# PERFORMANCE EVALUATION OF SHADING DEVICES USED IN TALL OFFICE BULLDINGS OF DHAKA CITY 

by
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A thesis submitted in partial fulfilment of the requirement for the degree of MASTER OF ARCHITECTURE


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#### Abstract

One of the characteristics of call office buildings in Dhaka city is the extensive use of glazing on the bulding facades. This incteasing use of glass has caused considerable changes in the relacionship between interior and ambicut climate, where the problem of overheating has become a major concern. So facades of tall buildings need protecrion from solat heat gan to achicve desicable indoor environment and to reduce the energy consumption in the buildings by the air conditioning system. External shading devices can be utilised to block the solar radiation before it teaches the window surface and hence more effecave than internal shading devices.

The problern was approached by performance evaluation of selected commonly used shading devices of tall office buildingy through simulation study. Shadow simulation allows study of the effect of changes in one aspect, keeping othcr factors constant. The observations of simulated performance that occurs due to changing parameters allow the identification of elements, the reduction or introduction of which in the design conmbute to solar heat gain. Through simulacion study, it is possible to analyse the performance of shading devices for any period of the year. The simulation studes were conducted for the months from March to September representing hot-dry and warmhumid period, which is most significant in terms of climatic severity. The simulation studies were performed to evaluate petformances of shading devices and idenify the cffects of diffetent patameters and correladion among parametets in terms of reducing solar heat gain. This study also helped to understand the influence of window orientation on the performance of shading devices.

After all the investigations and critical evaluations, a parametric srudy to exptote the strategies for optimum shading was pursued through a series of simularions as solar geometry is a predictable phenomenon and much of its impact is quantifiable. Paramencic study allows study of various alternatives with teference to performance of the model and identifying the best one. Based on the paramerric study, design recommendations and design gudelines were derived.

The findings of the thesis are concerned with the problem of solar heat gain in tall office buildings in ropical climate like Dhaka city. The results of the simulation studies and parameme studics have been expressed in terms of a number of climate responsive shading design guidelnes. It is expected that the application of these gudelines will reduce solar heat gain in comparison to chat of present praccices.


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CHAPTER: ONE PREAMBLE

### 1.1 Introduction

$\xi$
'The trend of recent development has slifted from low to high-rise buildings due to the pressure of population in much of the world, and Dhaka is no excepaon (Ahtned, 2003). Constnicion of tall office buildings in utban ateas of Dhaka is characterized by extensive use of glass. These glass facades remain unprotected or barcly protected from the scorchung solar tadiation of the tropich. These often lead to green housc like sinaton (Givoni, 1969).

Along with the high out door air temperature, solat taduation is a major source of heat gain for building in tropics (Koenizsberger at al, 1973). Vast verrical surfaces of tall buildings are exposed to solar radiation and glass facades may act as heat trap for incoming solar tadiation (Ahmed, 2003). So facades of tall buildings need protection in view of generating desirable indoor cnvironment. Solar radiation mansmimed through unprotected windows or transparent walls also cause a great increase in the cooling requrements of an air-condizoned building ot high air ternpctatures in buildings without mechatrical coolng systerns (Stephenson et al, 1962; Goulding at a/, 1992). This heat is particulatly unwanted in summer and has to be expelled ly the cooling system.

Solar radiation gain may be reduced by infercepting the radiation before it reaches the building surface. Jixternal solar shading can be beneficial in preventing unwanted solar teat gain thus reducing cooling load and thus can entance thermal comfort. Mformenct, the thermal effect of a glazed wall section depends on the shading provided and the spectral properies of glass (Givoni, 1969 ). Shading the glass affects the property of incident radiaion and hence modifies both the heat flow to the intenor and the indoor temperature.

Limitation of enctgy resources and evet iocreasing energy $\Gamma^{\text {rices and the global watming, }}$ the necessiry to reduce the energy consumprion in the buildings can be an important assue in a developing councry like Bangladesh. In such a context the need to develop passive means of solar conmol is important and efficient design of shading devices may address chus issue significantly.


Figure 1.1: Tall office triklings shoring present rend of facade design in Dhaka city.

### 1.2 Statement of the Problem

A good answer to overheating problems is controlling solar radiation incident on the buitdings. Using solar-protective glazing is one simple solution which can be easily integrated into the building design (Olgray and Olgyay 1957). One major clrawback of solar-protecave glass is that it reduces solar gains in the building cven during winter-time. Thercfore, in countries whth dominant hearing requircments, a moveable device is a hetter soluton (Dubois 1999). But again manual control of movable shadng devices is not reliable and may cause a constant disruption for the occupants and most of the perple of our councry can't afford the system of dynamic concrol of motorized shading devices. Shading provision should be considered as an integral part of fencstration system design, especially for facades with high solar gains. Shading devices may control solat gains, bleck direct sunlight and transmit diffuse daylight in the room, eliminating glare and high contrast and creatng a pleasant luminous environment (Haque, 2004). It is necessary, on the one hand, to classify the shading devices by their geometric characteristics; on the other hand, to analyse their energy and luminous performance through the definition of man made parameters and calculation medhodology.

In the context of Dhaka, there is no tested rule for shading devices. According to construction act, 1952 (E.B. Act II of 1953) section 18, (Rajuk, 1996) which is enforced by RAJUK, it is said that maximum depth of shadng device wall not exceed 0.5 m over compulsory serback areas. But this rule may not have come from any mvestigarion or analysis of shading performance nor any comparative soudy and evaluation for different climatic situations. Therefore, buildings are being consmucted without propet attention to the performance of shading devices.

Due to our increased concerri about energy efficient buildings and thermal comfort as well, expenments and analysis should be made for different types of shading devices. By thotough study of the relacionship between depth and other parameters of shading device and amount of shade that cast on the windowpanc, which is essential for thermal comfort and exclude heat gain (energy consumption) from solat radiation should be established and eventually incorpotated in the design process.

### 1.3 Objectives of the Study

The study is an atrempt to invesigate the performance of commonly applied shading devices on facades of tall office buildings as a method of passive cooling with the following objectives:

1. To evaluate the exisuing shading devices as solar control tool used in tall office buildings.
2. T'o assess the impact of shading derice on indoor environment as they relate to the solat heat.
3. To propose a guideline for designing cfficient shading device for control of solat radiation in tall office buildings.

### 1.4 Methodology

To aclueve the abowe objectuves the methodology that was followed for the entire work is stated below.

The problem was approached first by a survey of published information that provided the knowledge base for the research and information about the suate of the art regarding solar shading systems. By theorerical scudies the meaning and purpose of solat shading device was explored. Moreover, this study helped in analyzing factors influencing solar heat gain. The climatic characteristics of Dhaka Ciry were studied to set the climatic umperarives with regard to solar heat gain in tall office buildings in Dhaka City.

A physical survey was conducted to record and to idenuify the characteristics and performance of commonly applicd shading devices in refetence to tall office buldings. It helped in forming the models for simulation study.

The simulation process was pursued in two phases. The first one was conducted to ascertuin the performance of commonly used solat shading devices in teducing solar radiation gain. Simulation models with the external shading devices similar to the real ones in tall office buiddings were simulated for different ocientations. By the simulaion scudy findengs and results was analyeed to identify the effects of different parameters and correlation among parameters in terms of reducing solat heat gain. The second stage
involved a parametric study pursued through series of simulations to explore possible climatically sensitive design guideline for solar shading device.


Figure 1.2: Structure of the work.

### 1.5 Scope and Limitations

The research work presented in this study concentrates on performance evaluation of rarious shading devices in teducing solar heat gain in the tall office buildings in Dhaka city. Although solar heat gain is a combined effect of direct radiation from the Sun and diffuse radiation reflected from surounding environment, most of the solat heat gain to buidings is caused by direct radiacion through windows. The study is limited to the role of geometry of the shading devices to cut off drect solar radiaion hence reducing solar heat gain. Recommendations and design gujdelines are made tegarding geometry of shading devices. Other aspects like material of the devices, installation or construction systems are not considered in this research.

Besides, shading device has impact on daylight, ventilation and view through window. The performance of shading devices regarding daylight, venulation and other aspects are beyond the scope of this research.

With these opportunities and constrains, research on performance of shading devices with special reference to Dhaka ciry was carried out and described in the fotlowing chapters.

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## CHAPTER: TWO

THE CLIMATIC CONTEXT: DHAKA CITY

## THE CLIMATIC CONTEXT: DHAKA CITY

Amongst the innumerable constraints that the Architect faces during the design of buildings, climate probably is considered as one of the major factors. 'The climate of a tegion presents a set of conditions, which need to be addressed adequately in order to produce climate-responsive buildings. Climate-responsiveness results in comfortable, energy-cfficient, environmentally friendly buldings. Buildings consructed without regard to surrounding climate can, no doubt, operate given enough energy input to cortect resulting problems, whether they concern over heating, or datkness. But access to such energy is beyond the teach of much of the population of developing countries.

The chosen location for this work is Dhaka, the capital city of Bangladesh. The country is surrounded by India on the west, north and north-east. The Bay of Bengal bounds it in the south and with Myanmar on is south-castern part. The geographic location of Dhaka is, longitudes: $90^{\circ}$ East- $90^{\circ} 30^{\prime}$ East and latitudes: $23^{\circ} 40^{\prime}$ North - $23^{\circ} 55^{\prime}$ North.

The followng section is concerned with the analysis of climate of Dhaka city in terms of its challenges and potentials. This analysis will help to determine the climacic forces to be manupulated to provide sacisfactory design solutions for tall structures in uropical situations from the view point of energy efficiency.

### 2.1 Climate of Bangladesh - Gencral Overview

The climate of Bangladesh is categorized as warn-humid, based on the widely used classificanon of tropical clirnate by Ackinson (Koenigsbetger et al, 1973). There are three disninctive seasons, the hot humid, the hot dry and the cool dry season (Reported in, Mallick, 1994). Genetally, the winter is short and dry while the summer is long and wet The hot dry period is berween Match and May, the hot humid period covers Junct to September and the cold dry seasons starts from mid October to Febraary.

Again, meteorologically the climate of Bangladesh is classificd into four distinct seasons winter, pre-monsoon, monsoon and post- monsoon (Reporred in, Ahmed, 1995), wherthe winter is cool and dry, the pre-monsoon is hot and dry; monsoon and post-monsoon are hot and wet.

The winter months, December to February, are characterized ly infrequent rains, cold northerly winds, mean temperature $21^{\circ} \mathrm{C}$ and mean maximum below $26^{\circ} \mathrm{C}$. The premonsoon period covers the months March, April and May and is characterized by occasional thunderstorms, and an average maximum temperature of $34^{\circ} \mathrm{C}$. The monson is the longest season covering the months June to September, a period with torrencial rains, with the average relarive humidnty above $80 \%$ and an average temperature of $31^{\circ} \mathrm{C}$. 'The post-monsoon scason ranges between the months Ocrober and Novernber. It is also regarded as a unnsitional (to winter) penod with infrequent rains and icmperamres below $30^{\circ} \mathrm{C}$.

### 2.2 Microclimate of Dhaka City

The climatic characteriscics of Dhaks city differ from that of other cites of the country due to its dense physical developments and location. Again, wichin the same city these characteristics are further modified in different locations (Ahmed, 1995). It is due to the surface qualry of the atea - hard or soft, densiry of built environment, building type, building height and their orientations, proximity between buildings, material used for construction, dependence on electrical and mechanical appliances and ocher related Eactors.


Figure 2.1: Dhaka ciry: view of Dilkusha conmercial area.

Tabke 2.1: Clirratic den of Dhake.

| Chmanc period |  | Warm-fumid |  | $\begin{aligned} & \text { Cool-Dry } \\ & \text { Dec-Heb } \\ & \text { (Winter) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| Monthi |  | $\underset{\text { (MoneSept }}{\text { Jons }}$ | $\begin{gathered} \text { Oct-Nov } \\ \text { (Pont-Nomson) } \end{gathered}$ |  |
| Cimatic fiector |  |  |  |  |
|  |  |  |  |  |
| 2. Maximum | 37.60 | 36.10 | 34.90 | 3240 |
| 1. Ainimint | 13.80 | 20.90 | 1330 | 6.80 |
| c Averap | 28.02 | 2 A 8 | 25.42 | 19.43 |
| d. D'umal variation [averixe] | 11.60 | 7.12 | 11 | 14 |
| 2 Retative Huminity \% \|averapel | 69.91 | 64.78 | 8259 | 76.70 |
| 3. Rainfill (man) \|xerspl | 156.70 | 317.50 | 125 | 23.33 |
|  | 495 | 373 | 412 | 431 |
| 5. Sunshine [Houn (dzity aterest) | 7 | 4.5 | 7 | 8 |
| 6. W'ind Sperd (mfo) \|xatisg] | 26 | 22 | 1.5 | 1.5 |
| 7. Wrad Distection | S, S-1 | S. S-E, S.W | S. S.E | N, N.W ${ }^{\text {r }}$ |

(3amte Khast, 2005)


Fipure 2.2: Yeaty weather data shwoing tomperature profile and solar radiation firmat


### 2.2.1 Temperature

On the basin of meteorodogical dara, the temperature profile of Dhaka city shons similatity with that of the regional patem. The highest temperature is reeorded in the
monch of March, Aprl and May, wheh reaches to $37.8^{\circ} \mathrm{C}$ maximum in April. In the monsoon and post monsoon period, from June to October the temperature remains steady at an average of $28.8^{\circ} \mathrm{C}$. In cool period it drops to $19.43^{\circ} \mathrm{C}$ on average (I'able 2.2).

Table 2.2: Air temperanure in Dhaka city.

|  | Jan | Fcb | Mar | Apr | Ma | Jun | Jut | Aug | Scp | Oct | Nov | Doc |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Mcan maximum air <br> terap (deg C) | 26.2 | 279 | 32.3 | 312 | 330 | 31.8 | 31.2 | 31.1 | 31.7 | 313 | 28.8 | 26.4 |
| Avenge air ternp <br> (deg C) | 19.0 | 21.2 | 260 | 290 | 20.0 | 28.8 | 28.7 | 286 | 28.8 | 27.5 | 23.5 | 198 |
| Mean minimum air <br> tertp (deg C) | 11.8 | 145 | 197 | 23.8 | 25.0 | 25.8 | 26.2 | 26.1 | 25.9 | 23.7 | 182 | 13.2 |



Overheanng due to inexorable urlyan growth of Dhaka city is now a major environmental concern (Ahmed, 1995). Meteorological otservation in pre-monsoon period records a maximum temperatute of $37.8^{\circ} \mathrm{C}$, indicating a possible rend towards the inctcase of temperanure and overhearing.

### 2.2.2 Solar Radiation

Solar radiation can be considered as a single most deciding factor for assessing the climate of an area, because it affects the tempetanure and densiry of arr and thus affects the wind velocity, direccion and humidity (Ahmed, 1994). Renewable Energy Research Center of Dhaka University collects radiarion «lata for Dhaka city.

Figure 23 shows that in the hot dry perind, particularly in the months of March, Aprit and May solar radiation is high in comparison with that in the test of the year and it is maximum in April ( $5.5 \mathrm{KW} / \mathrm{h} / \mathrm{sqm} /$ day). From July to November (monsoon to postmonsoon) the radiation remains fairly constant.

From Figure 2.4 it has been observed that, the horizonell surface (commonly the roof surface of a built form) receives the maximum amount of solar radiarion tound the ycar in comparison with other common external vertical facades. But this is true for low rise buildings only. Fot tall buildings, horizontal surface is very negtigible in comparison to ocher fout vertical sutfaces and only the top Aloors of the tall buildings are affected by

$$
\because+\cdots
$$

incurring adiation on the roof of the trikdings. This rowult depinas the imponance of sdopted stretcgy fur venical surfaces of the built forms in tropical architerture.

 Cumb, Dlate U/aminis, 2005/


Figure 24: Amount of sobar radiation on different surfaces (horizontal and verical) for


As overheating is one of the key problems for the given climate, the issue of heat gain from solar radiation is highly significant and the vertical surfaces are observed as more imporcant than horizontal sutfaces of the built forms (for all buildings, specially when the suo is at a low angle).

## 2,2.3 Relative Humidity

The humidity of Dhaka city is high and the mean annual relative humidity is 77\% (Table 2.4). If all condations temain the same, then the relative humidity is inversely proporional to the temperatute. So, higher temperature yields lower relacive humudicy levels. Since ait temperame and radiation depend on the density of the built form, the humidity varies whth the density of the surrounding built environment.

Table 2.4: Relative humidity in Dhaka city.

|  | Jan | Feb | Mar | Apr | Ma | Jun | Jul | Aug | Sep | Oct | Nay | Dec |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Relatave Humidity | $69 \%$ | $63 \%$ | $61 \%$ | $70 \%$ | $79 \%$ | $83 \%$ | $86 \%$ | $85 \%$ | $86 \%$ | $81 \%$ | $75 \%$ | $7 \% \%$ |



### 2.2.4 Cloud Coverage

The cloud cover is only $38 \%$ for the whole pre-monsoon and post-monsoon period (Table 2.5). This clear sky condition cuhances the drect solat radiacion to reach on building surfaces. The cloud coverage is wery high in monsoon penod and is almost $70 \%$. The cloudy amospheric condution during this period helps in decreasing the incoming solar tadiation to the earth surface.

Table 2.5: Sky conduion in respect to cloud covet for a year.

| Typc of Sky | Hot-Dry | Hot-Humid |  | Cool-Dry <br> (Dec-Fel) |
| :---: | :---: | :---: | :---: | :---: |
|  | Fre-Monsæon <br> (Marth-May) | Monsoon <br> (June-Sept) | Post-Monsoon <br> (Oat-Nov) |  |
|  | $67 \%$ | $31 \%$ | $(4 \% \%$ | $85 \%$ |
| Overcast Sky | $33 \%$ | $69 \%$ | $36 \%$ | $15 \%$ |

(Sonte: Chmate Didusinn, Bangladesh Afetaotogioul Deparment, Dhaka, 2005)


Figure 2.5: Monthly average cloud cover (Suurce Chmale Ditisinn, Banghdesh Meseorodigat Deparment, Dhaka, 2005).

### 2.2.5 Sunshine Hours

The amount of solar radiation received by the surfaces also depends on the dutation of sunshune (Reported in, Ahmed, 1994). The sunshine hour in pre-monsoon and postmonsoon in quite long than that of monsoon period (Figure 2.6).


Figure 2.6: Monthly average sunshine hours (Soura: Chwate Division, Banghadesh Mettantmgeal Depirmment, Dhaka, 2005).

### 2.2.6 Wind Flow and Ditection

Wind speed in Dhaka in Hot period is relatively high and the direction is predominantly southerly and south-easterly (I'able 2.5). For winter period the direction of wind was found mostly from north and north-west. Accotding to the diurnal pattern of wind llow, in summer (except Aptil) the wind speed is low becween 12:00 and 15:00 hours (Reported in, Ahmed, 1995). During that period airllow may not be considered as reliable resource for cooling, tather depending on shading of surface from solar radiation would be mote pteferable.

Table 2.5: Monthly average wind speed and direction.

| Mfonths and seasoms | Wind sped in m/s | Wind direction |
| :---: | :---: | :---: |
| Jaturaty (Cool-Dry) | 1.4 | NW |
| Febreary (Cool-Dry) | 1.6 | N |
| March (1-0t-Dry) | 26 | sw |
| 4prol (Hot-Dry) | 3.7 | SW |
| May (1 fot-13) | 4.4 | S |
| June (wam-Humd) | 3.8 | SE |
| July (Warn-Humid) | 3.9 | SE |
| August (3'am-Humid) | 3.3 | SF , |
| Sepermber (W'arm-f Harnd) | 34 | SE |
| October (Warm-Hunid) | 25 | N |
| November (Warm-Humid) | 1.4 | NW |
| December (Cool-Dry) | 1.5 | NW |

(Sourt. Chmafe Divition, Bangladesh Mfteorolagka/ Dspartmont. Dhaka, 2005)

### 2.3 Problems in Oesigning in the Hot-Humid Climate

'The hot-humid climacic zone is chatactetized by high ambient tempetatures, high humudity, high and fairly evenly distributed rainfall, small diurnal and annual variations of temperarure, little seasonal variation, light winds, and long periods of still air.

The physiological themal tequirements and hence the building characteristics are the same for the whole year, as the scasonal clunaic variations are low (Yeang, 1990). The mann cause of discomfort is the subjecaive feeling of skin wemess (Koenigyberget ot al,
1973). Continuous ventilation is, therefore requited we ensure a sweat evaporation rate sufficient to maintain thermal equilibrium and minimum sweat accumulation of the skin. Radiation solar heat gain should be prevented.

The hot-humid zones present two problems to destgners:

- Avoidance of excessive solar radation, and
- Provision for moisture evaporation by breczes.

To cope with these, the structures and setdements need to be built to allow frec air movement. The roofs need to be insulated and provided with lange overhangs to protect against sun and tain.

Under hot condicions, the thermal controls in the building should:

- Prevent heat gain.
- Maximise heat loss
- Remove any excess heat by mechanical or passive cooling.


### 2.4 Conclusion

Alchough for most of the penod, overheanng is a major envitonmental concern for Dhaka, dise nanure of the problem is dictated by the combination of the environtental factors in the ambiance during those periods. From March to May chere is high anr temperature associated with hugh solar madiation, while from June to October, conditions with high hurnidity is associated with high air temperature. So from March to May+ reducing the impact of solar tadiation can potentially moderate the overheated condition and oprimizing shading can play a vital role towards moderation. For a topical wam humid climate like Dhaka ciry the minimum solar heat gan with the help of adequate shading is the major considetations to achieve chermal comfort.

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CHAPTER: THREE
TALL BUILDING AND SOLAR HEAT GAIN

## TALL BUILDING AND SOLAR HEAT GAIN

Increased land value, limited urban accessibility, expanding urban population, globalization of national economy and locational preferences of busincss make the all building inevitable. In addidion to accommodating living space for the purpose of habitation, tall buildings are now extensively used as working space. Alhough the principles of designing with climate are relaavely advanced for low-rise and md-nse buildings, adequate attention and research yet to be directed towards the tall building type (Yeang, 1990). A brief discussion on tatl and high-rise buildings, wich special reference to their climatic characteristics has been presented in the following scetions.

### 3.1 Tall Building

### 3.1.1 Definition

The experts differ in deluning the physical parameters of tall buildengs. According to the Council for Tall Buildings and Urban lrabitat (CIBUH), a tall bulding is not scrictly defined by the number of stories or its height. It also depends upon the context in which it scands. CTBUF defines tall buikding as a building whose built form, by virate of its height, requites its own special engineering systems (Yeang, 1997). The important criterion is whethet or not the design, use or operation of the buildng is influenced by some aspects of tallness.

As stated by Eli Atia in his seminar paper in "Fourth World Congress on Iall Building: 2000 and beyond' David Fisher defines the tall buildings as 'We build tall buildings of necessity; hiow we build them is a tefiection of sociery. Tall buildngs do not bave to be bcautiful, they simply must be functional; so it is the degree of our concern for their beauty that serves as a measurc of our humantry' (Attia, 1990).

According to Ken Yeang (Yeang, 1997), a tall building can be characteristics by
a) A small foot-print in comparison to its total built-up space
b) Tall facades due to its height
c) Smali roof-area in comparison to external-wall atca
d) Special engineering systems, different from the low building type simply because of its height.

According to Taranath, to define tall building from structural aspects, from scructural design and construction point of view, it is simpler to consider a building rall when its strucural analyses and design are in some way affected by the lateral loads (Taranath, 1998).

### 3.1.2 Justifications for Designing with Climate

Ken Yeang (Yeang, 1990) justifies the reasons for designing the tall buildings with climate very clearly. The most obvious justification must be the forwering of costs as a result of lowering the energy consumption in the operation of the building. This can be by as much as $40 \%$ of the overall life-cycle energy costs of the building. Significant savings in operational costs would justify incorporation of climarically-responsive design fearures despite a higher inidial capital construction cosrs.

Another rationale is from the impact on the users of the all building. The climateresponsive cill building would enhance its users' acstheric well-being whle enabling them wh be aware of and to experience the external climate of the place. The climateresponsive design would provide the building's users with the opportunity to experience the external covironment (and the diumal and seasonal changes where existent) and avert the blindness of spending their workng hour over a significant part of their day in an artificial environment that remains constant throughout the year.

A further jusufication is the ecological one. Designing with clmate woutd tesult in the reducton of the overall energy consumption of the building by the use of passive structural derices (i.c. non-mechanical). Cost savings in the operational costs means less use of electrical energy resources which is usually derived from the burning of non renewable fossil-fuels. The lowering of energy consumption would further reduce the overall emission of waste heat thereby lowering the overall heat-island effect on the locality.

### 3.1.3 Façade Design of Tall Buitdings in Tropical Climates

In passive low-cnergy tall building design, attention should be given to the facade design. For low volume-to-surface rato, tall buildings have more external surface than same volume of low nise bulding. In case of tall buldings, generally facades do not get mutual
shading from its surrounding like low aise buildings. That's why; external surfaces of tall buldings should be designed as an environmentally-responsive filter.

The façade should be multi-functional in its design. For instance, it can provide for teducing solar heat gain to the space through external shading devices, fresh air ventilation, acoustc barrier, maintenance access and a connriburion to the building's aesthetic.

Tall buildings are exposed more directly than others to the full impact of external temperanures and direct sunlight. The greatest source of heat gain in the tropical climate can be the solar radiation entering through the window. This solar heat gan can be reduced by using shading devices. These shadirg devices cut the huge solat heat gains directly through window. This crables the designer to use clear-glass, to give better dayight entering the intemat spaces, which then reduces the lighting energy-lond (Yeang. 1997).

### 3.2 Solar Radiation

Solar radiation influerecs the indoor thermal climate by direct heaning on penetraning the windows, and indrectly by heating the external envelope of the buulding. Heat flow through the wall and noof then determines the indoor surface and air temperatures. The effect of solar radiation on internal temperatures, as mentioned at the beginning, may be divided into two parts: 1) the effect on the temperanues of the external suffaces and toof and the resulting heat flow and indoor heating, 2) heaing caused by penetration of radianon through glazed or open areas (Givoni, 196\%).

Solar radiation is an elcettomagneric radiacion emitted [rom Sun (McMullan, 1992). The Spectoum is broadly divided into two regions i.e. the visible radiation and non-visible radiacion. Solar radiarion teaching the carch's surface consists of about 47 percent visibie, 48 percent short-wave infta-red (heat), and about 5 percent ultra violet radiation (1.echner, 2001).

Sunlight contuns no heat, both in the visible region and in the non-visil)le region (mainly infra-red with some ultra-violet) in about equal propomons. It is only when racliation falls on surfaces that it is converred into heat. The non-visible part of the spectrum often
referred to as 'thermal radiation', implying that only this part is the cause of hearing. But the visible part still carries half the energy that potentially can become heat (Steemers $e t$ $a l, 2002$ ).

### 3.2.1 Visible Radiation

The wavelengths of electromagneic radation that are visible to the cye range from ${ }^{\text {a }}$ [Proximately 380 nm to 760 nm [1 nanomere ( nm ) is $10^{-9}$ meter]. If all the wavelengths of light ate seen at the same time the cye cannot distingush the individual wavelengths and the brain has the sensacion of white hght (McMullan, 1992).


Figure 3.1: Electromagneac spectrum (Soure: Mahnhan, 1992).
White light is the effect on sight of combining all the visible wavelengths of light. Whute light can be separated into is component wavelengths. One method is to use the different teftactions of light that occur in a ghass prism. The result is a spectrum of light, whech is traditionally described in the seven colours of the rainbow although, in fact, there is a continuous range of hues (colours) whose different wavelengths cause different sensanons in the brain. Monochromatic light is light of one particular wavelength and colour If the colours of the spectrum ate recombined then white light is again produced. Varying the proportions of the individual colours can produce different qualities of 'white' light.

### 3.2.2 Non-Visible Radiarion

Electromagnenic radiations with wavelengths outside the range of visible wavelengths cannot, by definition, be detected by the human cye. However, those radiacions immedately adjacent to the visble range of wave lengths are emitted by the Sun, along with light, and are often relevant to lighuing processes (McMullan, 1992).

## Infra-Red

Wavelength range of infra-ted is from 760 om to above. Infra-ted (IR) radiation has wavelengths slighty greater then those of red light and can be felt as heat radiarion from the Sun and from other heated bodies. In[ra-red radiation is make use of in radiant heating devices, for detecting [afterns of heat emissions, for 'seeing' in the dark, and for communicaion links.


Figure 3.2: Solar spectrutn (Soutra: Stenters a al, 2002).

## Utta-Violet

Wavelength range of ultra-violet is below 380 nm . Ultra-violet (IV) radiation has wavelengehs slightly less than those of violet light. It is emitted by the Sun and also by other oljects at high temperature. Ulitra-violet radiation helps keep the body healthy but excessive amounts can damage the skin and the eyes. The compositon of the Earth's atmosphete normally protects the planet from excessive UV radiacion eminted by the Sun. Ultra-violet radation can le used to kill harmful bacteria in kitchens and in
hospitals. Certain chemicals can convert UV encrgy to visible light and the effect is made use of in fluorescent lamps.

### 3.2.3 Direct, Indirect Solar Radiation

Solar radiation is a dominating influence on all climatic phenomena. Of the total energy radiated by the sun towards the carth, part is reflected off clouds ourwards, part is absorbed by water vapour, polluants, dust particles and other atmospheric condicions, beng re-emitted as diffuse radiation, and the rest of it is drectly tanamitted to the carth's surface.


Figute 3.3: Direct, indirect solar radiation (Affer Abmet, 1987)
Whereas direct radiation is dependent only on the alcitude of the sun, and is independent of geographical position, diffuse radiation vaties with the time of the day, the weathct, the cloud cover and the portion of the sky from which it is received. According to Jones, no specific ditection can be assigned to diffuse radiation and therefore there is no direcrional shadow associated with it. Diffuse radianion also varies with solar alnoude, as direct intensities reach their highest values at midday, and there is much more radiation available for scattering than when the sun is low in the sky (Reported in, Ahtned, 1987).

### 3.3 Solar Heat Gain

The heat grin in a building by radiation from the Sun depends upon the following factors (McMullan, 1992):

- The geographical lairude of the site, which determines the height of the Sun in the sky.
- The orientacion of the building on the site, such as whether rooms are facing south or nord.
- The season of the year, which alio affects che height of the Sun in the shy.
- The local cloud conditions, which can block solar radiation.
- I'he angles between the Sun and the building sutfaces, because maximum gain occurs when surfaces are at right angles to che rays from the Sun.
- 'The nature of che window glass and whecher it absorbs or teflects any radianon.
- The nature of the toof and walls, because heavyweight matenals behave differendy to lightweight matectals.

Solar radiation falls on a surface varies throughout the day and the year. Most solar heat gain to buildings is by drect radiation through windows. The maximum gains through sourh-facing windows tend to occur in pre-monsoon and post-monsoon period when the lower angle of the Sun causes radiation to fall more directly onto vertical surfaces. The solar heat gains for a particular building at a specific time are relatively complicated to calculate, alchough it is important to do so when predicring summer heat gains in commercial buildings.


Figure 3.4: Typical proportions of incident solat radiation, reflected, absorbed, transmitted and tetransmitted by glass (souras: Smith of at, 1982).

The solat radiation falling upon a clear glass surface is reflected, albsorbed and transmitted in proportions similar to chose indicated in Figure 3.4. These quantities depend upon the angle of incidence (i) and che proporion of direct and diffuse radiation. The angle of incidence (i) is the angle measured between the incident light beam and the normal to the plane of the glass (Strith et al, 1982).

The alsorbed radiation heats the gitass and patt of this heat teaches the room surfaces by convection and radiation from the inside surface of the glass. The solar heat gain is obtained by adding the inwards released heat to the directly unnsmitted component of the incident solar radacion. Absoption of this solar heat gain by the internal surfaces raises their temperature. These heated surfaces behave as low temperature, long wave radiators. Since glass cransrnits shortwave radiation in the range 0.3 to $2.8 \mu \mathrm{~m}$ but is opaque to long wave tadiation from low temperature surfaces, the solar heat gained is trapped within the enclosure causing an intemal umperature ise. This phenomenon, frequently referred to as the greenhouse effect, may give rise to solar owcrheating. Heat gain is directly proportional to the atca of glass exposed to solar radiation and therefore large glayed areas will pertrit a large and rapid heat gain.

### 3.4 Conclusion

The extensive use of glazing in the building façades is one of the charactensics of moden architecture. This, and the increasing use of lightweight strucnures has caused considerable changes in the relationship between interior and ambient climates and the protslem of overheating has becorne a major concern. To face this problem, in most of the cases mechanically cooling system is the solution. But this becomes a hurden on total energy load of the country. The idea of a climate-responsive call building may change the prefetence to one away from the present fully araficial working environment. Tall buldings designing with climate arc evidenty justiffed on the ground of recurting savings in cost and energy use in the opetation of the building.

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CHAPTER: FOUR
SOLAR CONTROL AND SHADING DEVICES

## SOLAR CONTROL AND SHADING DEVICES

lall buildings are exposed to the full impact of direct solar radiation, which is the greatest source of heat gain in the tropical climate. Heat gain through window is ditectly proporional to the aren of glass exposed to solar radiation and thetefore lange glazed areas permit a large and rapid heat gain. Shading is a key stritegy to reduce solar heat gain in overheated periods. The most efficient solar control is provided by external shading devices. This chapter presents a brief discussion on methods and principles of solar concrol emphasising on external shading devices. It helps to develop a clear understuodung of the issues involved for the further development of design scrategies of shading devices in the later sections of this work.

### 4.1 Solar Control

Direct solar radiation can be presented from reaching all or part of the walls, teof or wndows of a building by the use of shading. Shading can be provided by namual vegctation, neighbouring buildings or the surrounding landscape. Shading devices on the building (fixed of movable, the latter being manually or automatically controlled) can present direct radiation reaching critical parts, such as windows, doors and even roofs. Indirect solar gaun from the sky, or reflected from the surrounding buildings or the ground and atr feated by irradiated sutfaces also enhance significantly to the cooling load.

### 4.2 Method of Solat Control

The greatest source of heat gain can be the solar madianion entering through a window. This could, in fact, increase the indoor temperature far above the out-door air temperature, even in modetate climates, which is known as the 'greenhouse effect' (Koenigsberget et al, 1973). Window glasses are pracically cransparent for short-wave infra-ted tadiation enitted by the sun, but almost opaque for long-wave radiation emited by objects in the room. The consequence of this is that the radiant heat, once it has entered through a window, is trapped inside the building.

There are four merhods available for the reduction of solar heat gain chrough windows:

## 1. Window Orientation

2. Internal blinds, currains
3. Heat absorbing/reflecting glasses
4. External shading devices

### 4.2.1 Window Orientation

Building orientacion affects the indoor climate in two tespects, by ats regulation of the influence of two distinct climate factors (Givoni, 1969):
a. Solar radiation and its heanong effect on walls and rooms facing different directions.
b. Venulation problems associated with the relation between the direction of the prevailing winds and the orientation of the building.

The effect of window orientation on the indoor temperatures is largely determined by the vencianon conditions and che degree and efficiency of the wirdow shading. When shading is not effective, solar radiation enters through the window's and directly heats the building interiot, the temperanures of which will obviously be influenced by the orientaion of the windows. The healing effect of solar cnetgy penetrating a glazed wall or closed unshaded windows is mannilied, as the energ) is transformed in the exterior or by longwave radiation, to which the glass is opaque.

In the equatorial location, if solar heat gain is to be avoided, the main windows should face north or south (Koenigsberget et al, 1973). At higher latitude, an orientacion away from the equator would receive the least sunshine, but here it may be desirable to have some solar heat gain in the winter, when the sun is low - so an onentation towards the equator may be preferable. In both locations ondy minor openings of unimportant tooms should be placed on the cast and west side. Solar heat gain on the west side can be particularly croublesome as its maximum intensity coincides with the hotest part of the day.

### 4.2.2 Internal Blinds and Curains

From an energy-rejecion point of view, the external shading devices are the most effectuve. But for a number of practical reasons, the incerior devices, such as curtains, roller shades, venetian blinds, and shutrers, are also very important. Interior devices are often less expensive than external shading devices, snce they do not have to resist the elements. They are also very adjustable and movable, which enables them to casily respond to changing requirements. Besides shading, these devices provide numerous other bencfits, such as privacy, glate control, insulaion, and interior aesthecics (Lechner, 2001).

Since internal devices are usually included whether or not external devices are supplicd, we should use them to our advantage. They should be used to stop the sun when it out flanks the exterior shadeng devices. They are ilso useful for those exceptionally hot days during the tratsition or under heated periods of the year, when exterior shading is not designed to work. In the form of venecian blinds or light shelves, they can also produce fine day lighting.


Figure 4.1: Interior shading devices for solar control (Sours: Leibstr, 200t).
Onc of the main drawbacks of interior shading devices is that they ate not always disceming. They cannot block the sun while admining the view, something that can be effectively done with an external overhang. Since they block the solar radiation on the inside of the glazing, much of the heat temains indoors.

It is tue that they stop the passage of radiation, but they themselves absorb the solar heat and can reach a very high temperature (Koenigsberger et a/v 1973). The absorbed heat will be parly convected to the indoor air and partly reradiated. Significant portion of this reradution is outwarls, but as it is of a long wavelength, it is stopped by the window glass. The usual narrow space between the window and the blind will thus be quite substantially overheated. 'The hot surface of the blend causes the indoor MRT to rise far above the air tempetature.

As a broad generalzarion the daily average solar gain factor of a single glazed window will be:
$\theta=72 \%$ without any solar control device, and
$\theta=55 \%$ with an internal venecian blind [i.e. the reducton is only $17 \%$.

### 4.2.3 Heat Absorbing/ Reflecting Glasses

Even the clearest and thinnest glass does not transmit 100 percent of the incident solar radiacion. The radiation that is not cansmitted is etther absorbed or reflected off the surface. The amount that is absorbed depends on the type and thickness of the glazing. The amount that is teflected depends on the nature of the surface and the angle of incidence of the radiation (Leclener, 2001).

One type of tinted glazing is called heat absorbing because it absorbs the shomave infra-red par of solat radiation much more than the visible part. But even this type of glazing reduces the solar heat gain by only a small amount. Although tinted glazing reduces the light ransmission, it usually does not dectexse the heat gan by much because the absorbed.radiation is then reradinted indoors (Givoni, 1998).

Glazing also blocks solar radiation by feflection. The amount of solar radation that is reflected ftom glazing can be incteased significantly by adding a reflecrive conting. One surface of the glazing is covered with a metallic coating thin enough that some solar tadiation suill penctrates. The petcentage reflectance depends on the thickness of this coating, and a mirror is nothing mote than a coating that is thick enough so that no light is teansmitted. Reflectave glazing can be extremely effective in blocking solar radiation while still allowing a view.


Figure 4.2; Heat gain through different types of glazing (Souns: Labner, 2) (1)

When reflective glazing became available in the 1970s, it quickly became popular for several reasons. It blocked solar radiation better chan heat-absorbing glass, and did so with out any color distortion.

Although tinted and reflective glazing systems can be effective shading devices, they are very undiscerning. They do not differentuate between hight from the sun and light from the view. They filter out Light whethet daylight is desited of not. And they block the desirable winter sun as much as the undesirable summer sun. Thus, tinted or reflecave glazing is not appropnate where cither day lighting or solar heanng is desired. It is also not appropnate when only the sum should be excluded, but not the view. When glazing is expected to do all che shading, it has to be of a very low ransmumance type. The view through this kind of glazing makes even the sunniest day look dark and groomy. Thus, external overhangs, fins, etc. which are more discerning, are usually still the best shading devices. Tinted or reflective glazing is excellent, however, for blocking diffuse sky radiation in very humid regions, and for glate control (Lechner, 2001).

When daylighting is desired and solar heating is not, having the visible component of solat radiation pass through while heat radiation is blocked would he advantageous. Cerain "specially sclective" glazing systems can do that to a limited extent Specially selecrive low-e-glazing transmits cooler dayluht than other glazing materials, because it transmits a much hugher ratio of visible-to-infrared radiation (Givoni, 1998).

In the near future, there might be even better glazing system than the "selective" copes mentioned above. These are known as responsive glazing systems because they change in response to light, heat, and electricity.

Responsive glazing can be either the passive or the acrive kind. Passive glazing responds directly to enfironmental conditions, such as light level or temperature (photochromics or thermochromics, respectively). The accive system can be conrolled as needed and can include such devices as liquid crystal, dispersed parricle, and elecrochromics.

Photochromitcs: These materials change their transparency in response to light intensicy. They are ideal for automatically controlling the quantity of daylight allowed into a building. The goal is to let in just enough light to eliminate the need for electeric lighting, but not so much that the cooling load woutd increase.

Themochromics. These matcrials change transpatency in response to temperature. They are transparent when cold and reflecuive, white when hot. They can be used in skylights, where the loss of transparency on a hot day is not a problem as it would be in a vew window. These materiats could also be used to prevent passive systems from overheating in the summer

Iiquid-Cyssal Glaping: When electric power is applied, the tansparent liquid crystals algn and become translucent. Thus, lequid-crystal glazing has some application for shadng, but its teal potential is in privacy control.

