	18	19	20	21	22	23	24	25	26	27	28
Turne					1																							
000	เม 4	162	124	13.5	13.9	13,4	17.0	18.0	17.8	18,4	16.9	18.0	20 R	21.6	20.6	22.5	237	24.4	23.8	22.2	23.8	21.0	199	202	t8 %	19.6	188	16.6
1.00	18.9	16.9	13.9	14.5	t5 2	15.6	18.3	19,6	19,4	20.5	189	197	21.9	22.5	21.6	232	24,3	24.7	24.1	27.9	24.6	22.2		21.1	t9.9	207	20.9	19.1
2:00	19.3	17.7	15.5	155	16.6	_17,8	19.7	21.2	21.0	221	21.0	21.5	23.1	23.3	22.63	23.9	25.0	25 t		23.5	25.4	23.5	22.1	21.9	21.0	21.9	229	215
3 00	19.8	184	17.0	16.5	17.9	200	21.0	22 N	22.6	24.0	23.0	23 2	24.2	24.2	21.6	24.6	25.6	25.4	247	24.2	26.2	247		22.K	22.0	23.0	25.0	24.0
4.00	20.9	197	18.2	183	19.9	21.8	22.9	245	24 3	25,0	24.3	24.9	26.1	25.6	25.2	25.7	26.7	26.7	25.6	25.3	27.7	25.6	247	241	23.4	24.8	26.4	29.0
5.00	221	21.1	19.3	20.2	22.04	23.6	24.7	26.1	25.9	26.0	25.5	26.7	28.1	27.0	_	26.9		27.9	26.4	26.4	29.1	26.4	26.3	25.5	24.9	26.6	27.9	28.4
6900	23.2	22.4	20.5	22.0	24.0	25.4	26.6	27.8	27.6	27.0	26.8	28.4	30.0	28.4		_			27.3	27.5	30.6	273	27.6	26.K	26.3	28.4	29.3	30.6
7.00	22.8	22.9	20.9	22.7	24.6	26 11	27.5	28 Z	28 L	27.4	27,2	29.1	307		29.3	287	2U X		26.2	28.3	30.9	27.5	28.5	27.3	27.1	29.0	29.5	30.7
8.00	22.4	23,5	21.4	23.5	25 L	26.7	28,5	28.6	28.5	27.9	27.6	29.9	313	29.3	30.0	29,3	30.6	<u> </u>	20,0	29.0		27.6	29.3	27.7	28.0	29.5	29 B	30.7
9,00	22.0	24.0	21.K	242	25.7	27.3	29.4	29.0	29.0	28.3	28.0	30.6	32,0	29.8	341.8	311 (1	11.4		29.9		31.6	27 R	30.0	28.2	28.8	301	30.0	30.8
10.00	21.7	22.9	21.1	234	24.7	261	28,3	27 K	28.1	27 5	27.1	29.6	30.7	287	29.9	29 G	305S	3/13	29.3		VIR	27.3	2940	27.3	27.9	29 Z	29.t	29 y
_0:00	21.3	21.9	203	22.6	23.6	24.8	27 t	26.7	27.1	26.8	267	28.6	29.5	27.6	28.9	29.2	29.6	29.5	28 к	29.5	30,0	26.9	27.9	26,3	27.1	284	28,3	291
12:00	21.0	2008	19.6	21 K	22.6	23.6	2640	25.5	26.2	26.0	26.0	27.6	2N 2	26.5	28.0	28.8	287	28.B	28.2	29.4	29.2	26.4	26.9	254	26.2	27.5	27.4	28.2
13/00	20.2	20,2	18.8	20.9	20.5	22.5	25.0	24.5	25.3	24 K	24.5	267	27.4	25.7	26.9	27.9	27.9	27.9	27.5	28.3	28.6	25.5	255	24.4	25.3	25.9	26.4	26,7
14:00	19.4	19.6		19.9	183	21.5	241)	Z3 4	24,5	23.6	22.9	25.8	26.6	25.0	25.9	271	_27.0	27.1	26.8	27.2	281	247	24.0	23,4	24.5	24.4	25.4	25.3
15-00	18.6	190	17.3	19.0	t6 2 ¹	204	23,0	22.4	23.6	22 -	21.4	249	25.8	24.2	24 8	26.2	26.2	26.2	26.1	26.1	27.5	23,8	22.6	224	23.6	22.8	24.4	23.B
16.00	18.3	18.5	17.0	18,3	156	199	21.2	21.6	22.9	214	213	24.4	25.4	235	24.0	257	25.7	25.6	24, B	259	26.6	23.2	22.1	21 H	23,1	21.7	231	22.7
17:00	1R.1	17.9	167	17.5	15.0	t9.5	21.4	208	22.3	20,4	21.3	24.0	24.9	22.7	212	25.1	25.3	25 L	23.6	25.8	25 R	22.6	21.7	21.3	227	20.7	21.8	21,7
18 00	17 8	17.4	16.4	16.8	144	19 11	20.6	200	21.6	124	21.2	235	245	220	22.4	24.6	24.8	24.5	22.3	25.6	24,9	22.0	21.2	2),7	22.2	176		206
19.IHI	t7.5	16.6	15.6	16 3	141	18,6	20.0	195	20.9	19,3	20.8	23.1	24.0	21.3	22.4	24 5	24.7	244	22.4	25,1	23.7	21.7	2)8	205	21.4	t9.4	196	20.2
20.00	17,3	15.8	14.8	15 1	139	18.2	194	12.0	2011	19.1	20.4	22.8	23,5	20.7	22 3	243	24.7	24 3	22.5	24.5	22.6	-	204	20.2	20.6	192	<u> </u>	19.8
21-00	17.0	<u>t50</u>	1411	152	116	17,8	18,8	185	194	1941	20 0	22.4	23.0	20,0	223	242	24.6	24 Z	22.6	24.0	21.4	21.2	2011	200	19.8	19.0	17.9	19.4
22.00	+	173	17.2	17.3	17.2	20.0	20.6	20 K	2017	20.5	21.6	22.2	224	20.5	22.0	23.9	24,1	24 t	22.7	23,8	22.4	22.8	208	2).2	201	2015	199	21.4
23 00	19.7	197	20.5	19,3	20.9	223	22.4	23.1	22.1	22.0	23.1	22.0	21.8	211	217	23.5	23.5	24 1	22.9	23.6	23.5	24.4	217	20.4	20.5	21.9	221	23.3

Hourly Dry Bulb Temperature (°C) Source Bangladesh Meesorological Department, Clumate Dansion, Agargaon, Dhaka Year. 2005 Month March