Dispersed-Particle Glaring: Although similar to liquid-crystal glazing, this material is mote promising for solat control because the applied power can change the transmitance of the material in a range between clear and dark states, thereby preserving the view.

Elechochromic Glaving: Thus is the most promusing material because it can change transparency-not translucency-continuously over a wide range (about 10 percent to 70 percent) and can be easily controlled. Consequently, either a computer, a photocell, a themostat, of the occupant can adjust the transpanency as the local condirions require.

### 4.2.4 External Shading Devices

Blocking the sun before it reaches che buildng, particularly the glazed, but also the opaque surfaces (including the roof) and reflecring the solat radiation, is fundamental to the prevention of heat gain (Goulding, 1992). The appropriate chore from a wide range of Eixed and movable shading systems will depend on location, orientation, building type
and the overall coolng, heating and daylighting strategies adopted in the design phase of the building.

While shading systems must provide good solar protection in summer, they should not reduce solar gains in winter, obstruct narural lighting or impede natural vencilation. Well designed shading systems can actually enhance natural ventilation and daylighting. Shading syscems can block the drect component of solat madiation but are usually not as effective in teducing the diffuse and reflected components.

### 4.3 Shading Devices

Once the window size has been established the most effecrive mechod of reducing solar heat gain is to ptevent the transmission of shorwave radiation through the glass by external shading.

The effecriveness of a trpical glazing and shading system may be measured in terms of the solar gain factor. 'Ihis is the proportion of incident solat radation cransmitred by the window and shading device to the interiot of an enclosure. The solar gain factor for an unglazed unshaded aperture is unit. 'This factor decreases as the shading system becomes mote effective in teducing solar heat gain (Srnith et al, 1982).

The requirements for daylight and ventilation may well conflict with the need to provide shading devices to control solat heat gain, reduce glare and prevent direct radiacion falling upon the occuptants of an enclosure. Traditional heavyweight building wich strall windows is unlikely to experience the solar overheating problems, which may occur in the excessively glazed lightweight modern office block.

### 4.3.1 Objective of Shading

Shading the glass affects the quanricy of incident radiation and hence modifies boch the heat flow to che interior and the indoor temperatures. It is useful to ser out the puppose of shading in some detail (Steemers et a/, 2002). They are mencioned as follows.

- To minimse the total solar energy entering a room and thereby reduce the average temperature of the room
- To prevent sunlight from falling directly ontor occupants, resuling in an effective increase of temperatutc of between $3^{\circ} \mathrm{c}$ and $7^{\circ} \mathrm{C}$
- To reduce the local inlumination of surfaces that may present glare soutces $t o$ the occupants
- To prevent the view of brighrly lis.outside surfaces, or clouds, or the surn itself


### 4.3.2 Types of Shading Devices

Shading devices are broadly classified into three categories based on its integration with the window (Goulding, 1992; Steemers et al, 2002; Lechner, 2001). They are classified again within these categones by their mophological charactensuics and physical foms. The broad categories of shading devices are:

- Retractable or removable shading dence
- Movable or adjustable shading device
- Fixed shading device


## Retractable Shading Device:

Retractal) means that these elements can be completely or pattially ternovable from the window aperture (Stecmers at al, 2002). It is impottant to note that shading devices of chis rype do not influence the availability of daylight in the room. That is, they will not influence switch-on time, because at tines of low light avalability they can be removed from the apernure. Clearly this property teconciles the conflict between allowing useful light in and keeping whwanted radiation out. Jf correctly operated, devises of this type whll not lead to an increase in artificial lighting energy.

## Movable Sbading Devices

Movable shadng is used extemally or internally. Control can be either manual or power assisted and may be automated to respond to changng conditions, such as curreat radiation levels and daylighting or themal requirements (Goulding, 1992). The configuration of operable shading devices can be changed, and thetefote their performance can be much betret that that of fixed devices. However, their posicion has
to be adjusted, daily or seasonally, to the changing patterns of the sun's relative mocion and the shading needs (Giveni, 1998). They usually need maintenance to keep them in good condition.


Overhang, Awning

fin Rotating, firs


Overbang: Rotating hormontal louvers


Ekgctate: Rotating I Jorizontal houvers

Figure 4.3: Some of movable shading devices (Source. I etiner, 2001 ).
The movement of shadeng devices can be very simple or very complex. An adjustment twice a year can be quite effecive and yet simple. late in spring, at the beginning of the overheated period, the shading devicess would be manually extended. At the end of the overheated period in late fall, the device would be rerracted for full solat sxposure (Lechniet, 2001).

There is a general convicion that since a bulding should be as low maintenance as possible, movable shading devices are unacceptable. The use of exising technology and careful detailing can produce trouble-free, low-maintenance movable shading devices.

## Fixed Shading Devices

Fixed shading systems include structural elements, such as halconies and projecring fins or shelves and non-srructural elements, such as canopies, blinds, louvers and screens. The orientation and shape of the opening to be shaded, relative to the position of the sun at different times of day and year, is critical to the design of lixed systems (Goulding. 1992). Fach onientation will need to be examined separately, taking account of direct and diffuse or reflected components of the overall solat tadiation throughout the day and ycat. Typically horizontal shadng is used for south facades, whereas vertical or diagonal fins or louvers are often more efficient on the east or west facades in northern hemisphere.

Fixed shading systems atc most commonly used on the cxtemal facades where they can prevent direct radiation from reaching glazing or ocher openings and where heat absorbed by the shading system can be dissipated to the ourside air. An obvious advantage of fixed shading is that it needs no handling by the occupants and is often maintenance free.

Fixed shading devices are of three types based on their physical forms (Koenigsberger et al, 1973; Givoni, 1998). They are horizontal shading device, verrical shading device and combination of the avo (eggerate). A brief discussion of these three types of fixed shading devices are presented below:

## Vemical Shading Devides

Vertical devices consist of louver blades or projecting fins in a vertical position. Natrow blades whth close spacing may give the same shadow angle as broadet blades with wider spacing (Koenigsberger of al, 197.3). Vertical fins are often presented as the shading devices of chore for east and west.

Vertical tims can be appropriate cither when thete is a desire to control the direction of view or when the view is not important. This ype of device is most effective when the sun is at one side of the elcvation, such as an castern or western clevation. A verical device to be effective when the sun is opposite to the wall considered, would have to give almost complete cover of the whole window.


Overhang Itraizonal pand


Overhang: Lourers in vetical plan


Vertical fin


Liggerate


Overhang lauvers in hovizontal plan


Overhang Vertical pramel


Vertical fin slanced


Eysctate with slanted fins

Figure 4.4: Some of fixed shading devices (Source: Iestinet, 200)).

## Horizontal Shading Devices

The horizoncal overhangy and its variations are the best choice for south facade. Because Lhey are directionally selective, they can allow the low wintet sun to enter while fully shading the high summet sun with minimum obstruction of the view.

Horizontal louvers have a number of advantages over sold overhangs. Horizontal louvers in a horizontal plane reluce structural loads by allowing wind to pass right thtough (Lechnct, 2001). In the summet, they also minimize the collection of hot aur next to the windows under the overhang, Forizoncal louvers in a verical plane are approprate when the projecting discance from the wall must be lemited. This could be imponant if a building is on or near the propenty line. Louvers can also be useful when the architecture calls for small-scale elements and a rich texrure.

When designing an overhang for the south facade, one must remenber that the sun comes from the southeast before noon and from the sourhwest after noon. Thetefore, the sun will outllank an overhang the same whth as a window. Narrow windows need either a very wide ovethang or vertical fins in addion to the overhang. Wide strip windows are affected less by this problem.

Horizontal devices will be the most effecrive when the sun is opposite to the building face considered and at a ligh angle, such as for north and south facing walls (koenigstberger et al, 1973). In summer they can block the rays of the sun and in winter they can admit radiarion from the sun's lewer posinion. To exclude a low angle sun, this type of device would have to cover the window completely, permitting a vicw downwards only.

## Egg-crate

Eggerate shading devices are mainly for east and west windows in hot climates and for the additional southeast and southwest oriencarions in very hot climates (Lechner, 2001). An eggerate is a combination of horizontal Overhangs (louvers) and vertical fins. By concrollhng sun penetration by both the alitude and azimuth angle of the sun, very effecrive shading of windows can be achieved. The Designer should first decide on the gencral appeatance of the eggerate system. As far as sun penetration is concemed, the
scale of the eggetate can be changed at any time as long as the ratio of herght/depth and widh/depth are kept conscant.

### 4.4 Conclusion

Shading is a key surutcgy of achieving thernal comfort in-the summer. Although.shading of the whole building is beneficial, shading of the glazed areas is ctucizl. Heat gain is directly proportonal to the area of glass exposed to solar radiation and therefore large glayed areas will permit a large and rapid heat gain. Existing heat-absorbing glasses can protect only $20 \%$ of the total incident radiation and reflective glazing prevents solar radiacion up to $50 \%$. Hence extemal shading devices can be a good answer to concrol the solar radiation. The most efficient solar control is provided by extemal shading devices, the design of which can only come from understanding the solar geomeny. Direct radiation is dependent only on the altitude of the sun and geographical position. That's why; direct radiatoon can be contonlled effectively by proper external shading devices.

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CHAPTER: FIVE
PERFORMANCE EVALUATION OF SHADING DEVICES

## PERFORMANCE EVALUATION OF SHADING DEVICES

The performance of shading devices and its impact on solar heat gain through windows can precisely be evaluated by simulation study. Because in reality, due to the sumuleaneous influence of many different conditions, it is difficalt to isolate the exclusive effect of one single aspect or the changes of it. Shadow simulation allows sudy of the effect of changes in one aspect, keeping other factors constant. The observations of simulared behaviour that occurs due to changing parameters allow the identification of elemente, the reduction or introfuction of which in the design conmibute to solar heat gain. Another significant achievement of simularion study is that, it is possible to analyse the performance of shading devices for any period of the year simply by assigning simulation parameters (e.g. temperature, radiation, wind specd and direction, relative humidity and cloud cover).

In this chapter, nine tall office buildings from different commercal areas in the Dhaka city have been considered to evaluate perfomnance of their shading devices, in temens of reducing solar heat gain through simularion study on the basis of set criteria. A dynamic computer simulation program named 'Ficonect' (version 5.20) has been used for thes simulation study.

### 5.1 Selection of Shading Devices for Evaluation

Before making seleccion of shading devices, tall office buildings are identificd nn the basis of certan considerations to be discussed in the following section. These tall office buldings are located in different commercial areas in the Dhaka city, such as Mocijheel, Dilkusha, Karwan bazaar, Panchapath, Banani, Mohakhali cte. After that, buildings were categorised considering the rypology (based on grometry) of shading derices installed on their front fraçade. Sketriches of window sections with shading device of these buildings were prepared with deail construction features, installation rechnique and geomerric features. After analysing the sketches, nine shading devires were selected movaluate performance in terms of reclucing solar heat gain considering shading device appology and similarities in geometric features.

## Tall Building Criceria

There is no fixed parameter of height to denote all and high-rise building. According to the Council for Tall Buildings and Urban Habitat (CTBUH), the number of stories or its height does not strictly define a tall building. It also depends upon the context in which it stands. The Council for Tall Buildings and Uban Habirt (CTBUH) considers for instance, call buildings as being buildings of ten stoteys or more.
a) Walk up limit / provision for lift:

- Accorling to Building construction rules (2006), buildings of seven storied and above in height shall have provision for lift.
- According to Bangladesh Nacional Building Codes (1993), lifte shall be provided in buildings more than six straried or 20 m in height.
b) Fire escape provision:
- Accarding to Fire Service and Civil Defence rules, buildings of seven storied and above in height shall have provision for Fitc escape/alternative staircase.
c) Structual analysis and design:
- According to Wolfgang Shueller, buildings with height-to-width rario above 5-7 are considered as high-rise smucture.

In view of the above considerations, in the present context of Dhaka city, buildings above six storeps may be conkidered as tall buildings.

## Selection of Shading Devices

Following the above criteria, cighty-four all office buildings of Dhaka cicy were identified for investigation. Among them, forry buildings are struated at Morijheel and Dilkusha area; twenty-four buildings at Mohakhali, Gulshan Avcirue and Barani Kemal Acarurk Avenue; fourteen buildings at Karwan Bazaar arca and six buikdings at Panthapath.

Among these buildings, twenty two buildings have horizontal shadiog devices, teven buildings have vertical shading devices, twenty bulldngs have composite type (combination of horizontal and verical) shading devices and thity one buildings do not have shading devices on their front façade. Among these eighty-four tall office buildings,
nine buildings sere sekered to ewhute performance of their shading dovices The list of buildings with loation beigh, orientation and rype of shading device inatalled is presented behowe

Table 5.1: List of the telected buildinga and shading devices.

| $\begin{gathered} \mathbf{s} \\ \mathbf{N o}_{0} . \end{gathered}$ | Idendifention Number | Location | Storey | Orkencation | Shadiaf Derice |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | H01 | Jenata Benk Buston, Moxitherd | 23 | Eat | Hocizonty |
| 2 | 1302 | Crintal Insumence Lind. Dimuta | 11 | South | Hotmontal |
| 3 | 1203 | Hrac Center, Motalthat | 20 | Nerth | Horimant |
| 4 | 701 | Rupuh Bant 1dd, Dilkusha | 10 | South | Vertical |
| 5 | 102 | 19+whati Bhatan, Dintuha | 9 | Wes: | Vertici |
| 6 | V03 |  | 9 | Easa | Verical |
| 7 | C01 | Krinhi Mhaben, Dillusha | 11 | South | Composite |
| 8 | CD2 | HCIC. Bhater, Diminina | 22 | Sourth | Comporite |
| 9 | C03 | Mephim Life lnarract, Dillusha | 10 | Fast | Composite |

Vica of front facndea of the selected building and sketches of windore tections with shading derices of these truiddings ere presented below.


Figure 5.1(a): Vicr of building FH 1 .


Figure 5.1(b): Windore rection of H 101.


Figure $5.2(\mathrm{a})$ : View of building H02.


Figure 5.3(a): View of building H03.


Figure 5.4(a): View of building V01.


Figure 5.2(b): Window section of H02.


Figure 5.3(b): Window seccion of H 03 .


Figure 5.4(b): Window section of V01.


Figure 5.5(a): View of building V02.


Figure 5.6(a): View of building V03.


Figure 5.7(a): View of building C 01.


Figure 5.5(b): Window secrion of V02.


Figure 5.6(b): Window section of V03.


Figure 5.7(b): Window section of C01.


Figure 5.8(a): View of building C02.


Figure 5.8(b): Window secrion of C 02 .


Figure 5.9(a): View of building C 03.


Figure 5.9(b): Window section of C03.

### 5.2 Performance Evaluation Process

Performance of the selected shading devices will be evaluated in terms of reducing solar heat gan through simularion study on the basis of set criteria to be discussed in the following secrion. Simulation is a powerful technique for solving a variety of problems. To simulate is to copy the behaviour of the phenomenon under study. It refers to some representation or model of a sysiem that can be studied in onder to understand the behaviour of the actual system italf and momake prodicrions about the furure. It involves developing a model of a system and carrying out experiments on it. It helps analyzing the effect of phenomenon and chcir interaccion on one another (Suri, 2005).
)
Evaluation process comprises the following steps:

- Setting criteria for perfommance cvaluation
- Preparing climate Jatabase
- Setting simulation parameters
- Devcloping simularion model
- Analysing results of simulation

In order to cyaluate the performance of shading devices in reducing solar heat gain, a base-case situacion is established by studying the unshaded window (without shading device) during the critual shading period of the yeat at different oricntarions.

### 5.2.1 Criteria for Performance Evaluation

- The percentage of the shade area, given by vanous rypes of fixed shading devices (Givoni, 1969; Stemers at of 2002). The percenmage of the shade areas refers to portion of the window area, which is not exposed to the direct solar radiarion. This also rellects the ability of a fixed shading device to protect the window area at critical tinc.
- Compuration of the shading coefficient, which is the ratio of the heat entering the window-shading combination to that entering an unshaded window. Shading coefficient ( $\mathrm{C}_{\text {sb }}$ ) can be expressed as below.
$\mathrm{C}_{\mathrm{kb}}=\frac{\text { Heat entring through the window with shading device }}{\text { Heat entering through the window without shading device }}$
Shading coefficients basically refer to the fraction of solar heat gain that passes through a mansparent solar aperture compared to the amount of solar adiation incident upon it. The shading coefficient is expressed as a dimensionless number from 0 to 1 . A high shading coefficient means high solar gain, while a low shading coefficient means low solar gain (Givonh, 1960; Givoni, 1998; Steemers et al, 2002; Lechner, 2001).


### 5.2.2 Simulation Ptogram

Simulations tegarding solar performance analysis are carried out using building analysis sofrware ECOTECT $55.20^{\circ}$. It features a usct-friendly 3D modelling interface fully
integrated with a wide range of performance analysis and simulation functions. 'Ihe visual nature of calculation feedback makes "HCOTECI' unique. 'The process can be started with a decailed climatic analysis to calculate the potential effeciveness of various passive design techniques or moprimise the use of available solar, light and wind resources.
'The original ECOTECT' sofware was writen as a dernonstration of some of che ideas presented in PhD thesis by Dr. Andrew Marsh at the School of Architecture and Fine Ante at The University of Westem Australia. The sofrware has undergone some major changes since then. Version 5.2 builds significantly on the functionality of previous versions incroducing a range of new analysis functions and real-time hidden line and sketch visualization. It also refines some of the major algorithms, such as the thermal and daylight factor calculations.

ECO'LECI provides a range of thermal and solar performance analysis options. At its corc, is the Chartered Institute of Building Scrvices Engneers (CMSE) Admittance Method used to determine heat loads. The Admittance Method is widely used around the wotld and has been shown to be an cxterncly useful design-tool This chennal algorithm is very flexible and has no restrictions on building geomery or the number of themal zones that can be simulaneously analyzed. Most importantly, with only a few precalculations for shading and overshadowing, it is very quick method to calculate and can be used to display a wide range of very useful informaton.

Whilst in summary it is a simplified method, the Admittance Method encapsulates the effects of conductive heat flow rhrough building fabric, mfilmarion and veatilation through openings, direct solar gains through mansparent materials, indirect solar gains through opaquecelements, internal heat gains from equipment, lights and people and the effects of inter-zonal hcat How.

Nicki Taylor validated ECOTECT as part of his research work for the degree of Bachelor of Engineering (Hons.) from Deparment of Environmental Engineering at Universify of Western Australis in 2002. He showed in his rescarch that the mean error of the estimated resulta is less than $2 \%$, indicating a reasonable degree of accuracy (Taylot, 2002).

### 5.2.3 Climate Database

The climate database stores filcs concaining houdy weather data. The weather files supplied wrh Ecotect cover different regions of the world and each represents a cypical year's weather for 2 particular region. The weather fite is not provided with the software. But facilities arc provided to allow creating own weather files and can be added to the climate database.

The weacher file 'Ban_Dhaka,wea' has been prepared for the research purpore by using the Weather Tool, associated sofrwate of Ecotect. The Weather Tool is a visualization and analysis program for hourly climate data. The weather file consists of a group of parametcers relaring to the weather site and hourily values of seven weather variables (drybulb temperature, relaive humidiry, direct radianon, diffuse radiation, wind spoed and direction and cloud cover). Hourly radiation data has boen collected from Renewable Energy Research Cenrre of Dhska University. Three hourly weather data regarding drybulb temperanure, relarive humidity, wind specd and direcrion and cloud cover has been collected from Climate Division, Bangladesh Meteorological Department Agargaon, Dhaka. Due to the simularion requirements, all three hourly data have been converted to hourly data by interpolation method. Houny wcather variables for Dhaks have been collected for the year 2005 .

The site parameters of Dhake for weather file are as follows:

| Parameters | Dernils |
| :--- | :--- |
| Latinude (degrecs North) | $23^{\circ} 50^{\prime}$ Norh |
| Longitude (degrees East) | $90^{\circ} 20^{\prime}$ East |
| Time Zone (hours ahesd of GMT) | GMT +06.00 |

The combination of site parameters and hourly weather variables forms the weather file, with which the simulation program Ecotect is capable to analyse any climaric characterisrics of the selected site.

### 5.2.4 Simulation Parameters

Before starting the simulanons a set of parameters are set. These are described below. To investigate the resuls of the simulations, a specific day has been selected (from the weather database for a year) on the basis of some specific atributcs to obscrve the results.

## Considerations for Identifying the Simulation Day

For individual daily profile analyषis, a day of the year has been sclettod in consideration of the cypical characteristics of the given climate.

The test day is $21^{\text {st }}$ of March (Day: 80). Outdoor air temperature range of this day is $24.5^{\circ} \mathrm{C}-35.4^{\circ} \mathrm{C}$ and sky condicion is clear. From $0900-1700$ hours the cloud sover is 1.1 out of 8.0 ( $13.8 \%$ coverage). This is a day with considerable hiph outdoor air temperature but not the extreme one and bears a common chatacter regarding the climaric feanures specially of the hot-dry season. The average temperature of this day (20 ${ }^{\circ}$ ) is very close to the average temperature of the scason $\left(28.02^{\circ} \mathrm{C}\right)$. It has been observed that the sky condition in the given climate is clear for 67 percent of the whole pre-monsoon period (earliet shown in table 2.3) and the 'clear sky' condirion prevail for the chosen day. This 'clear sky' condition of the chosen day is also important in investipate the impacte of solar radiation and this clear sky condition enhances the direct solar radiation to reach on building surfaces. Overcast sky condition impedes dircet radiation to reach the building surfaccs. Fixed shading device are effectuve to reduce heat gain from dircet solar radiation. These are the reasons techind choosing a day with clear sky condimon.

For a fixed shading device, the shading period is symmetrical about June 21 (Lechner, 2001). This is because the position of the sun cycles through the sky on a seasonal basis. Thus, the Sun will pass through the same parh twice every year, the first time when going from winter it summer and the second time when traveling back to winter. Thus, any shading device will ahways shade berween two dates. In the northern hemisphere, an oprimized shading device for the 21st of March will actually shade from the 21st of March, right through June until the 21st of September. Thus the whole overheated period (hot-dry and warm-humid) is taken into account for smulation.

## Considerations for Identifying the Time Period for Simulanion

For simulation to investigate the performance of the shading devices, the time period is considered when the space is onfy considered to be used during office hours. In genetal, the office time is from 0900 to 1700 and this time peniod is taken as a critical time periox for shading requirement-

### 5.2.5 Simulation Model

Foilowing models have been developed for simulation that represent the selected shading devices. These models refet to the high-rise buildings selected with identical facades with a similar treated floor area with the shading device with single glazed clear glass. The room size for simulaton model is $6000 \mathrm{~mm} \times 6000 \mathrm{~mm}$ which is considered as beated in an intermediate floor of a high-rise building. The room size is taken from the typical high-rise column grid. A fized window width 5400 mm has been considered with single glazed glass, as the window covers the whole span between two columns. Different shading devices are attached with it for sumulation sudy. For the ease of calculation, a study plane at the level of the exterior surface of the window wall is considered.

In terms of shading analysis and solar heat gain, the simulations are done for the following options of models:

- 'The 'without shading' option - which refer to the high-rise models with idenrical facades with a similar treated floor area without the shading device but with clear glass;
- The 'with shading' option which refer to the hyb-rise models with shading as designed by the architect


Section of typical high rise building


Typical floor plan of high rise building

Figure 5.10: Schematic drawings showing generation of simulation model from rypical high rise building.

The simulations are done for the following models generated by "Ecotect':


Figure 5.11: Simulation model of Shade H01.


Figure 5.12: Simulation model of Shade H 02.


Figure 5.13: Simulation model of Shade H03.


Figure 5.14: Simulation model of Shade V01.


## Parameters:

- Office room dimension:
$6000 \mathrm{~mm} \times 6000 \mathrm{~mm}$
- Floor height 3000 mm
- Window: Sill: 600 mm ,

Width: 5400 mm , Height: 1950 mm

- Vertical Fin: Depth: 300mm, Spacing 600 mm

Figure 5.t5: Simulation model of Shade V02.

## Parameters:

- Office room dimension:

$6000 \mathrm{~mm} \times 6000 \mathrm{~mm}$
- Floor heipht: 3000 mm
- Window: Sill: 600 mm ,

Width: 5400 mm , Height: 1950 mm

- Vertical Fin: Depth: 450 mm , Spacing. 600 mm

Figure 5.16: Simularion model of Shade V03.


Figure 5.17: Simulation model of Shade C01.


## Parameters:

- Office romen dimension:
$6000 \mathrm{mtrm} \times(\mathbf{0} 00 \mathrm{~mm}$
- Floor haght: 3000 mm
- Wrmarar: Sill 750 mm

Writh: 5400 mm , Height 2250 mm

- Vertical fin: Deputh: 450 mm , Spraing 1500mm
* Overbang depth: $\mathbf{2 2 5 m m}$

Figure 5.18: Simulation model of Shade C02

## Parameters:



- Ofice room dimension: $6000 \mathrm{~mm} \times 6000 \mathrm{~mm}$
- Fioor beight 3000 mm
- Windora: Sili 600 mm ,

Wedth: 5400 mm , Height 1800 mm

- Vertical Fin: Depth: 500 mm Spacing 1050mm
- Overhang depth: $\mathbf{3 7 5 m m}$

Fipure 5.19. Simubaion model of Shade C03.

### 5.3 Simulation Study for Performance Evaluation

Two studies about the peffomance of shading devices on solar radiation protection are carricd out as under. The first study investigated the impact of orientation on the performance of shading devices while the second study compared the performance among the selected shading devires in different orientations on the basis of previously set crizeria.

This study will help in idenafying the effect of different parameters and intemelation among parameters in terns of solar shading aspect. This study will also assist to understand the influence of window orientation on the shading petformance of shading devices.

### 5.3.1 Effect of Orientavion on Shading Performance

'The efficiency of the window shading is largely deternined by the oricntation of the window. When shading is not effective, solar radiation enters through the windows and heats up the building incrior directly. Hence the indoor temperature will obviously be influenced by the orientation of the windows.

The quantitative effect of window orientaion has been studied by simulation technique under different shading condition, which also reveal whether shading devices used are effecrive or not, according to orientation in order to cut direct sunlight penetration at critical times of the day. 'The results of the study are summansed in the following secion.

### 53.1.1 Perfomance of Horizontal Shading Devices

The three models with selected horizontal shading devices were oriented in the three cardinal directions (East, West \& South) and two oblique directions south-east and sourh-west. The results are given below with respect to individual cases.

Table 5.2 shows perteinage of shaded area with respect to whole window area of Shade H01 at every 30 -minute interval from sunnise to sunset. In the Feld invescigaion it was found that this shading device was attached mostly with an east-facing window. But through simulacion, it is found that this shading clevice iy not efficient at east orientanon. It is capable to shade below $50 \%$ of the window area at east but $u_{p}$ to $60 \%$ window area
at muth orientation．The performance at south is more consistent than that of other orienations．Figure 5.20 shown the shading performance of Shade H0t in different orianations and it erpressea 2 consistent performance only in south onennation．

Tuble 5．2．Percenuge of shaded are by Shade H01 for $21^{*}$ March．

| Orimitaion | 晨 | $8$ | 影 | 豆 | E | 号 | 耍 | 突 | \％ | 寊 | 奢 | $\pm$ | 戓 | $\stackrel{y}{*}$ | \％ | 3 | 安 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ＊ | 3. | ： | 4 | 4 | $:$ | ： | ＊＊ | $\%$ | 4 | ＊ | $\%$ | \＄ | 4 | $\because$ | 4 | ＊ |
| Hart | 27 | 78 | 3 | 51 | － | － | ＊ | ＊ | － | ＊ | － | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ |
| Southas | 21 | 27 | 31 | 37 | 45 | 9 | ＊ | ＊ | ＊ | ＊ | － | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ |
| South | 51 | 9 | 5 | \％ | 56 | 35 | ${ }^{6}$ | 5 | \％ | 57 | 54 | 55 | 5 | \＄ | 45 | 42 | 38 |
| Souttreest | ＊ | ＊ | ＊ | － | － | ＊ | ＊ | 63 | 5 | 41 | 36 | 28 | 22 | 19 | 15 | 12 | 10 |
| W＇ar： | ＊ | ＊ | ＊ | － | ＊ | － | ＊ | － | － | 4 | 41 | 30 | 3 | 26 | 13 | 11 | 7 |

＊Percentige of ahaded erea is not taken into sctount as ibe sun doan not tee the window．


Figure 5．20：Percentage of shaded aren by Shade HO；fot 21＂March at differcht arientatisna＇

In case of Shade H02，simulation feult athere that the device shades more window area at soruth orientatiom．In the field investigetion it ans found that this shading device was artached with＊routh facing window，As per simulation it is coprable to shade up to $53 \%$ of window area at south orientaion．The perfomance at south is more consiatent than

[^1]that of other orientations．At south－west orientation it shades up to $56 \%$ of window area but the performance is not convintent．Table 5.3 and Figure 5.21 show the performance of Shade H02 at different oriennations and it indicater a consistent perfomance onty in mouch oritentution．

Table 5．3：Peternuge of shaded area by Shade H02 for 21＂March．

| Ofintrinen | \％ | 多 | E | 名 | $\stackrel{\square}{1}$ | 号 | $\underset{4}{¢}$ | 8 | 豆 | 3 | 8 | 9 | 官 | 9 | 㫛 | 2 | E |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | \％ | \％ | $\div$ | $\because$ | $\cdots$ | \％ | $\%$ | 5 | ： | 4 | \％ | \％ | 4 | 3 | \％ | 52 | 46 |
| Fistr | 11 | 20 | 27 | 4 | ＊ | ＊ | ＊ | － | ＊ | － | － | ＊ | － | $\cdot$ | ＊ | ＊ | $\cdots$ |
| Sorrimess | 12 | 15 | 27 | 25 | 37 | 52 | － | － | － | － | ＊ | － | ＊ | － | － | － | ＊ |
| Sout | 43 | 4 | 41 | 51 | S 5 | 50 | 53 | $4)$ | 5 | \％ | 46 | 45 | 42 | 41 | 36 | 27 | 23 |
| Sontherat | － | ＊ | － | － | － | ＊ | ＊ | \＄ | 4 | 31 | 23 | 17 | 2， | F | 1 | 0 | ${ }^{\square}$ |
| W＇ra | ＊ | ＊ | ＊ | － | ＊ | ＊ | $\bullet$ | － | $\bullet$ | 5 | 17 | 21 | 12 | ＊ | 3 | 0 | $\square$ |




Figure 5．21：Percenuge of shaded area by Shade H02 for 21＂Murch at different orientations．${ }^{16}$ 57

Table 5.4 and Figure 5.32 sbow the performance of Shade H 03 at different orientationa and it expresses i comparativels better performenex at south orientation then thet for other orientations．It shade marimum $46 \%$ window erea at tocuth and more or less consistent for the whole day．

Table 5．4：Percentage of shaded area bry Shade H03 for $21^{*}$ March．

| Orimation | 8 | 最 | ？ | 을 | E | 熏 | 8 | 思 | 官 | 3 | $\underline{\square}$ | $\stackrel{9}{2}$ | 空 | 28 | $\stackrel{9}{9}$ | 3 | 宝 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 46 | ＊ | \％ | $\square$ | $\%$ | 4 | ＊＊ | \％ | \％ | \＄ | \％ | $\cdots$ | si | 9 | \％ | ： | 4： |
| Enst | 11 | 3 | 31 | 38 | ＊ | － | ＊ | $\bullet$ | － | － | $\bullet$ | ＊ | ＊ | － | － | $\bullet$ | － |
| Soothest | 13 | 7 | 21 | 3 | 34 | 4 | $\bullet$ | ＊ | ＊ | － | － | 4 | ＊ | ＊ | － | － | ＊ |
| South | \％ | 41 | 45 | 42 | 41 | 4 | 46 | 4 | 4 | 39 | 6 | 43 | 59 | 35 | 38 | 5 | 23 |
| Southerer | ＊ | ＊ | ＊ | ＊ | ＊ | － | ＊ | 45 | 35 | 31 | 27 | 21 | 17 | 13 | 12 | 7 | － |
| Hict | ＊ | － | ＊ | ＊ | ＊ | ＊ | ＊ | － | 4 | 47 | 31 | 23 | 17 | 17 | 4 | 7 | $\stackrel{\square}{ }$ |




Figute 5．22：Percentage of shaded ater by Shade H03 for $21^{*}$ March at different orientations．${ }^{(6)} 5$

## Finding

It has been observed from the resuls of the simubtions that the performance of horizoncal shading devicen remuins quite consistent at south orientation only．It works berer when the nun is opposite to che window pane at a high altitude．This pefformance drops when the run is in a lerrer alitude and oblique to the window pane．The horizoncal overiang is nor capable to prorect the window when the sun azimuth and aldiuade are low．So from these manhers，need for modificaion is evident when the sun is at low eximuth and eloitude．

## 53．12 Performance of Verical Shading Devices

The thrte selected vertial shading deriee were oriented in the three cardinal directions （East，West and South）and rwo obligur direcrions south－east and south－west to erahulte their performance at differant orientations．The result are given below with respect to individual cases．

Table 5．5：Percenrage of shaded area by Shade VOt for $21^{\prime \prime}$ March．

| Orichtarime | $\underline{8}$ | 官 | 空 | ¢ | 晨 | $\stackrel{9}{2}$ | $\underline{8}$ | 曷 | $\stackrel{E}{5}$ | 5 | 怱 | $\stackrel{9}{\square}$ | 5 | \％ | E | － | E |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ＊$\%$ | $\cdots$ | $\because$ | $\because$ | $\because$ | ＊ | ＊ | $\%$ | $\%$ | $\%$ | \％ | $\%$ | \％ | 4 | 4 | 4 | 46 |
| Fa＊： | 47 | 53 | 7 | 7 | $\bullet$ | ＊ | － | － | － | ＊ | － | － | － | ${ }^{+}$ | ＊ | － | ＊ |
| Shuthest1 | 46 | 5 | 50 | 51 | 7 | 91 | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | － |
| South | W1 | ¢ 7 | 67 | 94 | 91 | ［ ${ }^{4}$ | （\％） | 8 | E | F7 | 㿽 | 55 | \＄ | 7 | 69 | 57 | 36 |
| Snutheret | ＊ | $\pm$ | ＊ | ＊ | － | ＊ | ＊ | 54 | 7 | \＄ | 5 | ＊ | 4 | 45 | 45 | 44 | 53 |
| Wras | ＊ | ＊ | ＊ | ＊ | ＊ | $\bullet$ | ＊ | $\bullet$ | ＊ | 57 | 由） | 4 | 42 | 6） | 37 | 4 | 3 |

－Percentage of waded ater is not raten into account as the win does not aee the sindow．


Figure 5．23：Pereentage of ahaded area by Shade VO1 for 21＂March at different orientations．${ }^{36} 57$

Tible 5.5 shows percenage of shaded area with respect to whole aindory are of Shade V01 at erery 30 minute interal from suncise to sunset．In the field investigaion it was found that this sheding device ows attached with a south facing windov．But through simubtion，it is found that this shading device is not onfy efficient at south orienation，it
also wotk well at eart and west＇This shading，device is caprble to shade $60 \%$ of the windory area on an avenge at east nend uest and up to $94 \%$ pindown heter at mouth orientation．But one thing is ckeat that the large overhang that holds the vertical fing makes the whole shading device effective at south．Actually vertical fins do not have signifiant rote in protection of window at souch．

Table 5．6：Pereentage of shaded wea by Shade V02 for 21＂March．

| Qrimation | 害 | 矣 | E | 9 | E | $\stackrel{\text { 厚 }}{ }$ | 突 | 易 | 空 | 3 | E | 昜 | E | 㤩 | E | 2 | E |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\because$ | \％ | $\%$ | \％ | 4.4 | \％ 7 | ＊ | 4 | 46 | 7 | $\cdots$ | ＊ | \％ | 46 | 4 | \＄＊ | ＊ |
| L35t | ¢） | 4 | 4 | 社 | ＊ | ＊ | $\pm$ | ＊ | ＊ | ＊ | － | 4 | － | － | － | ＊ | ＊ |
| Southerst | 44 | 36 | 43 | 46 | 4 | 40 | ＊ | ${ }^{\circ}$ | － | － | ＊ | － | ＊ | ＊ | ＊ | ＊ | ＊ |
| South | 78 | F3 | H | H3 | 71 | 75 | $\boldsymbol{*}$ | 45 | 72 | 71 | 76 | $8 \%$ | ${ }^{6}$ | 73 | 6 | 53 | 21 |
| Snurtrictit | ＊ | ${ }^{*}$ | ＊ | ＊ | ＊ | ＊ | ＊ | m | 57 | 42 | 3 | 3 | 35 | $\cdots$ | 3 | 4 | 5 |
| Weal | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | － | ＊ | \％ | 64 | 5 | 45 | 46 | 41 | 94 | 28 |

－Percentrge of ahaded are is not biter into exconnt as the sum docs not ser the window


Figure 5．24：Percenage of shaded aren bry Shade V02 for 21＂Manch at different orientabions．${ }^{1657}$

Io case of Shade VOZ simulation results ahow that the deviec shades more window area at zouth orientation onty when the sum is at an angle with the windowpene．That is when the sun is in southuest and mouthessh this shading device is effective and capable to shade up to 87\％of window trea．In the fiek investigation it wets found that this shading
device was atriched with wers－facing window．Through simulation it is found that this shading devige is effective at pest orienation and it abo shades well at east and wert． This shading device is ceppable to shade $52 \%$ of the windory ures on an werage at east and west．

Table 5.7 shows percentige of shaded niex with mapect to whole window area of Shade VO3．In the fick invesagation it was found that this shading device was aturhed with an east facing windors．Through simulation，it is found that this shading device is efficient at south orientation；it also works well at south－ast and south－went．Ihis shading device is caprable to shade $50 \%$ of the window area on an werrige at east and west．This shading deriec iveffective in south fapade only when the sum in at an angle with the windory．

Table 5．7：Percentage of shaded ater by Shade V03 for $21^{\prime \prime}$ Mirch．

| Orinntion | $\frac{\mathrm{e}}{\mathrm{E}}$ | $9$ | 를 | 苞 | $\underline{E}$ | 星 | $\underset{\underline{y}}{\underline{g}}$ | $\underline{2}$ | ¢ | $\stackrel{2}{2}$ | 8 | $\underset{\sim}{\boldsymbol{\theta}}$ | E | 突 | \％ | 空 | 总 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ${ }^{6}$ | $\because$ | \％ | $\sim$ | \％： | 4 | 4 \％ | 4 | $\%$ | 5 | $\%$ | \％ | $\%$ | ＊ | $\%$ | $\cdots$ | $\%$ |
| Eas | 30 | 42 | 33 | 53 | － | ＋ | ＊ | ＊ | － | ＊ | ＊ | ＊ | ＊ | － | － | ＊ | － |
| Souihenst | 43 | 5 | \％ | 3 | 47 | 61 | － | － | － | $\bullet$ | － | － | ＊ | － | － | ＊ | － |
| South | （10） | \％ | － | \％ | 75 | \＄ | 31 | 63 | 6 | 73 | 72 | 92 | 10n | （ta） | （t） | （II） | （1a） |
| Southees | \％ | ＋ | $\cdots$ | － | ＊ | － | ＊ | 5 | \＄1 | 5 | 45 | 35 | 34 | 9 | $\cdots$ | 2 | 41 |
| West | ＊ | ＊ | $\bullet$ | － | － | － | － | － | － | 74 | 44 | 45 | 35 | 36 | 12 | 27 | 34 |

＊Pexcentyge of ahaded ater is ont tiken into tacount at the an does oot wee the windor．


Figure 525：Percentage of shaded area by Shade V03 for 21＂March at different orientations． 16 解

## Findings

The inverbigaion ahoras that vertial shading deriect tee efferive on west and cast facade．The simulation results shory that all thee three verical shading devices are eapable to shade above $50 \%$ of the windor area on an evergge at east and pest．Verical shading devices are atso coprble to shade up to $94 \%$ window area at south orientacion． But one thing has to be noriced that the lage overhangs that holds the vertical fins makes the whole shading device effective at south．Actually verical fins do nor have cigrifitant role in ahting of vindow at south．＇Ihey wort efficienty when the sun is at an angular position with the window．They are not effective when the sun＇s altitude is low and perpendiruthr with the frade．It has dso to be norieed that vertical fins tre not efficient at east and west onenavion when the sun is just in front of the window．Thit phenomenon needs further inverigation．

## 53．1．3 Performance of Composite Shading Devices

The three selected comprsite shading devicess（combination of vertical fin and horizontal overhang were oviented in the five directions－Best，Wesh，South，South－cast and Sourh－ west and then simubred to inverigate the influence of orientation on their shading perfommace．The tesules ate given betow with reapecr to individual cases．

Table 5．8：Peremape of shaded area by Shade C01 for 21＂March．

| Otikntaion | $\underset{S}{f}$ | $\begin{aligned} & 8 \\ & 88 \end{aligned}$ | 药 | $\begin{aligned} & 8 \\ & \text { e } \end{aligned}$ | $\underset{-}{8}$ | $\stackrel{8}{2}$ | 高 | $\frac{9}{4}$ | $\underset{\sim}{e}$ | $\underset{\sim}{2}$ | $\varepsilon$ | ¢ | $\varepsilon$ | $\underline{2}$ | E | 易 | 8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\because$ | 4 | $\because$ | \％ | $\%$ | \％ | $\%$ | $\because$ | 4 | 41 | $\stackrel{ }{4}$ | $\because$ | $\%$ | \％ | $\therefore$ | $9+$ | $\%$ |
| Fast | \％ | ＊ | 7 | ＊7 | ＊ | ＊ | － | ＊ | － | ＊ | － | － | ＊ | － | － | － | ＊ |
| Southerit | 58 | 5 | 56 | 4 | 75 | 5 | － | ＊ | － | － | ＊ | ＊ | ＊ | － | ＊ | － | － |
| South | $\overline{1(1)}$ | $\square$ | 93 | 71 | D1 | 5 | Es | 5 | ${ }^{10)}$ | 7 | ＊ | 58 | 10） | 101 | 103 | 171 | 10） |
| Southwes： | － | － | － | ＊ | － | ＂ | － | 9 | 34 | \％ | 5 | 5 | 5 | 35 | 57 | \＄3 | 37 |
| Weat | － | － | － | ＊ | － | － | － | － | － | 9 | 0 | $\pi$ | $\omega^{\omega 1}$ | 59 | 4， | 49 | 2 |



Table 5.8 shovs percenage of shaded area with reapea to whole windore area of Shade Cal at every 30 minute interval from sunnise to sunset．In the field suncer it was found that this shading device wis attheded with a south facing window．＇Ihrough simulation，it is found that this shading decice is not only effepient at south orientaion；it anso works
well at souch－east and south－west．This shading is capable to shade $60 \%$ of the aindow arez on an average at south－east and sourth－west and up to $100 \%$ window are at south orientation．


Figure 5．26：Percenuge of shaded are by Shade C0t for $21^{*}$ March at different －orientations ${ }^{1059}$

In ease of Shade CO ，simulation resuls show that the derice works berner at south orientaion specially when the sun is in an angle with the aindow pare．Thit is when the nun is in south－west and south－east，this shading derice is effective and epable to thade up to $100 \%$ windowe aren．In the freld usvey it was found that this shading device was atmehed with a south facing window．But through sitmulation it is found that thie shading derice is abo effective in enst，southenst and south－west orientation．

Table 5．9：Percentage of shaded area by Shade C02 for $21^{*}$ Mareh．

| Ofientatims | \％ | $\begin{aligned} & \mathbf{g} \\ & \dot{B} \end{aligned}$ | 品 | $\begin{aligned} & 9 \\ & 0 \end{aligned}$ | 8 | $\stackrel{9}{\square}$ | 曷 | 3 | 2 | 2 | 帝 | \％ | 告 | 晶 | E | E | $\underset{\sim}{5}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | 4 | \％i | $\because$ | $\bigcirc$ | 9 | \％ | $\%$ | 4 | $\pm$ | 4 | si | $\stackrel{*}{*}$ | ＊ | 4 | $\pm$ | $\%$ |
| Lant | 50 | 5 | 56 | 74 | － | － | － | $\stackrel{\rightharpoonup}{ }$ | ＊ | － | － | － | － | ＊ | ＊ | － | － |
| Southens | 4 | 4 | 4 | 52 | 58 | 73 | － | － | － | ＊ | － | ＊ | ＊ | ＊ | － | － | － |
| South | ＊${ }^{1}$ | 04 | 12 | 74 | 74 | 71 | 0 | 6 | $\cdots$ | 73 | ＊） | 15 | K | 5 | 10 | 30 | 101 |
| Southarat | － | － | － | ， | － | － | － | 83 | 43 | 56 | 4） | 46 | 43 | 48 | 41 | 41 | क7 |
| （10s： | － | ＊ | － | － | － | － | ＊ | － | ＊ | 0 | 62 | 50 | 4 | 43 | 99 | 31 | 21 |

[^2]

Figure 5.27: Percentage of shaded ares by Shade C02 for 21" March at different orientations. ${ }^{1635}$

Table 5.10 shows percentage of shaded area with respect to whole window aten by Shade C03. In the field surer it was found that this shading device wis arched with an east facing window. Through simulation, it is found that this shading device is effective at east and west orientation, but not consistent. The shading performance at southeast and south-west is more consistent than other orientations.

Table 5.10: Percentage of shaded area by Shade C03 for $21^{*}$ March.


[^3]

Figure 5.28: Percentage of shaded urea by Shade C03 for 21* March as different oriencabiona ${ }^{1525}$

## Finding

The asalfais shows that composite shading devicen are effective in south southeenst and south-west orientation They are effective both when sun is in perpendizular and angular position with the windor pane. Horizontal overhangs of the composite shading art effective to protect the sur when it is at perpendicular porizion to the orindort. And vertical fins of the componite shading are effective to protect the sun when it is at an naguat posision to the window. Hut their performance in east and weat orientation is not consistent.

### 5.3.2 Comparative Annlyzis of Shading Performance

To tratuate the shading perfortance on the basis of set critetin diseussed andier a compantive antyia among the selected shading derices has been summarised in the folboring section. This study will help in ikentifying the effect of differant parimetets and corrchaion among parimeters.

## 5．3．2．1 Comparison among Horizonul Shading Devices

From sbove invertigation on influence of orientation，it was observed that horizontal shading devices were effective on windows at south orienntion than other orientations． At south otienarion，all three shading dericea were caprble to ahade maximum ere of window pane at mid day．Simubtion rexulta show that among the three horizontal shading devices，Shade H01 can ahade marimum $60 \%$ of the whole windoupane，Shade H02 an shade maximurn $53 \%$ and Shade H 03 an shade maximum $\mathbf{6} \%$ of the whole windowpine．

Table 5．11：Percentage of shaded area at different orientations by hotizontal ahading devices for $21^{\prime \prime}$ Murch．

| $\begin{aligned} & \text { 膏 } \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { 知 } \\ & \text { 年 } \end{aligned}$ | 客 | $8$ | e | 㫛 | $\underset{\sim}{E}$ | 易 | 含 | N | 鲴 | \＄ | $\underline{\underline{E}}$ | 5 | 镸 | \＄ | ES | 9 | $\underset{\sim}{E}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | \％ | \％ | ＊ | $\because$ | \％ | $\div$ | 9 | \％ | 96 | 4 | $\%$ | 4 | 4 | $\%$ | $\because$ | ＊＊ | \％ |
| Fast | H01 | 2 | 2 | 35 | \＄7 | － | ＊ | － | ＊ | － | ＊ | ， | ＊ | － | ＊ | ＊ | ＊ | － |
|  | H62 | 11 | 30 | 77 | 4 | － | $\pm$ | ＊ | ＊ | － | － | ＇ | ＊ | ＇ | ＊ | － | － | ${ }^{*}$ |
|  | 1103 | 11 | D） | 31 | 51 | ＊ | ＊ | － | ＊ | ＊ | ＊ | － | ＊ | ＊ | ＊ | ＊ | － | － |
| Sounh <br>  | 1001 | 7 | 7 | 31 | 5 | 45 | 5 | ＊ | － | ＊ | ＊ | ＇ | ＊ | ＇ | － | － | ＊ | ＊ |
|  | 1105 | 12 | 13 | 3 | 28 | 17 | 52 | － | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | － | ＊ | － |
|  | 1F03 | 17 | 22 | 21 | 33 | ， 4 | 4 | － | ＇ | － | － | ＇ | － | ＇ | － | ＇ | ＊ | － |
| Sourt | J101 | 57 | 54 | 53 | 56 | 56 | 55 | $6)$ | 53 | 5 | 57 | 54 | 55 | 52 | 50 | 48 | 42 | 38 |
|  | H20 | 45 | 4 | 47 | 51 | 5 | 5 | 5 | \％ | 5 | $\cdots$ | 4 | 45 | 12 | 4 | $\cdots$ | 37 | 23 |
|  | H03 | W | 41 | 4 | 42 | 41 | 4 | ＊ | 4 | 4 | $\cdots$ | $\times$ | 43 | 5 | 31 | 38 | 3 | 28 |
| South wes： | H01 | ＊ | － | － | － | ＊ | ＊ | ${ }^{+}$ | 5 | $3 n$ | 41 | M | 73 | 2 | 17 | 15 | 12 | 40 |
|  | H02 | ＊ | － | ＊ | ＊ | ＊ | ＊ | － | $\underline{M}$ | 4 | 33 | 23 | 17 | 13 | ${ }^{8}$ | 4 | 0 | 0 |
|  | 7103 | ＋ | ＊ | ＊ | ＊ | － | ＊ | ＊ | 4s | 85 | 30 | 2 A | 21 | 17 | 13 | 12 | 7 | ＂ |
| Weat | 101 | － | ＇ | － | － | ＊ | － | ＇ | － | － | 82 | 41 | $\cdots$ | 24 | 15 | 13 | 11 | 7 |
|  | ＋109 | － | － | ＊ | ＊ | － | 4 | － | ＊ | － | 5 | 3 | 21 | 12 | 4 | 3 | 0 | 0 |
|  | F103 | ＇ | ＇ | － | ＊ | ＇ | － | ＇ | － | － | 4） | 31 | 23 | 19 | 19 | ＊ | 7 | ＊ |

－Percentafe of thaded mea in mot taken into account mat the run doca not see the window．
From uble 5.11 it is observed that it enst，southenst，west and south－west orientations ill three shading daricea are oor effectize．Sometimes these three shading derices an shade up to $63 \%$ of the windor we but the efficiency drops frequentry．Considering all these limitations，in comparison amomp these three thorizontal shading deviocs，Shade

H01 is capable to ahade better than other tro shading devices at all frie orientations. Shade H01 performs better in protecting sobar ndiztion in comparison to other two shading deviecs.

Table 5.12 shows that at south osientation, Shade H01 an block 3411 watt soler madiation which is $54 \%$ of the total incident radiacion ( $6,314 \mathrm{wsit}$ ). If it is compered with other two horizontal ahading deriess, it is found that Shade H02 can block $46 \%$ of the incident radiacion and Shade H03 can bloct $\mathbf{4 1 \%}$ of the incident madiation.

Table 5.12: Ammont of direct solar nadintion indident on windowpane at different orienations.

| Oricntation | Shade 1301 |  | Shade 1102 |  | Shate H03 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Shaud | Unshaded | Shaded | Unchaded | Shaded | Unthaded |
|  | in Went | in Wrat | 加Watt | in Whatt | in Wett | in Watt |
| Fest | 1885 | 3761 | 2153 | 3764 | 2126 | 3761 |
| South | 2903 | 6114 | 34.39 | 6319 | 376 | 6325 |
| Southeers | 2420 | 5020 | 2759 | 5005 | 2856 | 5013 |
| Sonth-mert | 1693 | 3983 | 1960 | 3981 | 20185 | 3980 |
| Wrat | 1138 | 2553 | 1318 | 2554 | 1421 | 2558 |



Figure 5.29, Comprason of percentage of shaded area at south orientation by horizontal shading device for $21^{*}$ Murch.


Firgure 5.30: Comparison of percentage of shaded area at east orientation by horizontal shading deviect for $21^{*}$ March. ${ }^{15}$ (5)


Figure 5.31: Comparion of percentage of shaded area at south-east orientaion by borizonal shading devices for $21^{*}$ March. ${ }^{\text {it }}$ ")


Figure 5-32. Comparison of perentage of ahaded are at south-wet ofientaion by horizontal shading devices for 21"Mareh. ${ }^{16}$ is


Figure 533: Comparison of percentage of shaded area at west orientation by horizontal shading devices for $21^{4}$ March. ${ }^{165} 59$


Figure 5.34: Comparion of shading coelfrient of three horizontal ahading devices at diffetent orientariona

Although Shade H01 is more effective in compation to Shade H02 and H03, the shading performance of Shade f101 is not up to the mast It an not block atmost $50 \%$ of the tosal incident radiation. This huge rediation enters through the unshaded part of the window pane into the spice. So, horizontal projection of this Shade H01 is not enough to protee the window from the molar radiation propenty.

## Findings

The invearigation shows that the horizontal shading device with leger ovetheng with respect to window height, shades more window wer and reduces heat gain than ather tgpe It indientes that projection depth of horizontal thading devices is the min detemining fector for shading the windon from direct solar radiation.

### 53.22 Compation among Vertical Shading Devices

From aforessid invescigation on influence of orientation, it was also obsenced that Vertical shating devices wete effecive on windows at souch-ast and anuth-west orimation. So firsity, the perfornances of the vertical shading derices tre cratured with seference to their performance at these two orientations

At south－east ind south－weat orientation，innost same chancter of performance of these verical shading devices has been observed．All three shading devices are capable to shade maximum arta of window pane at the time when the sun is just inted to cast or wert from sonth．Simulation resuls show that among the three vertial shading devices， Shade H0t can shade $53 \%$ of the whole windoupane，Shade H02 an shade $45 \%$ and Shade H03 an shadt $42 \%$ of the whole windowpine on in averige．

From table 5.13 it is observed that at east，south，west orientations all three shading derices ate not consistent in their performance．Sotmetimes these threx shading devices an protect almost $90 \%$ of the window are but the efficiency drops frequenthy to $15 \%$ ． Considering all these limitationa in comparison with theare three vertial shading devices， Shade V0t is eapable to shade better than ocher two shading derices at all five orientations．So Shade V01 gives better protection from sober ndintion in comparison to other two shading devices．

Table 5．13：Percenlage of shaded atez at difterent orientations by vertical shading derices fo： $21^{*}$ March．

|  | $\begin{aligned} & \text { 皆 } \\ & \text { 真 } \end{aligned}$ | \％ | $\stackrel{9}{8}$ | $\underset{\underline{E}}{\underline{E}}$ | 是 | $\underset{\sharp}{E}$ | $\stackrel{9}{3}$ | E | 2 | \％ | $\underset{\sim}{\mathrm{S}}$ | 8 | $\stackrel{9}{ \pm}$ | 罣 | $\begin{aligned} & \underset{\sim}{2} \end{aligned}$ | E | $\underline{8}$ | $\underset{\sim}{8}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 4 | 4 | $\because$ | 7 | $\%$ | $\%$ | 9 | $\stackrel{1}{6}$ | 9 | 5 | $\%$ | 46 | \％ | $\%$ | \％ | ＊ | 4 |
| Eas： | vir | 4） | \＄1 | T | $\pm$ | 5 | ＊ | ＊ | ＊ | ＊ | 4 | ＊ | 4 | － | 4 | － | ＊ | － |
|  | va | ＊ | 緼 | 4 | $\square$ | 4 | － | － | － | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ |
|  | V03 | 5 | 42 | 9 | 5 | ¢ | － | － | ＊ | － | 4 | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ |
| South <br> ［ax | FOL | 46 | 5） | 50 | 3 | 73 | 11 | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | － | － |
|  | V02 | 41 | $\cdots$ | 4） | 4 | ＊ | 01 | ＊ | ＊ | － | － | ＇ | － | － | － | ＊ | $\cdot$ | － |
|  | FBS | 43 | 32 | 30 | 4 | ＊ | 41 | ＊ | ＊ | － | 4 | ＇ | － | － | ＊ | ＇ | ＊ | － |
| South | Yal | 81 | 87 | 6 | $\cdots$ | \＄1 | B3 | ${ }^{1}$ | ＊ | \％ | 57 | 19 | \＄5 | E5 | T1 | 0 | 37 | $\cdots$ |
|  | V¢0 | \％ | a） | $\pm$ | 83 | 71 | 3 | 0 | 65 | $\overline{7}$ | 11 | 7 | 0 | 83 | 3 | 6 | 53 | 21 |
|  | vos | 151） | \％ | c | 6 | 73 | 5 | 51 | 4 | 65 | 73 | 72 | 5 | （0） | t0） | 100 | 100 | 101 |
| South ＝ | V0i | － | － | ＊ | ＇ | － | － | － | 9 | $\pi$ | 58 | 55 | 4 | 4 | 45 | 4 | 4 | 53 |
|  | V02 | － | － | ＊ | ＊ | ＊ | ＊ | ＊ | M | \＄ | 42 | 4 | 3 | 35 | $\cdots$ | $\cdots$ | ＊ | \＄1 |
|  | 503 | － | ＊ | － | ＇ | － | － | － | 50 | 51 | 5 | 45 | 35 | 4 | 3 | 9 | 32 | 41 |
| Wert | 701 | ＊ | ＊ | － | － | － | － | － | ＊ | － | $\cdots$ | H | 4 | 42 | 40 | 27 | 46 | 13 |
|  | Vm | ， | － | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | － | © | 4 | 50 | 40 | K | 31 | 3 | 36 |
|  | v03 | － | － | ＊ | ＇ | － | ＊ | ＊ | ＊ | ＊ | 76 | 4 | ＊＊ | 3 | m | 72 | t． | 14 |

[^4]Table 5.14: Amount of direct acolar radiation incident on window pane at different oritnacions.

| Orientation | Stade ${ }^{\text {rob }}$ |  | Sharle V08 |  | Shade V 03 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Shaded | Unthaded | Shaded | Unthoded | Shaded | Unshaded |
|  | in Wert | mu'ztt | $m$ Wett | in Wati | in Whtt | in What |
| Ein | 1248 | 3760 | 1461 | 3766 | 1443 | 3763 |
| Wouth | 1102 | 6319 | 1783 | 6326 | 1336 | 6318 |
| South-rat | 1493 | 5015 | 1962 | 5010 | 1998 | 5013 |
| South-mbit | 1022 | 3984 | 1465 | 4364 | 1492 | 4364 |
| West | 701 | 2556 | 906 | 2556 | 848 | 2556 |

Trable 5.14 shows that at south-cest and wouth-west orientition, Shade V01 an pretent abmost $70 \%$ of the tota! incident matiation. If it is compared with the other tro vertical shading derikea, it is found that Shade V02 can resist $\mathbf{6}-65 \%$ of the incident ndiation and Shade V03 an pritent $60-65 \%$ of the incident mdiation.


Figure 5-35: Comparison of perenage of shaded ates at elst oriencation by vertical shading devicen for $21^{*}$ March. ${ }^{14 \%}$ (])


Figure 536: Comparison of percentage of ahaded area at sowtheast oientation by vertical ahading devires for $21^{\text {K }}$ March. ${ }^{1659}$


Fipure 5.37: Comprison of percentage of shaded area at south orientation by verical shading device for $21^{\prime \prime}$ March.


Figure 5.3.: Compnision of percenrage of shaded aren at sounh-west orientation by verical shading deticen for $21^{\prime \prime}$ March. ${ }^{165)}$


Figure 539: Comparison of percentage of shaded tren at west orientation by vertied shading deriocs for $21^{\circ}$ Murch. ${ }^{143 s)}$


Fipure 5.40: Compurizon of shading eneficient of three vertiol shading devices at different orientations.

Although Shade V01 is more effective in comparion to Shade V02 and V03, the performance of Shade V01 is nor up to the mart Actualty it can not block $\mathbf{3 0 \%}$ of the tool incident radiation. This mediation enters through the unshaded par of the window pence into the rpace. So the depth, spring and angle of the vertieal fins of this Shade VO1 are not enough to protect the window from the moler radiation propert.

## Findings

The invesigation shows that the vertial shading device with luger fin depth ahades mote than other selected vertial darices. It indiates the role of effective depth of shading devices (disunce from windore face to outer face of fins) inchuding the $g^{2} \mathbf{p}$ berween them on shading performance.

### 5.3.23 Comparison among Composite Shading Devices

Firom ertier invercigaion on intluence of ocientation, it was observed that composite thading devices were effecive on windorer at south, southerest and south-wear orientation. So the performance of the comporite shading devices is evatuated aith refierence to their perfornance at these thrit oriennations.

At woutheast and south－west orientation，the anme chancter of performance of these composite shading devices has been observed Simubaion resulrs show that among the three composite shading devices，Shade C01 can shade maximum $96 \%$ of the whole aindoxpane Shade CO2 an shade maximum $83 \%$ and Shade C03 can shade maximum $67 \%$ of the whole aindoxpane．The percentage of shaded window erea decreases when sun moves to cast or wet from south．Table 5.16 dhows that at south－zest and south－ west orientation，Shade C01 an block almost $80 \%$ of the total incident tadiation．If it is compared with the other roo comporite shading devices，it is found that Shade C02 an block 65－70\％of the ineident madiation and Shade C 03 an also block $60-65 \%$ of the incident radiation．

Table 5．15：Percentage of shaded area at difterent orientations by composite shading devives for $21^{\prime \prime}$ March．

| $\begin{aligned} & \text { 冕 } \\ & \text { E } \\ & \text { 菅 } \end{aligned}$ | $\begin{aligned} & \text { ? } \\ & \frac{1}{4} \end{aligned}$ | § | 曻 | 宾 | $8$ | $\stackrel{B}{E}$ | $\stackrel{5}{i}$ | 8 | 20 | $\underset{\sim}{9}$ | $3$ | 雨 | $\frac{8}{7}$ | 缶 | \％ | 总 | 3 | 長 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | \％ | 41 | 4 | \％ | $\stackrel{1}{7}$ | ＊ | $\%$ | 9 | $\%$ | \％ | \％ | $\cdots$ | 7 | $\%$ | 9 | 4 | 4 |
| Fent | $\mathrm{CO1}$ | c | 4 | 7 | 07 | － | ＇ | ， | － | － | ＇ | － | － | － | － | － | － | ＊ |
|  | C02 | 51 | 52 | 5 | 7 | － | － | － | － | F | ， | － | － | － | － | － | － | － |
|  | CO3 | 35 | 4 | 54 | 7 | － | － | ， | － | ＇ | $\cdot$ | － | － | － | － | － | － | － |
| Sounth ex4 | CO 1 | 5 m | 51 | \＄ | 4 | 35 | 5 | ＊ | ＊ | 4 | ＇ | － | ＊ | ＊ | － | － | － | － |
|  | CO2 | 46 | 48 | 4 | 52 | 51 | 3 | ＊ | ＊ | 4 | ＊ | ＊ | ＊ | － | ＊ | ＊ | ＊ | ＊ |
|  | COS | 53 | 37 | 37 | 38 | 4 4 | 6 | ＊ | － | 4 | ＊ | ＊ | ＊ | － | ＊ | － | － | ＊ |
| Sonuth | C 01 | 1（1） | 9 | ＊ | 11 | 91 | \％ | m | m | ［15 | －7 | ¢） | 9 | In | 101 | 101 | 107 | 171 |
|  | CO 2 | 80 | \＄ | 12 | ＋ | 74 | 7 | 0 | $\omega$ | 5 | 73 | m | ＊ 5 | 11 | \％ 5 | 10 | 100 | 1 m |
|  | cos | 109 | 30 | 9 | 11 | 69 | 57 | 51 | 5 | 67 | 6 | 9n | 4 | 3 | 10） | 101 | 107 | 10 |
| South neat | 001 | ＊ | ＊ | ＊ | － | ， | ＊ | － | ＊ | $\cdots$ | 6 | 54 | 57 | 5 | 53 | 57 | 65 | 57 |
|  | 002 | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | 63 | 6 | 5 | 48 | 4 | 46 | 40 | 41 | 31 | 43 |
|  | 06 | ＊ | － | － | ＊ | ＊ | ＊ | ＊ | 67 | 51 | 43 | 35 | 35 | 39 | 4 | 31 | 41 | 50 |
| $\mathbf{W}^{\prime} \mathbf{c s +}$ | 001 | ＊ | ＊ | ＊ | 4 | ＊ | ＊ | ＊ | － | ＊ | ＊ | 0 | 76 | ${ }^{(1)}$ | 55 | ＊${ }^{1}$ | ＊ | $\mathbf{5}$ |
|  | 002 | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | 0 | 4 | 53 | 4 | 43 | 97 | 31 | 21 |
|  | （0）3 | － | － | － | ＊ | ＊ | ＊ | ＊ | ＊ | － | $x$ | 51 | \％ | \＄2 | 37 | 3 | 31 | 21 |

－Percentage of shaded area in not biten into mccount as the aun thocs oot nec the mindow．

Table 5.16: Amment of direct molar radiation incident on windory pane at diftetent orientations.

| Orichtatiom | Shade C01 |  | Shade CO2 |  | Shade CO |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Shader | Unatraded | Shaded | Unshamed | Shaded | Unakaded |
|  |  | m What | in What | in Wert | in Whast | in Wett |
| Heat | 900 | 3764 | 1255 | 3762 | 1342 | 3767 |
| Soruth | 364 | 6324 | 1211 | 5843 | 1180 | 6.319 |
| South-ert | 1461 | 5015 | 1697 | 5000 | 1869 | 5025 |
| South west | 788 | 3986 | 1159 | 3985 | 1388 | 4189 |
| WFen | \$31 | 2556 | 780 | 2558 | 501 | 255\% |



Figure 5.41: Comparison of pereentage of shaded ares at cast orientation by composite shading derices for $21^{*}$ March. ${ }^{1 \% 3)}$

The perfomence of comprosite shading devices is quite satisfatery at routh orientation They on thade up to $100 \%$ of window area. Although all three shading devicen en shade up to $100 \%$ of windory mees, only Shade C01 is consistent in its perfomence througtrout the day. It is deaty evident from figure 5.43. At south orientaion, Shade C01 an block 5960 Wan, which is etmost $95 \%$ of the incident radiation ( 6324 W/an).


Figure 5.42: Comparison of percenuge of shaded area at south-enst orienacion by composite shading devices for $21^{*}$ March. ${ }^{16}$ in


Figure 5.43: Compatison of percenuge of shaded aten at south oniencaion by composite shading derics for $21^{\text {T }}$ March.


Figure 5.44: Comparison of percentage of shaded area at south-west orientation by composite shading derices for $21^{*}$ March. ${ }^{\text {(6) }}$ (1)


Figure 5.45: Comprison of percentage of shaded area at west orientation by composite thading devices for 21" March. ${ }^{1 / 4} 19$

From able 5.15 it is observed that at east and wess orientations all three shading deriecs are not consiatent in their performanec. Sometincs these thrte shading devises an protect almost $90 \%$ of the mindow urea but the effiriency drops frequently to $15 \%$. Considering all these limitations, in compariton atrong these three composite ahading
devices Shade CO1 in able to shade betret than other mo shading derices at all fre orizntations. So Shade CO performs better in protecting molar medintion with compared to other two shading derices.


Fipure 5.46: Comparison of shading coeffieient of three composite shading devioes at different orienations.

Athough Shade C01 iv more effecive in comparion to shade C02 and C03, the performance of COl is not upto the mark at southeast and south-west. It an not block utnost $20 \%-30 \%$ of the total incident madiation This nadiation enter through the unshaded part of the window pane into the space. So the depth, npacing or angle of the vertical fins and horirontal overhang of this shade C01 can be modified to protect the window from the solar madiaion propenty.

## Findings

The investigation thows that the composite thading devices are signifienth efficient at south oriennatioas. The shading device with larger overhang and fin-depth and smalker spacing beracen fins performs berter than the others. It indiceres the role of depth and spacing of fins and overhang on shading performance. With same deph and apacing of fins and overhang, shading devices are not as effecrise at south-east and south-west lize sowth orientation. Here angle of fins may help to cut off the direct radiation at south-elst and south-wrest.

### 5.4 Conclusion

The influences of orientations on performance of vanous shading devices are now clearly evident. It is also evident that horizontal overhangs are effecrive on facades facing south, verrical fins on windows at cast and west onientation and composite shading devices are effecrive on whodows at south-cast and sourh-west. It has been also observed that vertical fins are not effecrive at east and west orientation when the sun is in east or west side.

After invesigaring the perfornance of commonly used shading devices it could be stated that the design of the shading devices are need to be explored for desired performance. The results of both the studics indicate that depth and spacing of overhangs and depth, spacing and angle of ventical fins has significant effect on shading performance. Modification of these parameters may make the shading devices effective in different orientations at the cricical periods.

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CHAPTER: SIX
PARAMETRIC STUDY FOR OPTIMUM SHADING

## PARAMETRIC STUDY FOR OPTIMUM SHADING

After investigating the selected commonly used shading devices, it is found that the performances of these selected shading devices are not consistent through out the critical period of the day. Heat gain is directly proportional to the arca of glass exposed to solar radiation and, therefore, unshaded glazed areas permit a large and rapid heat gain. Solat heat gain can be controlled effectivcly by oprimising shading. To achieve optimum shading, the design strategy of shading devices is needed to explore further.

An investigation through paramerric study to explore the strategies for oprimum shading is presented in this chapter. Paramene study allows stady of various specific alternatives with reference to performance of the model and choosing the best one. Series of parametric studics are performed where different parameters of shading devices ane subjected to adjustment. Only one parameter is changed at a cime in order to determine the relative influence of each. On the basis of the investigation and analyals that has been carried out in the previous chapter, some parametets have been chosen as variables to investigare through computer simulation for opumum shading. The simulation program 'Ecotect' (version 5.20) has been used for this parameric srudy.

### 6.1 Parameters for Oprimum Shading Aralysis

Before scaring the paramerric study, a set of parameters are considered as variables and some parameters are consideted as constant. Variables and constancs are considered separately for horizontal, vertical and compositr shading deviecs. Variables that have been taken into consideration as different alternatives for sirmulations are given below:
A. Cases with horizontal shading devices:

- Depth (D) of horizontal overhangs
- Side offset (W) of horizontal overhangs
- Minimizing the effective height (II)


Section


Jilcvation

Figure 6.1: Schemaic diagrams showing parameters of horizoncal shading device.


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Figure 6.2: Schemaric diagrams showing parameters of horizontal shading device.
B. Cases with verrical shading devices:

- Depth (D) and spacing (S) of vertical lins
- Horizontal angle of yerical fins (0)
- Hxtension (X) of verucal fins above window


Plan


Plan


Secuon

Figure 6.3: Schemaric dagmms showing different parameters of verical shading device.
C. Cases with composite shading devices:

- Depth (d) and spacing (h) of horisontal overhangs
- Depth (d) and spacing (w) of vertical fins
- Horizontal angle of vertical fins (6)


Figure 6.4: Schematic diagrams showing different parameters of composite shading derice.

### 6.2 Simulation Day and Time for the Parametric Study

The consideted day for simulaton is $21^{\text {th }}$ of March (Day: 80). The time period is considered from 0900 to 1700 . The considerations behind selecing the day and time period were mentioned earker.

### 6.3 Parametric Modelling

Models have been developed for the paramerric study by Fcotect'. 'Ihe following aspects have been considered for the parameric movels:

- The room size for simulation model is $6000 \mathrm{~mm} \times 6000 \mathrm{~mm}$, which is considered as located in an intermediate floor of a high-rise building. The room size is taken from the typical high-rise column grid.
- A fixed window size ( $5400 \mathrm{~mm} \times 2400 \mathrm{~mm}$ ) has been considered with single glazed clear glass for the paramerric study. 'The window width is detemined by the column span as it is assumed that the window covers the whole span between two columns. The maximum window height found in the field survey is taken as the height of the windlow for the parameric scudy. Different shading devices are arrached with it for simulation study.
- Fot casc of calculation, thickness of the shade has not been taken into account and a study plane at the level of the exterior surface of the window wall has been considered.

In order to evaluate the shading performance of shading devices in reducing solar heat gain a base case sinuarion is established by studying the unshaded window (without shading device) during the crincal shading period of the year at different omentations.

### 6.4 Paramecric Srudies for Horizontal Shading Devices

From case studies and literature reviews it has been observed that horizonel shading devices are effective at south oricntation. Through parametric study an attempt has been made to find out the size of the horizontal overhang for optimum shading at south oniencaion only. 'Ihree parameters (overhang depth, side offset of horizontal overhangs and minimizing the effective height) ate consideted as viriables for this parametric study.

Only one parameter is changed at a ime in order to detemninc the effect of each parancter on the shading performance. The parameric study is started with a cettain value of paramerers and then an increase in valuc of parameters has been considered to assess the impact of parameter on the shading performance. In all the cases, the shading performance is increased to a cerain level with the increase in value of parameters. After that, the shading performance is not increased any more with the increase in value of parameters. This value of parameter is considered as opumum value for makimum shading. The results of this study are summarised in the following sectons.

### 6.4.1 Effect of Depth of Horizontal Ovethangs

The paramerric study is started for horizonal shading devices of varyng depth, started from 750 mm up to 1350 mm from the exteriot sutface of the wall, over the window (moxdel shown in figure 6.5). In each step impact of 150 mm increment has been scudied.


Figure 6.5: View of the model with horizontal overhang (1050mm depth) used for patamerric study for $21^{\text {th }}$ March (Fcotect output).

The pereminge of ahaded are of the window varies for difterent depths of overhang． Table 6.1 shows percentuge of shaded ateat for difterent overhang depth．The percentage of shaded area is increased with the inerase of shading depth up to some extant．For 750 mm depth，in shades maximum $74 \%$ of the window area and for 900 mm depth it ons shade maximum $88 \%$ of the winchow area．For 1050 mm depth，it shadea maximum $100 \%$ of the window ares and after that the pereminge of shaded arer is not inereased with the increave of chadinf denth．But athough for 1050 mm depth，it shades maximum $100 \%$ of the winctrow aten，the percentage of shaded area is decreased along as rime passer before and after mid day（shoran in figure 6．6）．

Table 6．1：Percentige of shaded ares by horizontal overhangs with different depth for 21＊March．

| Dų¢b | E | $8$ | 空 | g | $\underset{\underset{y}{2}}{\underset{\sim}{2}}$ | $\stackrel{\Phi}{=}$ | $\underset{\sim}{E}$ |  | $\underset{\sim}{\boldsymbol{y}}$ | $\begin{aligned} & 5 \\ & \stackrel{t}{2} \end{aligned}$ | $\%$ | $\stackrel{\text { 务 }}{\stackrel{2}{2}}$ | 会 | $\stackrel{s}{\stackrel{\rightharpoonup}{2}}$ | $\underline{ \pm}$ | \％ | $\underset{\sim}{E}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| In mm | 4 | \％ | ＊＊ | $\stackrel{\square}{\square}$ | 0 | $\%$ | ！ | \％ | 9 | \％ | \％ | 4 | 9 | \％ | ¢ | \％ | \％ 4 |
| 750 | 57 | 58 | 43 | 45 | 67 | 47 | 74 | 6 | 88 | 6 | 85 | ＊） | 60 | 53 | 50 | ＊ 0 | 31 |
| 900 | $\omega$ | $\cdots$ | 75 | 7 | 7 | ＊3 | Et | W | E3 | 7 | 74 | \％ | 4 | W1 | 54 | 43 | 27 |
| 1050 | 73 | 78 | ET | 87 | 72 | 5 | 10 | 0 | 9 | 0 | m | 7 | \％ | 6 | 59 | $4{ }^{4}$ | 31 |
| 1200 | 74 | M） | 15 | 30 | 72 | 5 | 99 | W | 94 | 2 | － 7 | 12 | 7 | 6 | 60 | 45 | 3 |
| t350 | 7 | \％1 | $\overline{\text { M }}$ | 67 | \％ | \％ | $\infty^{\circ}$ | 67 | 9 | 7 | E5 | I2 | 74 | 70 | $\infty$ | 42 | 2 |



Figure 6．6：Pereentape of ahaded area by horizontal overhangs with different depth for 21＂March．

Frown table 6.2, it is evident that more energy is anved with the incresse of shading depth, which is not atwars applinable e.g. energy saving performance of 1050 mm device is same to 1200 mm and 1350 mm device. Hiphest percenage ( $81 \%$ ) of energy is anced by the device having 1050 mm to 1350 mm depth, while the kouest wias presented by 30ireber device, which ans onfy $61 \%$

Table 6.2: Shading cocfficient by horizontol overhangs with different depth for $21^{* \prime}$ March.

| No. | Shading depth | Wieh ahade | Without shade | Shating Cocflicient |
| :---: | :---: | :---: | :---: | :---: |
|  | in mm | in Watr | in Wiat |  |
| 1 | 750 | 2763 | 6327 | 0.39 |
| 2 | $9 \times$ | 1673 | 6377 | 0.26 |
| 3 | 1050 | 1202 | 6327 | 0.19 |
| 4 | 1200 | 1185 | 6327 | 0.19 |
| 5 | 13.30 | 1179 | 6327 | 0.19 |



Figure 6.7: Shading coxeflicient by horivontal avethangs with different depth for $21^{*}$ March.

From fapure 6.7, it has been observed that the mio of total energe recived between shaded and unshaded situation in lowest for 1050 mm to 1350 mum depth of shading device, while it is highest for 750 mm depth. The 1050 mm devier shown lowest shading cocthaient 0.19, which is equal to that of 1200 mm and 1350 mm derice. For 1050 mm depth the ahading device tracher the kroret shading coefficient and after that it goes
same for 1050 mm and 1350 mm depth. 'The lower the shading coeflicient is better against solar radation gain.

## Findings:

For 1050 mm depth, horizontal overhang shades maximum window atca and shows lowest shading coefficient. So, for 2400 mm window height, optimum depth of overhang for maximurn shading is 1050 mm which is $7 / 1 \mathrm{G}$ of window height.

### 6.4.2 Effect of Side Offyet of Horizontal Overhange

From the aloove investigation, it has been observed that honzontal shading device with 1050 mm depth can provide maximurn shading. After that, further inctoase in depth has no sipnificant improvement to increase shading area. To improve the performance of 1050 mm depth device at morning and afremoon, the effect of side offset of horizontal overharge from window edge is studicd. The parametric study is staterl for horizontal shading devices with varying side offset, started from 300 mm up to 1200 mm (model shown in figure 6.8 ). In each step 300 mm increment has been considered


Figure 6.8: View of the model with horizontal overhang ( 1050 mm depth) with 1200 mm side offset used for parametric study for $21^{\text {st }}$ March (Ecotect oupput).

The percentuge of shaded atre of the uindow varies for difterent side offset of oremang． Thble 6.3 belosy shows percentage of shaded areas for different aide offict．The percenage of shaded sres is inereased with the increase of side offset．for 1200 mm depth，it shades $91 \%$ of the windrow aren at 9 am，which is $18 \%$ higher than that of without aide oftsee of 1050 mm device．liot 1050 mm depth，it shades $84 \%$ of the window＇ area and after that，the percentage of shaded area is decreased as cime passes（shown in fegure 6．9）．At 5pm it can shade $44 \%$ of the winghat arco，which is $13 \%$ higher than that of without side offset of 1050 mm device．

Table 6．3：Percentage of thaded area by horizoncal overtang（ 1050 mm depth）with different side offert from windowe edge for $21^{*}$ March．

| Side <br> Oftret | 8 | 官 | 容 | ¢ | 总 | 兰 | 星 | － | 価 | \％ | E | 8 | 鲁 |  | $\stackrel{\text { E }}{\underline{6}}$ | E |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in mm | ${ }_{4}$ | 4 | － | \％＊ | \％ | 3 | $\%$ | ${ }^{\circ}$ | in | \％ | ＊＊ | 5 | \％ | \％ | 8 | \％ | \％ |
| 0 | 75 | 7 | 61 | ET | 92 | 93 | 1（4） | ＊ | ＊ | 6 | S | 79 | 5 | 6 | 59 | 41 | 31 |
| 3115 | 刀 | W | W | 73 | 94 | 101 | 1111 | \％ | 交 | \％ | 第 | 14 | －1） | 73 | 5 | 44 | 13 |
| 600 | 22 | 07 | 93 | क） | \％ | 7 | 101 | 4 | 101） | 9 4 | 92 | 69 | \％ | 77 | 7 | 53 | 36 |
| 900 | ＊ | W0 | 4 | 빼 | 970 | （1） | F | 30 | 1（1） | （1） | 53 | 54 | 벙 | E1 | 73 | 56 | \＄1 |
| 1203 | 91 | 72 | 玺 | को | 9 | 100 | 76） | Itx | 7 7 （1） | LTIF | \％ | 93 | 52 | 4 | 76 | 42 | 4 |



Figurc 6．9．Pereentage of shaded area by horizontal orecharigs with different side offset from window rdse for $21^{\prime \prime}$ March．

## Findings:

For 1200 mm side offiet from window edge, horizontal overhang shades maximum window arey So, for 2400 mm whon height, optimum side offset of orerhang for maximum shading is 1200 mm which is $1 / 2$ of window height. 900 mm side offset may also be used.

### 6.4.2 Effect of Minimizing the Effecive Height of the Window

From the above investigation it has been obsecved that horiontal shading device with 1050 mm depth with 1200 mm side offset from window edge can provide maximum shading.


Figure 6.10: Vicw of the model with horizontal overhangs ( 525 mm depth) with 600 mm side offset used for paramerric study for $21^{1 t}$ March (Ecotect output).