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9	ł	į				4 e				Ì	1					j ;	1 6				5				21.7
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28	t	ļ.	j s		1 5			0.04	1	2	i s	i î		31 =		5 / 5 7	ŝ F			1		ž) F	25.2
27	ſ	Ę	, F			2 7				1	:			11	i g	1	÷		i i	, <u>ज</u>	24.5	51.3	2	1	24.1
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53		Ĩ	ŝ	ŝ	77		X	i k		X X			к К	216	2		1 1		÷.	224	22.5	355		á	มี
2	ļ	7110		12		1	2 2	5		315	- ম	1		30	3 8	- - -	1		ر ۲	20.R	211.9	211.0	21.0	21.5	22 1
ន	ſ	1	Ē	23.8	214	5) X	1	22	52	24	20	212	R 61	Ę	100	1	213	ž	212		() 1E	21F R	22.9	24.9
5	Γ	30.0	27.7	ñ	2	Ţ	1.9	33.8	13 K	1	318	5	5		38.7	1	24		23.3	24.4	24 1	23.9	23.6	24.8	26.0
51		5	1	266	9 5		ŝ	32.5	335	ž	35.4	Ĩ	12.7	÷	315	1		171	315	26.8	4.22	25.9	25.5	34.8	24.0
ຊ		1	5	ន៍	38.4	Ē	19	, F		32.9	33.8	11,1	22	32.2	31.1	ļ	29.0	28.1	27.3	26.4	26.1	25.8	253	26.6	27.7
10	ľ	23.01	23.3	215	21,83	26.0	2 85	11.4	RON	31.2	Mé	111	30.7	302	8 GC	19.4	20.0	28,3	27.6.	26.9	26.2	25.5	24 K	25.7	26.7
18		34.0	5 5	12	2K 2	772	21	26.6	27.9	20		29.3	28°2	27.11	26.7	26.3	26.0	25.7	25.3	25.0	24.7	24.3	1142	24.3	24.6
1		21.11	24.2	25.4	26.6	27.0	51 52 52	10 J	31.3	32.0	32.8	31.0	31.1	3(1,2	295	с К К	2N.2	27.7	271	26.6	26.3	25.9	25.6	26 I	26,7
16		23.2	24.2	25.2	232	27.7	102	30.66	51.5	11 y	32.6	31.8	31.0	30.2	20S	38,9	2H 2	275	27.1	26.0	÷ X	25.4	24.8	25.4	25.9
15		न ह	22.7	241	25.4	27.0	2K 6	311.2	30-0	315	12.2	115	307	30 H	29+	1.% 1	27.1	20.5	25.R	25.2	34.4	23.6	ដ	23.0	34.9
14		21 ú	213	25.0	26.7	1 87	501	31.8	321	32.3	32.6	31.2	20 R	2 N ,4	281	ŝ	27.6	26.1	245	210	522	22.0	21.5	ដ	24.2
13		21.2	22.9	245	21.2	1.72	202	30.7	0.00	11.00	31.2	30.5	20.7	200	28.2	27.5	26.7	25.9	25.2	77.7	623	235	23.0	ទី	22.9
12		21.8	223	22.9	234	23 T	23.9	242	34.6	25.1	25.5	25.1	5	24.2	23.9	23.5	23.2	ន្ត	22.7	сį.	ลี	ลี	5	215	24.9
11		247	24.7	24,8	24 N	26.4	2K II	22.6	20.5	104	203	23.6	5 5	27.1	26.2	25 1	t to	24,1	3	234	ភ	ង	33.4	ដ	245
2		235	245	25.5	26.5	29.1	205 1	102	32.8	33.6	111	3.5	72.7	31.8	316.7	29.5	÷ ¥5	Ř	27.6	27.2	2	30.1	25 G	٥ <u></u>	26.3
÷		23.4	24.7	25.3	26.2	27.7	2J.1	30.6	ы. Ж	31.8	32.4	31.8	312	311.6	29.6	29.7	27.7	ŝ	27.0	26.6	ş	22.5	5	5	22.7
20		25.4	25.9	20.3	26.R	23 K	폾	N N N	30.9	¶. 14	33.0	32.0	310	3 (1)	ຄ ຄ	÷₹	27 (ŝ	ñ	2/i. R	292	ž	545	ສັ	ŝ
~		242	25.1	25.9	30.8 1	2.95	30.5	H H	11.7	55	112	10.1	313	ţ	2.02	2K.5	27.6	2.1	22	20.2	ž	ж К	25.6	¥. ¦ک	25.2
9		24.5	25.7	268	28.0	т Я	ς Ω£	321	32,R	315	342	5	ų	Ē	305	8	38,8	27.9	5	36.2	् श	5	255	25.4	25.3
ц		24.5	25.4	26.3	5	247	ų.	22	12.2	뉩	33.2	326	ŝ	31,4	Ĩ	24.0	29.2	2R.6	Ч. К	- 1 1	26.9	S.S.	÷ 30		ឡ
+		214	និ	22	ŝ	ยั	11.4	25	319	ž	35.2	Ŧ	17	ş	11	300	° KZ	27.5	2			_	ŝ	_	21.8
5		23.7	24.5	5	20.2	28.4	ų.	Ч. Г	5	2	Ŧ	33.3	125	Ē	Ъ.	22	÷ 20	2R 3	5	_		-+	,		22
~		22.0	232	24.3	25.5	27.8	30.1	32.4	32.9	314	910 1	RTE	33	ğ	20 81	ž	5	Ş	_ [23.2
-		21.0	27.1	23.7	155.1	27.1	± 62	9	11.5	321	32.6	4	í.	8.62	8. N N	21.8	26 H	24.2	ង	ຄື	÷,	3	ម ព	23.0	23.0
ΨŪ	Time	θů O	100	807 2	200	4.00	83	6:00	7.60	R R	0 11)-6	80 19	1950	[12,414]	11 11	8	15.0	IU-01	17,00	18 (H)	19-00	2002	8 17	년 8	8 2