Afrer that, to invesigate the impact of the effective height of the window on the shading performance of the devices, two oprions have been studied. At first oprion, wwo overhangs are considered, one at lintel level and another at mid pane of the window. The depth of both of the overhangs is 525 mm , which is half of the prevous depth ( $105(\mathrm{~mm}$ ) with 600 mm side offset from windew cdge (model shown in figure 6.10). At second option, four overhangs are considered, one at lintel level and the other three are distributed evenly at 600 mm intervals. The depth of both the overhangs is 262 mm
inches，which is half of the provixus depth（ 525 mm ）with 300 mm wide offset from windons edge（model shown in firgure 6．11）．


Fipure 6．11：Virw of the mexdel with horivonal overtange（ 262 mm depth）with 300 mum side offart used for paranterie study for $21^{*}$ Manh（Iizotect output）．

Table 6．4：Percentage of shaded area by horizontal overhangs with different effective heights of the windorw for $21^{*}$ March．

| Encth | 晨 | 8 | 曷 | 易 | $\underline{8}$ | $\stackrel{9}{\square}$ | \％ | 8 | 官 | 祭 | 旁 | \％ | \％ | 3 | P | 安 | $\cdots$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in mm | \％ | $\because$ | $\stackrel{*}{6}$ | \％ | $\because$ | 5 | ＊ | $\pm$ | $\because$ | 4 | $\%$ | 6 | 7 | $\%$ | $\%$ | \％ 6 | \％ |
| 1060 | 91 | 92 | 9月 | 핵 | \％ | 191 | 1111 | 97 | 101） | 1（1） | 5 | 5 | \％ | ${ }^{4}$ | \％ | 12 | 4 |
| 525 | 3 | 0 | 7 | 97 | 97 | \％ | （6） | 7 | 1（1） | \％ | \％ | 57 | 53 | （5） | 8 | 72 | 67 |
| 262 | 9 | ＊＊ | \＄ | ）（\％） | 15 | 7 | （ ${ }^{(1)}$ | I（5） | 101 | 3（\％） | V7 | 9 | 9 9 | \％ | 97 | ES | 82 |

The perecntage of shaded area of the windors increases with minimiring the effective height of the window．Table 64 shoos percentage of shedet areas for different options． For first opion，it shades $95 \%$ of the vinckw arra at 9 am and $67 \%$ of the window area at 5 pm while for scoond option，it ahades $98 \%$ of the window arez at 9 am and $8 \% \%$ of the window mee at 5 pm At 5 pm the percentage of shaded ater for second option is $15 \%$ higher than that of for first option．


Figure 6.12: Percenage of shaded are try horizontal overhang with different effecive heights of winckw for $21^{*}$ March.

From table 6.5 it is evident that more energy is aved with minimizing the effective height of the window. Highest percentage ( $95 \%$ ) of energy is suved by wecond option which is $4 \%$ higher than that of first option. The ratio toral energy recxived betaren shaded and unshaded situation is krwest for second option In the second option the lowest shading co-eficient is 0,05 . The lower the shading co-efficent is better aginst solar mdiation gain.

Table 6.5: Shading coefTecient by hotizontal overtangs with different depth at different height for 21" March.

| No | Effective height of <br> the vinutne in mum | Wish thade <br> in Wiat | Without ahade <br> in Wint | Shating Coneftrient |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 2400 | 714 | 6327 | 0.11 |
| 2 | 1200 | 582 | 6327 | 0.09 |
| 3 | 600 | 330 | 6327 | 0.05 |

## Findings:

Minimizing effecrive height of aindox is beneficial to improwe the petformance of shading derice futher. 'This could be done by using neveral overthangs on the window' pane instend of one lape overhang.

### 6.5 Pammerric Studies for Vertical Shading Devices

Fiom case sardies and litenture mevicas it has been observed that vertial shading devices are effective at west and enst orientation Through paramerric aridy an attempt has been made to find out the size and grometry of the vertical fins for optimum shading at cust and weat orientation only. Parnmetric atudy is done for optimum shading at west orientinion. As sun path is symmetrical about 12 prim same sotution will be applicable for ast orientation. Three paramerets (depth and apacing of vertical fins and angle of vertical fins) art considered as varinbles for this patametric study. 'The results of this study are summarised in the following sections.

### 6.5.1 Efrect of Depth and Spacing of Vertical Fins

'The panmetric study has been started for vertical shading devicea of narying depth from 600 mm to 1200 mm from the exterior surface of the tall , over the window (model showen in figure 6.13) while the spacing berween the fins in comsidered 25 consunt In each step impact of 300 mm increment has becn obscrved.


Figure 6.13: View of the model with sertial fins ( 600 mm depth at 600 mm intervil) used for parametric study for 21" March (tixutect ourput).

Table 6．6：Peroentage of shaded area by vertical fins with different depth fot 21＂March

| Depph | S | E | 空 | 安 | E | $\underline{8}$ | ${ }_{6}$ | ＋ | E | 号 | E | 7 7 | E | g $\underset{7}{3}$ | E | 豈 | 它 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| int mim | 9 | \＄ | 4 | \％${ }^{2}$ | $\pm$ | 4 | \％ | \％ | $\stackrel{*}{*}$ | 4 | \％ | 4 | 5 | $*$ | 4 | 8 | 4 |
| 600 | ＊ | － | ＊ | － | － | ＊ | ＊ | ＊ | ＊ | $\cdots$ | b1 | ＋4 | 57 | 31 | 2 | 21 | 5 |
| 900 |  | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | 70 | 72 | 4 | 51 | 4 | 32 | 77 | 14 |
| 1200 | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | － | 71 | 72 | 7 | 43 | 51 | 41 | 36 | 34 |



The percentage of shaded area of the aindow naries for different depths of fins Tnble 6.6 shows percentage of shaded arges for different fin－depith．The percentape of shaded area is increased with the increase of shading afoth but not very significantly．for 600 mm depth，the device shades maximum $70 \%$ of the window area and for 900 mm depth it enn abso shade maximum $70 \%$ of the window aren and for 1200 mm depth it an shade maximurn $71 \%$ of the windore aree．Fior 600 mm 900 mm ，and 1200 mtm depth，the minimum percentape of shaded arez is $9 \%$ ， $14 \%$ and $24 \%$ respectireh．So，onk incrensing of depth of fins is not effective to shade the window from solar radiation．


Figure 6．14 Percentape of shaded are by verital fins with different depth for 21 ＂ March．＇

[^5]
## Findings:

The percentage of shaded aren is increased with the increase of shading depth but not very significanty. So, only increaing of depth of lins is not effective to shade the window from solar ndiation.

### 6.5.2 Effect of Angle of Vertical Fins

firom the above investigation it has been observed that for verical ahading onty increasing of depth of fins is not effective to protect the window from solat radiation. After that the increase in depth of fins is not further effecrive to increase shading area. 'To improve the performance of vertical devices, the effect of difterent angk of rerical fins with window nurface is sudied. The parmetric study is done for 600 mm , 900 mm and 1200 trin decp verical fras with $30^{\circ}$ and $45^{\circ}$ anglea with the line perpendicular to the uindow surface (model shown in figure 6.15, 6.16).


Figure 6.15: View of the model with vertial fins ( 000 mm depth $30^{\circ}$ slanted) used for panmetric study for $21^{\prime \prime}$ March (Teotect output).


Figurt 6．16：View of the model uith vertical fins（000mm deph $45^{\circ}$ shanted）used for parantetric study for $21^{\prime \prime}$ March（Theotect output）．

Table 6．7：Percentage of shaded area by vertial shading devices with different depth und angle for 21＂Merch．

| $\begin{gathered} \text { G E } \\ \text { E } \\ \hline \end{gathered}$ | $\begin{aligned} & \text { N } \\ & \mathbf{k} \end{aligned}$ | E | 옹 | $\underset{ \pm}{E}$ | e | E | $\stackrel{y}{4}$ | 各 | 突 | 莖 | S | $\underset{y}{5}$ | $3$ | g | $\underset{\sim}{\underline{\sim}}$ | E | ¢ | $\underline{E}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | خ | ＊ | \％ | 5 | 9 | \％ | ： | \％ | \％ | ${ }^{\text {b }}$ | $\%$ | ＊－ | ； | 7 | $\stackrel{\square}{*}$ | \％ | $\because$ |
| 600 | $30^{\circ}$ | － | ＊ | ＊ | ＊ | ＊ | ＊ | － | ＊ | ＊ | m | 4 | ${ }^{0}$ | 7 | 73 | 70 | 4 | 34 |
| 600 | 45＊ | ＊ | ＊ | ＊ | － | ＊ | ＊ | － | － | ＊ | 易 | 47 | W | 11 | N | 5 | F | 33 |
| 900 | 30 | － | ＊ | ＊ | － | － | ＊ | － | ＊ | ＊ | ${ }^{3}$ | 13 | W | n） | m | ${ }^{1} 1$ | 11 | 87 |
| 900 | $45^{\circ}$ | － | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | － | ＊ | ${ }_{4}$ | \＄ | －1 | 9 | 92 | 9 | 97 | 97 |
| 1200\％ | $30^{\circ}$ | － | － | － | ＊ | － | ＊ | ＊ | ＊ | － | ＊） | 83 | 5 | 87 | 5 | \％ | 11 | \％ 5 |
| 12000 | $45^{\circ}$ | ＊ | ＊ | ＊ | － | － | ＊ | ＊ | － | $\bullet$ | \％ | $\Delta$ | ＊ | \＄${ }^{\text {d }}$ | क | 9 | 53 | $\star$ |


The pereentage of shaded area of the aindow varies for diffarent depths of fins with different angle．With changing the angle from perpendiculat to the window surface the percentage of shaded ater of the windkry is incrased significonty．lable 6.7 shows perventige of shaded areas for different findepth with difterent angles．The highorst
performance is seen by vertial fing, 900 mm depth with $45^{\circ}$ angle. For 900 mm depth with $45^{\circ}$ angic pertical fins, in shades maximum $97 \%$ of the window ares and afier that the percentage of shacted aren is ner incrensed with the increase of ahading depth. The Performance of 900 mm depth with $30^{\circ}$ angle vertial fins is very ckrse to that of 900 mm depth with $45^{\circ}$ angle vertical fins.


Figure 6.17: Pereentake of shaded area by vertical shading devices with different depth and angle for $21^{*}$ Murch. ${ }^{16 m}$

Table 6.8: Shading coefficient by vertical shading devices with different depth end anger for $21^{-1}$ March.

| Ne. | 13epth |  | With ahade | W'ttrout shade | Shading cocficient |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | in mm | Angre | 戒 Wrat | in Wian |  |
| 1 | 600 | 30 | 564 | 255 | 0.22 |
| 2 | 60) | $45^{*}$ | 3 m | 2558 | 0.15 |
| 3 | 900 | $30^{*}$ | 444 | 2558 | 0.17 |
| 4 | 900 | $45^{\circ}$ | 346 | 2558 | 0.14 |
| 5 | 1200 | $30^{*}$ | 439 | 25.58 | 0.17 |
| 6 | 1200 | $45^{*}$ | 347 | 25.58 | 0.14 |

Prom table 6.8, it is evident that more enengy is saved with the increase of shading depth, which is not atuyss nppticable e.g energy saving performance of 900 mm depth with $45^{\circ}$
angle verical fins is same to that of 1200 mm depth with $45^{\circ}$ angle verical fins. Hipheat percentage ( $86 \%$ ) of energy is saved by the devices hating 900 mm depth with $45^{\circ}$ angle verical fins, while the bowest is presented thy 600 mm depth with $30^{\circ}$ angle vertial fins, which is only $78 \%$.


Figure 6.18 Shading coefficient by vertical shading devies with different depth and *ngle for $21^{*}$ March.

## Findings:

For 900 mm deprth, werical fin at $45^{\circ}$ angle with the line perpendiculat to the window surface, athades maximum window are and thows loweat shading coefticient. So, for 600 mm spring, optimum depth of fins for maximum shading is 900 mm which is $3 / 2$ of spacing berween fins.

### 6.5.3 Effect of Extending of Venical Fing above Window

Firom the abowe invertigation it has been observed that for varial shading incrensing of depth and angle of fins is effective to proceet the uindes from solar radizion. After that the inerase in depth and angle of fins is not further effective to increase shaded area. To improve further the performsnce of vertical denices, the effect of extending of vertical fins abowe window is studied for 900 mm depth with $45^{\circ}$ angle vertical fins. The pramerric study is atared for vertical shading devices with ançing extension of verical
fins above winderov，started from 150 mm to 600 mm （model shown in fipure 6．19）．In each step 150 mm indroment has been considered．


Figure 6．19：View of the model with verical fins with 600mmentention sbove windsw used for prometric study for $21^{10}$ March（Ficotect ourput）．
＇The percentage of shaded are of the window＇satice for diffetent extension of verical fins sbove window．Tiable 6.9 thowe pereentage of shaded tetes for different extersion of vertical fins abowe window．The higheat performance is seen by veriogl fins with 600 mm extension above window，which shadea commantly $100 \%$ of the window atea．

Table 6．9．Percentage of shaded area by verical firs with varying extension of venical fins abone window for $21^{*}$ March．

| Deph | $E$ | $\begin{aligned} & \text { 最 } \end{aligned}$ | 突 | en | $\underset{\underset{\Xi}{\leftrightarrows}}{ }$ | 总 | 呙 | 즉 | $\underline{5}$ | $\underset{\sim}{E}$ | $\underset{ \pm}{5}$ | 8 | E | $\stackrel{\text { Q }}{\sim}$ | g | 단 | $\underbrace{}_{ \pm}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| En man | － | 46 | \％ | \％ | \％ | 9 | ：－ | ＊ | 46 | \％ | \％ | $\stackrel{\square}{6}$ | \％ | 36 | \％ | 4 | © |
| 150 | ${ }^{*}$ | ＊ | ＊ | ＊ | － | － | ＊ | ＊ | ＊ | 9） | 93 | ＊ | $\cdots$ | 7 | \％ | 7 | 101 |
| 300 | ＊ | ＊ | ＊ | ＊ | ＊ | － | － | ＊ | ＊ | 3 | \＄8 | \＄ | 9 | （10） | 1（1） | 111） | 107 |
| 450） | － | ＊ | ＊ | － | － | － | ＊ | ＊ | － | 9 | $1(1)$ | t（0） | 1（0） | ${ }^{2} \mathrm{Fl}$ | $1{ }^{10}$ | 14 | 115 |
| （\％） | － | － | ＊ | ＊ | － | － | ＊ | － | ＊ | （1） | 5010 | （1） | （1） | （ti） | （ii） | jin） | 107 |

[^6]

Figure 6.20: Percentage of shaded area by verical fins with varying entension of vertical Lins above window for $21^{*}$ March. ${ }^{1690}$

From table 6.10 belour, it is erident that more energy is sured with different extension of vertical fins abowe windkrs. Highest procencare (99\%) of enerfy is naved by the draicer


Table 6.10. Shading coefficient thy vatical fins with varing extension of vertical fins sbove window for $21^{-2}$ March.

| No. | Jxtersion | Writh shatic | Without shade | Shating Coclficiont |
| :---: | :---: | :---: | :---: | :---: |
|  | in mm | in W'st? | in watt |  |
| 1 | 150 | 218 | 2588 | 0.07 |
| 2 | 301 | 132 | 25,8 | 005 |
| 3 | 450 | 67 | 2588 | 0.03 |
| 4 | 600 | 32 | 2558 | 0.01 |

## Findings:

 shows hrwerl shading coefficient. So, for 600 mm spacing optimum extension of vertical fin abore window for maximum shading is 600 mom, which is equal to the apring berween fins.

### 6.6 Parametric Studies for Composite Shading Devices

Case studies and literature neviews so fat done, teveal that composite shading devices ate effective at south-east and south-west orientation Through this patametric study an attempt has been made to find out the size and geometry of the horizontal overhangs and the vertical fins for optimum shading at south-cast and south-west oricntation only. Parametnc swady is done for optimum shading at south-west orientation. As sun path is symmetrical about 12 pm , the same solurion will be applicable for sourh-east orientarion also. Two parameners (depth and spacing of horizontal overhang and vertical fins and angle of vertical fins) are considered as variables for this parametric soudy. The results of this sudy are summarised in the following sections.

### 6.6.1 Effect of Depth and Spacing of Hotizontal Overtangs \&e Vertical Fins

The paramerric srudy has been done for composite shading devices of varying spacing of horizontal overhangs and vertical fins, while the depth of the fins and overhangs is considered as constant. As composite shacting devices are combination of horizontal overhangs and verical finy, spacings of borh devices have impact on the shading performance of composice shading devices.


Figure 6.21: View of the model wich composite shading device used for parametric study for $21^{31}$ March (Ecotect output).

Two options have been studied．At first option spacigg of verizal fins is considered as constant along with the depth of therizuntal everthangs and vertical fins；only spacing of horizoninl overhungs is a veriatse．The prometric atudy is done for 600 mm and 1200 mm spacing of horizontal overtangs．Ae second option，spring of horizontal overhangs is considered as consmat along with the depth of horizonral owethanges and verical fins， only spacig of rertiol fins is a variable．The parametric atudy is done fot 600 mm and 1200 mm spacing of vertionl fins（moded showo in figure 6．21）．In both ases，Jepth of hurizontal ovorhangs and vertical fins is 600 mm

Table 6．11：Pereentage of shaded nere thy composite shading devices with different spacing for $21^{4-}$ March．

|  <br> in m | 晨 | 或 | 空 | g | 8 | $\stackrel{9}{7}$ | 亚 | 3 | $\underset{7}{8}$ | 5 | E | 爯 | 㝰 | 3 | E | 全 | E |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | \％ | \％ | 74 | ＊ | 46 | $\stackrel{*}{*}$ | \％ | \％ | \％ 6 | ＊ | \％ | 4 | 4 | ＊＊ | \％ | ＊ | 8 |
| $\begin{array}{ll} 600 & 2 \\ 1200 \end{array}$ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | 2（1） | 20） | E | $\boldsymbol{R}$ | 67 | 68 | 66 | To | \％ | $\cdots$ |
| 6017 | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | 1（0） | （1） | I（！） | 1（\％） | 1（4） | ¢ | E］ | E | 8 | E |
| （2m） | ＊ | ＊ | ＊ | － | ＊ | ＊ | ＊ | t（M） | 9 | 1fi） | m） | 1（0） | 纤 | \％ | T | 64 | 6 |
| $\begin{array}{ll} 1200) \\ 120010 \end{array}$ | ＊ | ＊ | ＊ | ＊ | ＊ | ＊ | － | IM | t（1） | 5 | 47 | 61 | 56 | 5 | 97 | $\rightarrow$ | 17 |

－Petcentax of thaded ater is not talen into account as the wan docs not wee the window．


Figure 6．22：Percentage of ahaded are by compraite shading device with different rparing for $21^{\mathrm{m}}$ March．${ }^{169 \%}$

The petcentage of shaded area of the window varies for different spacing of fins and overthanks. Table 6.11 shows percenage of shaded areas for different spacing of fins and overhangs. The percentage of shaded area is increascal with the decreasc of spacing of eins and overhangs. The highest performance is seen by 600 mm spacing verical fins with 60 mm spacing horizontal overhangs. For 600 mm spacing vertical fins widh GOOmm spacing horizontal overhangs, it shades from 79 to $100 \%$ of the window area at different time of the day. The performance of ocher alternatives is not consistent (shown in figute 6.22).

## Findings:

For 600 mm depth of fins and overhangs at 600 mm interval, composite shading devices shade maximum window area and shows lowest shading coefficient. So, at 600 mm interval, opimum depth of vertical fins and overhangs for maximum shading is 60 Omm , which is cqual to the spacing between tins and overhangs respectively.

### 6.6.2 Efiect of Angle of Vertical Fins

From the above investigation it has been wbserved that for composite shadiny only increasing of spacing of fins and overhangs is not effecive to protect the window from solar radiacion throughout the day. To improve the performance of composite shading devices, the effect of different angle of vertical fins with window surface is studied in the following section. The parametric study is done for 600 mm spacing horizontal overhang and 600 mm sfracing verical fins with $30^{\circ}$ and $45^{\circ}$ angles with the line perpendicular to the window surface (model shown in figure 6.23).


Figure 6.23: View of the model with composite shading device with slanted fins used for parametric stualy for $21^{* 1}$ March.

The percentage of ahached pres of the window sariss for vertial fins of composite shading devioe with diflerent anube．With changing the angle from perpendinular to the window surface the percentage of shaded vies of the window is increased significanth． Table 6.12 shonst percentige of ahaded areas for vertical fins with differant angtes．For 600 mm spacing hotizontel overhangs with 600 mm spacing vertical fins with $\mathbf{3 0} 0^{\circ}$ nogife，it shader maximum $100 \%$ of the window ares．The performance of（ 00 mom spacing horizontal overhange with 600 mm spacing vertiol fins with $45^{\circ}$ ange is nimost game to that of 600 mm spacing herrizomeal overhangs with 600 mm spacing vertionl fins with $30^{\circ}$ angle（shown in fipure 6．24）．

Tnble 6．12：Percentape of shaded area by componsite shading devices with different angte for $21^{\prime \prime}$ March．

| Arge | E | $8$ | 올 | $\underset{\underline{\theta}}{\underline{\theta}}$ | $\frac{8}{=}$ | 星 | $\underset{X}{x}$ | $5$ | $\underset{\sim}{\xi}$ | $\stackrel{5}{2}$ | $\underline{\square}$ | $5$ | 江 | 宗 | $\underset{\underline{y}}{\underline{E}}$ | E | $\underline{\square}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 9 | T | 4. | ${ }^{4}$ | 8 | \％ | \％ | 4 | \％ | ＊ | \％ | \％ | ＊ | ！ | 5 | 5 | \％ |
| 0 | － | ＊ | － | － | ＊ | － | － | 110 | tirs | 1（F） | （15） | 1（0） | ＊ | ${ }^{\square} 7$ | $\pm$ | E | As |
| $30^{\circ}$ | ＊ | ＊ | ＊ | ＊ | ＊ | － | ＊ | 14 | （17） | \％ | （1］） | $\cdots$ | 47 | 97 | tin | $1(1)$ | 00 |
| $45^{*}$ | ＊ | － | ＊ | ＊ | ＊ | ＊ | － | 107 | 19 | 9 | ＊ | $\cdots$ | ¢ | 97 | M | Im | D0 |




Figure 6．24：Percentage of shaded ntay by composite shading dervices with difterent angle for $21^{*} \mathrm{Narch}^{1 / 4 m}$

Fookwoing Table 6.13 shows that, energy saving perfomance of 600 mm spacing horizontal averhangs with 600 mm apraing vertical fins wirh $30^{\circ}$ anyte is very dose to that of 600 mm epreing horionnal overtanyer with 600 mm apacing vertical fins nith $45^{\circ}$ angle. Hiphest percentage ( $9 \%$ ) of energy is saved by the devices having 600mun apicing horifontal overhangs with (x)0mm spacing vertical fins with $45^{\circ}$ anple

Table 6.1: Shading coefficient by composite thading devices with different angle for 21*Mreh.

| Na. | Anyle | With ohade | Without shade | Shading Coefticient |
| :---: | :---: | :---: | :---: | :---: |
|  |  | in Wert | in matt |  |
| $t$ | $0^{2}$ | 81 | 4015 | 0.02 |
| 2 | $30^{\circ}$ | 36 | 4015 | 0.01 |
| 3 | *5* | 27 | 4015 | 0.01 |

## Findings:

For 600 mm depth of fins and overhanges at 600 mm interval, comporite shading device at $45^{\circ}$ angle with the tine perpendirular to the windore surfice shader maximum window atres and sheron howert ahading enefficient.

### 6.7 Conchusion

Based on the ofsectration made in the parametric studies, it can be sated that with the help of some simple stratepies and modifications of shading devices, the optimum solution conceming solar heat gain isure within tall office buildings can be achieved for considerable period of office hours at fine critiol orientations for periods requiring shading. By providing : bettet protection pgainst wolar heat gain the enerfy consumpuion to dissipgte that heat could be rechuced.

## GUIDELINES FOR DESIGN OPTIMIZATYON OF SHADING DEVICES

Shading is the major consideration to reduce solar heat gain in overheated periods. Shading of a window offers the first lne of defence against heat gains from solat radiation. External shading device is the most efficient solar control as it cuts off solar radation before reaching the window. The design of shading devices can primarily come from understanding the solar geomerry. 'The efficiency of the window shading derices is Lagely determined by the orientation of the window. Every orientation of the wndow requires appropriate shading strategy.

In the previous secions, the theoretical basis and the results of the simulation studies were discussed. Based on the set criteria nine selected shading devices were evaluated mrough simulation. The evaluacion of these selected shading devices in terms of solat concrol helped in identifying the factors that affect in reducing solar heat gain. To explore the stratcgies for oprimum shading, a parametric stady was pursued chrough series of simulations. The observations of the simulated behaviour that occurs due to changing parameters allow the identification of geometric elements, the reduction of introduction of which in the design contribute to reduce solar heat gain. The following sections present recommendations and guidelines.

### 7.1 Proposed Guidelines for Efficient Shading System

In view of all the investigations and on the basis of findings ourlined above, a set of gridelines has been drawn for efficient shading to teduce solar heat gain. Invesigaions showed that different types of shading devices were appropriate for different orientations. The following recommendations arc made for different orientations and for different rypes of shading devices. The recommendations and guidelines are parricularly applicalle for tall office buildings of Dhaka ciry (longitudes: $90^{\circ} 23^{\prime}$ East and lariudes: $23^{\circ} 46^{\prime}$ North).

### 7.1.1 Guidelines for Horizontal Shading Device

- It has been found from the invesigation that horizontal shading devices were efficient at south orientation only. Hence honzontal shading devices are appropriate
to protect the windows from solar heat gain at south orientation. It works efficiendy from 10 am to 2 pm when the sun is opposite to the window pane and at a high alitude.
- The depth of the overhang depends on the window height and is independent of the window width. 'Ihe petformance of horizontal shading device increases with the increase of depth of the overhang. After a certain depth, the performance does not increase significantly with the increase of shading depth. The important factor is the ratio between depth of the overhang and height of the window.
- For optimum shading, the ratio between depth of overhang and height of the window is

$$
\mathrm{D}=7 / 16 \times \mathrm{H}
$$

Where, $\mathrm{D}=$ depth of overhang
$\mathrm{H}=$ IFcight of window


Figure 7.1: Schematic diagram showing patameters of horizontal shading device.

- When designing an overhang for the south facadc, one must remember that the sun travcls from the sontheast before noon and to the southwest after noon. Therefore, the sun will outlink an overhang with the same width as window-width. Windows need wider overhang offset from the window cdge (figure 7.2). The side offset from window edge also depends on the height of the window.
- The tario between the side offset from window edge of overhang and height of the window is

$$
w=H / 2
$$

Where, $\mathrm{W}=$ side offset from window edge

$$
\mathrm{H}=\mathrm{Height} \text { of window }
$$



Figure 7.2: Schematic diagram showing parameters of horizontal slading device.

- Fiot large height of windows, minimizing effective height of window is beneficial to umprove the performance of shadng device further. This could be done by using scveral overhangs on the window pane instead of one large overhang (ifigue 7.3). Installing several overhangs on the window pane is also appropriate when the projecting distance from the wall is limited for structural of other reasons. This could be important if a building is on or neat the property line or there are certain resmictions by building regulations. As far as sun penetration is concerned, the scale of che overhangs cat be changed at any time as long as the racio of $\mathrm{D} / \mathrm{H}$ and W/H ate kept conscant

0


Secrion


Licuauon

Figure 7.3: Schematic diagrams showing parameters of horizontal shading device.

### 7.1.2 Guidelines for Vertical Shading Device

- It has been found from the invesciganon that vertical shading devices were efficient at cast and west orientation only. Hence veracal shadng devices ate approptinte to protect the wndows from solar heat gain at east and west oricntation. It works efficiently with the sun at a low alninde.
- The depth and spacing of verical fins is independent of window height and width. 'The performance of vertical shading devices increases with the increase of depth of verrical fins and with the decrease of spacing between vertical fins. After achieving certann depth, the performance does not increase with the increase of shading depth. The depth of verrical fin depends on the spacing berween vertical fins and vice versa. The important factor is the tatio berween the depth of vertical fio and the spacing between verucal fins.
- For oprimum shading the ratio between the depth and the spacing of vertical in is $\mathrm{D}=1.5 \mathrm{x} \mathrm{S}$

Where, $\mathrm{D}=$ depth of vertical fin
$\mathrm{S}=$ spacing of the verlical fin


Figure 7.4: Schemaric diagrams showing different parameters of vertical shacling device.

* This type of dericc is most effective when the sun is at one side of the devation. A verical device to be effective when the sun is opposite to the window considered would have to give almost complete cover of the whole window. With changing the angle from perpendicular to the window surface to clock-wise drection, he performance of verucal fin increases significandy. Vertical fins at $45^{\circ}$ angle with the line perpendicular to the window surface are most effecive. This type of vertical slanted fin can be appropriate either when there is a desite to conrol the drection of view or when the view is not important.
- When desbging a vertical fin for west facade, one must remember that the sun cravels telative to earth from the southwest. 'Therefore, the sun will outflank a vertical fin with the same height as a window-height Windows need higher vertical fin extending over the window edge. The extension over the top edge of window depends on spacing betweco verucal fins.
* The ratio betwecn extension of fins over the window edge and the spacing between vertical fins is
$\mathrm{X}=\mathrm{S}$
Where, $\mathrm{X}=$ cxtension of fin over the window edge
$S=$ spacing berween vertical fins


Figure 7.5: Schemacic diagram showing different parameters of verical shading device.

### 7.1.3 Guidelines for Composite Shading Device

- The investigation showed that the composite shading devices wete efficient at souchcast and south-west orientation. By concrolling sun penerration by looth the alritude and azimuth angle of the sur, very effecuive shading of windows can be achieved.
- The depth and spacing of vertical fins and horizontal overhang of composite shading device is indcpendent of the window height and width. 'The performance of composite shading devices increase with the increase of depth and with the decrease of spacing bewween vettical fins and horizontal overbangs of composite shading device. The depth of verrical fin and horizontal overhang depend respectively on the spacing between verrical fins and horivontal overhangs and vice versa. The imporant factor is the ratio between the depth and the spacing between vertical fins and horizontal overbangs.
- For optimum shading, the tatio berween the depth and the spacing of the vervical fins of composite shadng device is

$$
w=d
$$

Where, $d=$ depth of vertical fin
w= spacing between veruical fins

And the ratio becween depth and spacing of horizontal overhangs of composite shading device is

$$
\mathrm{h}=\mathrm{d}
$$

Where, $d=d e p t h$ of horizontal overhang

$$
\mathrm{h}=\text { spacing between horizontal overhangs }
$$

It means that depth of verrical fins and depth of horizontal overbangs has to be equal.


Secrion


Plan

Figure 7.6: Schematic diagrams showing different parameters of composite shading device.

- With changing angle of vertical fin from perpendicular to the window surface to anti-clock-wise direction, the performance of composite shading device increases. Vertical fin at $30^{\circ}$ angles with the line perpendiculat $m$ the window surface are most effecive.


Figure 7.7: Schematic diagram showing different patameters of composite shading device.

- The Designer should first decide on the general appearance of dhe composite system. As far as sun penctration is concerned, the scalc of the composite shading device can be changed al any time as long as the ratio of $\mathrm{h} / \mathrm{d}$ and $\mathrm{w} / \mathrm{d}$ are kept constant.


### 7.2 Conclusion

This work was an attempt to explore design strategics of efficient shading devices in tropical urban climatic context with a focus to teduce solar heat gain in overheated periods. T'o achieve the oljectives, through investigations a set of strategies has been dawn that could help to design an efficient shading device in place of commonly practised ones in Dhaks. This work may also insugate designers design efficient shading devices with a reference to climate issues.

At present the necessicy to reduce the energy consumption in the buildings is an important issue in Bangladesh. 'The design strategics of efficient shading devices that have emenged as a direct outcorne of this study are important in producing energy efficient design solutions. It may be extremely useful to have such strategies in mind during the pre-design and design stages of buildings, as passive solutions allow buildings to responsive with environment, thereby reducing energy consumption.

### 7.3 Suggestions for Future Research

Some of the most important ateas that need to be explored furcher are summarized below:

- More research needed to assess the impact of shading devices on daylight and vencilation through the window.
- Performance of shading devices can be evaluated in reducing heat gan for diffused solar radiation.
- Performance evaluation can be done with various thickness of shadeng devices with different types of materials. The use of shading materials and methods of installation with regards to their thermal properties need to be invesugated for detailed recommendanon for their uses.
* Possibility of mechanized movabie shading device can be explored. The cost effectiveness of fixed shading device with comparison to movable shading device can be done considering maintenance and construction cost.
- Combination of shading devices (interior and exterior), movable shading devices and shading devices combined with special (solar-protective, low-e) glazing should be studied.
- 'Dhaka Metropolis Building Construccion Rule 2006' can be examined considering solar shading in buildings.
- Impact of shading optimizanon on building energy consumption may be studied in view of energy saving potencials.


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APPENDIX A: Hourly Dry Bulb Temperature ( ${ }^{\circ}$ )
Hourly Dry Bulb Temperature ( ${ }^{(C)}$
Sousce Bangadceh ineteorvlogeal Department, (.lmane Duston, Agargacon, Dhaka
Year 20003 Month: ]anury


Hourly Dry Dub Temperature（ ${ }^{\circ} \mathrm{C}$ ）

Yeir 2005 Month：Febrnary

| Day | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 1.3 | 14 | 15 | 16 | 17 | 18 | 11 | 20 | 21 | 22 | 23 | 24 | 25 | 20 | 27 | 28 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tise |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 010 | 14.4 | 15.2 | 124 | 13．5 | 13.9 | 13，4 |  | 181 | 17.4 | 18.4 | 16.9 | 1R1 | 2114 | 215 | 2116 | 225 | 227 | 24.4 | 2 H ， | 222 | 23.8 | 21．1） | 199 | 2 L 2 | try | 9， | 18s | $\underline{6} 6$ |
| 1 （i） | t H ．${ }^{\text {d }}$ | 1 L 9 | 13.9 | 14.5 | 152 | 156 | ［43 | 19 fi | 19.4 | 3．， | R | 11） | 21．21 | 25 | 21. | 21 | $3+$ | 24.7 | 24.1 | 22.4 | 246 | 22 | 210 | 21.1 | 19.9 | 107 | 209 |  |
| 2.0 | 19.3 | 17.7 | 15.5 | 155 | turn | 17．k | 19.7 | 21.2 | 2111 | 221 | 21.0 | 215 | 2.1 | 23,3 | 22 | 230 | 25 | 25 | 24. | 235 | 25.4 | 23.5 | 22. | 219 | 19.11 | 21.9 | $22 \cdot 1$ |  |
| 300 | 14.8 | 18. | 1711 | 16.5 | 13.9 | 210 | 21.11 | 22\％ | 22.6 | 2412 | 23, | 23.2 | 242 | 24.2 | 21. | 24 fr | 25.6 | 25 | 247 | $2+2$ | 26. | 24 | 23 | 22．15 | 22 （1） | 2.31 | 250 |  |
| （0） | 20.9 | 197 | 182 | 18 | 19 | 2 t ． | 27 | 24 | 243 | 25.4 | 24. | 249 | t（a） | 256 | 25.2 | 25 | $2{ }_{5} 9$ | 76.7 | 256 | 25 | 27. | 25，6 | 247 | 241 | 23．－ | 24.8 | 26.4 | ， |
| 501 | 22 | $21 .!$ | 19 | 21.2 | 231 | 23.6 | 24.7 | 26 | 25. | 200 | 25.5 | 25.7 | 28.1 | 270 | 261 | 269 | 27.9 | 27.1 | 26 | $2(.4$ | 29．1 | 26 | 2！ | 255 | 24．1） | 246 | 27.9 | 2 H 4 |
| $1{ }^{1}$ | 23 | 224 | 20.5 | 22， | 240 | 25．4 | 26. | 27.9 | 276 | 276 |  | 2 S 4 | 3， 11 | 27．4 | 285 | 2R，1） | 214 | $2{ }^{21}$ | 27. | 235 | 31 | 27 | 27，${ }^{\text {，}}$ | $2 \mathrm{~L} . \mathrm{K}$ | 26．3 | 2r． | 29.3 |  |
| 7．141 | 22 | 22.1 | 21.9 | 29 | $2+6$ | 24.1 | 27.5 | 2 L 2 | 241 | 27. | 27.2 | 2以！ | K17 | 24．2． | 20.1 | 2 F 7 | 21） | 29 | $2 \mathrm{k}, 2$ | 2， 3 | 309 | 27.5 | 24 | 27.3 | 27.1 | 29. | 215 |  |
| （1） | 224 | 33.7 | 21.4 | 23.5 | 25 | 267 | 2R．5 | 2R， | 245 | 27. | 27． | 2）．$)^{1}$ | 3 H. | 29． | （11） | 20. | 316 | （1） 4 | no． 1 | 2）II | 31.5 | 276 | 293 | 27.7 | 240 | 20.5 | 29 B |  |
| 9，14） | 224 | $2+11$ | 21． K | 242 | 25.7 | 27.1 | 21） 4 | $2{ }^{21}$ | 2041 | $2 \times 4$ | 2314 | ma | 32.0 | 294 | ， 1 | 311 | 11.4 | 113 | 25 | $29 . \mathrm{H}$ | 1.16 | 23 R | 319．1 | 282 | 285 | W11 | 估 |  |
| 1.8111 | 21.7 | 22.9 | 21. | 23 | 247 | $x_{1} 1$ | 2x， 3 | 27 K | 2 x 1 | 27 \％ | 27.1 | 29 | 317 | $2 \times 7$ | 31.9 | 210 | \％19， | \％ | 2．． | 297 | \％ | 27.3 | $29+1$ |  | 27．9 | $2{ }^{2}$ |  |  |
| ［1］： $1 / 4$ | 21 | 219 | 20 | 23 | 2. | 24. | 27 | 26.7 | 27 | 26.4 | 20，7 | 2h6 | $2 \cdot 15$ | 27.6 | 2 H | 202 | 296 | 29.5 | з $\boldsymbol{4}_{6}$ | 29.5 | K1， | 2（6） | 27.2 | 26.3 | 271 | 244 | 2\％3 | \％ |
| 12 | 21 | 21 R | 19. | $2{ }^{\text {I }}$ | 22a | 23. | $2(1)$ | 235 | 26.2 |  | 20.0 | 276 | 272 | 265 | 2 H | 284 | 247 | 2R，R | 2.42 | $29+$ | 21 | 26. | 26．） | 254 | 26，2 | 275 | 27.4 | 2 k 2 |
| 13 m |  | 21，2 | 18.8 | 21 | 205 | 225 | 25 | 24.5 | 25.3 | 244 | 245 | 267 | $27+$ | 257 | 20.9 | 274 | 2 F 9 | 37. | 27.5 | 2 F | 286 | 255 | 35 | 244 | 25.3 | 25. | $2{ }_{\text {chis }}$ | \％ 2. |
|  | 12.4 | 19，0 | Lht | 1． | $1{ }^{1} 3$ | 21 | 24 | 234 | 24.5 | 236 | 2211 | 25． | 26.6 | 25．91 | 254 | 271 | 27.1 | 27.1 | 26， | 27. | 2 N 1 | 24 | 2411 | 23，4 | 24.5 | 34.4 | 25.4 | 25.3 |
| Of | In． | 100 | 17 | 19.0 | tur | 3） 4 | 23，0 | 22. | 2 t .1 | 224 | ． | 9 | 25 | 2． 2. | 24 | 26.2 | $23_{1}$ | 21.2 | 26.1 | 2 t .1 | 27. | 23，8 | 226 | $22+$ | 2.3 | 228 | 24． | 23， |
| 16．09 | 18.3 | 185 | 17 | 1k， 3 | 13 n | 10. | 272 | 21.6 | 22.9 | 21 | 21.3 | 24.4 | 254 | 2aj | $2+$ | 25 | 25.3 | 236 | 24，k | $2{ }^{5} 9$ | 26.6 | 27.2 | 22.1 | 21 H | 2.5 | 21.7 |  | 227 |
| 17：00 | $1 \mathrm{R}, 1$ | 17 | $1 r_{1} 7$ | 17 | 15. | t）． | 214 | 2 | 22 | 21.4 | 213 | $2+1$ | 249 | 22.7 | 212 | 2.1 | 5 | 25 | 2ヶヶ | 25．4 | 258 | 22.5 | 21 | 21.3 | 23．3 | 20.7 |  | 21.7 |
| 1890 | 174 | 17. | tict |  |  | 1911 | 2）．t． |  | 21 | 12.4 | 21.2 ． | 235 | 245 | 220 | 22. | 24， | 248 | 24.5 | 213 | 256 | －24，9 | 2241 | 21.2 | 2）． 7 | 222 | 176 | 21.5 | 206 |
| t9．141 | 13. | 11.6 | 15. | 16 | 141 | 18．6 | $2 \mathrm{x}, 0$ | V | 21.2 | to． 3 | 210 | 27.1 | 2411 | 21. | 22. | 245 | 24.7 | 24. | 224 | 25.1 | 29.7 | 21.3 | 2）${ }^{4}$ | （2） | 214 | 19.4 | 19 | 202 |
| 2（1， 1 M$)$ | 12.3 | 15. | 14.8 | $15:$ | 1.31 | 18.2 | 104 |  | 2112 | \％ 1 | 21.4 | 212 | 3.5 | 31.7 | 22 | 24 | 24.7 | 24 | 225 | 4 5 | 22.6 | 21.5 | 2） 4 | 202 | $\underline{16}$ | 19 | 18.7 | 198 |
| －14． | 17．13 | t5 | 1411 | 15 | 13 | 17. | 15，R | 145 | 0 | － | 2 m | 22. | 2311 | 211， | 227 | 24 | 24．6， | 242 | 22 | $2{ }^{2} 11$ | 21. | 21.2 | 2 L It | nu | 19 y | to | 17.4 | 194 |
| ， | 19， | 173 | 17．2 | 17.3 | tis | 2013 | X1，6 | 210 | 217 | 21.5 | 21. | 272 | 24 | 215 | 2211 | 23. | 24， 1 | 241 | 22］ | 23，8 | 22.4 | 72.4 | 3，${ }^{1}$ | ） 2.2 | 21 | 21．5． | 199 | 214 |
| 2300 | 19.7 | ［1］ | 205 | 12 | 20.9 | 223 | 22 | 23.1 | 231 | 220 | 231 | $\underline{23}$ | 21．8 | 211 | 217 | 23.5 | 235 | 241 | 22.5 | 236 | 335 | 34.4 | 217 | 204 | 20.5 | 21.9 | 221 | 23.9 |