Hourly Dry Bulb Temperature (°C

Source: Bangladesh Meteorological Deparement, Climate Division, Agargaon, Dhaka

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Year, 2005 Month April

1Day -	1	2	3	4	5	6	7	8	9	10 1	11	12	13	14	15	16	17	18	12	20	21	22	23	24	25	26	27	28	29	30
ว๊เกเต																									÷.'		2r i		- 27	
0.00	23.0	22.6	23.8	2012	22.8	25.2	2540	26.3	26.0	26.6	25.6	26.4	22.8	25.6	26.0	26.5	27.2	249	27.6	2Я К	233	27.2	27.0	22.6	23.0	25.4	24.0	25.0	22.2	222
1.00	24.3	24.7	25 9	22. 1	24.6	26.3	25.9	27.2	26.8	27.5	26.4	26.8	249	26.7	27.2	27.1	2H [267	28.5	29.5	261	28 2	28.0	2511	249	26 4	25.9	26.5	23.6	239
2:00	25.7	26.9	27.9	24.1	26.3	27.3	26.9	28.1	27.5	28.3	27.2	27.2	26.9	27.9	28.4	27.5	291	28.4	29.4	30.5	29.0	292	29.0	27.4	267	ZN 2	27.9	28.1	251)	257
<u> 100 -</u>	27.0	29.0	300	26 0	28.1	28.4	27.8	29,0	28.3	29.2	26.0	27.6	29.41	29.0	29.6	28,4	3040	3(12	30,3	31.0	31.8	30.2	30.0	29.8	2 8 6	29.6	29.8	29.6	26.4	27.4
400	28.1	30.3	31.2	27.7	29.1	29.5	29.1	29.9	29.5	30.4	29.3	29.2	31E1	30,3	316	29.9	31.2	31.3	31.6	32.0	32.7	31.6	10.8	30.8	29.6	30.7	30.9	31.1	28.1	28.5
5-10)	29.2	31.7	32.4	29.3	30.0	305	34,3	9.IK	30.8	31.6	311.5	30.9	31.3	317	31.5	31.5	32.5	32.4	32.9	33.0	_	33.0	31.7	31.8	30.6	31.8	32.1	325	29.9	29.5
6-00	311 3	33.0	33.6	3t.0	31.0	31.6	31.6	31.6	32.0	32.8	31.8	12.5	32.4	330	32.5	33,0	33.7	315	14.2	34.0	346	34.4	32.5	32.5	31.6	329	33,2		31.6	
7,00	30.5	33.2	138	31.5	31.3	32.1	32.1	32.4	327	33,3	32.4	329	331	336		13.1		34.1			34.6	34.9	331	332	32.1	333	33.2		30.3	306
R 00	30.8	31.3	14 I)	32.0	31.7	327	325	11.1	33,3	33, R	33.0	33.2	33,9	34.1	14 2	337	34,3		35.0		<u> </u>	353	336	336	127	33.6	331	<u>.34.5</u> 34.9	291	31.1
9.00	31.0	33.5	¥2	325	32.0	33 Z	33.0	13.7	34.0	343	33.6	33.6	346	34.7	35.1	3413			35.4	35 t	346	35.8		340	332	340	331		· · · · ·	31.7
10:00	10,8	32.7	334	31.2	31.6	32.6	32.5	33.0	333	32.2	32,0		337	34.0	34.7	332	337		34.7	344	145	35.1		335	129	<u>.,</u> 303	323	35.4 33 3	27 B = 26.2	32.2
11.00	30.5	11.8	32.6	31.2	31.2	324	32.1	32.3	32.5	30.1	304		32.9	33,3	342	32.4	32.9		33.9	33 K		343	33,1	37 [14.9	271	31.4	31.1	20.2	31.5
12.00	341,3	31.0	318	30.6	. 311 K	114	31.6	31.6	31 K	28.0	28,8	317	32(1	12.6	338	316	3241	33.6	33.2	33.1	344	33.6	32.6	32.6	124	236	30.4	29.0	230	<u>307</u> 300
13(0)	28.9	29.9	29.1	29.5	30k.t	30,7	30.7	307	311.5	27.5	281	341,3	31.2	31 H	32.6	30.9	31.3		32.7	121	33 5	32.7		31.9	29,8	24.2	28.7	27.7	23.1	287
14/00	27.6	28,9	26.3	ZH.5	29 \	30,1	29.9	29.9	29 1	26.9	27.3	29.0	30.4	31.0	3.4	30.2	3917	324	12.1	314		31.7		31.3	27.1	24.9	26.7	26.3	23.2	27.3
15:00	26.2	27.8	23.6	27.4	28.6	29.4	29.0	29.0	28.0	26.4	26.6	27.6	29.6	31,2	30.2	293	300	31.2	31.6	306		30 K	309	30.6	24.5	25.5	24.8	25.0	23 1	27.5
16.00	25.7	277	23.3	26.7	28.2	28.6	28,1	28,3	27.B	26.3	26.4	27.1	29.0	29.7	295	28,9	294	30.6	311	28.7	31.1	30.4	30.2	300	24.9	25.3	248	25.0	23.5	24 5
17986	25.2	27.5	22.9	25.9	27.8	27,8	27.3	277	27.6	26 1	26.2	26.7	28.4	29.2	28,9	28.4	28.8	29.9	30.5	26.9	301.6	29.9	295	29.3	25.2	25.2	248	25.0	237	24.5
18-00	24.7	27.4	22.6	25.2	27.4	27 0	26.4	27.0	27.4	26.0	26.0	26.2	27.8	28.7	28.2	27.8	28.2	1	<u> </u>	25.0	30.0	295	28.8		25.6	25.0	24.8			<u> </u>
19.00	24.3	26.7	21.9	24.8	27.0	26.7	26.3	26.8	27.2	26.0	25.9	25.3	27.5	28,4		27.7	26.5		29.7	24.8		29.0	28.2	28.1	255	24.9	24.7	25.0	23.9	21.6
20.00	23.8	26.1	21.3	24.4	26.6	26.3	26.2	26.7	271	26.0	25.9	24.5	<u> </u>	281	27.4	27.5	247	28,4	29.5	246	28,7	28.5	276	27.4	255	24.9		247	23.6	21.6
21.00	23.4	25.4	316	240	26.2	26.0	261	26.5	26.9	26.0	25.8		<u> </u>	27.8	• •	27.4	23.0	28.0	29.2	24.4	•	28.0	27.0	<u> </u>		<u> </u>	24.7	24.3	233	21.6
22 (60	22 K	247	21.7	24.6	25 3	24.9	25.2	261	28.3	26.7	26.3	25.3	26.2	26.4	26.6	27.3	23.4	25.9	28.8	24.0		28,0	26.3	26.8	25.4	24.6	24.6		23.0	21.6
23.00	22.2	24 1	22.9	25.2	24.5	23.7	24.9	25.6	29.8	27.5	26 9	27.1	25.6	249	26.3	27.3			28.4	23.7	25.6	28,0 28,0	26 3	26.8 26.8	26.0	25.9	251	25.7	24.9 26.7	23.8

Hourly Dry Buib Temperature (°C)

Source, Bangladesh Metcorological Department, Climate Division, Agurgaon, Dhala

Year 2005 Month: May

Day	1	2	3	4	5	6	7	8	9	10	n	12	13	14	15	16	17	16	19	20	21	22	23	24	25	26	27	28	29	30	31
Time]																							-0				,117	<u> </u>
0:00	21.6	23.4	24.0	25.R	236	22.6	23,4	25 2	31.2	28.2	27.4	26,6	25.0	23.5	25.9	27.2	24.2	21 R	2841	23.3	24.4	28.0	25.0	26.8	27.3	28 6	26.2	29.0	28.6	28.2	28.4
1.00	216	25.3	25.6	26.3	25.8	241	25 L	24.6	29.5	291	28.5	28,7	26.7	25.3	25.9	286		214	-	24.7	24.9	26.2	26.2	27.9	27.9	29.3	27.8	29.8	29.5	20.2	29.6
2.00	25.6	27.1	27.2	26.7	28.0	25.5	26.9	219	27.7	29,9	29.5	28.5	283	27.2	26.0	301		25.0	29.6	261	25.5	24.4	27.4	28.9	28,4	30.1	29.4	30.5		29.9	
3 00	27.6	29.0	28.8	27.2	30.2	27.0	28.6	23.3	26,0	30.8	30.6	28.4	30,0	29.0		31.5		26.6	30.4	27.5		22.6	28,6	3 0,0	29,4	30.8	310		30.3		308
+ 00	28.9	29.7	29.9	27.3	27 1	20.0	29.6	25.1	26.7	31.8	31.7	29.9	31.3	3413		32.3	2H K	28.2	31.0	28.6		22.8	28.2	29.4		31.8	32.2	31.3	1312	30.8	32.0
5:00	1 01	30,5	30.9	27.3	24.1	29.0	30+6	26.8	27 3	12.8	32.9	314		317		330	_	29.7	31.6	297	287	2111	27.8	29 4 28 8	31.7	32.8		321	32.0	31.9	328
6.00	31.4	31.2	32.0	27.4	21.0	30.01	31.6	28.6	28.0	33.8		32.9		33.0	29,0	33 B	304.0	31.3		<u>- 2-2-1</u> Эн К	<u> </u>	23.2	27.4	28.2	33.0	33.8		32.8			336
7a0	31.6	31.5	32.4	27.5	24 2	30.4	31.9	29,2	29.1	.H 5	347	335		33.7	297	343	30.7	321		29.3	30.6	24.5		28.7	337	140 140	34.6 34.8	34 Z	33.6 34.1	.34.0	344
8,00	31.8	31.7	32 K	27.7	27.4	30,8	32.3	29 R	30,1	35.1	35 5	34.0	34.6	34.3	3413	14.7	31.3	33.0	<u> </u>	27.9	31.2	257	28.7	29.2	34.3	346		347	34.5	34.3	· · · · ·
9.00	32.0	32.0	332	27.9	30.6	31.2	32.6	30.4	31.2	35 K	16.2	34.6	35.0	35,0	310	35.2		31.K	-	26.4	31.8	27.0	29.3	29.7	35.0	350		35,3	35.0	347	
10.00	29.7	31.1	32.5	28.0	285	347	31.2	29.5	313	33.9	35.7	3.1	144	મર	311,3			33.3	25. t	26.1	30.5	27.0		29.7	34.1	34.4		34.9	345	350 347	í – "
11.00	27.5	30,1	31.9	28.1	26.5	<u>341,1</u>	31,3	28.7	31.3	31.9	35.1	27.5	13 N	337	29.7	343		32.9	25.1		29.3	27.0		20.6	33,3	33.9	í —	34.4	33.9	.14 5	
12:00	<u>25 7</u>	29.2	31.2	28.2	24.4	29,6	30.6	27.8	31.4	30.0	.346	24.0	33.2	33,0	2940	338	21.2	·	25.2	25.4	28,0	27.0		29.6	32.4	333		34.0	33.4	34 2	
13:00	25.0	28.6	29.5	27.7	245	2930	29.9	27.0	30.7	29.1	333	237	29.4	315	28.5	32,9	21.7	31.6	25.0	25.3	27.9	26.7	28,4	291	31.9	32.5		33.0		33.4	
14.00	24,7	28.1	27.7	27.1	24.6	28,3	291	26.2	301	2B 1	32.1	235	25.5	30.1	27.9	321	22.3	30.8	- ···	251	27.8	26.3	281	28,5	313	31.6	31.5	320	32.9		
15.00	24.5	27.5	26.0	26.6	247	7 72	28,4	254	29.4	27 2	30.8	23,2	21.7	28.6	27.4	312	228	30.0		<u> </u>	· · ·	26.0	27.9	28.0	30.8	30.8	30.6			32.7	32.5
16:00	24.0	27.3	26.2	26.3	24.6	27.1	27.8	25.6	289	27.1	30.4	24.0	22.5	26.5	27 1	30.5	22.9	297			27.9	25.0	27.8	27.9	30.4	30.3	301	31.0	31.9	11.9	3t.8
17:00	23.5	27.0	26.4	26.1	245	26.4	27.3	25.8	28.5	26.9	299	24.8	23.2	28.3	26.7	297	22.9	29.5		25 3		25.7	27.7	27.9	30.0	29.9	297	29.9	1	<u>M.4</u>	-
18:00	23.0	26.8	26.6	25 R	24 4	25 N	267	26.0	28.0	26.8	295	25.6	24.0		26.4	· · ·		29.2	_	254	† ·		27.6	27 8	29.6	<u> </u>			30.6		3/07
19400	23.0	26.4	26.4	24 H	23.9	25.4	26.4	25.9	28.0	26.9	29.3	25.7				267	22.8	28.9			28.2	25.5	27.5	27.8	29.0	28.5	29.2 29.1	20.4 20.2	<u>30.0</u> 29.7	30.3	
20.00	23.0	25.9	26.2	23,8	23 3	24.9	26.1	25.7	28.0	26.9	29.2	25.7		26.5	26.9	243	22.6	<u> </u>	<u> </u>	-	212	25.4		27.8	28.8	27.7	29.1	29.2		29.7	311.0
21.00	23.0	25.5	26.0	22,8	22.8	24.5	25.B	25.6	28.0	27.0	1		<u> </u>	25.6	272	22.0	22.4	28.2		25.0	+ · ·	25.3	- · ·	27.8		26.8			29.3	29.2	<u> </u>
22(0	24.9	26,8	27.1	235	24 ()	25.0	26.6	25.9	28 5	27.6	29.0		· · ·	26.2		24.4	24.1		<u> </u>	26.3	28.4	26 +	27.7	278		26.9	29.0 28.0	23 8 27.7	29.0	28.6	
23:00	26.9	26.2	28 3	24.3	25,2	25.5	27.4	26.1	29,0	28.2	29.0			26.9		26.B		<u> </u>	<u> </u>	27 5	-	<u> </u>	27.9	27.8	27.5	27.1	28 0	26.5	†	27.0	

Hourly	Dry	Bulb	Temperature (°C)	
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Source Bangladesh Meteorological Department, Clemate Division, Agorgaon, Dhala