Hourly Dry Bulb Temperature（ ${ }^{\circ} \mathrm{C}$ ）

| Diy | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 4 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0 O） | 21.11 | 22.1 | 237 | 21 | 34.5 | 24，5 | 242 | $25+$ | 2.4 | $2: 5$ | 247 | 21，8 | 21.2 | 214 | 21.4 | 232 | 2t．lt | 24．1） | 23！ | 24 | 24．5 | 26.0 | 225 | 21，6 | $3) 4$ | 234 | 24.2 | 27.3 | 23.4 | 25.1 | 7 |
| 100 | $\underline{22} 3$ | 232 | 24.5 | 235 | 254 | 257 | 25.1 | 259 | 24.3 | 245 | 243 | $\underline{22}$ | 22.9 | 27.3 | $22 ?$ | 24.2 | 24.2 | 25.7 | 23.3 | 3.1 | 25.5 | 20.7 | 27. | 211 | 22.16 | 245 | 251 | 26.0 | 2t． 1 |  |  |
| 2，00 | 23.7 | $\stackrel{2}{4}$ | 254 | 25.7 | 26.3 | 268 | 259 | $2 \mathrm{f}_{3} 3$ | 25.3 | 25.5 | 24，${ }^{2}$ | 220 | 245 | 25.1 | 24 | 25 | 25 | 2 | 235 | 267 | 266 | 275 | 2. | 21.7 | 292 | 25.6 | 26.1 |  | 26.9 |  |  |
| 3.00 | 25.11 | 25. | 251.2 | 278 | 27 | 2 S 1 | $251,{ }^{2}$ | 2 ar | $26_{1}$ ？ | 2 L 5 | 274 | 234 | $22_{1} 2$ | $25_{2} 7$ | 254 | $\bigcirc$ | 26 | 2k2 | 23， | 284 | 296 | R，2 | 244 | 322 | $24+$ | 26， | 270 | 27. | 27， |  |  |
| 400 | 27.11 | 27. | $2 \mathrm{R}, 4$ | 29 | 247 | $\underline{\underline{x}}$. | 2R，2 | 27 K | 27.7 | 24： | 2＊－4 | 237 | 27.7 | 284 | 271 | 27.7 | 27 | 277 | 20.1 | 2\％ | $2{ }^{2}$ | 以， 1 | 336 | 223 | 23.4 | 274 | 27， 1 | 29.5 | 245 |  |  |
| 5 M | 2り11 | 301 | 31f | 31.4 | 3112 | ． 317 | 20，6 | 24 n | 2נ1． 1 | ，112 2 | 2k 1 | 239 | 2 | （1）］ | 2 K 6 | 2 | $2{ }^{2}$ | 271 | $2{ }^{2}$ | 31） | 319 | 31.9 | 22K | 213 | 26， 5 | 272 | 21） 3 | 29.7 | 253 |  |  |
| from | 11，1） | 32.4 | 32． | 332 | ．11．7 | 321 | 314 | 29 K | ${ }_{3}^{11}(1)$ | 3214 | 21， | 24 | 310.7 | 7 L | 312 | 3l．fi | \％） | 20.6 | Bil． 4 | 31 | 32.5 | 33 k | 2렌 | 224 | 275 | R9 | 319.4 | ． |  |  |  |
| 7 CHI | 315 | 329 | 13. | 379 | $\underline{22}$ | 32，R | 4.1 .7 | 30， 1 | 112 | 32.8 | 5 | $2{ }_{4}$ | 3101） | 32 | 3120 | \＄1，${ }^{\text {3 }}$ | ． 1 | 272 | 5194 | ． 3 | 335 | 3，K | 22 | 22.9 | 2R | 297 | 1 | 31.5 | 11.0 |  |  |
| $\mathrm{B}_{3} \mathrm{H}$ | 321 | 314 | 33.0 | $3+5$ | 127 | 335 | 325 | 81］ | 318 | 32，6 | 린 | 25.1 | 11.1 | 32.3 | 315 | 114 |  | 21） 2 | 31.2 | 32 | 34. | $1 . \mathrm{K}$ | 23, | 245 | 2 B | 31 | 31.6 | 32. | 117 |  |  |
| 9－14． | 326 | 33．4 | 34，4 | 352 | 33.2 | 4.42 | 312 | ． 3.311 | 32．4． | 34.4 | 293 | 25．5 | 31．2 | 326 | 372 | 320 | 22． | 3125 | 316 | 33 | 35.4 | 318 | $2+1$ | 341 | 2 | 12 | 322 | 32.4 |  |  |  |
| lick | 217. | 32 C | 33．7 | 34.3 | 32－6 | 3.3 | 323 | 3 313 | ${ }^{3} \mathrm{t}, \mathrm{k}$ | 335 | 28 | 25.1 | 3 | 312 | 115 | 318 | 3 t. | 293 | 311 | 33. | 3，4， 1 | 32） | 226 | 27 | 2 F 8 | 0.7 |  |  |  |  |  |
| 13.041 | 3 31.7 | 31.7 | 7.21 | 32.3 | 32，1） | 123 | 317 | 31．1） | 312 | 32.7 | 378 | 24 亿 | 297 | 29 R | 31） | 3．11\％ | 3 t .1 | 28． 2 | 307 | 32.7 | 327 | 312 | 212 | 22 | 2R2 | 30.7 |  |  |  |  |  |
| ［2．14］ | 29.4 | 30 | $3{ }^{11}$ | $\underline{23} 1$ | 31.4 | t1．4 | Kin | （x， 1,1 | 3116 | 31．2 | 27.1 | 242 | 주） | 2x，4 | 311 | －30 2 | 31.2 | 27.1 | 302 | 32.2 | 314 | 311 | 19 | 2311 | 27.6 | 208 |  |  |  |  |  |
|  | 20，${ }^{2}$ | 2）3 | 3113 | 311.16 | 311.7 | 15 | $\underline{2}$ | 292 | 2115 | 310.7 | 262 | 274 | 2 n 2 | $2 \times 1$ | ） | $\underline{2} 5$ | 295 | $2 \mathrm{ch}^{2}$ | $\underline{29} 8$ | 31. | 316 | 29，7 | 213 | 21．4 | 26.9 | K6 |  |  |  |  |  |
| 14 （1） | 27.8 | 2 H 5 | －29．7 | 29.6 | 20．1） | 29 | 26．5 | －$\square_{4}$ | 24.7 | 29.5 | 25 亿 | 235 | 27.5 | 7， | 2 k 1. | 2k，9 | 24 | 26,5 | 22.4 | 311 | ${ }^{11} \mathrm{k}$ | 2 t, | 20 | 21.5 | 25 |  |  |  |  |  |  |
| 15.10 | 26.4 | 274 | 29） | 랜 | 29.2 | 2R， | 23.1 | 276 | 27.7 | 2R 4 | 2＋4 | 23.2 | 20.7 | $\underline{27}$ | 27.1 | $2 \mathrm{~K}=$ | 2 x 2 | 260 | 210 | 23， 0 | 290 | 2411 |  | 21 ！ |  |  |  |  |  |  |  |
| trime | 32 | 26.7 | 2 R | 27.5 | 2R． | 27. | 27.1 | 27.3 | 273 | 230 | 24.1 | 2211 | 25． | 34，1 | 205 | 377 | 27.7 | 257 | 3n，3 | 28.1 | 22.3 | 24.1 |  |  |  |  |  |  |  |  |  |
| 17．111！ | 254 | 259 | 23.5 | 26.4 | 2 H | 27．1 | 26.7 | 27 | 2 | 27.6 | 3.7 | 227 | 25.2 | 245 | 25．k | 27.1 | 271 | $\underline{25}$ | 276 | 27 | 27.5 | 24. |  |  |  |  |  |  |  |  |  |
| 18．19） | 250 | 25？ | 2 fin | 20.2 | $27+$ | 262 | 26.2 | 2rik | 2ftil | 27.2 | 23.4 | 2근 | 24.4 | 230 | 25．2 | 26 （1） | 266 | $\xrightarrow{2}$ | 2t．1） | 26. | 20，8 | 24. | 2 |  | 224 |  |  |  |  |  |  |
| 19（0） | 24.3 | 249 | 25.7 | 25．8 | 26． 1 ） | 26 | 2 t, | 2 亿r1 | 26t | 24.7 | $27!$ | $22 \%$ | 3，9 | 225 | 24 | 2615 | 26.3 | $\underline{-1}$ | $2 t_{1}$ | 26 | 31.4 | 241 | 711 |  |  |  |  |  |  |  |  |
| $2 \boldsymbol{n}(x)$ | 23．7 | 247 | 24.5 | －25．4 | 265 | 257 | 25 R | 252 | 25.5 | 24．1 | 22 | 21 | 235 | 22.11 | 27. | 25.4 | 259 | 243 | 23.5 | 25 |  |  |  |  |  |  |  |  | 24.7 |  | 4.3 |
| 2t（x） | $\underline{13}$ | 24.4 | 2.3 | 25 | 26.1 | 255 | 256 | 24.4 | 25.1 | $25{ }_{1}$ | 224 | 2211 | 230 | 21.5 | 22 H | $2+4$ | 25.6 | 241 | 24 x |  |  |  |  |  |  |  |  | 25 k |  |  | 23.9 |
| 73（ 4 ） | 27，0 | 23 h | 23.5 | 23.4 | 24.9 | 25. | 254 | 25 ！ | 35.3 | 35.9 | 235 | 275 | 229 | 229 | 230 | 25.4 | 291 | 243 | 257 |  |  |  |  |  |  |  |  |  |  |  | ， |
| 23．0） | 23.0 | 232 | 23.7 | 21.8 | 23.1 | 25.3 | 25.2 | 257 | 25.7 | 24.3 | 245 | 249 | 22.9 | 242 | 24.9 | 259 | 2n， 7 | 24，6 | 26.3 | 27.7 | 24.0 | 2 O | 2 | 20． |  |  |  | 2 | 234 | 21. | 15.7 |

Houtly Dry Bulb Temperature（ ${ }^{\circ} \mathrm{C}$ ）

Year， 2005 Munth Aprl

| 14 | 1 | 2 | 3 | 4 | 5 | $\underline{\square}$ | 7 | 8 | 2 | 10 | 11 | 12 | 13 | 14 | 15 | 14 | 17 | 18 | 19 | 23 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 2 R | 29 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7ime |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| M， x | 2311 | 27 | 278 | 2112 | 22.1 | 5.2 | 25 | $21_{3}$ | 2511 | $2{ }_{2} 6$ | 25 | 2fr． | 23 | 254 | 2511 | 26 | 272 | $2+5$ | 27.6 | 2 ak | 243 | 2. | 27，0 | 220 | 231 |  | 4.0 |  |  |  |
| 11 | 243 | 24 | 259 | 221 | 246 |  | 250 | 37．2 | 263 | 275 | 34. | 2 c \％ | 24.9 | 267 | 27.2 | 27.1 | 241 | 26.7 | 2R5 | 295 | 261 | 2h2 | 280 | 25 | 24. |  | 25.9 | 26 |  |  |
| $2($ 나 | 25. | 2（1） | 27.9 | 24.1 | 24.3 | 27.3 | 3，${ }^{2}$ | $2{ }^{4.1}$ | 27 | 24．3 | 27. | 27.2 | 20. | 27．） | $\underline{314}$ | 27，4． | 24 | 2 L | 20 | 31） 3 | 2v0 | 292 | 291 | 7 | 267 | 2N？ | 27.9 | 88. | 211 | 57 |
| 3 cm | 2，1．1） | 2） | 310 | 2611 | 231 | 2．4． 4 | 27.4 | 20， 11 | 2 n 3 | 29.2 | 2hin | 27. | 214 | 29.1 | 29 | 2R， 4 | 3， $1 \times 1$ | 312 | 310， 3 | 1311 | 313 | 312 | （1， 10 | 29 | 2R6 | 296 | $2)^{2}$ ， | 25．1． | 26.4 | 27.4 |
| 400 | 2 R .1 | to． 3 | 312 | 277 | 20． 1 | 29.5 | 20.1 | 298 | 215 | 313， 4 | 293 | 21 | 111． | 30.3 | $\times 16$ | －11 | 312 | 31.3 | 31.6 | 1211 | 32.7 | 31.6 | 11．4． | \％ 8 | 29.6 | 30.7 | 30．1） | 31.1 | 28.1 | ， 5 |
| S－14） | $2{ }^{2} .2$ | 31.7 | 32. | 29. | 3 1 L 11 | 31.5 | 31.3 | 311.9 | 31．n | 12. | 3115 | 31.2 | 31 | 31？ | 31.5 | 31.5 | 125 | 32.4 | 32.9 | $33.1)$ | 337 | 37．N1 | 31. | 315 | 3115 | 31.8 | 321 | 325 | 3.9 | 925 |
| 6.10 | 313 | 33. | 33 | $3 \mathrm{t}, 0$ | 311 | 316 | 316 | 31 h | 320 | 328 | 3.1 | 125 | 32.4 | 330 | 325 | 37， 12 | 33，7 | 31 | 14 | 34.0 | 34 | 34.4 | 225 | 32.5 | 31.5 | 仁り | 13.2 | 340 | 316 | \％ |
| $7.1 \times$ | 305 | 31 | 7．3． | 315 | 31.2 | 32.1 | 32.1 | 324 | そ7 | 3，3 | $32+$ | ざリ | 231 | 336 | 4.3 | 晾 | H0 | 34．1 | 346 | 344 | 34．51 | 3.49 | 1.31 | 332 | 32.1 | 373 | 132 | 34.5 | 30.3 | 31.1 |
| R00 | 36． 4 | 3.7 | 3＋11 | 3211 | 31.7 | 227 | 325 | 37. | 3，3 | 41，${ }^{3}$ | 11.16 | \％3．2 | 33.9 | 34.1 | 4 | 137 | 34.3 | 14， 5 | $5{ }^{1}$ | 347 | 34\％ | 55 | 36 | 33.6 | 127 | 3．1． | 131 | 34.9 | 29 | 1.7 |
| 0.101 | 311 | 3 L .5 | H2 | 32 | 12.15 | 332 | 3．．．11 | 32.7 | 34，） | 4.43 | 3 | 36 | 346 | 34.7 | 35.1 | H13 | 346 | 15.3 | 354 | 35 t | 44 | 354 | 4 | 34 | 4.2 | 341 | 031 | 35.4 |  | 2 |
| 10，（x） | IN， 8 | 12.7 | $33+$ | い1 | 316 | 32.1 | 52.5 | 3.71 | 33 | 12.2 | 12．11 | 1311 | 337 | 3＋11 | 4.7 | 332 | 337 | 14？ | 34.7 | 34. | 445 | 15.1 | 337 | 335 | 129 | \％） | 22.3 | 3.3 | 20.2 | 1.5 |
| 11 （\％） | W15 | 318 | 32 | 31.2 | 31.2 | 느네 | 121 | 32 | 32.5 | un． | 314 | 32. | 42. | \％． 3 | 42 | 32.4 | 121 | 37 | 339 | $1{ }^{1} \mathrm{~K}$ | 345 | 3.4 \} | 33,1 | $3{ }^{3} \mathrm{t}$ | 127 | 271 | 31.4 | 31.1 | 246 | 57 |
| （1） | k1， 3 | 12.11 | 41. | H14 | 1115 | 11. | 31 | 710 | 37 k | $22_{11}$ | 2R， 4 | 3 | 22.1 | 3 Cr | 378 | 316 | 3네 | 33，6 | 332 | ห\％． 1 | 34 | 3，${ }^{\text {cr }}$ | 326 | 32 |  | 236 | n6 | 29.0 |  |  |
| 13 （ $\mathrm{H} / \mathrm{l}$ |  | 21.9 | 29.1 | 295 | 31.2. | 313， 7 | 30.7 | $3: 17$ | u1．5 | 27. | 2 Sl | ห1， 3 | 11.2 | $11 \%$ | 32.6 | 3119 | 41.3 | 32 R | 32.7 | 123 | 3.35 | 32.7 | 32.1 | 31.9 | 29．8． | 24.2 | 25 | 27.7 | 27.1 | 287 |
| 1416t | 27．6 | 2 S | 20.3 | 24.5 | ＊） | 3,1 | 29.3 | 2リリ | 29 | $3{ }_{3} 9$ | 273 | 201 | 11 | 3119 | 3.4 | u12 | ． 117 | 3211 | 12.1 | 314 | 326 | 31.7 | 31.5 | 31.3 | 27.1 | 24. | ［17 | 26.1 | 2 | 27.3 |
| 15 | 26.2 | 278 | 236 | 274 | 236 | 2）， 4 | 22.11 | 2951 | 2 n ） | 26. | 26\％ |  | $2)^{3}$ | H1， 2 | 3112 | 2 ys | ， | 312 | 316 | 3.16 | 31.7 | 311 | 19 | 30， 0 | 24.5 | 35 | 24.8 | ${ }^{5}$ | 237 | 27.0 |
| 16 Mil | 257 | 27 | 23.3 | 26.7 | 28 | 28. | 2R， 1 | $2 \mathrm{n}, 3$ | 27，k | 26.3 | 56 | 27.1 |  | 11． 7 | 295 | 28， 9 | 21） 4 | M1， | 31. | 2 N ， | 31.1 | 311． 4 | 30 | 310 | 241 | 25. | 2＋4 | 251 | 23.5 | 45 |
| 15：3m | 252 | 27.5 | 229 | 259 | 27.4 | 27.8 | 27 | 27.7 | 37.4 | 281 | 21.2 | 26.7 |  | $2^{1 / 2}$ | 24. | 2 K 4 | 2．4．4 | 2） | 31.5 | 24） | bilf | 29. | 29 | 21 | 25 | 2 | 248 | 25.1 | 237 | ？ 31 |
| 18.00 | 24.3 | 27.4 | 226 | 25 | 27，4 | 27 | 22.4 | 27，0 | 27 | 2011 | 3 m 0 | ¢12 | $27 \times$ | 287 | 2 B 2 | 27， | 2x2 | $20 \%$ | आस्रा | 25 | （1） 1 | 2y 5 | $2 \mathrm{~F}, \mathrm{~B}$ | 24 | 25 | 25.1 | 248 | 25. | 23.9 | 21.1 |
| 1950 | 24.5 | 26 | 219 | 24.4 | 2714 | 26.7 | $3 \mathrm{~L}, 3$ | 2，${ }^{1}$ | 272 | 26 | 259 | $\pm 5$ | 27. | 29，4 | 278 | 27.7 | 26.5 | 2h9 | 碰 7 | 248 | 29.1 | 2 | 2n， 2 | 28.1 | 35 | 24.9 | 24.7 | 24 | 23，6 | 21.6 |
| 2000 | 23 | 26 | 21.3 | 24. | 266 | ［13 | 26.2 | 26.7 | 271 | 2 | 25. | 245 | 27.1 | 2k．1 | 27.4 | 23.5 | 247 | 2n， | 295 | 246 | 2R，7 | 28.5 | 2：6 | 274 | 255 | 247 | 24.7 | 24 | 233 | 1．6 |
| 21，（0） | 23，4 | 254 | ， | 24 | 26 | 2 L | 361 | 26.5 | 26.9 | 21 | $\underline{35}$ | 23.1 | 36， 4 | 27 | 30 | 27. | 2311 | 24 | 2 l | 24.4 | 2 O | 2 S | 27.1 | 26.4 | 25.4 | 24，6 | 246 |  | 23 | 21.6 |
| 22 （n） | 22 K | 27 | 21.7 | 24.6 | 25.3 | 24．） | 25.2 | 2，${ }^{1}$ | 2 F .3 | $\square 7$ | 20.3 | 253 | 26.2 | 2 L 4 | $2 \mathrm{~T}, 6$ | 271 | 23.4 | 25.5 | 2x． | 2411 | $22^{2} \mathrm{~B}$ | 2k，${ }^{\text {r }}$ | $2{ }_{3}$ | 26 | 26. | 25. | 251 | 25.7 | 2 | 23.8 |
| 23.00 | 222 | 241 | 229 | 25 | 2. | 23. | 249 | 25 | 29．B | 27.5 | 269 | $\underline{7 .} 1$ | 25 | 24 | 363 | 27.3 | 238 | 23.9 | 28.4 | 23.7 | 256 | 3 HO | 257 | 268 | 26， 7 | 27. | 257 | 27.3 | 26.7 | 20 |

## Houty Dry Bulb Temperature（ ${ }^{\circ} \mathrm{C}$ ）


Year 3005 Mforth：Mlay

| Day | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 11 | 15 | 16 | 17 | 18 | 19 | 210 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1） 610 | 216 | 2.3 | 24.0 | 25．h | $22^{4}$ | 22. | 33.4 | 25.2 | 312 | 2 H ？ | 27．4 | 26，${ }^{\text {R }}$ | 25.11 | 23，5 | 25，9 | 27.2 | 242 | 218 | 2 Al | 23 \％ | $2+4$ | ご家 | 25.0 | 268 | 273 | 2\％ 6 | 362 | 29.1 | 2R 6 | 28.2 | 28.4 |
| 100 | $2{ }^{1} 1$ | 25．3） | 256 | 26.3 | 25．8 | 241 | 251 | 24．亿 | 22.5 | 2） 1 | $2 \times .5$ | 20，7 | 26.7 | 25.1 | 259． | $2{ }^{4} 6$ | 25.5 | 214 | 28． | 24．7 | 24.9 | 䊽 2 | 262 | 27.9 | 279 | 㒭， 3 | 27．8 | 29.8 | 295 | 20．1 | 1 |
| 2.00 | 25.6 | 27.1 | 232 | 26.3 | $\underline{2517}$ | 35.5 | 26.9 | 21リ | $\underline{27} 7$ | 20.2 | 29.5 | 245 | 2 3 3 | 27.2 | 20.11 | S0） 1 | $3{ }^{-9}$ | 250 | 29， | 26.1 | 25.5 | 244 | 274 | 289 | 29A | 30.1 | 294 | ． 30.5 | W0， 3 | 29．9 | H |
| 300 | 276 | 29．11 | 2r．n． | 27.2 | 30， 2 | 270 | $\underline{2 H} G_{1}$ | 23， 3 | 24.1 | $310 \times$ | 30.1 | 24．4 | 31）， 1 | 210 | 26.11 | 31.5 | $2 \mathrm{k}, 2$ | 2ti．6 | 304 | 27.5 | 260 | 22ム | 2R， 6 | 30.0 | 2川．11 | 31．4 | 310 | 31.2 | ． 12 | 316．8 | 32．0 |
| ＋ $\mathrm{O}_{6}$ | 239 ${ }^{\text {a }}$ | 29.7 | 29， 2 | 27，${ }^{2}$ | 271 | 2H01 | 20．f． | 25.1 | 20,7 | 31.8 | 31.7 | 29.9 | 31.3 | －193 | 27．01 | 32．3 | 2 HR ． | 28. | 31，1t | $22^{6} 6$ | 273 | 22N | 2R．2 | 204 | 312． 3 | 3.318 | 32.2 | 121 | 320 | 31.9 | 128 |
| $5 . \mathrm{m}$ | W1 | 311，5 | 30.9 | 27， | $2+1$ | 2り） | 3116 | 26.8 | 273 | 32 K | 32.9 | 314 | 225 | 317. | 2811 | 330 | 214 | $\underline{29} 7$ | 31.6 | 297 | 2987 | 2711 | 27 K | 24n | ． 31.7 | 12.8 | 发 4 | 32 K | 32， B | 32 d | 336 |
| G．（1） | 31 f | 31.2 | 32.6 | 27.4 | 210 | \％ 3 S． 11 | ． 116 | 2R， 6 | 24．11 | 3.38 | 34．11 | 22．リ | 33 B | 37.11 | 32.16 | 33 k | औ｜，．11 | 31.3 | 32.2 | आ1k | आkil | 233 | 27.4 | 242 | 130 | 23，8 | 34，6 | 336 | 37.6 | 34.0 | 44 |
| 7－4，4 | 31．斤 | 315 | $3{ }^{2}-4$ | 27．6 | 242 | 3un 4 | 319 | 20，2 | 29］ | H5 | 347 | 335 | 342 | 3.3 .3 | 297 | 3.41 | 317 | 321 | 20R． | 2り ${ }^{\text {\％}}$ | 319 | 245 | $2{ }^{2} 11$ | 28.7 | 337 | 343 | 34.18 | 342 | 34.1 | 34.3 | 34.5 |
| R， $\mathrm{H}_{1}$ | 31.8 | 31.7 | 32 K | 27.7 | 274 | H0． 8 | ． 173 | $2{ }^{2} \mathrm{R}$ | 313， 1 | 35.1 | 355 | 340 | 340 | 4.3 | － 113 | 34.7 | 31.5 | 37 rl | 374 | 27.9 | 31.2 | 257 | 28． 7 | 29.2 | 24， 7 | $3{ }^{3} 6$ | 350 | 14.7 | 34.5 | 347 | 34．7 |
| 9 NL | 3211 | 32112 | 372 | 27．9 | $30 f_{1}$ | 31．2 | 32.6 | แ． 4 | 112 | 35 K | 142 | 346 | 35.11 | ． 35.17 | 310 | 152 | 3211 | 31,1 | 2511 | 2¢．） | 31\％ | 27，0 | 29.3 | 29.7 | 35，1） | 350 | 352 | 35.1 | 35.0 | 350 | 3.8 |
| ［1．1．1．1］ | 297 | ．31．1 | 32.5 | 2811 | 2\％5 | 317 | 31.1 | $2 川 .5$ | 31.3 | 319 | 17，7 | $3: 1$ | $3+4$ | 34， 3 | 311,3 | 547 | 2 k 4 | 33.3 | 25． 1 | ¹． 1 | 305 | 27，0 | 2川．1 | 29.3 | 34.1 | 344 | 345 | 349 | 345 | ． 747 | 5 |
| 11.4 | 275 | 313， 1. | 31.9 | $2 \mathrm{~s}, 1$ | 265 | 31.1. | 31.3 | 20.3 | 37.3 | 31．1） | 35，1 | 275 | 1.78 | 337 | $22^{2} .7$ | － 4.3 | 24 \＃ | 32．5 | 25.1 | 25.7 | 20．3 | 27.0 | 2094 | 20．f． | 33， 3 | 339 | 330 | 34.4 | 31.4 | 445 | 34．1 |
| 12．（x） | 25.7 | 38.2 | 31.2 | 2 L 2 | 244 | 29.6 | 31. | 278 | 314 | 31）．11 | 246 | 24.11 | 37.2 | 31，0 | 2911 | 338 | 212 | 124 | 25.2 | 25.4 | 2K，${ }^{\text {c }}$ ） | 270 | 28．斤 | $29 \%$ | 32.4 | 337 | 33.2 | 34.11 | I． | 34.2 | 338 |
| 13 CO | 25 （1） | 2 hf | 295 | 27.7 | 245 | 29.11 | 255 | $\underline{7711}$ | 31.7 | 29.1 | 333 | $\underline{23.7}$ | 27.4 | 315 | 285 | 32.9 | 21.7 | 11 亿 | 25 \％ | 25．7 | 279 | $26_{1} 7$ | 28.4 | 291 | 319 | 3.3 .5 | 323 | 7.8 | 12.9 | 35.4 | 3.11 |
| 1＋1010 | 24.7 | 28， 1 | 27.7 | 27.1 | $24!$ | 28.3 | 291 | $20_{1} 2$ | 3191 | $\stackrel{\text { ² }}{ } 1$ | 32.1 | 235 | 255 | 311.1 | 27．9 | 321 | 33.3 | ． 21.8 | 247 | 25， 1 | 27．1 | 26.3 | 23． 1 | 2k， 5 | 313 | 31.5 | 31.5 | 320 | 124 | 327 | 32.5 |
| 1500 | 245 | 275 | ？ 71.11 | 26．6 | 247 | $77^{7}$ | 28， 4 | 254 | 2 N 4 | 272 | 3 l H | 23，2 | 21.7 | 28.6 | 27.4 | 312 | 2マロ | 31， | 245 | 250 | 27.7 | 365 | 279 | 갠） | 41） R | 30． 4 | 30¢ | 31.6 | 31.9 | 11.4 | 3t， 8 |
| 16．0． | 34.0 | 27.3 | 2 ta 2 | 24.3 | 246 | 27.1 | －7．4 | 256 | 2R9 | 27.1 |  | － 411 | 22.5 | $2 \mathrm{sb}$. | 2゙ | 3115 | 22.9 | 2ท17 | $\underline{7} 4$ | 25.1 | 27.1 | $251]$ | 27， 6 | 279 | 364 | 30.3 | $3 \times 1$ | 3.15 | 3.3 .3 | ．11．4 | 31.3 |
| 17．0） | 2．3， 5 | 27.1 | 264 | $\underline{3} 1$ | 245 | $2(1.4$ | 279 | 25 स | 2R5 | 2 2.15 | 2919 | 248. | 23.2 | 2 L .1 | 26． 7 | 297 | 229 | 21） 5 | 241 | 253 | 2817 | 35.7 | 27.7 | $2{ }^{2} 9$ | 3010 | 29，$)^{2}$ | 297 | 20 | 3.106 | ．0．8 | 317 |
|  | 2311 | 2 CH | 266 | 25 R | 24． | $25 \%$ | 267 | $2{ }_{4} 11$ | 2H9 | 26.8 | 2） 5 | 25.4 | 24.11 | 2K， 2 | 26.4 | $\underline{38}$ | 2才，1） | 끼 2 | 2\％．R | 254 | 2 K 2 | 256 | 23.6 | 274 | 29 亿 | 3.4 | 2 l 2 | 294 | 31019 | ． 01.3 | H1 |
| リリオ！ | 230 | 2 t .4 | $2(1,4$ | 24 H | 271 | 35.4 | 212.4 | 259 | 2x， 11 | 260 | 20.3 | 25.7 | 2413 | 27，3 | 26.7 | 267 | 22.10 | 249 | 27 f | 25．7 | 2 kr 2 | 25.5 | 27.5 | 27.4 | 292 | 28．5 | 24） 1 | 27． 2 | 297 | 29.7 | 311.0 |
| 2014. | 230 | 25.5 | 2 C 2 | 21．is | 273 | 240 | 36.1 | 257 | 2811 | 269 | 20.2 | 257 | $\underline{24} 1$ | $2 r, 5$ | 261 | 243 | 226 | $2 \times .5$ | 235 | 25.1 | 2 k 2 | 234 | 27.5 | 27.4 | 285 | 77.7 | 2）！ | 2】．11 | 293 | 29.2 | 29.7 |
| 21 （4） | 2301 | 255 | 26.11 | 22：4 | 2ご | 245 | 25，k | 256 | 2816 | 2711 | 20， 14 | 258 | $2+4$ | 256 | 272 | 220 | 22.4 | 2 SK 2 | 231 | 35.11 | $2 \mathrm{~K}_{2}$ | 253 | 274 | 278 | 2 H 4 | is，$k$ | 24， 11 | 234 | $\underline{29} 0$ | 2HG | 27.5 |
| 㬵（0） | 24，${ }^{\text {a }}$ | 26,8 | 27.1 | 235 | 2411 | 25，1） | 20.6 | 23.1 | 2 3 | 27，6 | 24 | 267 | 25， 19 | 26.2 | 271 | 34.4 | 241 | 枵5 | 357 | 26.7 | 2¢ 4 | 2at | 27.7 | 278 | 37.9 | 2 $3^{19}$ | 281 | 27.7 | 28.0 | 27．） | 19.7 |
| 2300 | 36.9 | 28.2 | 283 | 24.3 | 25.2 | 25.5 | 274 | 26． 1 | 39,0 | 28.2 | 29.0 | 276 | 27.7 | $2 x^{1} 1$ | 27.1 | 26.8 | 3.7 | 289 | 37.1 | 275 | 296 | 27.5 | 27 ¢ | $\underline{27.8}$ | 27.5 | 27.1 | 270 | 26.5 | 270 | 27.1 | 9.8 |

## Hourly Dry Dulb Temperature（ ${ }^{\circ} \mathrm{C}$ ）


Year． 2005 Mior．he Jurs

| Day | 1 | 2 | 3 | 41 | 5 | 6 | 7 | H | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 15 | 2） | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fome |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 003 | 20，${ }^{2}$ | 2 J 5 | ？ | 2513 | $\underline{2}$ | 2611） | 2k， 2 | 281 | 21 |  | 21） | 래 5 | 29 | 27.5 | 27．11 | 292 | 27. | 21.2 | 2¢5．11 | 2R ${ }^{\text {R }}$ | 28．8 | 28 | 2 | 27 k | 27.1 | 27.2 | 200 | 25.4 | 30.1 | 26. |
| $1 \cdot(0)$ | 24） 9 | ．al． 3 | （1）． 1 | 26.3 | 23 H | 27.7 | $\underline{\sim}$ | 2 Cb | H16 | 29） | 29 H | 2113 | 316 | 20k | 2 fi 5 | 200 | $2 k$ | 312 | 259 | 297 | 72.5 |  | 2R．7 | 래9 | 27. | 27.8 | 26. | 35.5 | 26 | 26.7 |
| 2.10 | 313 | 312 | 31．2） | 27.7 | 24 | 2） | 3 | 21.2 | 31.7 | 31 | 319 | $31+11$ | 51.2 | 311 | $3{ }^{3}$ | 05 | 2 y | 31 t | 317 | \％1，5 | 310 | 302 | 29.3 | 29.9 | 28.5 | 24. | 7.5 | 25. |  |  |
| 3 Cl | 12 | 324 | 316 | 그） | 311.5 | ． 31.1 | 31 | 312 | 32 K | 12， | ไ1． | 312 | 32010 | 31. | 25 | 712 | \％ 1,6 | 32 t | ． 315 | 314 | 11. | 31 | 2） | 31 | 25． | 29 th | 2 s | 25 b | 27 | 274 |
| 4 CK | 32， | 12.1 | S2 | W） 2 | 31.1 | 31.5 | 32.2 | 319 | 337 | 3 31.15 | 125 | 311 | 11 | 32.1 | 26 | 2） | 313 | 12.5 | \＄214 | 32 t | 31．8 | ． $\mathrm{k}_{1} .3$ | 21） | 31.3 | 29.2 | 0 | 291 | 24 | 27 | 279 |
| $5 \% \mathrm{~h}$ | 33，5 | 3.3 .7 | Si．3 | 31.3 | 322 | 31.9 | 32.4 | 3－5 | 34r． | 4.41 | 3.5 | 13.1 | 310 | 32 | 272 | 280 | 32.1 | 34.6 | ． 32 | 327 | 32.7 | 293 | 21） | 31.7 | 29.1 |  | 28． |  | 271 |  |
| 60 m | 54 | 14.6 | H7 | 3.25 | $3.3,1$ | 12. | 331 | 37.2 | 35.5 | 352 | 14 | ． 342 | 29，1 | 31.10 | 2k | 31 | 32 R | 344 | 3312 | 3．1．4 | 3.1 | 2\％ | 29.1 | 320 | 29 | 320 | 29，9 | 26 |  | 1 |
| 7.01 | 345 | 352 | 34.9 | 32.7 | ． t ． $\mathrm{F}_{1}$ | 331 | 33.2 | 31 h | 34 | そ | 34.6 | ． 14.5 | 21） 3 | 32.5 | 근， | 20n | 37.11 | 346 | 33.1 | 31.5 | 37 | 28.4 | 293 | 3 3 ｜l1 | 29. | 313 | 23 | 36， 2 | 27.1 | 5 |
|  | 34.9 | ． 15.8 | 351 | 32，4 | 34． | 34，4 | 34.7 | 544 | $3+$ | 35.5 | 14 | 3. | ？ 7 | 33.5 | ．${ }^{1} 1$ | 27.3 | 4.33 | 14 | 33 | 370 | 34 | 239 | 29.5 | 27. | 2 F | 31.7 | 24. | 26. | 37. | 37.8 |
| 9.00 | 35. | \％ | 35.3 | 31.0 | ． 254 | 344 | 15 | 35 | 33. | ． 15. | 34，4 | 35 | 101 | 13 | 315 | 27．6 | t． 5 | 35.1 | 33，4 | 342 | 2 | 275 | 2y | 23 | $2 k$ | 30 | 28 | 2 h | 27.4 |  |
| $\underline{1+1 / 2)}$ | 34 | 35，6 | 34 h | 125 | 31 | 34.3 | 35.2 | 347 | 326 | 3.5 | 33．7： | $34+$ | 2r．斤斤 | 6， 6 | 314 | 27.5 | 33.1 | 34.4 | 321 | 13 | 33，4 | 28 | $2 \% .3$ | 26 | 29.2 | 2 | 27 | $2(0,4$ | 27.5 | 27.4 |
| 1］：내I | 341 | 34， K | 34.4 | ． 315 | 27 | 37 | 1 | 24 | 3 t | 34.5 | 22！ | 37 | 212 | 27．4． | 11 3 | 27.5 | 127 | 33.7 | 32.3 | 37 | 32.2 | 3 | 27. | 26. | 215 | $2{ }^{2} .2$ | 27.5 | 26．） | 27. | 273 |
| 12 1 Hf | 33. | 3，4．11 | 311 | ． 31 | 긋 | 37 | 34.3 | $3+$ | आ | 3.4 | 12 | 34 | 2.4 | 25，0 | 312 | 27 | 32.5 | 33.0 | 31 H | 13 | 31 | 24 | $\underline{2}$ | $\underline{77.2}$ | 2 l 成 | 29. | 27.2 | 273 | 27. | 27.5 |
| 1.3 （H） | そ27 | 37.1 | 33. | 31 | 2 \％．亿 | 32.5 | 31. | 345 | 111 | 312 | 313 | $\underline{29}$ | 3k | 252 | （！） | $2 \overline{7}$ | 317 | \＄2 3 | 31.2 | 32 | 3n， 1 | $2{ }^{2}$ | 23 | 27. | 21 | $2{ }^{2} 5$ | 36.9 | 27 | 27 | 37.1 |
| 14，$x_{1}$ ） | 31.15 | 323 | 32. | 3117 | 24 | 31 | 27. | 12\％ | 11 | 24． | 20， 5 | 51 | 2 k 2 | 25.5 | ${ }^{1} 1.5$ | 27 | 313 | 11.7 | 碞 | 31 | 31.7 | 2 k, | 2 n | 271 | 2\％5 | 2） 1 | $22_{1}$ | 26 | 27 | 270 |
| 1509 | 412 | 3 t | 31.7 | 29 | 25 | 311 | 24 | 12 | 29 | 37 | 20，4 | ． 3 | 27） | 25. | 21，2 | 23 | 3112． | 31， | 䓣 | 31. | 31） | 2 HC | 2 | 270 | 27 \％ | 2f | 2¢．13 | 26 | 2681 | $2 \mathrm{f}, \mathrm{B}$ |
| 16－（ H | 3 | 31.1 | 31 | 28.6 | 25 | 311 | $\underline{25}$ ？ | 31. | 297 |  | 24.6 | आ， | 27.7 | 25 | 311,0 | 27. | H2， | $\square$ | 2リR | \％｜k． | 31.3 | 2 C 5 | 24 | 27. | 27．7 | $2{ }^{2} 5$ | 2 k | 36.4 |  | 2 a .7 |
| －17 ing | 3 l | 31． 5.5 | 30 | 27.5 | 25. | 1112 | 35 | 11.1 | 吅 | 2r | 23） 4 | 3113 | $\underline{73}$ | 2r， | 2）R | 275 | 301 | ${ }^{7} 1.5$ | 21）．in | 3 | 2.9 | 2 CH | 28. | 37 | 27.6 | 2\％． 1 | 26. | 20.2 | 2 t ， | 24.7 |
| 18.10 | 20．1 | （U） | ท | 20 | 25 | 3010 | 2 C 2 | 314 | 2r．n | 29 | 292 | 31， 11 | 272 | 26 | 29. | 27. | W1， | H13 | 25 | 22. | 24， 6 | 382 | 2 | 27 | 275 | 27．8． | 262 | 2at | 266 | $\underline{4}$ |
| 1001 | 29. | 29. | $2 \pm$ | 76 | 25 | 2） 6 | 2ti． 1 | 31．2． | 29.5 | 29 | 24 | 290 | 27. | 20.4 | $\underline{7}$ | 27.5 | 293 | 3114 4 | 29.2 | 295 | 21.4 | 28. | 27. | 269 | 27．4 | 27.6 | 3 | 25.9 | 26 | 36.5 |
| 20.00 | 24. | $2{ }^{2} 6$ | 28， 7 | 24. | 25 | 292 | 26.1 | T13 2 | $2{ }^{2}$ | 24， | 뇨 | 2 y 21 | 26. | 2 亿． | 29 | 27 | 29.7 | 2） 7 | $\underline{2}$ | 21） 3 | $22^{2} .1$ | 232 | 27.9 | 267 | 27.3 | 27.4 | 259 | 25.7 | 26. | 26.5 |
| $\underline{2}$（ k ） | 29.6 | 21 | 部 | 26，2 | 258 | 2 HK | 76011 | （11）11） | 2） 1 | 293 | 246 | $29 \times$ | 268 | 7f1， 5 | 29.1 | 275 | 겐 6 | 29.4 | 284 | 그） $\mathrm{O}_{1}$ | 20． 9 | 282 | 27．${ }^{2}$ | 266 | 27.2 | 27．2 | 25．8． | 35.11 | 261 | 264 |
| 2n¢0， | 286 | 23，2 | 20.1 | 26.1 | 35.9 | 27．6 | 26.4 | 2\％． 2 | 28.5 | 293 | 27 4 | 2911 | 27.1 | 20.2 | 27 f | 27.1 | 2 4 6 | 2\％ R | 285 ． | 256 | 2H． 1 | 27 | 27 | 368 | 272 | 27 方 | 25.4 | 26.1 | 26.5 | 36.7 |
| 23くイス | 27.5 | 27.0 | 75.18 | 26 | 26.1 | 20.19 | 26：4 | $2{ }_{5} 4$ | 2 P .1 | 2ヶリ | 271 | 28.3 | 27.3 | $7 . .8$ | 262 | 20.8 | 276 | 282 | 2831 | 래 1 | 27.2 | 27.0 | 276 | 27.0 | 27.3 | 277 | 27.0 | 26.7 | 271 | 36.9 |