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Year: 2005 Month June

Day	1	2	3	4!	5	6	7	н	9	10	11	12	13	14	15	16	17	16	19	20	21	22	23	24	25	26	27	28	29	30
Tone																											21	20	- 27	
0.00	28,8	29.5	29.4	25 0	26.4	26.0	28.2	26.4	29.5	28.8	29.0	ZH 5	29.6	27.5	2730	29.2	274	29.2	29.0	2R #	28.8	28.6	2K 2	27 R	27.0	27.2	26.0	25.4	26.0	26.4
1:00	29.9	.આ, ૩	30.1	26.3	27.6	27.7	29.4	28 Q	31.6	29.9	_29 K	29.3	30 4		26.5	29.9	28.5		29 H	297	29.5	29.4	26.7	28.9		27.8	26.7		26.5	
2.00	30.9	31.2	30.9	27.7	29 t	29.4	30.6	29.6	31.7	311-9	3016	31141	31.2	301	26.1	30.5	29.5	31 t	30.7	341,5		30.2	29.3	29.9		25.4	27.5	25.7	26.9	
3.00	32.0	32.0	31.6	29.0	30.5	31.1	31 B	31.2	32 в	32.0	31.4	304.8	32.0	3] 4	25.6	31.2	3/I.G	32.1	31 5	31.4		31.0		31.0		29.0	28.2	25 K	27.4	
4:00	32,7	<u>, 12.9</u>	32.6	30.2	31.3	31.5	32.2	31.9	337	311	12.5	319	31.0	32.1	26.4	29.6	31.3	32.9	32.0	32 t	31.8	303	Z9 5	313		30.0		26.0	27.3	Z7 9
5:00	_33,5	33.7	33.7	313	32.2	31.9	32.6	32.5	34.6		33.5	33.1	RUU	32,9	27.2	28.0	32.1	33.6	32.5	32.7	32.7	295			29.1	31.0			271	28.5
_6.00	34.2	34.6	H7	325	33,0	323	334	31.2	35.5	35.2	34 6	34.2	29,0	33.6	28.0	26.4	32 K	344	3313	33,4	33.5	28.8	· ·	32.0			29.1	26.3	27.0	
7.00	45	35.2	34.9	32.7	33.8	331	33.9	33.8	34.8	353	34.6	34.5	29.3	11.5	29.2	26 R	33.0	34.6	33.1	31.7	33.9	28.4	29.3	30.41	29.0	313		26.2	27.1	28.5
8.00	34.9	35.8	35 t	3 <u>2</u> .H	_34.6	34,0	34.7	34 4	341	35.5	14 6	347	_29.7	33.5	3113	27.2	333	34.9	333	33.9	34.2	27.9	29.5	27.9			28,4	26.1	27.3	27.9
9:00	35.2	36.4	35 3	33.0	.35.4	34 8	35.6	35,0	33,4	35.6	34.6	35.0	30.0	33.4	31.5	27.6	13.5	35.1	33,4	34.2		27.5	29.8	259		30-0	28.0			27.4
104060	34.6	35.6	34.8	32.5	31 2	34.3	35.2	347	32.6	35.1	33,7	34.4	29.6	30,6	314	27.5	131	34.4	32.9	137		281	29.7	263	<u> </u>	29.9	277	26.4		27.4
11990	34.0	34, K	34.4	31.9	27.0	319	34.7	.14.5	3t 7	34,5	329	379	2U Ç	27.8	313	27.5	327		32.3	331		28.8		26.8		29.9	27.5	26.9	27.5	27.3
12(0)	334	34.0	33.9	314	22.B	33,4	34.3	34.2	311.9	34.0	120	313	28.8	25.0	31.2	27.4	32,3		11 8	326		29.4		27.2		29.8	27.2	27.3	27.6	<u> </u>
13 (8)	327	33.1	33.2	.301 R	23.6	3,2.5	31.1	315	3115	31 9	313	325	28 5	25.2	30.9	27.5	317		31.2	32.0	30,9	291	;	27.1	291	29.5		-	27.3	
14.00	31.9	323	32.4	311.3	24.4	315	27.9	32.7	3010	29.9	30,5	318	2K 2	25.5	¥0,5	27.5	31.2	31.7	30.6		30,7	28.9		-	28.5	291		26 H		27.0
15 👀	31.2	3t 4	_31.7	29.7	25.2	30.6	24.7	320	29.6	27 M	29,8	31.0	27.9	25.7	3(1.2	27.6	304.6	31.0	300	3068	30.6	28.6			27.8	28 8		26.6	_	
16-(10	30.7	30.9	31 1	28.6	Z5 2	30.4	25 2	31.5	297	28 3	_29,6	341,7	27.7	25.9	_30,0	27.6	30.4	¥18	29 R	30.5	30,3	28.5			27.7	28.5	<u> </u>	26.4	26.7	<u> </u>
_17.00	30.3	30.5	-30.6	27.5	23.2	302	25.7	31.1	29.7	28.9	29.4	3113	27.4	26.1	29 B	27.5	30.2	341,5	29.6	301	29.9	28.3							26.7	<u> </u>
18.00	29.K	30.0	391,0	26.4	25.2	30,0	26.2	30.0	29.8	29.4	29.2	30.0	27.2	26.3	29.6	27.5	300	3413	29.4	22.8	29.6	28.2					<u> </u>		1	
19 (0	29.7	29.8	29.3	26.3	25.4	29 (26.1	301.4	29.5	291	29.0	29.9	27.1	26.4	29.4	27.5	299	30-0	29.2	29.5	· · · ·	28.2	27.9					25.9		
20.00	29.7	296	28.7	26.3	25.6	29.2	26.1	30.2	29 3	28.9	28.8	29.9	26.9	26.4	29 2	27.5			29.0			28.2		<u> </u>				_	26.2	
21:00	29.6	294	28.0	26,2	25 8	281	26.0	30.0	29.0	28.6	286	29 X	26.8	26.5	29,0	27.5			28.8			28.2							1	<u> </u>
22.00	28.6	28.2	26.9	26.1	25.9	27.1	26.4	29.2	28.5	283	27 8	29 11	27.1		27.6	27.1	28.6		285	28.6		27.6	_ //			<u> </u>				264
23:00	27.5	27.0	25.R	26 1	26.1	26.9	26.8	28.4	28.1	27 9	27 1	28.3	27.3				27.6		283		27.2	27.0				273	26.4	26.1 26.7	26 S	

Hourly Dry Bulb Temperature (°C) source. Bangladrah Metrorolopical Department, Chriate Dirusion, Apargaon, Dhaka Year 2005 Month, July

=		000	0		2	2 1		20	10	32	5	5		12.0	1		1110	ģ	29.5	និ	28.7	2.62	i fi	28.3	28.5
ę		ŝ	1					1		u E		20	Ģ	202	5		Ê	8	H R	28.6	35	* 7	197	28.2	58
Ŕ	ŀ	27.6	71 1		2 5	Ţ		1 4	10.00	37 B.		20	9415	5.12	i c		Ē	2 R	38.9	2 전	З. Ж	Ĩ	- R	З.Н.	28.3
28								2	1	ţ	32.0	Ē	5	31.2	Ĭ	1		্র ম	ŝ		9 8	28.4	ې ج	2 8	
5	t	27.6	27.5	1		7	ġ	2	Ē	5	33.2	2	, E	0	F R			5	<u>ត</u> ភ	8.82	+ ភ	5¥.=	27 6 27	275	37.5
26	┞	28 O	8	i R	318	F	1	N.	546	5	5115 1	ŝ	5	10. 4	0.2	<u>्</u> र	20	Ę	38	28.4	28.5	28.1	ŝ	27.5	27.3
ង	╞┈	1	Ţ	30.51		1.2			32.3	ŝ	32.2	10.5%	1. 1.	31.6	Ĵ,	1.06	Ř	ลิ	ŝ	202	а Н	18.7	*	277	26.9
2	Ţ	222	2			I.	1	32.2	325	12	33.0	32.6	22	H X		۲.	8.62	្តិត	Ri	21.2	ŝ	26.8	88	26.8	27.0
5	Γ	27.5	27.9	3	14	Ř	9.0%	31.5	31. 4	1.3	51.2	1.2	1 2	312	ļ.	ΩX.	20.R	2115	29.1	RRE	28.4	27.9	27.5	27.7	28.0
ដ		7	ਸ ਨੀ	8	8		28,#	, T	715	ж Т	112	0.416	30.5	30.2	ъ Х	1	20.0	28 R	2H 7	29.5	5 HZ	28.2	28.0	27.6	27.1
21	F	÷	5	â	Ţ,	2	ģ	30.6	1.1.	34.5	32.0	31.6	31.6	11.4	ж. Э	۲. پ	5	20,4	20 L	2N R	27.7	20.5	23.4	25.9	26.3
20		27.7	2X,4	ลี	ЧĽ		31.3	32.0	31.2	30.3	205	2K 7	28 C.	27.2	27.3	275	27.6	274	27.2	27.0	26.9	24.7	2r 6	26.9	271
19		с Ж	2R 7	5	2		7	12	32.1	32.3	4.51	32.2	32.0	н н	311	3115	21J.H	28.4	27.0	25.6	25.7	25.9	261)	26.3	26.7
38		37.6	181	28.5	ŝ	5	р С	5 W.	31,01	31.5	32.01	7241	3241	1211	71 5	313	20 5	202	29 K	2N.5	2N 4	24.1	28.2	27 H	27.4
17		206	27.6	2H6	20.6	¥П.	1.11	31.8	323	32.9	33.3	32.5	31 K	314	5115	29.7	29.N	2K 9	28.7	2K 6	17 81	2H.2	с Ж	27.7	275
16		26.4	21 () 21 ()	27.6	다 53 53	28.9	20.7)II 4	311.6	Ji H	11.11	319.9	30.8	30.7	207	74'NZ	27. K	27.6	5	51	ŝ	26.9	36.8	268	26.8
15		24.H	15.52	25.2	ដ	25.4	25.5	25.5	25 K	20,0	26.3	36.4	26.4	26.5	26.5	20 2	26 O	36.0	26.41	26.11	26.11	2611	 ភ	992 97	26.9
14		25.4	25.5	25.5	25 (25.0	26.3	200	27.0	27.4	27 R	27.5	27.t	26.8	26.7	265	707	20.3	ž	101	261	35 X	250	20	274
13		27.6	27.5	27.3	272	272	27.2	27.2	26.7	26.1	25.8	25.9	ŝ	200	26.1	26.1	26.2	26.1	2	2,5	ม	5.5	ŝ	202	27.1
엽		27.5	28.11	2,45	29 H	29.9	309	31.5	F	711.7	30.2	ŝ	5	26	ស៊	6 N2	1 28.H	뚪	243	138.4	28.3	ž	24	. 1.	27.3
F		26.3	26.8	27.2	21.7	27.3	2711	26.6	27.2	27.9	28.5	245	3	3	2	ភ	38.0	ň	2HII	2 2K ()	27.9	27.9	22.		3 26.9
9		27.6	27.7	27.9.	1) NZ	28.4	28.8	202	ຄົ	5.02	5 ZU 4	20 C	20 X	11411	295	R	я 28 б	0 28.5	28.3	2.82	ন	61: 8	G 27.8		273
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œ		12	0 28.5	t 205	3 ¥14	31.0	31 6	122	1.12	12.2	72.2	2	3	1 AU K	1	297	4 292	200	1 2X.H	0 28.6	5 29.3	9 2K1	4 27.8	-	4 277
~		27.2	L ZRO	S ZK Ki	20.02	+ IK	312	2 32.0	22	2	12.4	20	3 32 K	11	5 31.8	316	1 29.4	5	2	0 23 0	5 2.K 5	9 27.9	+ 21 +	5	5
J		259	X.1.1	4 2R3	1 29.5	314	31.3	12.2	7 12.3	3 12 5	12.6	H 12.5	7 32.3	12.2	1.5	6 30.8	1 16	7 20 7	4 29.4		U 285	9 279	+ L2 	_ [7 27.1
ŝ	_	20.2	53	3 254	5 25.11	8 25.7	1 26.3	4 27.0	1 277	7 ZN.3	29.11	K 23 H	1 23.7	2 2R.5	7 2H U	1 27 6	2 31.1		9 264		220		5		0 26.7
4		7 260	8 262	0 26.3	0 265	26.8	200	27.4	1	2	26.3	5 26 8	1	8 27 9	4 27.7		(27.2		5 26.9			7 207	200		5 27.0
e.	_	R R	248	5 24 9	220	3 25.1	5 25 2	8 25.3	7 25.6	5 20.0	4 26.3	2 265	20	890 8	7 2/14	7 264						_			265
~		ŝ	1 26.2	1 26.6	9 27.0	9 273	2	0 27.8		3 27.5	БÌ Э	1 27.2	1 230	R-02 2	7 26.7	3 20.7	8 266		1						7 28.2
-	_	2(1.5	27.1	28.1	28.9	27.9	27.0	0.% %	26.7	27.4	0.82	ž	E.	ñ	277	27.3	╼┼	+	╉	2	-+-	+	╺┼╴	┿	27.7
цц	Ľ	000	118	2 .00	300	4 8	5.01	979	ŝ	9 *	8	10.00	11.00	5 21	13.00	i‡‡	15 (0)	291 12	13 (H	38.00	13 IO	88	318	ខ្មា ព	2300

Hourly Dry Bulb Temperature (°C)

Source Bangladesh Meteorological Department, Connute Division, Agregann, Dhala

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Year: 2005 Month' August

916	8°1Z	69Z	0.72	z iz	1.02	VLT	1.25	592	1°ŽŽ	£ 9Z	137	L'LZ	1.82	CLZ	\$°LZ	S'9Z	6.97	5 / Z	977	592	1107	A'07	9'9Z	1 IZ	L 92	0.14	6.77	1.17	0.05		440 A 1
216t	7°,4	LLZ	872	Z"(Z	30 B	112	5.22	2'22	\$ 17	Ľ%	\$192				\$ 22 \$			1.92	<u> </u>		1 22	ļ	·							584	52.00
8 KZ	0 6 Z	9 8Z	5970	27.2	₹4Z	0 <i>1</i> 2	1692	<u>s /z</u>	0'82		0.12					<u> </u>		0.62								<u> </u>			0 RZ		22,00
1.62	Z (iZ	R 82	2 KZ	262	572	1.12	5270	LLE			1722						1	1 67	1	በግረድ					t 17				0.85	· · · ·	00.12
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5 62				517		<u> </u>		1 112		5.75		7 85	<u> </u>			·		<u> </u>	L	Z KZ		1,85			6°22°			2,82	t (C	ነ ሀኒ	AREAT
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5.05	946	<u> </u>		5.02	1 -		_	55.0		_	<u> </u>			018								Z 6Z		9 GZ			F 12	8.62	t'o£	1.27	00.01
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			125					815			1 .	L	1	1								946	0.75	2 Z E	262	8406	N IN	RTE	7.88	2.28	1026
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†°22				2008		I		6'0£		<u> </u>	2.62	<u> </u>	<u>.</u>				1	ĹΚ		1767 -				8.15	6.67	CIE	E'DL	111	8 26	+ ££	0042
								† 1)£			0.15	282	11.62	0.17	5 15	8.00	-		-				UIK	916	0.01	976	0'0¢	2.08	+ 25	232	0060
	211			1'UK		•	_	116		· · · ·	_	-							<u> </u>	5 xZ			8.62	5.05	5.95	ZIKE,	5 6Z	2415	1.15	1771	THUS
ZIE			<u> </u>	8 65				¥ 6Z	- 1				11 872	<u> </u>	1 ····	502		17 M	r 1.2	L 17	2.75	ε'žč	L 6Z	662	0.6Z	6.65	54.0	2.62	6'62	1.15	004
	000					↓	L	5 GZ			L GZ	L		-	10.85			9.62	5702	1120	0-22-0	1 22	5 GZ	11.62	<u>5 x5</u>	062	† 8Z	Z'6Z	9.85	<u>S</u> IIE	0045
				500	_	<u> </u>		1.62	<u> </u>		6 HZ	1		<u> </u>	972			0.65	2.62	R 92	0.72	1722	28.11	582	(1 8 <u>2</u>	† \az	10.82	†'HZ	8.82	<u>7.65</u>	0.07
	-	L	111	· ·	Ľ LZ		2.2.2	1	<u> </u>		2'9 2				₹°.ĺŻ	L		1 82	8.92	20.05	0.72	18 9Z	2 KQ	51.0	5722	¥ 17	9.22	272	567	0.62	00:0
286	0.82	4.85	042	F.T.C	0.12	2792	2.72	ž hz	2790	8.65	F 12	11.75	072	tž	8192	1772	5.82	8745	0.72	\$ 97	0 <i>1</i> Z	592	922	\$720	0.1Z	Z 17	2.72	¥ 97	5073	र ४२	00-0
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ເເ	30	5Z	58	LZ	92	52	ÞZ	57	55	54	αz	6[81	LΙ	91	SI	+1	51	15	ü1	01	6	8	L	. 7	5	1.	£	z	<u> </u>	Δīzα