Hourly Dry Bulb Temperature（ ${ }^{\circ} \mathrm{C}$ ）
surce，Hargladesh Metrorolokical Departmeml，Cl：mare Divsion，Apargation，Dhaka
Year＇ 20015 M［crett．lulf

| D1\％ | 1 | 2 | 3 | 4 | 5 | 4 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0 | 26.5 | 25： | 247 | 2612 | 20,2 | 25. | 272 | 274 | 27，6 | 276 | 7 F （1．3） | 27.5 | 27.6 | 254 | 24．1 | 2 t 4 | 266 | 27．a | 2k 0 | 27.7 | 264 | 26.4 | 27.5 | 27.2 | $2{ }^{2} .31$ | 2R 0 | 27.6 | 27.2 | 27 | 2 | 28.0 |
| 1.100 | 27.3 | 262 | $\underline{2} 48$ | 26.2 | 25 \％ | 27.1 | 2ho | 2 x 5 | $\underline{2} 0$ | 27.7 | 76．⿺𠃊⿳亠丷厂犬 | 24．11 | 27.5 | 255 | 25.11 | 2719 | 27.6 | 28． 1 | 2R 7 | 2N， 4 | 27.3 | 364 | 27.9 | 27 B | 28.4 | 289 | 27.5 | 27.4 | 24 | 1 | ． 9 |
| 2.001 | 24.1 | 266 | 24. | 26.1 | 254 | 2R．t | 2 k | 가） 5 | 2R， 4 | 279 | $\underline{27.2}$ | 2 5 | 27．3 | 35.5 | 25.2 | 27.0 | 2H6 | 28.5 | 22.5 | 29 t | 24.1 | 36.5 | 2k，${ }^{\text {a }}$ | 24 | $2{ }^{2}$ | 20.7 | 275 | 24.4 | ， 0 | 28.1 |  |
| $\left.3 \cdot()^{\prime}\right)$ | 28， 9 | 27， 5 | 25.1 | 263 | 25.11 | 각 | 20.6 | 314 | 2hth | 2\％${ }^{1}$ | 27.7 | 2 c 1 1 | 27.3 | 256 | 254 | 2 S 2 | 20.6 | 291 | 312 | 2．） H | 313，4 | 265 | $\underline{2}$ | 29，0 | 310 | ． 1 | 27.4 | （1） | ． 7 | 29.8 |  |
| 4.00 | 27.4 | 273 | 25.1 | 26.8 | 25.3 | 314 | प्र1．4 | 31.0 | 29.7 | 2 C .4 | $\underline{7} 3$ | 23.9 | 272 | 25.2 | 25.4 | 28．9 | ओ 3 | 잔 5 | ओ，R | 31.5 | W，${ }^{3}$ | 27．7 | 296. | 312． 1. | 31.2 | 317 | 2 H | 29.7 | 30.4 | ．07 7 |  |
| $5 \cdot \mathrm{CHI}$ | 27， 1 | 275 | 257 | 271 | 26,3 | 31.3 | 312 | 316 | H1，7 | 28： | 2711 | 相 | 27.2 | 363 | 255 | 자．7 | 11.1 | 90） | 314 | 31.3 | 305 | 23，${ }^{\text {H }}$ | 30.6 | 31 | ＋1 8 |  | 29.4 | 30.5 |  | 31．6 |  |
| $6 \times 14$ | 2 k | 27.8 | 25.3 | 27.4 | 271 | 172 | 3211 | 522 | 31.4 | 29） 7 | 2f， 61 | 318 | 27.2 | 366 | 25.5 | 3114 | ， 11 \％ | 31，5 | 1211 | ． 32 | 31.6 | 3110 | 31.5 | 32.2 | 324 | 30.4 | 304 | 31.2 |  | 325 |  |
| 7 ？ 6 | 267 | 27.7 | 25.6 | 27．11 | $\underline{27}$ | 123 | ． 12.1 | 322 | 31） 7 | ¹： | 27．2 | 313 | 26.7 | 27.1 | 25 k | 3114 | 323 | 31,1 | 321 | 312 | 14.1 | 3124 | 31.4 | 32.5 | 32.3 | ，${ }^{\text {d }}$ | ， |  |  |  |  |
| $8(0)$ | 27.4 | －77，5 | 20.01 | 26， 7 | 2\％． 3 | 32 S | 22.3 | 12．27 | 297 | 3） 7 | 27，${ }^{2}$ | 41， 7 | 263 | 271 | 20，0） | 31 H | 129 | 31.5 | 32.3 | ※13 | 315 | U11\％ | 31. | 327 | 3 | 31.1 | \％ |  |  |  |  |
| 9.0 | 24．17 | 27 | $26_{3}$ | 36.3 | 24．11 | 122 6 | 72 | 32．： | 26s | 219 | 28.5 | 312 | 25．8 | 27 k | $2 ¢ 13$ | \＄1，11 | ． 3.3 | 3211 | 12.4 | 295 | 3211 | 112 | 31. | 33 | 322 | \＄1．2 | ． 332 | 320 |  |  |  |
| $1(5)$ | 28， 1 | 27.2 | 265 | 26． 8 | 28 H | 32.5 | 320 | 317 | 3） 2 | 2y！ | 245 | 23 | 25. | 275 | 36 | 31P．${ }^{2}$ | 32.5 | 1211 | $2 \cdot 2$ | $\underline{2}$ | 31．1． | 31．${ }^{2}$ | 31.2 | 32.6 | 324 | 309 | 32.1 | 317 | 32 | 31）． 2 |  |
| 11．0x | 24 | 270 | 260 | 27.4 | 247 | 32.3 | 32 K | 31.3 | 216 | 29 ¢ | $\underline{24} 4$ | 2） | 259 | 27.1 | 26.4 | 310 \％ | 31 K | 3211 | 32 19 | 2 n （1） | 31.6 | abs | 32 | 722 | 31． h | 317 | 71 | 31.5 | आ1．¢ | 310 | 1 |
| 12.01 | 2R | 7 C .4 | 368 | 272 | 2ris | 322 | 311 | 3 M K | 3111 | 引111 | 2K 4 | 30 | 200 | 76 ${ }^{\text {¢ }}$ | 36,5 | 307 | 311 | Y닌 | 31， 5 | 272 | 31.4 | 31） 2 | 312 | 71 ， | 31.6 | ．5） | 31 | 31.2 | 2川．2 | 31 | 32.0 |
| 13 cm | 277 | 267 | 21.4 | 27.7 | 2Fh | 11．5 | 31，8 | 31189 | 21．al | 295 | 28， | $2)$ | $\underline{3} 1$ | 36.7 | 26.5 | 297 | 3113 | 31.2 | 3 l | 27.3 | （1） H | 29.4 | 307 | 31.1 | 3． 1.1 | स1） | 20.7 | 31 H． | 29 | 30 | 313 |
| 17414 | 27.3 | 26.7 | 2011 | 274 | 774 | 30.8 | $\mathrm{j}_{1} \mathrm{f}_{6}$ | 25 | 29， 2 | 29. | 2 H | 래4） | 20.1 | 265 | 24.2 | 3x，4 | 29.7 | ． $\mathrm{H}_{1} 1$ | 3115 | 275 | 3017 | \％0．4 | ． 31.3 | प15 | 3）， | 20.6 | 215 | 31）． | 2. | 2 |  |
| 1500 | 26.8 | 206 | $25{ }_{4}$ | 27.2 | 27.1 | 311 | 29.4 | 292 | 3t．K． | 246 | 28 | 24．h | 26.2 | $2(1,4$ | 2¢0 | 23 | 29.11 | 20 | 21J． 4 | 27 （1） | 20.7 | 210 | 20， R | 22.4 | 29 | 20.2 | 24.2 | 30 | 29.1 | 292 |  |
| 1 HO | 26.7 | 26 | 25.5 | 23 | 26.7 | 2リ | $\underline{2}$ | $2 \mathrm{2}, 11$ | 246 | 2 x .5 | 2 2 $_{2}^{11}$ | 247 | 26.1 | 光 3 | 2 fi | 27.4 | 2h5 | 212 | 28 | 27 | ？ 2 ， 4 | $2 \mathrm{R} R$ | 的5 | 28， | 20 | 21 | 29.1 | 296 |  |  |  |
| 13 （1） | 2 Cl .5 | 266 | 25.5 | 26．${ }^{2}$ | 2 L 4 | 29.4 | 24 | 28.4 | 74 | 28， 3 | 2kII | $2^{4} 5$ | 2¢1 | $2{ }^{2}$ | $2(1.11$ | 27 | 2k， 7 | 2.8 | 27.1 | 27.2 | $\underline{13}$ | 24 | 29.1 | 23 | 3 | 28 | 220 | 22.2 |  |  |  |
| 18．14 | $2 \mathrm{ri}, 4$ | 246 | 254 | 268 | $20_{1} 0$ | 201 | $2{ }^{2}$ | 2 Bf | 282 | 2 R 2 | 2 X （t | 2k， 4 | 20.61 | 7 ¢ı．2 | 26．11 | 272 | 2 K 6 | 2ra 5 | 25.6 | 270 | 2 NR | 2\％， 5 | 28，${ }^{\text {4 }}$ | 27 | 212 | 22 |  |  |  |  |  |
| 1919 | 265 | $2 r_{1}+$ | 25.5 | 26.7 | 25.1 | 2 S 5 | $2{ }^{4} 5$ | 25.5 | 2511 | 231 | 27．9 | $2 \mathrm{R}, \mathrm{t}$ | 259 | 2¢11 | 2611 | 271 | 23 | 24. | 25. | $3 \times 19$ | 27.7 | 까 | 28 | 27 | 간 | 28．5 |  |  |  |  |  |
| 3），（h） | 26.5 | $2 \pi_{1} 1$ | 25.7 | 26.7 | 25．リ | 27.1 | 77.9 | 2K］ | $27 \times$ | 379 | 27．9 | 2 K | 25．9） | 25 K | 2611 | 36 D | 2K． 2 | $3 \times 3$ | 25.9 | $2 \mathrm{r}, 7$ | 2 L 5 | 242 | 27．4 | 26 | $\underline{2}$ | 28. |  |  |  |  |  |
| 31 l | 266 | 25．） | $\underline{59}$ | $2(0,6$ | 3 | 374 | 27.4 | 27.8 | 276 | 27， $\mathrm{R}^{\text {d }}$ | 27， H | 2 k 1 | 255 | 250 | 2 x 11 | 264 | 28 | 232 | 261） | $2{ }^{2} 16$. | 254 |  |  |  |  |  |  |  |  |  |  |
| $\underline{2300}$ | 27.1 | 27.11 | 361 | $2(1)$ | 26.3 | 27.3 | 27.4 | 27.7 | 272 | 275 | 27 \％ | 27.7 | 265 | 3 r | 265 | 26 \％ | 237 | 27 － | 2， 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 23．（\％） | 27.7 | 28，2 | 265 | 274 | 36.7 | 27.1 | 274 | 277 | 20.5 | 273 | 76.9 | 273 | 27.1 | 274 | 269 | 26.8 | 275 | 27 7 | 26.7 |  | 26.3 | 371 |  |  |  |  |  |  | 2 H | 2. | 28 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2 | 27 | 28 | 27. | 269 | 27. | $\underline{7}$ ， 5 | 27. | 28,3 | 28.1 | 28.5 |


| 96 | $8{ }^{\prime} / z$ | 6 F |  | ritz |  | Itz | Ls | 9 O | 1ZZ̄ | F9\％ | C52 | L－zz | 1＇sz | ¢ ¢ | ＋${ }^{\text {LIL }}$ | 5＇\％ | $16 \%$ | ¢ | L2 | 5\％ |  |  |  | Iiz | L\％ | ＇R2 | 412 | LLz |  | ＋4\％ |  |
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| 86 | ＋＇4c | Liz | RLi | 己くて | \＃2 | 12 | 5 | E＇ż | S 5 | L\％ | －̇̇ | ctz | 1 1＇S | Liz | ＋$\ddagger$ | 退 | 「ご | 18 | （iti | 6\％ | i， | s＇z | 12 | kiz | l＇z | ITE | 9：Z | pit | irkic | Fra | 人izz |
| Wh | $0, \mathrm{z}$ | 放 | ग\％ | 2\％ | \＃ 4 | －12 | 17， | 52 | 0\％ | U12 | ItL | ，$\overline{L \bar{L}}$ | ह14\％ | 1182 | ¢ $¢$ | \％${ }^{\text {a }}$ | （rise | $116 \bar{L}$ | ¢ kz | Hit | Utz | O¢z |  |  |  | 2 |  |  | \＃ri | （1） | wizz |
| 1＇62 | 2 行 | R88 | 2kz | 2i | S＇L | ILI | cis | LLC | ${ }^{11+2}$ | Tiz | Izz | LEL | ¢ ${ }^{2}$ | fiz | Ez | こく | ＂192 | 16 | $1 \times 2$ | 4 | －2 |  |  |  | 2 | 12 | ＋2 | 5 L̄ | 1\％\％ | 2 2代 | 0112 |
| Etiz | ＇tic | 佑 | ${ }^{6} \mathrm{Bz}$ | \＆it | 4 4 | I＇żz | risz | 92.2 | $1 \%$ | 2iz | をこ | 7 | 5，$\times 1$ |  |  |  |  |  | － | \％ | を＜ | 14\％ | 8 | 1192 | SL2 | ¢ $2 \overline{2}$ | SLI | 2 Lz | \％ | Liz | alve |
| \％＇6z | \％ | て＇id | $10^{\circ} 8$ | i 12 | 9\％ | ¢ $\bar{L}$ | प्र：c | $0 \times 2$ | $18 z$ | tiz | \％ | Tis | ： | －ut | 1 kc | 97 | $14 \%$ | ¢ 3 | $5 \geqslant 2$ | CLI | 522 | I 42 | $1 \cdot \underline{2}$ | ［\％ | ¢ | 2K | iz | Cz | L＇\＄2 | \％ | ${ }^{10161}$ |
| F＇6z | Liz | 5 \％ | \％ 8 | ＋ 2 | Ez | tiz | －ct | 14 L | व182 | riz | प＜z | 5 |  | bá | ＋$\times 2$ | ＂ 18 | 11 hi | d | \％${ }^{\text {c }}$ | 17 kc | ＊ 12 | z\％ | Fiz | 2 2 | צ： | ¢ Cz | Riz | N：t | वR | 1 Fmf | m81 |
| ¢ | Ciz | $66^{\circ}$ | sba | Ez | ciz | GLE | ¢＇\％ | 3 Hİ | BLZ | s 2 | St |  | 10\％ | こfil | ＇${ }^{2}$ | 4 $\overline{\bar{c}}$ | \％ | ） | ［ $\overline{\text { ¢ }}$ | \％ Hz | 912 | \％ | fri | LR | RLC | 1 | kii | 2＇\％ | ¢ | \％ | HHLL |
| b＇bc | （501\％ | p＇nt | \％ | 92 | 9 $2 \overline{2}$ | LEL | t＇sz | Fis | cz | s＇z |  |  | ${ }^{\prime \prime}$ | Stic | \％ | Hit | ki | 4 | 析 | 2 | LL | 5 kz | 5 RT | ＋${ }^{\text {che }}$ | ${ }^{12 \times 1}$ | \％ 8 \％ | Stz | \％${ }^{2}$ | Skù | ， $\mathrm{k}_{i}$ | ｜ki＇l |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | \％ | jkz | \％ F | （11／k | ${ }^{116} 6$ | 542 | ciz | गx\％ | $58 \stackrel{\rightharpoonup}{0}$ | ＋${ }^{2}$ | $14 \%$ | H 2 | प12 | ＂18 | cie | 18 | chis |
| $50{ }^{2}$ | 18 | bit | 2if | Ėً | ¢＇\＄8 | $z \bar{z}$ | R8\％ | 1082 | $\bar{z}$ | 92 | 11 ki |  |  | 家 | － 11 | ${ }^{6}$ | \％ | ¢12 | ＋ | ＂N1\％ | 13 1\％ | \％ | к＂ni | ${ }^{16}$ | CRz | ＇42 | rī̀ | \％ | － | \％ | （mict |
|  | Izt | ck | Izi | 162 | $9 \mathrm{a} \overline{\bar{c}}$ | $t{ }^{\text {a }}$ | 1／2 | GG | 24z | 6．27 | ：cz | 3 F |  | － | Tif | Pr | H12 | 2z， | ${ }^{9}$ | 4， $1 \times$ | ${ }^{9}$ | 5 | 176 | 6， | ，17\％ | \％ | zizu | （10） | 16 | \％ | $1 \mathrm{l}+\mathrm{C} 1$ |
| 208 | 5zE | at 1 | 2zi | 1iz | 1915 | ＂， | $5 \%$ | $6{ }^{\prime \prime}$ | t $\%$ | 2\％z | E＇tz | ，oiki | cus | 㲀 | ${ }^{\text {a }}$ | 2115 | 714 | \＆${ }_{\text {ct }}$ | que | $1{ }^{1}$ | L行 | 662 | \％ F | $6 \\|$ | R＇行 | $1{ }^{1}$ | ＋ | Lus | cte | （1¢ ¢ | （0， 1 |
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| s＇z |  | 726 | rait | 1\％ N | प्रIE | Gig | 5 位 | （＇1） | 4 C | 5 | ＇62 | \％ | ［iz | fir | 9 | 312 | Vit | Lit | （50） | F＇x： | \＆亿ü | 4 ¢ | 0x2 | ${ }^{\text {cizi }}$ | $\underline{L}$ | ITE | ¢＇凶 | †18 | t\％ | Et | 1968 |
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| 3ın！ | 31.5 | 0，7 | 20.0 | 304 | SO 4 | 314 | 31.51 | 282 | 2R，R | 27， 1 | $2{ }^{2} 3$ | 3118 | 2d 4 | 22．5 | 3106 | 316 | 310 | 31.11 | 3211 | 2R18． | 24.1 | － 29 | 21．3 | 20.1 | 2 d 2 | 2\％ 7 | 31．6． | 31.6 | 23.6 | 24．4 |
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| 8int | 2 nk | 32.5 | \＄1．9 | 314 | 261 | 344 | 25.0 | 125 | 314 | 31.9 | 316. | 325. | 123 | 12.3 | 344 | 34．1 | $3 ? 2$ | 1215 | 13 n | 25 年 | 317 | 28 | 新2 | 313 3 | 3112 | 321 | 525 | 301 | 2 R 6 | 26.7 |
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| J16，${ }^{\text {chi }}$ | 2x 4 | 315 | 31.5 | 如稆 | 27.9 | 1.14 | 25．7 | 32 4 | 31.9 | 31.7 | 11 R | 31.7 | 3112 | 313 | \％\％， 1 | 结》 | 323 | 322 | 32.5 | 24.9 | 3118 | 265 | 92， | 3102 | 리 5 | $31 \mathrm{t}_{1}$ | 31.4 | 28．7 | 21 | 34 R |
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| 120） | 29， $4_{1}$ | 1111 | ． 1.0 | 31.51 | 27．7 | 310） | 32,5 | 31.2 | いh | P115 | 311 | $\underline{99} 9$ | $22_{1,2}^{2}$ | 214 | 320 | 32 （1） | 31．］ | 14．1） | 르늬 | $\underline{24}$ | $2 \times 5$ | 26.4 | 277 | 21） 4 | 288 | 310 | 2） 1 ． | 290 | 292 | 23.1 |
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| 20.110 | 2k | $2{ }^{2} .2$ | 2k ${ }^{\text {a }}$ | 28 1 | 26.2 | 282 | 26.1 | $25 \%$ | 2 x 1 | 26， 3 | 267 | 2） 2 | 27.7 | 27.1 | 28， 11 | 27.4 | 293 | 285 | 28， | 26.2 | 27 1 | 3（1，） | 27.4 | $2(1.2)$ | 25.9 | 27.7 | 275 | 2311 | 27.7 | 25.4 |
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| 22.10 | 2：1 | 2681 | 235 | 20k |  | 266 | 257 | $2 \square_{1} 1$ | 27.2 | 2f， 11 | 2t．4 | $2 \square_{1} 7$ | 271 | 2 1,18 | 264 | 27 \％ | 2 h 1 | 27.6 | $26{ }_{2}$ | 253 | $\left.22_{2} 1\right)$ | 359 | 2611 | 25. | 244 | 2f， 1 | 20,3 | 26.4 | 26.6 | 25.1 |
| 23 （x） | 26.1 | 35.6 | 26.7 | 26 U | 262 | 25， 1 | 25.3 | 263 | 26．4 | 26.4 | 262 | 26.4 | 26.7 | 20.7 | 35.3 | 271 | 27.2 | 26.7 | 252 | 24，3 | 25.2 | 245 | 24.5 | 23.8 | 23.5 | 24.7 | 25.7 | 26.2 | 25.7 | 247 |


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| ZTE | を＇¢ | 1tí | É大 | Z＇IE | F\％ | 2115 | च\％ | F＇LE |  | ${ }^{6} \mathrm{ra}$ | t | ${ }^{\text {j k } 2}$ | 15 | 12 | 11 5 | 6 6\％ | $1{ }^{1}$ | If | ¢ze | त＇si | － | F！ | DK | Fis | $1{ }^{\text {c }}$ | （1）${ }^{\text {cit }}$ | 交 | FHz | ¢ | 5 | r＇s |
| Cric | jor | 6\％ | 促 | 1302 | － | D＇M | （is | $5 \cdot \mathrm{~L}$ | 5 C | O＇s | ＋ | ＋ $\mathrm{RL}^{2}$ | ¢＇\％ | ［＇K | \＄1E | Et | ir | \＆ 2 | Fat | $11 / 8$ | ¢ZC | －2\％ | L＂t | 518 | くた | S | L＇sz | ＇k | 5\％ | 56 | （6） 6 |
| EE | F1ヶ | Com | の＇y | F0y |  | S＇z | 85 | 8TE | 10 | 7＇c | 5 | £ ${ }_{\text {c }}$ | 1sis | 2\％ | 9 ¢t | ＋22 | Ti |  | 2is | $\bar{\square}$ | Zit | ＋ 26 | for | 吅 | Fil｜ | W\％ | F | ＋82 | \％ | － 5 | （mis） |
| Vivi | 0\％ | ¢0 | E＇K | ¢tic | 5 | （fidz | 5 | 2 亿 | 2 z | E＇si | 2 | ＋$\quad \bar{z}$ | 1182 | 218 | L＇r | Nă | 1 ¢ | 120 |  | T\％ | Lut | ＇18 | $\mathrm{c}^{\prime \prime}$ | \％${ }^{\text {a }}$ | L化 | b： | （iL | ＇sz | ＇sa | Csc | iniz |
| zaz | 右㑑 | G＇6 | CiLz | \＆${ }^{\text {Rz }}$ | ก゙ね | ［＇\％ | isc | 512 | \％\％ | $0^{\prime} 52$ | （rı | \％ | Uk | こ＇く的 | for | 10． | 2\％ | ！ | Elit | 5112 | ale | R＇K | $17{ }^{\text {a }}$ | \％14 | $1 / 2$ | \％ | ¢して | \％${ }^{\text {c }}$ | － | $\bar{\square}$ |  |
| \％＇sz | F＇zz | \％iz | 5 | E＇Lz | 䂭 | で砍 | ¢ +2 | $\mathrm{F}^{\prime} 12$ | F\％ | C．ja | －＂\％ | $\mathrm{C}^{\prime} \mathrm{FE}$ | 108C | 2 | ${ }^{11}$ | ¢ 12 | ¢ İ | \％ | ¢ | ＇！ | 5＇ld | 119 | 祏 | Uu | P＇sz | 1102 | tiz | L | \％ | 家 | D0＇t |
| LV2 | 12 | 6＇Z | （6）\％ | d | 6 | $L^{\prime} c z$ | $4 ヶ$ | 612 | 55 | ＇cr | 9 ¢ | \％ 12 | \＆ | 9＇2 | 0xit | ＋ | L | 682 | －sk | ＋ | is | \％ | C＇s | ¢ 0 | r\％ | \％ | 5 ग2 | L | － | 2 2 | We |
| ＇SI | $\mathrm{Cr}^{\text {cin }}$ | \＆ | ＋${ }^{2}$ | ${ }^{\prime} \mathrm{S}$ | ¢ 2 | Lit | 12 | ciz | tot | Crā | $5 ¢$ | 5 | 9 | $6 \%$ | 氏と | でK | ［＇tz | EL | ， | 2 | R＇iL | L | ¢ | 5 | E＇s | \％ | 65 | ¢ | ${ }^{\text {P }}$ | Eç | 01 |
| 92 | F\％ | L | \％ | 15 | ごに | Cz | て | 1它 | 45 | 12 | $t^{+}$\％ | だ々 | Sz | 5 | H＇\％ | 19 | 5 | － 2 | ＇\％ | 19 | $11 /$ | J 5 | ＋13 | 8＇ヶ | L＇sz | マ況 | \％¢ | K＇ș | t＋z | \％ 52 | M10 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | ${ }^{161}$ |
| İ | $0 ¢$ | 62 | ${ }_{4}$ | 12 | 2 | 52 | pz | iz | 2 | 17 | $\overline{\mathcal{L}}$ | 61 | ¢ 1 | 4 | 91 | ¢t | \＃ | £1 | I | II | 05 | 0 | R | $\checkmark$ | 9 | $\bigcirc$ | ¢ | \＆ | $\overline{\text { u }}$ | 1 | ${ }^{\text {Kig }}$［ |

## Hourly Dy Bulb Temperature（ ${ }^{\circ} \mathrm{C}$ ）


Year 2005 Monle Noveminter

| D | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8. | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | $11)$ | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| True |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | 220 | 21 | 23 | 21.8 | 21 | 2211 | 21 | 22 | 24.6 | 24. | 22 | 21 | 7.9 | LH | 188 | 12. | 9 h | 212 | ¢！ | 178 | 198 | 1 | 90 | 19.1 | 185 | （1） | R， 2 | 18 |  |  |
| 1 ¢ht | 23.4 | 23 | 24.2 | 22 | 231 | 27. | 23 | 23，5 | 250 | 24.7 | 235 | 230 | ［ N, | 21 | 21 | 21. | 22 | 21 | 1， 7 | 19.5 | 21 | 210 | 21,2 | 21.5 | 97 |  | \％， 6 | 9， |  |  |
| 2010 | 256 | 2512 | $25^{5}$ | 34. | 245 | 24. | $2+5$ | 24 | 20.6 | 24 | 2＋9 | 24 | 2 L, | 23 | 21 | 232 | 24 | 22 | 21.1 | 21. | 22 |  | 22. | 21．4 | 220 | $1{ }^{1}$ | 0.4 | 210 |  | 27 |
| tilki | 27. | 26. | 76 | 25 | 2rill | 26.1 | 26.1 | 25. | 27 | 25 | $2{ }^{2}$ | 25 | 24. | 25 h | 23 | 2¢10 | $2{ }^{2}$ | 24. |  |  | 23， 2 |  | 24 k | 23 |  | 15 | 21 | 22.2 |  |  |
| $4(x)$ | 3 | 23. | 27. | 26 | 27. | 271 | 27. | 20.3 | 24 | 3 | 27.1 | 20.3 | 25 | 2 t .3 | 26. | 23 | 27 | 254 | 24.7 | 24 | 245 | 24.9 | 25 R |  | 234 | 21， 2 | 216 | 276 |  |  |
| 5 | 24． 7 | 23． | 28， | 2 B | 28.3 | $2{ }^{4}$ | －R | 27. | 2y | 2.4 | 38 | 27. | 26. | 2 a ， | 37. | 2 x | 2 | 36 | 259 | 23 | 25 | 25.1 | 26，${ }^{\text {a }}$ | 25. | 346 | 220 | 29.2 | $23_{3} 1$ |  |  |
| Gun | 29.1 | $29)$ | 10， | 210 | 295 | 290 | 20．4 | 20， | 2\％ | 2 | 2.4 | 24 | 27.5 |  | 27. | 29 | 29 | 2 x | 27 | 2 | $25 \%$ | 25 | 27 | an | 25．R | 21.2 | 24＊ | 36.4 |  |  |
| 7 CHI | 29. | 29 | 31 | 20． | 2. | 21， 4 | 29. | 28.3 | 294 | 212.5 | 2） 3 | 2. | 27. | 27.5 | 27 | 2K | 21 | $2 \times 5$ | 27 | $2 r^{5}$ | 26 | 26 | 27 | 26. | 20.1 | 24.1 | 25.5 | 20.4 | 6， |  |
| 8.04 | 2 L | （1）1 | 311 | 30.3 | ． X, | 21.4 | 20 | 23．6 | 20.9 | 217 | 297 | 296 | 27. | 27.7 | 27.7 | $2 \mathrm{R}, 9$ | 21） | 2.4 | 27. | 27 | th． | 27.1 | 27. | 27 | 20.5 | 24 | 261 | 27.5 | 27.2 | 析 |
| ग．114 | 2 P 6 | 20，4 | $31+$ | 3 | 3116 |  | Will | 2 2 9 | 315 | 294 | \＃， 1 | 24.9 | 2k 1 | 27，k | 27 | 245 | 29.5 | $2 \mathrm{R}, \mathrm{R}$ | $27+$ | 27 | 27.2 | ${ }_{2}^{21}$ | 2 cok | 27. | 268 | 258 | 2 5,8 | 28.0 | 23.4 | ？ |
| 1414， 4 ） | 27．2 | 29. | 2！ | 2） | 21） 2 | 29 | 2 K | 2k | 2） | 28， | 2 | 27 | 35.5 | 2.5 | 763 | 27 | 27. | 24.2 | 25 ， | 2 Cl | 25.7 | 20,9 | 25 | 25，${ }^{\text {R }}$ | 25 | 249 | 25.2 | 242 | 26 |  |
| $11: 1$ | 2r． | 28．5 | 23 | 2 K | 27.1 | 3R， | 27. | 276 | 24.5 | 27 | $2 k$ | 2r， | 256 | 25.3 | 249 | 2t1 | 3 | 25 | $2+5$ | 25 | 24.5 | $25 \%$ | 24 | 24.2 | 24． | $2+1$ | 23.6 | 24.4 | 25.1 |  |
| 12－（x） | 36 | 27. | 27 | 27 | 265 |  | 20.8 |  | 27.1 | 2713 | 27.2 | 256 | 23 | 241 | 23，6 | $2+1$ | 241 | 23 | 2.1 | 23 | 22. | 24, | 232 | 2 r | 24，16 | 232 | 220 | 22.6 | 23.4 |  |
| 19 C | 2.7 | 2a， | 26. | 20.4 | 2611 | 26 | 25 | 245 | $2{ }^{2}$ | 3 | $2 \mathrm{r}, 5$ | 25 | 275 | 나2 | 23.1 | 23. | 23. | 22.3 | 22.1 | 23 | 22 | 23.2 | 229 | 22 | 230 | 22.3 | 215 | 225 | 23.3 |  |
| 14 cki | 25 | 26.1 | 25. | \％ | 25 | 25 | 24. | 2 ta | 258 | 25 ¢ | 25.7 | 24 | 21.5 | 22.4 | 22.7 | 23 | 23 | 21.4 | 22 |  | 22. | 22 | 225 | 22 | 22 | 21.3 | 201 | 215 | 22 |  |
| 15 ¢ 4 | 250 | 25. | 251 | 25 | 25. | 2511 | 21 | 256 | 34 | 25 | 251 | 24.11 | 2） | 21.6 | 22 | 2 | 22.4 | 21. | 228 | 2 t ． | 211 | 21.4 | 22 | 32.2 | 210 | 21. | 210.4 | 224 | －－ |  |
| f（ith） | 2 | 24 | 24 | 248 | 24 | 34.1 | 23.3 | 25 | 24 | 25.1 |  | 326 | ${ }^{x}$ | 21.3 | 21.1 | 22 | 21 K | 19 | 225 | 21. | 20. | 20 | 21.7 | 21.5 | 2leri | 21.1 |  | 218 | 21.6 |  |
| 17\％${ }^{\text {a }}$ | 23 ： | 24 | 24 |  | 23 |  | 23. | 25.3 | 24 | 25.1 | $2+1$ | 21 | 1 | 21. | 位 | 21. | 21.1 | 1 B | 22.1 | 21. | 2n！ | 21.5 | 21.1 | 2119 | 2012 | 19.7 |  | 21.1 | 21.1 |  |
| 叫 | 23.2 | 24 | 23. | 2414 | 23. | 22 | 234 | 25.2 | 24.4 | 25 | 23.5 | 119 | 192 | I11 | 21. | 21. | 3） | 1 L | $21 . \mathrm{K}$ | 21 | 2111 | 20,2 | 2116 | I212． | 19 | 19 | 210 | 20.5 | 215 |  |
| 19，00） | 22 | 23 k | 2i．2 | 23. | 2 | 231 | 21.2 | 25.1 | 24 | 24.7 | 23 | ty．4 | 1． 1 | 20. | 21.2 | 21. | $2{ }^{1} 5$ | 17. | 21 | 21. | 20.3 | 以成 | 211 | 20 | 19 | 19 | 20 | 21.1 | 20 |  |
| ， | 22 | 23， 7 | 22 | 233 | 22. | 22. | 27 | 251 | 2 | 24，3 | 22 | （189 | 1n， | 201） | 2 t | 21.1 | $3{ }^{3}$ | 173 | 12. | 3， | $\underline{9}$ | 切 | 210 | 197 | 19 | 18.9 | 라3 | 19 | 12 | 1） |
| 21.15 | 22 | 21 | 2211 | $23 n$ | 22 | 221 | 끄N | 251 | 24.4 | 2411 | 22. | 18.4 | 18.4 | 197 | 30，6 | 21. | 3 | 13.6 | 18 | 2. | 112 | 115 | 12 | 19. | 196 | t8 | 20.0 | 12. | 192 | 77. |
| 22 | 218 | 21. | 23.3 | 21 | 2117 | 219 | 211 | 21 | 21 | 211,7 | 195 | 136 | ［181 | 18.4 | Lh： | 19.4 | 19 | 178 | $1 \times$ | 19.1 | 1 R 1 | 1.7 | ！ 1. | 18.6 | 18.6 | 17 | in | 17.4 | 17 | 15 |
| 23： | 18. | 18.6 | 18 | 20 | 1 | 18. | 18 | $\mathrm{LB}_{3}$ | 17.7 | 17.5 | 16.1 | 168 | 17.3 | 17 | 14.5 | 17.8 | 176 | 185 | 17.7 | 173 | 15.7 | 20.0 | 197 | 17 | 17.7 | 109 | 10.4 | 15.4 | 152 | 14. |