Hourly Dry Bulb Temperature (°C) Source Hangladush Meteurological Department, Climate Division, Agargion, Dhala Year 2005 Month September

S	Г	27 2	27.9	28.7	20.4	n R	ģ	31.0	38.9	26.7	24 6	14 E	24.0	5	12	25.3	۲. ۲	5	255	255	25.5	25.4	25.4	25.1	74.7
23	╞	26.0	26.5	31.1	3.5	27.7	a Ri			2B 6	20 0	23	29.1	29.2	29.0	582	28.5	r S	종	U R	6.5	27.7	19 17	19 สิ	7.7
28	╞	502	- I	<u></u> _	21%	31.5	32.3	12	316	۲. ور	285	83	× K	เก	6 85	C HC	38.85	۳ Ť	۲.	27.2	37.1	21 1	- -	26.6	26.2
2 1	┢╌	212	28.5	ន៍	31.0	31.4	× C	32.2	12	ដ	32.6	7	Ģ	л Г	ะ ณ	¥ K2	28.7	28 G	5 स	두 왕	31.9	Z1 5	27.0	ŝ	25.7
26	┢╌	25.5	15		۲. ۲	้ ม	30			2	12.4	316	30.8	Ξg	10	5	9 HC	Ŕ	28.2	1 1 1 1 1 1 1	8	27.7	31.0	7	247
35	┢	27.22		29.5	29.2	र हा	ģ	310	3	21.2	30 R	2) 5	ы П	28.8	580	5	2K.0	3).R	2	1	24.7	25.9	525	7	23.5
24	┢	9 7	23 1	35.5	26.0	27.2	7.83	พ	क हि	30.3	316	311.2	20, R	20.4	28.8	28.3	27.7	Z) 3	27.0	26 G	26.7	26.9	27.11	254	33.8
23		2	27.5	2R 4	50 F		E.	99		ہ ا پر	е У	5	ي 28	27 T	Z7 R		2H II	8 53	27.5	27.3	+ [;	27.4	23 S	3	24.5
52	┢	9 72	27.7	28.7	77 80	101	s X	30.8	7 8	58 Q 58 Q	26.6	26.5	26.5	26.4	26.3	ж Х	20.2	26.3	36.1	- R	26.0	36.0	9.V.O	35 1	245
5		5 57 0	2V. 0	27.7	2N.G	204	313.2	11 0	31.3	31.7	32.0	31.8	29.7	2N 5	23.3	38.0	27 B	27.6	27.4	27.2	27.1	27 1	26.9	26.0	25.2
20		÷ ส	26.3	27.5	28 K	28.5	Ř	- 8 Fi	26.9	25.0	25.0	24.9	24.9	24 K	25.1	25.4	25.7	25.9	26.61	26.2	20.2	26.2	26.2	25.1	512
10 i		х С	29.2	115.61	32.0	12.7	13.7	ž	33.6	10.2	32 H	32.5	121	12 0	31.6	31.2	30 H	Nu:	29.2	28.4	2H 3	2H.T	23.0	26.6	25.2
1Ķ	-	28.2	29 L	30.6	31.ft	117	32.3	33.0	32.9	12.9	12.8	12.2	117	31.1	341 5	311.0	21.4	29.2	200	2K.B	2H 7	28.5	2K 4	27.6	26.7
-		27.0	3 8.0	20,0	310	30 G	312	11.94	32.0	32.2	32 4	32 (1	315	31.1	30,9	30.6	+ K	30.2	101	29 H	295	8	30.0	2K 1	27.2
16		27.4	2N.R	30.2	31.6	32.5	11.1	342	14.1	14.3	÷.	11	32.7	32.0	11.7	115	άK	3(12	29.2	28.2	2N.01	27.H	27.6	ä	271
15		26.4	27 R	16	30.6	31.7	32.9	34.0	34 2	34.4	140	U.11	11	32.6	32.1	717	31.2	30.8	1 1 1	31LU	1) (IE	2H,CI	27.0	264	25.7
ž		26.4	+ {1	2H 5	20.5	31.5	31.6	32.6	32.4	32.3	5	ŝ	311.6	2') H	19 10	201	28 B	29.3	27.9	214	273	27.1	27.0	26.8	26.7
5		26 R	27.1	27.9	28.4	29.8	31.2	32.6	12.5	123	12.2	112	2K2	2r.2	20.5	26.9	27.2	27.5	27.9	282	27.0	27.7	1.1	27	26.7
13		27.2	3R.4	হ হ	318	31.5	31.7	32.2	34	32.5	32.7	1.7	101	29.7	20.2	2H, H	28.3	28.1	27 4	27.6	27.4	Z 1 2	27.11	г- 91	26,4
≒		26.2	21.9	27.6	24.3	29.0	20.8	JIIS	31 о	31.6	V2 I	VI R	1.16	31.1	315	20 K	<u>5</u> 2	が	27.6	26,4	24.7	26.7	26.6	1	26.2
2		242	254	26.6	27.R	2N D	30.1	312	3t 5	31.9	32.2	31.7	11.1	711 N	205	ñ	27.0	ឝឹ	27.0	50	5	26.3	2	ੜ	26.0
6		204	5	38.1	28,X	204	ЗЧI Г	30.7	51 S	M 9	32.5	31.9	1 + 15	4 11	2.0.7	ž	ŝ	ଛ	24.5	28.2	281	æ.	5% 5%	37.5	26.4
æ		2r.2	26.9	275	28.2	29.3	34.5	31.6	32.0	12.5	33.11	124	31.8	31.2	0.116	207	515	38.6	27.11	2.4	25.6	. 25 %	36.0	ž	203
۲-		- 12	О Я	311,3	31.6	292	26.9	24.5	24 K	25.0	5	7.57	3	24.5	54.4	26.3	. 26.2	5	15	26.41	32	ž	28.2	25.7	25.3
G		Ř	28.1	20.7	114	32.0	32 (33.2	334	34.4	15.0	5	11.7	30.0	20.H	20	202	N 20	6 6 5	28.6	2%4	282	1 1 1 1 1 1	26.6	25.1
י ח		27.0	24.1	33.	30 4	28.T	27.1	25.4	25.8	26.1	265	2r.9	5	27.7	ត	27.0	26.6	265	26.3	2V.2	21/2	26.2	192	26.2	26.2
4		ñ	2 R .K	30 G	101	31.0	317	323	H.18	31.4	30 U	216	ΥL Υ	11_51	25.7	5.02	0.62	29.4	30.0	20.0	28.5	12	27.6	3 26 K	7 26 U
ŝ		27.8	28 5	202	29.9	MEG	11 1	32.0	31.9	6.15	31,8	31.5	1	31.0	315	1(1)1	29.5	29.3	11.11	28.H	583	2,8.5	28.4		20.7
61		UFK2	28.0	23.8	ĽX.	117	32 R	33.8	11.1	32.5	31.8	315	5.17	M II	t of	29 R	2,1,2	39.0	28 R	28.6	28,4	E K	1 23 1	1	25.6
		27.8	001	30.3	33.5	31.1	30.6	30.2	Ż	ч ж М	37.8	+ 1 22	102	9. E	29.1	285	2B.0	я Я	287	28.2	28,1	뙲	0%2	5	26.1
Day	J'inté	900	101	2 (II)	10	8	5.00	(H) (1)	190-2 1	B (NF	9 (H)	10501	11:11	12(N)	13(3)	1400	15.00	(e).91	17.00	18.00	19-111-	30,00	21.00	3 3	23 (0)