Hourly Dry Bulb Temperature（ ${ }^{\circ} \mathrm{C}$ ）
Source＇Bargladesh Meteoroiogical Department，Climate Divisum，At siryapn．Dhaka
Yeqr 2005 Month．December

| D2y | 1 | 2 | 3 | 4 | 亏 | 6 | 7 | 8 | 9 | 10 | 11. | 12 | 13 | 14 | 15 | 10 | 17 | ${ }^{11}$ | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 2 t | 29 | 30 | 31 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0, | 16. | 15 | 17 | 112 | 17. | 16 | 17. | 151 | 144 | 12 | 14. | 10 | Lrta | 15.9 | 4. | 4 | 16,2 | 123 | 172 | 130 | $15+$ | 21，2 | 19.3 | （5） | 14， 7 | 50， | 46 | I | 13.2 | 2．B |  |
| （＇ch） | 18 | 14 | $1 \mathrm{k}, 7$ | 21.1 | 18 | 17 | 18.2 | 17. | 169 | 16.5 | ！ | 17 | 17. | 171 | $1 \mathrm{l} / 4$ | 18 | 17 | Il｜ | 18 L | 178 | 175 | 211, | 20.5 | 碞 | 179 | 10.7 | 16.2 | 159 | 15.1 |  |  |
| $2 . \mathrm{MI}$ | 21 | 21 | 21.5 | 21.7 | 18 | 15 | $\underline{1} 2.5$ | 19.7 | （1） 5 | 1， 1 | 18， | 1） | 10．6 | 1 k 2 | ！ 4 | n | LH | 21. | 20，4 | 199 | 125 | 21.1 | 21. | ［1 | 12.0 | 1. | 17.4 | 178 | 17.1 |  |  |
| ［171 | 23.4 | 23. | 22 | 31 | 19 | 211 | 20.7 | 22 | 220 | 21.2 | 212 | 211 | 1）t | 12. | 21） | 22 | 12 | 21.9 | 2211 | 2？ 1 | 1. | 21 | 220 | ？ 1 | 20.2 | 18 | 19.4 | 2011 | 190 |  |  |
| m） | 24. | 24 | 2 | 241 | 21.1 | 21， | 225 | 234 | 23.4 | 22 K | 22 | 22 | 21.5 | 21.4 | 22 | 24 | 21.7 | 2 | 23 | 23.4 | 233 | 22 | 279 | 22 | 21.5 | 12.2 | 21， 2 | 220 | 219 | 20 | 1.7 |
| （0） | 25.5 | 25 | 25.5 | 24.9 | 22.9 | 21 | 242 | 349 | 24.0 | － | 241 | 24 | 23 | 23 | 24 | 36. | 2.3 | 24 | 24 | 24.7 | $24+$ | 227 | 23. | 23 h | 220 | 21.7 | 22 | 24 | 22.7 | 23.10 |  |
| G（h） | 2ri． | 26,4 | 27.2 | ${ }^{5}$ | 24 | 23.5 | 20.0 | 26.3 | 3 （1．） | 2\％ | 25 | 25. | 25 | 35.3 | 27.1 | 27. | 2 L. | 37. | 26 | $25_{1}$ | 2 t | 23.2 | 24 R | 25.1 | 24.2 | 27.1 | 23. | 26.0 | 24 | 250 | 24.2 |
| 7．14） | 26 | 26 | 27.5 | 25. | 25. | 25 k | 26 | $2 r_{1}$ | 2 a | 162 | 25 | 26， 1 | 25. | 25 | $2{ }^{2} .5$ | 379 | 25.2 | 26 | 26.6 | 20.4 | 27.3 | 23.1 | 25. | 25 | 55.2 | 24. | 244 | 26 | 24.9 | 25.0 | 248 |
| R，（b） | $2{ }^{2}$ | 274 | 27. | 25.7 | 25 H | 26 | 26 | $2{ }^{2}$ | 265 | 26 | $2 ¢$ | $3 \times, 4$ | 25 ？ | 25 | 27. | $2 \mathrm{R}, 2$ | $2{ }_{2}$ | 36 | 27. | 2 C R | 27. | 22 | 25 | 25.8 | 24.2 | 24 | 25 | 36.5 | 25. | 250 | 54 |
| 2.01 | 27 | 27．3 | 2 R | 25.6 | 2 （t．） | 285 | $\underline{3}$ | $2{ }_{1}$ | 2 f | 2fick | $2 r_{1}$ | 2n，7 | 2 | 36 | 2k，4 | $2 \mathrm{~K}, 4$ | 26.8 | 21. | 27， | 27.7 | 2 M | 22.5 | 26.2 | 26.2 | 27. | 250 | 25 | 26.5. | 23.6 | 250 | 27.11 |
| 10109 | 25. | 2 l 1 | 3r， | 2－． 11 | $\pm 5$ | 24 | 245 | 2＋4 | －24．5 | 24 | 24 | 255 | 2511 | 24 | $2 r_{1} 5$ | 21.7 | 25. | 25 | 25 | 235 | 27 | 22.2 | 25. | 241 | 259 | 24 |  | 35.2 | 23 | 23，k | 24. |
| 11 （x） | 23 | $3+8$ | $\underline{257}$ | 24 | 21？ | 231 | 22.5 | 23. | 223 | 227 | $2 \pm 3$ | 24 | 27 | 22 | 24.5 | 24 | 24 | 25， | 2. | 23. | 26 | 21. | 2.1 | 23 | 24. | 230 | 231 | 21.7 | 21.7 | 227 | 27.3 |
| 1200 | 21 | 235 | 34 | 21 | 22. | 21. | 21.5 | 21 | 2ㅔㅔ | 216 | 21. | 27. | $22 \times$ | ${ }^{2}$ | 22 | 232 | 23. | 34 | 21. | 2 | 248 | 21 | 23 | 224 | 23 | 22 | 21.8 | $\underline{32}$ | 19 | 21.5 | 220 |
| 17 O | 21． | 22.6 | $2: 5$ | 27. | 2 t | 21. | 19 | 21 | 1） | 19，7 | 19. | 21. | 22 | $\pm 1$. | 224 | 2 | 234 | 210 | 21. | 21 | 23 | 21 | 22. | 21． | 222 | 21 |  | 21. | 184 | 2 | 21.4 |
| 14.1 | 21） | 21.6 | 23 | 22 | 24. | 21. | 197 | 12 | 191 | 18， | 185 | 21 | 21. | 211 | 22 | 21.3 | 2.52 | 212 | 208 | 2 | 22 | 21. | 21.3 | 2 | 211 | 22.3 | 20 | 20.3 | 17.9 | 19. | 21.21 |
| 15．00 | 20 | 211． | 22 | 22. | 21 | 21 | 1R | 18.2 | 18 | 18 | 17 f | 19，6 | 21 | $\underline{211}$ | 22 | $\times 1.3$ | 2t． 1 | 21 | Y， | 190 | 21 | 21. | 20 | 191） | 21. |  | 10 | 20.0 | 17 ll： | 12 l | 20.3 |
| 16.10 | 124 | 21）， | 21 | 21 | 2） | 21.7 | 18t | 17. | 1k1 | 17. | 171 | 19 | 311 | $1 \times$ | 21 | $1{ }^{10} 7$ | 22 | 215 | $1{ }^{1 / 5}$ | 18. | 211. | 219 | 12.2 | 19 | 12 | 2 | 120 | 19.5 | 16.4 | t4．12 | 19．3 |
| 17．0x | 1 1．s | 2. | 21. | 20.9 | 196 | 18.2 | 17.3 | 17. | 17 | 17 | 10.7 | 1 H | 12． | 17， | 2 t ． | 112 | 2 | 21.2 | 176 | 10，5 | 218. | 21 | 1 L | 19 | 11 | 1 | 18 | 188 | 15.9 | 18.7 |  |
| 18.00 | 18 | 21 | 21.2 | 20．2 | 192 | 12.2 | 16.5 | 16.8 | 14 | 13.5 | 1 fi | 180 | 183 | 16 | 211. | 18 | 219 | 21.0 | 17 K | 18.2 | 29,6 | $2 x_{1}$ | L 4 ！ | 19．h | 14. | 18 | 17．4 | 184 | 15.3 | 18.6 | 185 |
| 19．4．h） | 17．8 | 211 | 193 | $1{ }^{1}$ | 1 CR | 18. | 163 | 11 | 16．5 | 17 | 1.58 | 17.7 | 18．3， | L | 17.5 | 18 | 216 | 以12 | 17.5 | 178 | 21.7 | 211 | 18.1 | 19.4 | 183 | 17. | 16 | 17 | 14k | 17．9 | 17.9 |
| 23），00 | 17 | 11. | 1R7 | 10.5 | ${ }^{1}$ | 147 | 1 10，2 | （ 19 | 16， 9 | 17 ？ | 15.4 | 17 | 17 L | $\mathrm{t}_{6} \mathrm{~L} 2$ | 18． | 17 | 213 | 18.7 | 173 | 17.4 | 219 | 212． | 17．9 | 19 | 17 | 16.3 | 156 | 16.5 | 14．3 | 171 | 2 |
| 21， 181 | 171 | 19 | 18.0 | （1）． | 18.11 | $1 \mathrm{R}-$ | 1 fr, | 171 | 15 ： | 1719 | 15，11 | 1713 | $17+$ | 16，11） | 17 | 15， | 21．11 | 17 | 171） | 17.11 | 211 | 12. | 17 | 1 B | 17 | 16.1 | 136 | 15 | 17， | 16 |  |
| 23（ $x_{1}$ | 18.3 | 127 | 120 | －12．7 | 1211 | 12 | 1117 | 11.3 | 1 （1） | $1{ }^{1}$ 3 | 14111 | 11.3 | 126. | （11．7） | 11.5 | 1 t 2 | 1411 | 11，3 | 113 | It 3 | 141 | 13.2 | 119 | 12.4 | 11 | 10.1 | 91 | 10 | 9.2 | 10. | 1 |
| 23 （\％） | 57 | 6.3 | 6.0 | 63 | 6.0 | 6.1 | 53 | 5.7 | 53 | 5.7 | 50 | 571 | 5.51 | 53 | 57 | 56 | 30 | 5.2 | 5.7 | 5.71 | 70 | 6． 6 | 5， | 62 | 5.8 | 53 | 45 | 5.2 | 46 | 5.5 | 5.5 |

APPENDIX B：Hourly Dircet Solar Radiation in Watt／m ${ }^{2}$ Hourly Direct Solar Radiation in Watt／m ${ }^{2}$
Year 2005 Month：］anuary

| Day | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 1＋ | 15 | 19 | 17 | 18 | 19 | 30 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | $\underline{28}$ | 29 | 30 | 31 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tanse |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 500 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | d | 0 | 0 | $1)$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | ［ | 0 | 0 |
| 600） | 0 | 6 | 0 | 0 | 0 | D | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| 7.00 | 14 | 12 | 4 | $t$ | 7 | 15 | 16. | 14 | 15 | 14 | 1 | 4 | 8 | 14 | 11 | 12 | 13 | 15 | 16 | 18 | 21 | 23 | 25 | 28 | 30 | 32 | 33 | 32 | 2 | 4 | $\frac{5}{5}$ |
| 8：00 | 62 | 22 | 52 | 5 | 48 | 85 | 92. | 97 | 83 | 85 | 16 | 49 | 81 | 79 | 56 | 78 | 7 | 79 | B0 | 91 | 102 | 113 | 123 | 134 | 145 | 153 | 129 | 122 | 5 | 7 | 5 |
| 9：00 | 16， 5 | 34 | 119 | 13 | t，32 | 166， | 178 | 194 | 210 | 188 | 1 | 79 | 152 | ［ ${ }^{1}$ ］ | 54 | 197 | 154 | 110 | 67 | 107 | 146 | 186 | 226 | 265 | 30.5 | 312 | 273 | 167 | 8 | 17 | 72 |
| 10：00 | 290 | B8 | 195 | 2b | 218 | 24＋ | 254 | 245 | 347 | 307 | 2 | 395 | 215 | 300 | 142 | 285 | 204 | 122 | 41 | 96 | 152 | 208 | 264 | 320 | 375 | 378 | 293 | 158 | 113 | 89 | 53 |
| 1100 | 379 | 49 | 197 | 12， | 278 | 206 | 313 | 331 | 388 | 376 | 1 | $\underline{+57}$ | 24 | 366 | 204 | 327 | 260 | $19 ?$ | 125 | 178 | 231 | 284 | 337 | 390 | 443 | 339 | 371 | 114 | 96 | 75 | 56 |
| 12：00 | 3BB | 97 | 16.7 | 88 | 357 | 239 | 265 | 384 | 373 | 408 | 1 | 436 | 179 | 340 | 335 | 2 BO | $\underline{214}$ | 149 | 83 | 143 | 208 | 270 | 3，32 | 395 | 457 | 429 | 368 | 16＋ | 152 | 135 | 125 |
| 13.06 | 353 | 175 | 172 | 21 | 325 | （9） | 204 | 374 | 340 | 334 | 1 | 365 | 233 | 333 | 300 | 272 | 275 | 177 | 130 | 161 | 232 | 282 | 333 | 384 | 435 | 402 | 368 | $16+$ | 32 | 28 | $\underline{105}$ |
| 14.00 | 24］ | 152 | 106 | 34 | $\underline{294}$ | 140 | 212 | $\underline{75}$ | 233 | 250 | 1 | 285 | 28 | 236 | 191 | 1 AG | 168 | 150 | 1：2 | 163 | 194 | 22a | 25 | 288 |  |  | 171 | 101 | 72 | 51 | 37 |
| 1500 | 124 | 62 | 33 | 17 | 165 | 108 | 108 | 13¢ | 113 | 124 | 0 | 173 | 56 | 121 | 117 | 116 | 111 | 107 | 100 | 118 |  |  |  |  |  |  |  |  | 72 | 35 | 32 |
| 16．00 | 26 | 13 | ¢ | 3 | 46 | 25 | 28 | 24 | 27 | 23 | 0 | 43 | 17 | ？ 6 | 21 | 27 | 28 | 30 | 31 | 37 |  |  |  |  | 67 |  |  | 24 | $\underline{3}$ | 1， | 10 |
| 17：00 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 1 | 1 |  |  |  | 3 |  | 5. | 91 | 67 | 5. | 37 | 2 | 1 | 4 | 4 |
| 18：00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |  | 0 |  | 0 | \％ |  | 1 | 1 | 2 | 0 | 1 | 2 | 1 |
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| 7:00 | 65 | 62 | 3 | 5 | 42 | 37 | 26 | 4 | 14 | 23 | 14 | 3. | 74 | 108 | 71 | 64 | 58 | 12 | 3- | $5{ }^{7}$ | 91 | 6 | 56 | 2 | 77 | 11 | B' | 6 | 22 | 31 | 50 |
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| 9.90 | 399 | 410 | 378 | 38.5 | 301 | 321 | 118 | 17 | 302 | +33 | 22.1 | 4 | 483 | $\underline{+25}$ | 311 | 282 | 253 | 2 t | 408 | 195 | 230 | 165 | $4)$ | 4 | 68 | 133 | 250 | 97 | 85 | 11 | 131 |
| 10.00 | 526 | $5+4$ | 556 | 524 | 432 | 459 | 218 | 73 | 402 | 519 | 35 | 3 | 604 | 502 | 380 | 494 | 305 | 21 | 356 | 240 | 516 | 265 | 30 | 19 | 286 | 303 | 302 | 336 | 82 | 211 | 323 |
| 1t:00 | 577 | (6)5 | 652 | 620 | +7+ | 535 | +10 | 101 | 499 | 495 | $57^{\circ}$ | 8 | 701 | 533 | 479 | 479 | 478 | 29 | $\underline{206}$ | 3 ch | 611 | $t 10$ | 58 | 7 | 635 | 584 | 39] | 298 | 351 | 296 | 327 |
| 12.00 | 563 | 594 | 660 | 621 | 422) | 414 | 400 | 367 | 525 | 507 | $\underline{.7}$ | 28 | 6.7 | 533 | 525 | 512 | 495 | 143 | 293: | 447 | 620 | 171 | 66 | 6 | 493 | 623 | 416 | 267 | 92 | 348 | 253 |
| 13.00 | 527 | 509 | 607 | 536 | 404 | 415 | +61 | 363 | 517 | 565 | 20 | 16 | 396 | 302 | 482 | 459 | 360 | 70 | 148 | 493 | 582 | 391 | 1 | 65 | 570 | 593 | 434 | 268 | 273 | 173 | 141 |
| 1+40 | 429 | 364 | 461 | 402 | 302 | 313 | 376 | 2B! | +13 | 372 | 108 | 3 | 368 | 235 | 367 | 304 | $3+4$ | 227 | 49 | 431 | 449 | $\underline{298}$ | 9 | 45 | 5.39 | 200 | 296 | 268 | 240 | 176 | 209 |
| 15:00) | 321 | $\underline{216}$ | 307 | 266 | 180 | 187 | 219 | 122. | 2+3 | 171 | 77 | 1 | 226 | 101 | 237 | 263 | 232 | 36 | 52 | 27 | 243 | 67 | 1 | 1 | 351 | 186 | 23+ | 178 | 123 | 68 | 119 |
| 1690 | 132 | 79 | 127 | 116 | 73 | 64 | 54 | 46 | 58 | 34 | 19 | 0 | 76 | 2 | 93 | 115 | 91 | 32 | 37 | 119 | 63 | 68 | 1 | 1 | 173 | 42 | 90 | 60 | 3 | 9 | 38 |
| -1700 | 11 | 7 | 14 | 15 | 3 | 4 | 8. | 1 | 9 | 6 | 1 | 1 | 11 | 0 | 9 | 7 | 14 | 10 | 5 | 16 | 8 | 0 | 2 | 3 | 17 | 18 | 13 | 14 | 3 | 0 | 5 |
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Year 2005 Month: April

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| 7:00 | 70 | 89 | 123 | 126 | 90 | 119 | 14 | 68 | 9 | 97 | 11 | 6 | 88 | 69 | 51 | 32 | 25 | 117 | 56 | 8 | 141 | 59 | 7 | 12 | - 6 | 8 | 2 | 9. | 16 | 42 |
| 80 | 146 | $21^{7}$ | 283. | 333 | 237 | 146 | 103 | 177 | 6 | 48 | 96 | 31 | 282 | 333 | 185 | 137 | 126 | 243 | 10 | 60 | 285 | 83 |  | 10 | 10 | 5 | 1 | - | 32 | 223 |
| 9:00] | 252 | 373 | 484 | 511 | 321 | 156 | 287 | 250 | 225 | 291 | 267 | 213 | 463 | 416 | $4{ }^{4} 5$ | 482 | 371 | 34 B | 317 | 163 |  | 118 |  | 175 | 12 |  |  | 190 | 251 | 284 |
| 10:00 | 434 | 346 | 548 | 628 | 302 | 353 | 370 | 269 | 235 | 403 | 212 | 145 | 583 | $5 \mathrm{i}+$ | 44.4 | 375 | 535 | 457 | 371 |  |  |  |  |  | 1 | 8 | 386 | 196 | 143 | 271 |
| 11:00 | 358 | 388 | 564 | 650 | 49.7 | 3,54 | 510 | 423 | 101 | 316 | 315 | 392 | 674 | 503 | 562 |  |  |  |  |  |  |  |  | 237 | 405 | 337 | 504 | 382 | 342 | 50 |
| 12:00 | 157 | 61 | 598 | 574 | 530 | 436 | 624 | 469) | 4,36 | 365 | 375 | 452 | 593 | 547 | 5.7t | 455 | 02 | 249 |  |  |  |  |  | 503 | 40 | 432 | +63 | 252 | 329 | 287 |
| 13.00 | 109 | 78 | 377 | +40 | 50-4 | 517 | 596 | 376 | 421 | $40]$ | 23ㄱㄴ | 45, | 554 | 512 | 470 | 128 | 148 | 304 |  |  |  |  |  | $+10$ | 480 | $\underline{73}$ | 491 | 401 | 404 | 454 |
| 14:00 | $\underline{3}+7$ | 275 | 134 | 518 | 38.j | 3+7 | 3017 | 276 | 410 | 254 | 204 | 351 | +01 | 343 | 284 | 295 | 210 | 277 |  |  |  | 44 |  | 40 | 435 | 375 | 503 | 410 | 83 | 222 |
| 1500 | 170 | 221 | 169 | 359 | 기6 | 263 | 332 | 295 | 303 | 232 | 217 | 717 | 243 | 206 | 16 | 132 | 180 | 17 |  |  |  |  |  |  | 218 | -313 | 4 | 184 | 1 | 385 |
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Houtly Direct Solar Radiation in wath／m ${ }^{2}$

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Year 2005 Month：June

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| m |  | d |  |  |  | 筞家 | P－ | 15 | 令： |  |
| $\therefore$ |  | 7 | \％ |  |  | － | $8$ | $\frac{e_{1}}{c_{1}}$ | $9$ |  |
| －1 |  |  |  | $\stackrel{\square}{4}$ |  | 8 | 空気 | \％ | ${ }^{7}$ |  |
| 9 |  |  | 이 | 2 | ${ }^{2}$ | $17$ | $50$ | $\sqrt{2}$ | 事 | $\bigcirc$ |
| $\bigcirc$ | $-\cdots$ | 守 |  |  |  | 考 | 言管 | in | 二 |  |
| $\infty$ | $\cdots$ |  |  | 悪 | $\stackrel{7}{7}$ |  | 㝵商 | 南 | 헝 | ${ }^{7}$ |
| $\stackrel{\sim}{\sim}$ | 5. |  |  |  |  | 会枵 | 気阾 | ${ }^{\text {a }}$ | $\cdots$ |  |
| \| | P |  |  | $\cdots$ | $\bigcirc=$ | 二 ${ }^{\text {I }}$ | $\pm$－ | $\cdots$ | $\bigcirc$ | 7 |
| $\cdots$ | $\therefore \because$ | ＝ |  |  |  | $\mathrm{m}_{\mathrm{m}} \mathrm{n}$ | 成盛 | ${ }^{\text {c }}$ | － | $=$ |
| $\pm$ | $\square$ |  |  | 熍 | ${ }_{8 i}$ | $\stackrel{( }{\infty}$ |  | －7 | F |  |
| $\stackrel{m}{m}$ | \％ |  |  | ${ }^{-}$ | $\stackrel{i n}{7}$ | $\overline{i n}$ | ${ }_{3}{ }^{-1}$ | $\cdots$ | －${ }^{\text {a }}$ | $\cdots$ |
| t | － | 2 |  | + | $\mathrm{Cl}_{1} 9$ | 号 | 8 | 匀家 | 아웅 | $\bigcirc$ |
| $\cdots$ | S | O | $\stackrel{\sim}{2}$ | ＋ | $0$ | $\stackrel{F}{90}$ | －${ }_{1}{ }^{3}$ | 5 | ${ }^{2}$ | 3 |
| $\underline{7}$ | － | 河 |  | 風等 | 感家 | － | $\cdots$ | $\cdots$ | nc | ${ }^{\text {F }}$ |
| － | - 盛 |  |  | 웅 |  | 等葆 |  | 90 |  | $\bigcirc$ |
| $\infty$ | $0$ | 分 | 容苐 | 芯突 | 缡 | 0 |  | $x_{1}$ | 动包 | $\stackrel{\text { c }}{\sim}$ |
| $\cdots$ | 華\| | 5 | 5 | $\bigcirc$ | ${ }_{\sim}^{+}$ |  | 同 | 氛 | $\cdots$ | $\mathrm{Fic}^{\mathrm{F}}$ |
| 0 | $\stackrel{\rightharpoonup}{2}$ |  | $5$ |  | $\underset{\substack{\dot{n}}}{\stackrel{\rightharpoonup}{n}}$ | $3$ | 刺 | $\stackrel{\square}{\square}$ | 9 | ${ }^{301}$ |
| W | $\pi$ |  | 気会 | 令守 |  | $\cdots$ | A ${ }^{0}$ |  |  | $\pm$ |
| ＋ | A |  | C ${ }_{\text {c }}$ | 7\％ | 可声 | 执気 | 鱼 | ${ }^{\text {O }} 0$ | 0 m | $-0$ |
| 3 | － |  |  | 号吉 | 啶感 | 哈合 | 盛 | － |  | $\mathrm{Cl}^{-1}$ |
| －1 | $7$ |  | ${ }_{9}$ | ${ }_{-}^{1}$ | 号 | 产 | （ ${ }_{4}$ |  | 事 | $\mathrm{C}^{3}$ |
| － | － |  | 袁 | $\frac{7}{7}$ | 悊合 | 咢哭 | \％ | 気 |  | $\cdots$ |
| 合 | $\stackrel{8}{6}$ 웁 |  | 80. |  | $8$ | $3$ | $1$ | $$ | 家 웅 | $$ |

## Hourly Ditect Solar Radiation in watt/m $\mathbf{m}^{2}$


lear To0. 5 Nenth: luly

| Duy | 1 | 2 | 3 | 4 | 5 | 6. | 7 | 8 | ${ }^{4}$ | 16 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | $21)$ | 21 | 22 | 23 | 24 | 35 | $\underline{2}$ | 27 | 28 | 29 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 30 | 31 |
| $5-00$ | 0 | 0 | , | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:00 | 9 | 5 | 0 | 19 | 10 | 2 | 7 | 11 | T | 5 | 2 | 2 | 2 | 2 | ? | , | , | 0 | , |  | 1 | D | 0 | 0 | 1 | 0 | 0 | 0 | $t$ | 1 | 0 |
| 7:00 | 16 | 8 |  | 73 | 38 | 2 | 2 | 15 | 4 | 4 | 3 | 3 | + | 4 | 5 | 5 | 5 |  | - | 87 | , | 8 | , | 6 | 69 | 35 | 19 | 3 | 57 | $2+$ | 30 |
| 8:00 | 8 | 4 |  | , | 가늬 | 397 | 523 | 51 | 52 | 5 | 65 | 59 | 5,3 | 47 | 4 | 35 | 29 |  |  |  |  | 9 | 5 | 33 | $\underline{3}$ | 21 | 134 | 5.5 | 174 | 43 | 42 |
| 9.00 | +1 | 64 | 1 | 1 | 38 | 75 | 189 | $3+1$ | 35 | 5 | 26 | + ${ }^{\text {c }}$ | 53 | 58 | 6 | 69 | 75 |  | T |  | [17 | 9 | 76 | 5 | 416 | 336 | 226 | 117 | 237 | 288 | 177 |
| 10.00 | 34 | 18 | 0 | 12 | 5 | 455 | 216 | 422 | 154 | 11 | 18 | 25 | 1 | 2 | 1 | 12 | 17 |  |  |  |  | 168 | 313 | 45: | 602 | 63 | 152 | 241 | 180 | 110 | 8 |
| -1100 | 18 | 10 | 1 | 12 | 7 | 311 | 232 | 167 | 407 | 38 | 38 | 35 | 33 | 30 | 27 | 25 | 22 | 2 | A | 25 | 10 | 34 | 38 | 332 | ${ }^{\text {che }}$ | 334 | 62 | 333 | 128 | 242 | 279 |
| $12: 60$ | 44 | 35 | 4 | 23 | 17 | 188 | 578 | 533 | 57 | 14 | 11 | R | 5 | 2 | 16 | 30 | 4 | 58 | , |  | - | if: | 1.3 | 423 | . 14 | 25 | 113 | 104 | 70 | 112 | 205 |
| t3.00 | 42 | 64 | 7 | 7 | 25 | 287 | 486 | 224 | 0 | 27 | 24 | 20 | 16 | 12 | 4 | 7 | 1 | 15 | 2 | 12 | 32 | 101 | 169 | 316 | 463 | 416 | 369 | 25 | 186 | 164 | 239 |
| 14:00 | 10 | ? | 8 | 2 | 161 | 146 | 235 | 150 | 95 | 1 | 42 | 70 | 98 | 126 | 4 | 111 | 218 | 325 | 197 | - | 101 | - | \% | 28. | 371 | 307 | 24.2 | 322 | 46 H | 99 | 258 |
| 15:00 | 12 | 13 | 5 | 16 | 13 | 374 | 295 | 182 | 213 | 1 | 39 | 67 | 95 | 123 | 3 | 143 | 283 | 423 | 330 |  | 36 | - | 58 | 107 | 2 | 162 | 163 | 469 | 310 | 100 | 1+8 |
| 16.00 | 9 | 3 | 7 | 17 | + | 263 | 300 | 156 | 11 | 42 | 39 | 37 | 34 | 32 | 1 | 77 | 152 | 27 | 90 | 0 | $\underline{1}$ | 157 | 32 | 106 | 181 | 145 | 194 | 23.4 | 3.13 | 19-1 | 154 |
| 17:00 | 3 |  | 5 | \% | 3 | 05 | tt7 | 11 | 1i1 | B | 6 | 4 | 2 | 1 | 1 | 21 | 42 | $1 i 3$ | 55 | 0 | , |  |  | 0 | 35 | 13 | 24. | 56 | 6 | 105 | 108 |
| 18.00 | 0 | 0 | 1 | 6 | t | 6 | 8 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 |  | 0 | 0 | 0 |  | - | O | 4 | 5 | 40 | 3 | 40 | 23. | 4 |

Year 2005 Month: Augut

| Day | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 14 | 20 | 21 | 22 | 23 | 24 | 25 | 36 | 27 | 28 | 29 | 30 | 31 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 3 t |
| 5.00 | 1 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | , | 0 | () | 0 | 0 | 1 |  | 0 |  |  |
| 6:00 | 16 | 3 | 2 | 11 | 3 | 2. | 8 | 1 | 1 | 0 | 0 | 1 | 0 | 1. | 2 | 15 | 28 | 1 | 1 | 1 | 1 | 1 | 0 |  |  | 0 | 0 | 0 | 0 | O | 0 |
| 7:00 | 22 | 2 | 12 | 19 | 14 | 7 | $1(1)$ | 80 | 41 | 1 | 2 | 2 | 3 | 3 | 5 | 118 | 181 | 1 | 8 | f | 1 | 1 | , | 2 | 2 | 4 | 3. | 2 | 1 | 3 | 5 |
| 8:100 | 11 | + | 14 | 24 | 18 | 15 | 17 | 12 | 6 | 1 | t | 2 | 3 | 4 | 20 | 53 | 86 | 6 | 5 |  | 4 | 2 | 3 | + | 3 | 24 | 28 | 31 | 35 | 38. | 41 |
| 9.00 | 26 | 44 | 301 | 143 | 25 | 行 | 26 | 18 | , | 1. | 19 | 37 | 55 | 6 | 102 | 197 | 111 | 4 | 4 | 5 | 5 | 4 | 10 | 10 | 7 | 34 | 64 | 23 | 123 | 152) | 160 |
| 1000 | 316 | 353 | 89 | 106 | 72 | 158 | 30 | 21 | 12 | 2 | 3 B | 73 | 102) | 8 | 32 | 323 | $16+$ | 5 | ) | 1 | 19 | 6 | 11 | 6 | 9 | -108. | 121 | 134 | 27 | 69 | 111 |
| 11:00) | 299 | 392 | 56 | 45 | 164 | 72 | 75 | 51 | 27 | 3 | 73 | 1-4 | 215 | 26.7 | 284 | 354 | 376 | 10 | $3{ }^{2}$ | 32 | 20 | 3 | 9 | 15 | 10 | 128 | 199 | 270 | 67 | 42 | 158 |
| 1200 | 313 | 38B | 23 | $1]$ | 191 | 72 | 5 | 45 | 34 | 23. | 11 | 3.5 | 59 | 116 | 132 | 86 | 215 | 16 | 4 | 20 |  | 6. | 11 | 1.3 | 2 | 141 | 229 | 31. | 51 | t11. | 6 |
| 1300 | 417 | 576 | 346 | 173 | 129 | 59 | 29 | 23 | 16 | 10 | 17 | 22 | 26 | 180 | 4 | 54 | 342 | 1 | 102 | 60 | 24 | 87 | 43 | , | 12 | 135 | 243 | 352 | 2 | [83. | 6 |
| 1400 | 197 | 246 | 241 | 82 | 8 | 44 | 172 | 119 | 67 | 15 | 77 | 101 | 120 | 103 | 59 | 15 | 233 | 363 | 118 | 61 | 1 | 16 | 13 | 10 | 10 | 262 | 367 | 272 | 9 | 162 | 378 |
| 1500 | 110 | 65 | 231 | 1+2 | 3 | 22 | 110 | 83 | 56 | 29 | 171 | 165 | 150 | $5{ }^{\text {i }}$ | 49 | $4]$ | 333 | 354 | 65 | 41 | 16 | 176 | 10 | 10 | 17 | $2+6$ | 371 | 295 | 52 | 116 | 119 |
| 16:00 | 111 | 18 | 94 | 8 | 5 | 33 | 36 | 25 | 14 | 3 | 221 | 156 | 9 | 37 | 96 | 156 | 33 | 304 | 14 | 9 | 3 | 101 | 10 | 10 | 13 | 295 | 334 | 213 | 71 | 6 | 150 |
| $17 \cdot 00$ | 68 | 1 | 3 | $?$ | . | 5 | 1 | 1 | 1 | 1 | 58 | +0 | ? | 3 | 25 | 47 | 26 | 29 | 20 | 22 | 24 | - | , | 1 | 28 | 2 | 45 | 87 | 94 | 26 | 14 |
| 18:00 | 2 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 3 | 2 | 1 | 0 | 0 | 0. | 0 | 0 | j | 2 | 3 | 0 | 0 | 0 | 0 | 1 | ${ }^{6}$ | 12 | 12 | 2 | 0 |

Hourly Direct Solat Radiation in watt $/ \mathrm{m}^{2}$

| Day | 1 | $\underline{2}$ | 3 | 4 | 5 | 6 | ? | 8 | 9 | 10 | 11 | 12 | 13 | $1+$ | 15 | 16 | 17 | 18 | 19 | 20 | 2 t | 22 | 23 | 24 | 25 | 26 | 27 | 2 O | 29 | 30 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thne |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5:00 | 0. | 0 | 0 | 0. | 1. | $1)$ | 0 | 0 | 0 | (1) | 16. | 5 | 0 | 8 | 1 | c) | 1 | 1. | ט | 0 | 0 | 0 | 0 | 0 | 0 | 0 | (1) | 0 | 0 | 0 |
| 6:00 | 24 | 9 | 16 | 27 | 29 | 3.5 | 12. | 1 | 0 | $t$ | 0 | 14 | 0 | 5 | 0 | 5 | 1. | 64 | 20 | 2 | $?$ | 6 | , | 3 | 4 | 6 | 7 | 8 | 10 | 11 |
| 7:00 | 96 | 102. | 108 | 113 | 119 | 127 | 43 | 26 | 19 | 5 | 15 | 182 | 1 | 38 | 100 | 172 | 37 | 213 | 153. | 4 | 9 | 141 | 3 | 9 | 14 | 14 | 33 | 27 | 32 | 36 |
| 8:00 | 63 | 87 | 1(M) | 233 | 314'3 | 378 | 203 | 116 | 24 | 137 | 80 | 520 | 18 | 68 | 151 | 234 | 50 | 269 | 171 | 9 | 105 | 102 | 30 | 20 | 10 | 181 | 33 | 48 | 62 | 77 |
| 900 | 241 | 261 | 344 | 426: | 509 | 591 | 264 | 327. | 47 | 31 | - 5 ? | 625 | 101 | 293 | $\underline{+26}$ | 345 | 29. | 523 | +5,31 | 16 | 342 | 184 | 37 | 24 | 12 | 293 | 242 | 191 | 140 | 89 |
| 10:00 | 93 | 70 | 47 | 24 | 2 | 692 | 5 | 12 | 20 | 24 | 248 | $5+8$ | 216. | 178 | 566 | 372 | 147 | 4륵 | 근 | to | 415 | 73 | 165 | 94 | 24 | 348 | 247 | 224 | 202 | 179 |
| 11.00 | 2 | 2 | 2 | 2 | 2 | 658 | 1 | 312 | 36 | 314 | 161 | 010 | 406 | 25 | 574 | 57] | 136 | 478 | 108 | 3 | 251 . | 173 | 54 | 36 | 19 | 324 | 184 | 134 | 83 | 33 |
| 12:00 | 1. | 2 | $?$ | 3 | 4 | $62{ }^{2}$ | $d$ | 264 | 541 | 93 | 488 | 659 | 391 | 43 | 480 | 722 | 4 | 3433 | 3301 | 2 | 163 | 238 | 7 | $1+$ | 22 | 136 | 32 | 135 | 99 | 133 |
| 1300 | 1 | 3 | 4 | 3 | 3 | 172 | 1 | 363 | 398 | 94 | 503 | 343 | 138 | (6) | 291 | 586 | 301 | 418 | 46.1 | 7 | + 61 | 300 | 203 | 107 | 10 | 28 | 10\% | 92 | 83 | 75 |
| 14:00 | 2. | 4 | 5 | 7 | 7. | 124 | 1 | 344 | 371 | 1+0 | +69 | 136 | 121 | 181 | 318 | 3132 | 24 | 277 | 412 | 1 | 228 | 5 | 7 | 13 | 17 | 2 . | 122 | 88 | 55 | 22 |
| 15:00 | $+$ | 3. | 3 | 3 | 8 | 6 | 3 | 282 | 121) | $\underline{27}$ | 16 | Y5 | 23. | 61 | 192 | $2{ }^{2} 9$ | 25 | 368 | 2600 | 1 | 28. | 1 | 5 | 8 | 13 | 11 | 11 | 131 | 11 | 11 |
| 16:00 | 7 | 6 | 5 | 4 | 5 | 4 | 4 | 99 | 5. | 34 | 190 | 128 | $+$ | 3 | 59 | 149 | 28 | t ${ }_{\text {c }}$ | 126 | 1 | 82 | $t$ | 2 | 3 | 4 | 4 | 5 | 5 | 6 | 6 |
| 17.00 | 4 | 3 | $\underline{2}$ | 2 | 3 | 0 | 2 | 3 | 1 | 14 | 22 | 16 | 1 | 1 | 5 | 13 | 0 | 19 | 11 | 0 | 1 | d | 0 | 0 | 1 | 6 | 6 | 6 | 6 | 6 |
| 18:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0) | 0 | 0 | 0 | 0 |

[^7]| Dir | 1 | 2 | 3 | 4 | 3 | 6 | 7 | b | 9 | 10 | 11 | 12 | 13 | $1+$ | 15 | 16 | 17 | 16 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 'lime |  |  |  |  | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5\% 04 | 0 | 0. | 0 | 0 | 1 | 0 | 0 | (1) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | d | 0 | 0 | 0 | 0 | (1) | 0 | 0 |  |
| 6:001 | 8 | 4 | 1 | 4 | 7 | 10 | 13 | 16 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | (m) | 40 | 0 | 0 | 2 | , | , | , | , | 0 | 1 |
| 7:00 | 31 | 26 | 21 | 34 | 32 | 48 | 57 | 66 | 75 | 73. | 71 | 68 | 66 | 64 | 62 | 34 | 46 | 37 | 29 | 21 | 4 | 5 | 5 | 5 | 18 | 26 |  | 0 | 5 | 10 | 4 |
| 800 | 93 | 110 | 126 | 142 | 157 | 173 | 188 | 204 | 219 | 215 | 211 | $2(7)$ | 202 | 198 | $19+$ | 166 | 138 | 111 | 83 | 55 | 10 |  | 5 |  | 寿 | 20 | 13 | 1 | 29 | 52 | 78 |
| 90 k | 88 | 86. | 85 | 1.95 | 232 | 306 | 379 | +5.3 | 527 | 444 | 439 | 434 | 428 | 423 | 4 | 30 |  | 131 | 67 |  |  |  |  |  | 3.3 | 0 | 65 | 90 | 115 | 140 | 164 |
| 1000 | 1 | 4 | 169 | 239 | 309 |  | 448 | 518 | 588 | 194 | $2+5$ | 295 | $3+5$ | 396 | 446 | 233 | 175 |  |  |  |  |  |  |  |  | 349 | 25 | 63 | 101 | 1,39 | 177 |
| 11:00 | 1 | 2 | 41 | 100 | 160 | 219 | 278 | 337 | 396 | 12 | 187 | 247 | 3 ta | 368 | 420 |  |  |  | 5 | $\square$ | 0 | 2 | 3 | 269 | 335 | 46 | 157 | 172 | 185 | 201 | 215 |
| 12:00 | $6)$ | 5 | 1 | 26 | 52 | 77 | 102 | [28 | 12 | 337 | $3+5$ | 35 | 359 |  |  |  |  |  |  | 0 |  | 0 | 0 | 199 | 397. | 101 | 701 | 599 | 498 | 596 | 294 |
| 13.00 | 51 | 27 | 3 | $5 \%$ | 100 | 141 | 197 | 246 | 354 | 3 | 340 | 310 | 200 | 250 | 720 |  |  |  |  | 1 |  | 1. | 3 | 3 | 331 | 54 | K28: | 525 | 422 | 320 | 217 |
| 14.00 | 24 | 25 | 27 | 23 | 19 | 15 | 12 | B | 186 | 71 | 13 |  | 758 |  |  |  |  | 57 | 3 | ! | 1 | 0 | 1 | 2 | 32 | 167 | 482 | 401 | 321 | 240 | 159 |
| 15:00 | 9 | 7 | 4 | 8 | 12 | 16 | 20 | 24 | 151 | 94 | 1 | 13 | 15 |  | 3 C | 0 | '8 | 17 | 26 | $!$ | 1 | 0. | 2 | 21 | 232 | 134 | 316 | 317 | 319 | 321 | 322 |
| 1600 | + | 2 | 0 | 4 | 8 | 12 | 16 | 츼 | 36 | 17 | $2+$ | 37 |  | 18 |  |  |  | 1 | , | , | 1 | 0 | 1 | 116 | 36 | 98 | 143 | 151 | 159 | 167 | 174 |
| 1700 | 4 | 1 | 3 | ! | 6 | 7 | 9 | 10 | 1 | 0 |  |  |  |  | , |  | , | 12 | 0 | 0 | 1 | 1 | 2 | 15 | 9 | 6 | $\underline{13}$ | 25 | 27 | 29 | 31 |
| 1800 | () | 0 | 0 | 10 | d | 0 | 0 | 0 | (1) | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | 3 | 0 | 1 | 1 | 1 | 1 | 0 | 1. | $1)$ | 0 | 0 | 0 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  | - | 1 | 0 | 0 | 1. | 0 | 0 | 0 | 0 | 0 | 0 | [10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