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Hourly Dry Bulb Temperature (°C)

Source: Banglideth Merencological Department, Climate Dr. 1810r, Agaegaor, Dhaba

Yean 2005 Monthy October

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		112	я(Z	21.2	202	5013	6 61	\$uZ ∣	Z 1Z	861	1'61	512	817	7.12	S 1Z	\$T7	50.9	182	5762	1 SZ	0.25.1	212	5.52	117	52.4	53.3	612	672	6.22	53'00
511	23' 1	+ tē	t {Z	7 GZ	5170	a (S	20'0	612	9 ZZ (812	510	536	K EÇ	23.6	ë+ē	ī ≠2	57.9	6'ŧĉ	615	11 SZ	2'92	54.0	540	1 †Z	2375	677		_	· · ·	55'00
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Houth	/ Dry Bulb	Temperature	(°C)

Source, Bangladesh Meteorolopical Department, Clamate Division, Agargaon, Dhaka

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Year, 2005 Month: November

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12:00	26.0	27.5	27.0	27.0	26.5	27.0	_26,8	27.0	27.N	<u>27</u> 0	27.2	25.6	23.4	24.0	23.6	24.6	24.6		23.0			24.8	23.2			232			23.8	22.2
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15 (8)	25.0	25.4	254	25.2	25.0	25.0	233	25.6	24 K	25.2	25.0	24.0	2016	21.6	22 C	22.4	22.4	20.5	228	21.6		21.4		22.2	-	20.4	20.4		22 2	194
16:00	24.4	24.9	24.6	248	24 4	24.1	23.3	25.5	24.7	25.1	24.5	22.6	201	21.3	21.9	221	21 K		22.5		20.8	20.9		21.5		20.1	20.6			18.9
17:00	23.8	24.5	24.2	244	23.8	23.1	23.4	25.3	24.5	25.1	240	213	197	21.0	21.7	21,7	21.1	18.8	22.1	21.3	21.9	20.5		_		19.7	20.8		21.1	18.4
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Hourty Dry Bulb Temperature (°C) Source Hangladesh Metrorotogical Department, Climate Division, Agrigaon, Dhala Yene 2005 - Month, December

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APPENDIX B: Hourly Direct Solar Radiation in Watt/m² Hourly Direct Solar Radiation in Watt/m²

Source: Renewable Energy Research Centre, Dhaka University Year: 2005 Month: January

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Hously Direct Solar Radiation in watt/m²

Source: Renewable Energy Research Centre, Dhaka University Year: 2005 - Month: March

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Hourly Direct Solar Radiation in watt/m² Source: Renewable Encepy Research Contro, Dhaka University Year 2005 Month May

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Hourly Direct Solar Radiation in watt/m²

Source: Renewable Process Research Centre, Dhaka University

Year 2005 Month: July

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Hourly Direct Solar Radiation in watt/m² Source Renewable Eucrys Research Centur, Diaka University Year 2005 Month September

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Houry Direct Solar Radiation in watt/m²

Source: Renewable Energy Research Centre, Dhaka University

Year 2005 Month: November

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Hourly Diffuse Solar Radiation in watt/m² Source, Renewable Paneogy Rest arch Centre, Dlada University Year 2005 Month May

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Year 2005 Month: June

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Hourly Diffuse Solar Radiation in watt/m²

Source: Renewable Energy Research Centre, Dhaka University

Year, 2005 Month July

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Hourly Diffuse Solar Radiation in watt/m² Source, Renewable Forcey Research Centre, Dhaka University Year: 2005 Month September

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Hourly Diffuse Solar Radiation in watt/m²

Source: Renewable Energy Research Contre, Dhaka University

Year, 2005 Month: November

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APPENDIX D: Hourly Relative Humidity (%)

(%) viibimuH avnelan vimoH

Source, Bangladesh Metteorological Department, Climate Diseanor, Agargaon, Dhaka

Years 2005 Month. January

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Hourly Relative Humidity (%)

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Source Bangladesh Meteorological Department, Climate Division, Agargann, Dhala

Hourty Relative Humidity (%) Source: Bangadesh Meteorological Department, Climate Division, Agrepson, Dhaka Year 2005 Monthy March

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Hourly Relative Humidity (%)

Source: Hangladeah Meteorological Department, Climate Division, Agarguon, Dhaka

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Hourly Relative Humidity (%) Source Bangladesh Meteorehoneal Depurtment, Climace Division, Agargaon, Dhala Yeare 2005 Mench, May

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Hourty Relative Humidity (%) Source Bangladesh Meteorological Department, Climate Division, Apupeun, Dhala Year: 2005 Month June

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Hourly Relative Humidity (%) Source: Handjadesh Meteorological Department, Umate Durator, Aparguon, Dhaka Year 2005 Month: July

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Houdy Relative Humidity (%)

Source Bengladesh Meteorological Department, Climate Division, Agargaon, Dhaza

Year: 2005 Month: August

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Hourty Relative Humidity (%) Source Bangladesh Mereorological Department, Clarate Division, Agargaon, Dhala Year. 2005 Monthy September

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Hourly Relative Humidity (%) Source: Bangladesh Meteorological Department, Llimate Division, Agargaon, Dhiska Year 2005 Monthe Oemlee

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APPENDIX F: Daily Total SunShine Hours

Daily Total SunShine Hours

Source: Bangtadesh Meteorological Department, Climate Division, Agargaon, Dhaka Year: 2005

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