## Hourfy Ditect Solar Radiation in watt／m ${ }^{2}$


Year 2005 MIonth：Nowerber

| Day | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 1.5 | 16 | 17 | 18 | 19 | 20 | 21 | 32 | 33 | 24 | 23 | 26 | 27 | 38 | 20 | 30 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T＊ッ¢ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1 |
| 5：00 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 4. | 0 | 0 | 0 | 0 | 0 | 0 | ） | 0 | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 600 | 19 | 16 | 24 | 36 | 40 | 39 | 26 | 23 | 20 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 13 | 10 | 1 | 2 | 8 | 5 | 2 | 2 | 1 | 3 | 5 | ， | 14 | 12 |
| 7：00 | ［17 | H2 | 140 | 181 | 169 | 108 | 154 | 140 | 126 | 112． | 112 | 112 | 112 | 12 | 112 | 112 | $9+$ | 75 | 56 | 38 | 35 | 2） | $\underline{2}$ | 27 | 21 | 38 | 56 | 74 | 4 | 17 |
| 8：00 | 189 | 278 | 312 | 356 | 391 | 356 | 319 | 321 | 304 | 288 | 280 | 286 | $2{ }^{26}$ | 286 | 286 | 296 | 245 | 204 | 163 | 122 | 101 | 81 | 60 | 77 | Bt | 30 | 9 | 8 | 7 | 278 |
| 9：40 | 215 | 447 | 488 | 524 | 573 | 573 | 528 | 503 | 477 | 472 | 452 | 452 | 45 ？ | 452 | 452 | 452 | 399 | 346 | 293 | 14 | 90 | 5.4 | 133 | 14 | 19 | d | 10 |  |  | $\cdots$ |
| 1000 | 230 | 569 | 607 | 6.336 | Gat | 6.54 | 630 | 605 | 581 | 556 | 556 | 556 | 576 | 550 | 556 | 556 | ＋34 | 312 | 1 cro | 195 | 123 | 52 |  |  |  |  | ， |  | 421 | 404 |
| 11：00 | 193 | 652 | 055 | 695 | 69 근 | 67.3 | 633 | 594 | 554 | 515 | 515 | 515 | 515 | 515 | 515 | 515 | 430 |  |  |  |  |  |  |  |  |  | 438 | 4 4 | $5+3$ | 498 |
| 12：00 | 114 | 533 | 600 | 652 | 541 | 428 | 388 | 342 | 310 | 271 | 229 | 186 | $1+4$ | 10 | 59 |  |  |  |  |  |  | 38 | 223 | 137 | 257 | 377 | 497 | 486 | 601 | 380 |
| 13：00 | 78 | 121 | 520 | 316 | 495 | ＋5＋ | ＋24 | 395 | 365 | 335 | 307 | 279 | 251 | 223 | 195 | 335 |  | －-9 |  | 141 | 12t | 96 | 463 | 108 | 248 | 3 B 7 | 527 | 404 | 506 | 323 |
| t $4: 00$ | 24 | 280 | 312 | 344 | 344 | 312 | 236 | 200 | 144 | BB | 28 | 10 B | 1 | 12 | 130 | 120 | 113 | 101 | ， |  | 160 | 191 | 114 | 25 | 16.4 | 303 | ＋42 | 278 | 381 | 331 |
| 15：00 | 3 | 119 | 133 | 147 | 157 | 210 | 166 | 121 | 77 | 33 | 33 | 3.4 | 34 | $3+$ | 35 |  |  |  |  | ， | 102 | 108 | 71 | 58 | 134 | 210 | 286 | 210 | 211 | 209 |
| 16.00 | 1 | 17 | 17 | 24 | 26 | 22 | 17 | 12 | 7 | 2 | 4 | 5 | 7 | 8 | 10 |  |  |  | 3 | 30 | 32 | 23 | 18 | 19 | 35 | 91 | 126 | 92 | 96 | 83 |
| 1700 | （ | 0 | 1 | 0 | 0 | 0 | U | 0 | 0 | 1 | 0 | 0 | （1） | 0 |  | 8 |  | 4 | $-$ | 4 | ＋ | 3 | 2 | 2 | 3 | 8 | 11 | 8 | to | 8 |
| 1800 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | （1） | O | ， | 0 | 0 | － | d | 0 | 0 | 0 | 1 | 2 | （1） | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 0 | 0 | v | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Year 2005 Month：Deceribur

| D3y | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 1 B | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 24 | 27 | 28 | 29 | 30 | 31 |
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| 5－00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $1)$ | 0 | 0 | d | 0 | 0 | 0 | 0 |  |  |  |  |
| 6：00 | 4 | 7 | 9 | 11. | 13 | 15 | 17 | 19 | 17 | 14 | 12 | 10 | 7 | 5 | 5 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | $\square$ | 0 | 0 | 0 | 0 | 0 | 0 |
| 704 | 35 | 73 | R6 | 28 | 110． | 122 | 135 | $14{ }^{-}$ | 138 | 128 | 112 | 110 | 1 tat | 91. | 56 | 106 | 4 | 3 | 3 | 4 |  | 5 | 14 |  |  | 1 | 1 | 2 | 1 | 1 | 0 |
| $8: 007$ | 163 | 122 | 2145 | 215 | 237 | 238 | 250 | 361 | 257 | 253 | 248 | $2+4$ | 2391 | 235 | 218 | 241 | 23 | 16 | 38 | 61 | 5 | 3 | 4 | 2 | 3.3 | 42 | 52 | 61 | 29 | 24 | 19 |
| 9：00） | 272 | 333 | 335 | 338 | 341 | 343 | 346 | 3.46 | 354 | 360 | 36.5 | 371 | 377 | 3 B 3 | $+23$ | 303 | 26 | 147 | 167 | 61 | R3 | 106 | 11.9 | 132 | 145 | 159 | 172 | 185 | 94 | 83 | 72 |
| 10.00 | 377 | 407 | 411 | 416 | 420 | 425 | 429 | 43.4 | 434 | 433 | 433 | 433. | ＋32 | 432 | 472 | $+13$ | 62 | 110 | 158 | 析 |  |  |  | 205 | 278 | 290 | 302 | 314 | 185 | 178 | 172 |
| 1100 | 400 | 345 | 352 | 360 | 368 | 375 | 38.3 | 3.91 | 347 | 404 | ＋11 | 418 | 424 | 431 | 412 | 329 | 5 | 55 | 17 | 25 |  | 311 | 1 |  |  | 372 | 389 | 407 | 263 | 272 | 281 |
| 12：00 | 426 | 350 | 312 | 274 | 236 | 198 | 100 | 122 | 173 | 233 | 289 | 344 | $4(10)$ | 453 | भf | $38+$ | 24 | 9 | 174 |  |  |  | 4 | 391 | 379 | 368 | 356 | 345 | 226 | 277 | 128 |
| 13：0） | 314 | 280 | 370 | 200 | 250 | 240 | 2.0 | 220 | 237 | 275 | 272 | 284 | $30 \times 3$ | 323 | 278 | $1 \mathrm{R}^{2}$ | 00 |  |  |  |  |  |  |  | 324 | 333 | 341 | 350 | 260 | 303 | 345 |
| 1490 | 166 | $23+$ | 215 | 195 | 176 | 156 | 137 | 117 | 132 | 146 | $16 t$ | 176 | $19 t$ | 205 | 126 | 161 | 48 | 2 | 136 |  |  |  | 189 | 267 | 225 | 243 | 261 | 280 | 298 | 316 | 335 |
| 1500 | 7 | 126 | 114 | 95 | 79 | 64 | 48 | 32 | ＋1 | 49 | 57 | 65 | 73 | 82 | 47 | 96 | 11 | 4 | 13 |  | 224 | 26 | 263 | 257 | 251 | 246 | 240 | 234 | 236 | 238 | 23.1 |
| 16.00 | 7 | 15 | 13 | 11 | 10 | 8 | 6 | $+$ | 3 | 5 | 6 | 6 | 7 | 8 | 4 | 1.1 | 2 | 20 | 31 | $\overline{5}$ | 7 |  | 160 | 153. | 146 | 139 | 133 | 136 | 125 | 123 | 124 |
| ［7：00 | 0 | 0 | 0 | 1 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 6 | 17 | 13 | \％ | ， | Bt | 68 | 55 | 41 | 28 | 15 | 18 | 20 | 23 |
| 18：00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | d | 0 | 0 | 1 | 18 | 24 | 30 | 25 | 20 | 15. | 10. | 5 | 0 | 0 | 0 | 0 |
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APPENDIX C：Hourly Diffuse Solar Radiation in $W$ att $/ \mathrm{m}^{2}$ Hourly Difinse Solar Radiation in watt $/ \mathrm{m}^{2}$
Fear 2005 Mionth fanuary

| Day | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 2 t | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 3 t |
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| 5：00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| 6：00 | 4 | 3 | 4 | 3 | 3 | 3 | 3 | 4 | 3 | 3 | 3 | 4 | 4 | 3 | 5 | 5 | 5 | 3 | $j$ | 5 | 5 | 5 | 4 | 4 | 4 | 4 | 5 | 4 | 5 | 5 | 4 |
| 7：00 | 50 | 45 | 3.2 | 30 | 54 | 55 | 55 | 54 | 54 | 55 | 29 | 42 | 58 | 55 | 81 | 57 | 56 | 56 | 55 | 55 | 5.5 | 55 | 54 | 54 | 54 | 54 | 63 | 64 | 57 | 54 | 53 |
| 8：00 | 112 | 99 | 126 | 103 | 130 | 129 | 127 | 136 | 129 | 127 | 135 | 137 | 139 | 134 | 150 | 129 | 136 | 132 | 133 | 130 | 128 | 125 | 122 | 120 | 117 | 112 | 134 | 159 | 150 | 152 | 157 |
| 9.00 | 166 | 95 | 181 | 164 | 194 | 190 | 18． | 183 | 185 | 185 | 136 | 172 | 307 | 195 | $\underline{24}$ | 187 | 195 | 203 | 211 | 202 | 192 | 183 | 173 | 164 | 154 | 149 | 194 | 247 | 23 | 244 | 257 |
| 10．00 | 193 | 168 | 241 | 222 | 240 | 226 | 223 | 279 | 202 | 210 | 110 | 206 | 269 | 219 | 269 | 217 | 24 | 271 | 299 | 289 | 279 | 269 | 259 | 249 | 239 | 212 | 260 | 309 | 291 | 269 | 244 |
| 11：00 | 200 | 183 | 251 | 362 | 256 | 250 | 246 | $2+0$ | 226 | 224 | 107 | 214 | 310 | 236 | 330 | 244 | 289 | 333 | 378 | 356 | 335 | 313 | 292 | 270 | 249 | 288 | 320 | 331 | 334 | 339 | 343 |
| 12－00 | 198 | 176 | 249 | 297 | 235 | 268 | 274 | 29 | 232 | 221 | 7 | 234 | 3106 | 252 | 257 | 259 | 293 | 3－15 | 300 | $3+0$ | 320 | 300 | 2 BO | 260 | 240 | 236 | 317 | 347 | 365 | 387 | 401 |
| 13：00 | 184 | 220 | 340 | 237 | 21.1 | 270 | 243 | 202 | 220 | 214 | （i） | 215 | 290 | 222 | 229 | 260 | 382 | 305 | 327 | 317 | 287 | 366 | 246 | 226 | 206 | 228 | 271 | 336 | 303 | 262 | 217 |
| 14：00 | 152 | 186 | 193 | 223 | 137 | 209 | 191 | 180 | 195 | 178 | 6.2 | 177 | 208 | 193 | 206 | $\underline{12}$ | 233 | 233 | $27+$ | 259 | 24 | 231 | 216 | 202 | 188 | 199 | 287 | 282 | 26.8 | 243 | 219 |
| 15：00 | 108 <br> 51 | $\frac{12}{50}$ | 107 | 138 | 120 | 134 |  | 134 | 140 | 126 | 48 | $12{ }^{1 / 2}$ | 138 | 140 | 144 | $t 53$ | 174 | 195 | 236 | 203 | 190 | 177 | 165 | 152 | 139 | 153 | 200 | 164 | 142 | 124 | 103 |
| 17：00 | 51 | 5 | ＋ | 5 | 5 | 5 | 62 | $\frac{64}{6}$ | 67 | 61 | 47 | 6） 1 | 73 | 69 | 6t | 61 | 65 | 64 | 6ut | 69 | 72 | 75 | 78 | 81 | 83 | 86 | 111 | 50 | 53 | 57 | 62 |
| 18.00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | \％ | 9 | 11. | 13 | 15 | 18 | 1.5 | 16 | 5 | 6 | 7 | 8 |


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Hourly Diffuse Solar Radiation in watt $/ \mathrm{m}^{2}$

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| 6：00 | 16 | 19 | 10 | 17 | 18 | 18 | 22 | 10. | 21 | 31 | 32 | 33 | 25 | 20 | 21 | 30 | 43 | 31 | 31 | 32 | 40. | 29 | 50 | 15 | 42 | 29） | 45 | 29 | 49 | 49 | 50 |
| 7：00 | 88 | 99 | d 4 | 40 | $10 t$ | 100 | 11.5 | 61 | 86 | 112 | 84 | 55 | 109 | 100 | 103 | 115 | 126 | 139 | 123 | 106 | 127 | 120 | 140 | 35 | 136 | 117 | 145 | 124 | 134 | 137 | 133 |
| R：C0 | 135 | $14^{7}$ | 201 | 132 | 193 | 193 | $21 ?$ | 96 | 116 | 136 | 122 | 109 | 151 | （6） | 161 | 191 | 222 | $2 \mathrm{~B}+$ | 239 | 194 | 204 | 252 | 188 | 102 | 339 | 159 | 241 | 2.57 | 243 | 201 | 19 |
| 900 | 162 | 167 | 191 | 161 | 230 | 203 | 306. | 200 | 273 | 165 | $14+$ | 122 | 1 14 | 205 | 214 | 265 | 315 | 281 | 271 | 330 | 318 | 303 | 280 | 113 | 220 | 280 | 332 | 312 | 317 | 268 | 250 |
| 10006 | 176 | 182 | 172 | 175 | 239 | 217 | 376 | 319 | 300 | 213 | 38. | i0 | 173 | 294 | 257 | 269 | 352 | 236 | 30.3 | 350 | 259 | 372 | 279 | 312 | 2 Ch | 360 | 370 | 364 | 324 | 447 | 38 |
| 11：00 | 207 | 198 | 164 | 178 | 266 | 233 | 386 | 311 | 302 | 267 | 430 | 216 | 175 | 277 | 260 | 314 | 338 | 296 | 340 | 383 | 238 | 363 | 270 | 176 | 310 | 314 | 351 | 417 | 439 | 464 | 409 |
| 12：00 | 220 | 208 | 162 | 180 | 294 | 316 | 337 | 3.40 | 289 | 250 | 363 | 351 | 192 | 245 | 252 | 327 | 341 | 401 | 416 | 337 | $2 \ddagger 3$ | 317 | $\underline{59}$ | 199 | 312 | $\underline{3}+9$ | 367 | 405 | 435 | 449 | 309 |
| 13：00 | 198 | $\underline{214}$ | 162 | 180 | 266 | 271 | 276 | 340 | 252 | t83 | 273 | 274 | 200 | 278 | 243 | 293 | 406 | 277 | 345 | 273 | 217 | 349 | 34 | 352 | 222 | 240 | 33 | 367 | 424 | 39\％ | 350 |
| 15．00 | 133 | 16B | 136 | 135 | 184 | 169 | 181 | $\underline{194}$ | 213 | $\underline{196}$ | $\underline{248}$ | 35 | 192 | 294 | 23 | 26 | 320 | 383 | 242 | 229 | 1918 | 31.3 | 123 | 282 | 183 | 2 t （ ${ }^{\text {a }}$ | 297 | 315 | 333 | 333 | 317 |
| 16.00 | 97 | 10.4 | 97 | 91 | 108 | 102 | 127 | 125 | 121 | 122 | 136 | 36 | 133 | 20 | 161 | 111 | 134 | 177 | 132 | 121 | 109 |  | 69 | 27 | 155 | － | $\underline{23}$ | 237 | （1） | 4 | 37 |
| 17：00 | 32 | 28 | 32 | 26 | 30 | 28 | 45 | 30 | 40 | 41 | 37 | 25 | 34 | 12 | 55 | 34 | 45 | $4{ }^{4}$ | 48 | 39 | 42 | 16 | 28 | 39 | 46 | 59 | 46 | 50 | 46 | 51 | 2 |
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Hourly Difiuse Solar Radiation in watt $/ \mathrm{m}^{2}$

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| 0 | F－ | 8 | $\mathrm{Si}_{1}$ | 号 | 品 | 家 | 露 |  |  | 客 | $\begin{array}{\|c\|} \hline 8 \\ \text { ci } \end{array}$ | $\cdots$ |  |  |
| \％ | $a$ | 士 |  | $\begin{array}{\|l\|} \infty \\ 8 \\ 8 \end{array}$ | 侖 | 合 | $\stackrel{9}{2}$ |  | 霛 | $\cdots$ | $\begin{array}{\|c} \hline \text { C } \\ \hline \end{array}$ | $\begin{array}{l\|l}  \pm \\ \stackrel{N}{n} & \vec{n} \end{array}$ | ？ |  |
| 1 | 剆 | $\underset{\sim}{2}$ | 悹 | $\stackrel{8}{8}$ | c | + | + |  |  | $\ln _{\operatorname{con}}^{8}$ | 总 | 管 | － |  |
| 佼 | 0 | 今 | $\stackrel{m}{e n}$ | $\begin{array}{\|c\|} \hline \mathrm{F} \\ \mathrm{Ci} \\ \hline \end{array}$ | 呂 |  | $9$ | $\frac{7}{7}$ |  |  | © | 心会 | － |  |
| 岩 | ＊ | 9 | $\begin{array}{\|c} \stackrel{C 1}{2} \\ \stackrel{1}{3} \end{array}$ | $\vec{m}$ | 表 | $\stackrel{5}{9}$ |  |  |  | $\stackrel{\rightharpoonup}{2}$ | $\underset{c}{ \pm} \mid \stackrel{\rightharpoonup}{c}$ |  | － |  |
| ल | 0 | \％ | $\bar{\square}$ | $\underset{\sim}{9}$ | $\pm$ | $\cdots$ | s占 |  | - | $\stackrel{\rightharpoonup}{n}$ | 合 | $8$ | － |  |
| $m$ | $\cdots$ | 딩 | ${ }_{0}$ | $\stackrel{\otimes}{\circ}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{1}{\mathrm{C}}$ | $8$ | $\vec{a}$ | $$ | 容宫 |  | $\underset{c}{7}$ | ， | 8 |
| ct | $\bigcirc$ | 心 | $\stackrel{m}{2}$ | ? | 合 | $\underset{\sim}{20}$ | Br | 空 | $\stackrel{\text { A }}{\sim}$ | $9$ | 早官 | 気边 |  | ？ |
| F | $\hat{8}$ | 穴 | 是 | 畕 | 帯 | 佥 | B | $9$ |  | $\stackrel{8}{4}$ |  | － | $\cdots$ | ？ |
| 8 | c | $\stackrel{\mathrm{C}}{\mathrm{C}}$ | $\stackrel{\sim}{2}$ | $\begin{aligned} & \infty \\ & \infty \\ & \vdots=1 \end{aligned}$ | $3$ | $\frac{\mu}{2 n}$ | 年馀 | 守 |  | $9$ | $\stackrel{\circ}{\stackrel{\circ}{C}}$ | \％ | ＋ | $\sigma$ |
| $\geqslant$ | $\checkmark$ | 3 | 吉 | 宗 | $\frac{\infty}{9}$ | $5$ | $\left\{\begin{array}{c} x \\ x_{0} \end{array}\right.$ | $\stackrel{8}{7}$ | \％ | $0$ | 을 | $\stackrel{3}{3}$ |  | $\theta$ |
| $\infty$ ． | 1 | \％ | $\stackrel{\rightharpoonup}{\sim}$ | $7$ | 亖 | $8$ | $\begin{aligned} & 8 \\ & + \\ & \hline \end{aligned}$ |  | $\underset{\sim}{9}$ | $\stackrel{n}{7}$ | $\stackrel{n}{m}$ | 矿 | \％ | （ $n$ |
| $\stackrel{+}{*}$ | $\square$ | \％ | 会 | 䀎 | 安 | $\underset{\sim}{9}$ | $\infty$ | $\infty$ |  | $0$ | ） | － |  | $\bigcirc$ |
| 9 | $\cdots$ | E | 或 | 令 | $\stackrel{\mathrm{r}}{-}$ | $0$ | 安 | $\cdots$ |  | $\therefore$ | 会免 | $\underset{\sim}{8}$ | $\stackrel{\rightharpoonup}{-}$ |  |
| $\cdots$ | $\stackrel{4}{4}$ | ＋ | $\stackrel{\circ}{\circ}$ | $\pm$ | 范 | 䓵 | 克敛 | $\stackrel{1}{2}$ |  | $\begin{array}{l\|l\|} \hline 8 & \text { 18 } \\ \hline \end{array}$ |  |  | 8 | m |
| $\pm$ | 30 | \％ | 을 | $\frac{8}{7}$ | 吕 | 或 | $5$ |  | $5$ | $3$ | $\stackrel{\rightharpoonup}{\mathrm{C}}$ | $\underset{\sim}{9}$ | 志 | E |
| \＃ | $\bar{\square}$ | $\stackrel{\square}{2}$ | $\stackrel{\infty}{\sim}$ | 家 | $\begin{array}{\|l\|} \hline \frac{r}{c-6} \end{array}$ | $\underset{\sim}{\sim}$ | $m$ | 穻 | $\begin{array}{l\|l} -1 \\ \hline \end{array}$ | n | $\underset{\sim}{9}$ | $8$ | S | 気 |
| $\stackrel{+}{5}$ | 成 | $\|\stackrel{\rightharpoonup}{\dagger}\|$ | 盆 | $\left\lvert\, \begin{aligned} & \mathrm{F} \\ & \times 1 \\ & \sim 1 \end{aligned}\right.$ | 总 | $\underset{m}{m}$ | $8$ | $\frac{5}{7}$ | 河 | 只容 |  | 河 | ${ }^{3}$ | N |
| $=$ | 里 | in | $\stackrel{\sim}{ \pm}$ | $\left\lvert\, \begin{gathered} r- \\ x-1 \\ x-1 \end{gathered}\right.$ | $\underset{\sim}{2}$ | $\frac{\pi}{\pi}$ |  | 5 | $5$ | $3$ |  | － | 5－－ | 可 |
| $\bigcirc$ | 士 | 5 | § | $\hat{\vec{c}}$ | $\left\lvert\, \begin{gathered} 3 \\ \rightarrow 人 \end{gathered}\right.$ | $\stackrel{8}{\square}$ | $\left\lvert\, \begin{gathered} \mathbf{c}_{1} \\ \hline \end{gathered}\right.$ | $\underset{\sim}{9}$ | $\underset{\sim i n}{2}$ | i 若 |  | 可 | $\stackrel{\square}{\square}$ | ＊ |
| c | I | 沓 | $\stackrel{s}{马}$ | $\stackrel{0}{\square}$ | $\underset{\sim}{\underset{c}{1}}$ | $\left\|\begin{array}{c} \mathrm{r} \\ \mathrm{~N} \end{array}\right\|$ | $9$ | $\mid$ | $3$ | $9$ | $4$ | O | 8 | m |
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| 1－ | $\stackrel{10}{2}$ | C1 | ＋ | 呺 | $\begin{aligned} & 9 \\ & c \\ & c \end{aligned}$ | 㖛 | 5 | 号 | 总 |  | 잉 | $\xrightarrow{+}$ | 鸟 | $\bigcirc$ |
| $\bigcirc$ | に | 5 | 冾 | $\left.\begin{aligned} & 61 \\ & 0 \\ & 01 \end{aligned} \right\rvert\,$ | $\stackrel{\text { 示 }}{ }$ | $\frac{5}{51}$ | 号 | － | － | 盛 |  | － | 3 | N |
| －5 | 1 | $\bigcirc$ | － | $\underset{A}{9}$ | 盆 | 估 | 気 | － | $9$ | $\overline{5}$ | $\underset{\sim}{5}\|\underset{i}{5}\|$ | $\underset{\sim}{\square}$ | 3 | － |
| ＋ | $\cdots$ | 9 | 部 | c | $\overline{5}$ | ＋ | 号 | $\begin{array}{\|l\|} \hline 4 \\ \hline 7 \\ \hline \end{array}$ | $5$ | $8$ | cis | 咢 | ${ }^{1}$ | 寸 |
| H | $\cdots$ | $\infty$ | ㅍ | $\stackrel{\text { a }}{ }$ | ${ }_{\sim}^{\sim}$ | 品 | $\cdots$ | $\begin{aligned} & \overrightarrow{0} \\ & \overrightarrow{i n} \end{aligned}$ | $\mathrm{c}_{\mathrm{c}}$ | $$ | $\underset{\sim}{7}$ | 家 | － | $\cdots$ |
| C1 | 会 | 完 | 尽 | $\underset{\sim}{\infty}$ | $\stackrel{\sim}{2}$ | $\begin{aligned} & \mathbf{7} \\ & \mathrm{m} \end{aligned}$ | $\left\lvert\, \begin{gathered} \text { Th } \\ \text { Cl } \end{gathered}\right.$ | 苚 | 空 | 氟 | ，凩 | 只 | can | त |
| $\rightarrow$ | $\cdots$ | 0 | 染 | $\cdots$ | $\stackrel{\square}{\square}$ | $\begin{array}{\|c\|} \hline 0 \\ i \end{array}$ | － 8 | $\overrightarrow{\mathrm{F}}$ | ${ }_{2}$ | ${ }_{6}^{6}$ | $\stackrel{\text { c }}{ }$ | 家 | P1 | N |
| $\underset{3}{2}$ | 䍃 | 莺 | 帚 | $3$ | $8$ | $$ | 各 | 官 | 宫 | $\begin{aligned} & 9 \\ & \underset{\sim}{\mp} \\ & \hline \end{aligned}$ | $\begin{aligned} & 5 \\ & 4 \\ & 8 \end{aligned}$ | $5$ | $3$ | 号 |

Year： 2005 Morsth：June

| P |  |  | $\stackrel{\sim}{\square}$ | $\overbrace{0}{ }^{\text {c }}$ | 忥 | 奖 | 甭 | 악 | 守， | \％ | S | Sa | 哑 | 『 |  |
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| 7 |  | $\Rightarrow$ 我 | 吅 | ， 9 | $=$ | 4 | － | 뮹 | 感 | 잉 |  | $\underset{\sim}{\text { a }}$ | T |  |  |
| 宊 |  |  | 9 | 等 | 袻 | 亨 | 天 | 它发 | ¢ | \％ |  | $\bigcirc$ | － | 事 |  |
| Fris |  |  | － | 哭哭 | $9^{2}$ | $3$ | $\mathrm{Fi}$ | $\mathrm{m}$ | 管 | \％ | 気高 | Cic | － | F |  |
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| $\cdots$ |  |  | 6． | $\begin{array}{c\|c\|} \hline 0 \text { 管 } \\ \hline \end{array}$ | 管 | 豆 | Cric | ${ }^{\text {a }}$ | त1 | 200 |  | 式空 | S | 5 |  |
| － |  | Fir |  | $\stackrel{r}{n}+\overrightarrow{i n}$ | $\underset{\overrightarrow{A l}}{\substack{2}}$ | $\underset{\sim}{9}$ | in | $9$ | $\xrightarrow{\mathrm{c}} \mathrm{m}$ | $\xrightarrow{\sim}$ |  | 刮 | S | $\therefore$ |  |
| ค． |  |  | $\vec{y}$ | $9$ |  | $\cdots$ | 9 |  | 氟気 | 空 |  | 高 ${ }^{2}$ | ＂ | 9］ |  |
| 8 |  |  | $\stackrel{3}{2}$ | $\underset{m}{7}$ | ${ }_{\mathrm{m}}^{7}$ | 式 | $$ | 令 | \％ | F | 吻到 | 䆚 | 守 | 家 |  |
| － |  |  |  | $\frac{\square}{91} \frac{1}{n}$ | $\bar{m}$ | $3$ | $3$ | $\underset{\sim}{\infty}$ | 옹 | $\underset{m}{2}$ | \％ | － | $\bigcirc$ | 3 \％ |  |
| 8 |  |  | 5 |  | $\stackrel{\mathrm{ran}}{\mathrm{ra}}$ | $\cdots$ | $8$ |  | $\underset{\rightarrow}{3}$ | 路 | 鬲家 |  | 茓 | Ci． |  |
| $\geqslant$ |  |  |  | $\overline{r-1} \bar{n}$ | $\stackrel{y}{4}$ | 8 | $\overrightarrow{\mathrm{s}} \mathrm{~F}$ | mor | 窘 | 雱 | 害菅 | 会克 | $\pm$ | P |  |
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| $\cdots$ | $\cdots$ | ，${ }^{\text {P }}$ |  | girn | cive | P | $\underset{\sim}{2}$ | 我 | 品 | － | 5 | 5 三 | $三 \mathrm{C}$ | ［5］ |  |
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| $=$ | 한 | $\stackrel{3}{2}$ | 综 |  | 成 | 閉等 | 宗 | 守安 | ＋ | ${ }^{6}$ | $9$ | Cif | 澼 | $F$ |  |
| $\stackrel{\square}{\square}$ | ＇ | － | 5 | 合空 | 耍商 | 家 | 会 | $\mathrm{m}_{2}^{2}$ | $\begin{gathered} 90 \\ =10 \end{gathered}$ | $\underset{\sim}{m}$ | $\begin{array}{c\|c} 9 \\ \hline 9 \\ \hline \end{array}$ | $\stackrel{7}{7}$ | $\bar{\ddagger}$ | Sio |  |
| $\cdots$ | \|-i| | 1 | 貧 | 家可 | 악 | 쇽 | 年 | $\begin{gathered} 90 \\ 0 \end{gathered}$ | 谷空 | $\mathrm{S}_{3}^{1}$ | $\stackrel{0}{3}$ | $9$ | $\underset{i}{3}$ | \％ | － |
| $\infty$ | $\%$ | 5 | 知 | 䎟 | \％ | 令台 | 至 | 䒯 | 而卉 | $7{ }^{+}$ | $\cdots$ | ${ }_{0}^{\infty}$ | 3，${ }^{2}$ | $\stackrel{5}{2}$ | $\sim$ |
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| 0 | $1-$ |  | 高宫 | 郤彮 | 盛 | $\cdots$ | $\stackrel{\rightharpoonup}{2}$ | $\mathrm{m}_{10}$ | $87$ | $7$ | 呂 | $\stackrel{5}{7}$ | $\underset{7}{7}$ | 닫 | 9 |
| $n$ | $\bigcirc$ | $\stackrel{-}{*}$ | 枵 | 合灾 | ， | ？ | Sis |  |  | j | 羚 | 领 | 두 | $\sim^{10}$ | $\cdots$ |
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| 1 | －1 |  |  | 年 | 告 | n | $8$ | $8$ | $\cdots$ | $\stackrel{\text { \％}}{\sim}$ |  | $\xrightarrow{\square}$ | ${ }_{\sim}^{7}$ | $\cdots{ }^{1}$ | a |
|  | Hi |  | 合 | ${ }_{-1}^{2}$ | 袘 | $\underset{\sim}{2}$ | 势 | $8$ | $5$ | $\sqrt{n} \cdot \frac{2}{m}$ | $9$ | O | \％ | 20 | $\bigcirc$ |
| 5 | 8 |  | \％ | $\dot{z}$ | $5$ |  |  | 为 |  |  |  |  |  | 88 |  |

## Houtly Diffuse Solar Radiation in watt／m ${ }^{2}$




| Day | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | t2 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 20 | 27 | 28 | 29 | 30 | $3 t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Stime |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5：00 | 19 | t0 |  |  | 7 | 14 |  | 19 | 8 |  | 13 |  | 12 | 12 | 11 | 10 | 10 |  |  | 13 | 1 | 16 | 15 |  |  |  | 15 | 1. | 19 | 13 |  |
| 6：00 | 76 | 4. | 6 |  | 37 | 7 | 88 | 102 | 88 | 64 | 40 | 4 | 49 | 33 | 53 | 6 | ${ }^{6}$ | 70 | 74 | 112 | 123 | 115 | 10 | 9 | 67 | 102 | 87 | 72 | 90 | 10 |  |
| 7：00 | 127 | 31 | 15. |  | 35 | 68 | 105 | 141 | 13 （1） | 118 | 116 | 129 | 12 | 133 | 139 | 144 | 150 | 156 | 162 | 19 | 258 | 24 | 228 | 212 | 11 | $14+$ | 16 | 194 | 50 | 189 |  |
| 8.06 | 6 | 43 | 18. | 190 | $\underline{2} 7$ | $2 \times 14$ | 301 | 240 | 27 | 282 | 288 | 284 | 283 | 281 | 278 | 276 | 274 | 27 | 26 | 2 C | 36 | 259 | 259 | 25 | 138 | 207 | 234 | 2 （0） | 21 | 22 | 1 |
| 9：9］ | 280 | 415 | 27 | 214 | 271 | 326 | 369 | 390 | 33 | 133 | 253 | 373 | 383 | 393 | ＋10 | 413 | 423 | 433 | 43 | 328 | 32 | 281 | 24 | 19 | 15 | 308 | 28 | 263 | 337 | 35 | 8 |
| 10.00 | 28 | 21 | 12 | 3，3 | 173 | 363 | $28-4$ | 350 | 415 | 268 | $27+$ | 27 | 82 | BB | 15 | 22 | 28 | 353 | 420 | 467 | $25+$ | 353 | 452 | 370 | 248 | 360 | 432 | 300 | 2 28 | 19 | 40 |
| 11：00 | 258 | 300 | 47 | 369 | 223 | 317 | \＄ 3.30 | 32 | 351 | 370 | 372 | 375 | 379 | $3 \cdot 3$ | 3.85 | 389 | 392 | 393 | 473 | 465 | 33 | 398 | 458 | 337 | $\underline{1}$ | 38 | 38 | 39 | 353 | 315 | ， |
| 12：00 | ＋1 | 49 | 112 | 460 | 376 | 328 | 31 | 332 | ＋37 | 411 | 340 | 268 | 196 | 125 | 217 | 30 | ＋0 | 493 | 471 | 487 | 40 | 411 | ＋22 | 344 | 267 | 290 | 31 | 395 | 316 | 284 |  |
| 13：00 | 352 | 547 | t17 | 140 | $+27$ | 304 | 282 | 29 | 218 | 320 | 316 | 306 | 296 | 286 | 175 | 24 | 312 | 350 | 363 | 32 | 44 | 39. | 3.47 | 32 | 29 | 284 | 27 | 20 | 2 | 275 |  |
| 1＋100 | 13 | t5 | 250 | 75 | 406 | 273 | 28 | 26 | 360 | 219 | 27 | 340 | ＋0 | 461 | 177 | $25:$ | 338 | 4 | 38 | 166 | 36 | 50 | 2－4 | 27 | 29 | 374 | 21 | 245 | 224 | 312 |  |
| 15：00 | 176 | 265 | 150 | 286 | 20 | 128 | 198 | 216 | 271 | 199 | 229 | 259 | 2 2 ． | 319 | 152 | 156 | 160 | 163 | 307 | 22 | 297 | 231 | 165 | 21 | 273 | 306 | 25 | 20 | 24 | 26 |  |
| 16： $16 y^{4}$ | 1093 | 94 | 120 | 151 | 121 | 93 | 1.5 | 175 | 1102 | 135 | 154 | 173 | $19:$ | $\underline{10 .}$ | 106 | 112 | 119 | 125 | 178 | 18 | 237 | 186 | 145 | 178 | 211 | 154 | 167 | 21 | 21 | 182 | 14 |
| 17：00 | 39 | 38 | 65 | 81 | $\because 6$ | 71 | 52 | 79 | 80 | 15 | 55 | 6. | 6） | 75 | 80 | 82 | 84. | 85 | 5 F |  | 79 | 87 | 96 | 46. | 78 | 95 | 60 | 48 | 102 | － |  |
| 18.00 |  | 7 | t4 |  | 19 | 23 | $1{ }^{1}$ | 16. | 12 | 12 |  | 2 |  | 4 | 4 | 5 | － |  | 5 | 1 |  | 11 | 15 | ， | ， | ， | 6 |  | $\underline{5}$ | 6 |  |

Year 2005 AFontlu August

| Du | 1 | $\xrightarrow{2}$ | 3 | 4 | 5 | 6 | 3 | 6 | 9 | 10 | it | 12 | 13 | $1+$ | 15 | 16 | 17 | 18 | 1） | 20 | 21 | $\underline{2}$ | 23 | 24 | 25 | 26 | 27 | 38 | 29 | 30 | 31 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tinle |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3.00 | 10 | 11 | 10 | 3 | 13 | 1. | 1.3 | 6 | 3 | 0 | 2 | 4 | 4 | 4 | 5 | 7 | 10 | 0 | 4 | 4 | 3 | 2 | 4 | 3 | 6 | 11 | 10 | 9 | 8 | 7 | 6 |
| 6：00 | 78 | 60 | 36. | 80 | 75 | 36 | 108 | 50 | 30 | 10 | 20. | 31 | 21 | 12 | 58 | 64 | 69 | 13 | ＋1 | 35 | 29 | 24 | 31 | 33 | 3 B | 90 | 75 | 6 | 7 | 36 | 4 |
| 7：00 | 82 | 32 | $1+3$ | 136 | 120 | 121 | 123 | 194 | 111 | 2 B | ［6］ | 52 | 64 | 76 | $1+5$ | 171 | 197 | 43 | 117 | 97 | 79 | 57 | 20 | 33 | $3{ }^{\text {a }}$ | 9 | 15 | 1 | ， | 81 | $6{ }^{60}$ |
| $8: 00$ | 171 | 132 | 155 | 179 | 212 | 229 | 230 | 2ヶヶ7 | 133 | 19 | 40 | 61 | 82 | 163 | 166 | 193 | 220 | 145 | 137 | 127 | 118 | 109 | 211 |  | 8 | 14 |  | $1{ }^{1}$ |  | ， | 7 |
| 9：${ }^{\text {ch }}$ | 251 | 321 | 322 | 345 | 285 | 23－1 | 306 | 211 | 117 | 22 | 113 | 204 | 295 | 176 | 335 | 463 | 278 | 134 | 125 | 2316 | 335 | 189 | 201 |  | 118 |  |  | 4 | 5 | 85． | 293 |
| 10：00 | 384 | 367 | 398 ． | 274 | 361 | 564 | 475 | 337 | 20 NJ | 62 | 173 | 284 | 395 | 203 | 284 | dić | 314 | 15.3 | 297 |  |  |  |  |  |  |  |  |  | 361 | 5 | 372 |
| 11：00 | 350 | 367 | 398 | 311 | ＋28 | 328 | 390 | 280 | 17： | 61 | t87． | 313 | 430 | 383 | ＋ 77 | 465 | 178 | 279 | 225 | 376 |  |  |  |  |  |  |  | 458 | 390 | 394 | 419 |
| 1200 | 369 | 322 | 257 | 329 | $+38$ | 394 | 501 | ＋62 | 473 | 384－ | 343 | 335 | 325 | 379 | 240 | 378 | 415 | 260 | 460 | 346 |  |  |  |  | 171 | 360 | 404 | 449 | 244 | 476 | 125 |
| 13：00 | $\underline{72}$ | 271 | 353 | 395 | 41i | 320 | 149 | 299 | 250 | 201 | 3．1 | 312 | 243 | 389 | 211 | 374 | 754 | 107 |  |  |  |  |  |  |  |  | 414 | 440 | 74 | 497 | 177 |
| 14.06 | 278 | 273 | 270 | 252 | 133 | 294 | $3{ }^{3} 5$ | 328 | 261 | 1144 | ＋22 | 411 | 4041 | 31 |  |  |  |  |  |  |  |  |  | 120 | 280 | 410 | 400 | 390 | 157 | 431 | $3 \mathrm{B2}$ |
| 1500 | さ12 | 180 | 238 | $16:$ | tis | 233 | 238 | 251 | 264 | 230 | 357 | 340 | กวา |  |  |  |  |  |  |  |  | $2(4)$ | 231 | 134 | 318 | 339 | 336 | 334 | 271 | 274 | 356 |
| 1600 | 11／ | ｜09， | 180 | 129 | 9tr | 218 | 1.36 | 118 | 101 | H． | 18. | 29¢ | 27， | 10 | 150 | 1 | 14 | 127 | －6． | 239 | 191 | 300 | 153 | 190 | 334 | 20980 | 221 | 235 | 185 | 153 | 327 |
| 18.00 | 14 | 0 | 7 | 11 | 11 | 7 | 0 | 2 | 4 | 2 | 37 | 26 | 15 | 3 | 4 | ， | 4 | 3 | 3 |  |  |  |  | 23 | 57 | ！ 1 | 36 | 59 | 32 | 36 | 15 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1 | ， | － | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |


| 0 | 0 | 0 |  |  |  | ， | 0 | 0 | 0 | 19 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | ® | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | （1） | 0 | 0 | 0 | 00：41 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \％ | ${ }_{8}^{0}$ | ¢ | $\bar{z}$ | 0 | ＋5 | 10 | tt | － | E | － | 1 | 0 | 1 | Z | i | $t$ | \％ | 5 | 9 | 9 | L | $t$ | 6 | O1 | 01 | 01 | 91 | 11 | 11 | te | 00：21： |
| 56 | 16 | 06 | 68 | 18 | st | git | tt | $\frac{104}{35}$ | ¢i | ！ | ${ }^{6}$ | 10t | tel | 迷 | 56 | dit | $6{ }^{6}$ | 8 | ${ }^{8+}$ | ${ }_{\text {8 }}+$ | 4 | $\stackrel{+}{ }$ | 06 | 18 | $z_{i}$ | E9 | ＋5 | 5 | St | 68 | $00^{\circ 9} 1$ |
| LE1 | ¢ | act | 9 L | ¢ 71 | 号 | 6za | toz | ¢¢ | 15 | \％ | L | O5， | Eat | 9 | tII | 201 | LD1 | CIt | 911 | 121 | 101 | ¢ | 1081 | ＋91 | 8 c 1 | Eit | 211 | 101 | ［51 | $10 \stackrel{ }{ }$ | 00：5！ |
| ¢9 | ¢ | ¢0a | ¢ 21 | Et1 | कn | 161 | coz | 201 | 5 | $\bar{z}$ | 0.1 | zis | tiz | 5 | ${ }^{\text {KL }}$ | 6tl | ［5］ | tsl | 9 | 951 | （191 | โП | 691 | ZSI | ＋61 | 9 g | 6ict | Las | gice | sct | 00：＋1 |
| piz | zLz | 0 EL | 881 | Sti | ＋52 | 18 ¢ | E61 | 951 | 551 | Tz̄1 | 94 | 655 | 9St | ¢ | ${ }_{\text {P2 }}^{81}$ | $06 \overline{0}$ | 192 | 02 c | ＋st | it $\overline{\text { a }}$ | Oū | $19 \%$ | 9＋${ }^{\text {a }}$ | 56 | t＋a | cid | tıl | 06 | OL̄ | $6+\varepsilon$ | 00：¢81 |
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| OSE | ¢q¢ | Li | 068 | prot | tis | 26i | tgl | 1061 | 搨 | ¢t | 16 | CI | \％ | 6 | SLi |  | 跳 | 25 | 1） | 为 | th2 |  | －1E | $90 \%$ |  | ¢9\％ | 1LL | 652 | 861 | c | 00：11 |
| ¢ 8 \％ | L $\angle 1$ | $16 \overline{1}$ | 56 | $66 \overline{1}$ | です | SIC | 691 | ¢ | HSE | 0sz | $9 ¢ 1$ | 894 | 102 | fci | $59 \bar{L}$ |  | ＋s， | 河 | Lic | Oaz | $86 \%$ | $81 \bar{C}$ | 洨 | ciz | 60 | こ६彑 | 09\％ | 849 | 951 | ti | 0001 |
| 1 | zoz | 2na | いた | Siz | 諒 | 611 | I¢1 | $10 \overline{1}$ | izu | でて | 1 | 0t | 6 | （11 |  | Sfal | Lž | 9tz | 59 | 18¢ | E0\％ | niz | Líz | $15 \bar{L}$ | 2Lz | £ 6 ū | ＋1E | ¢¢¢ | 10： | 2\％ | 006 |
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| 4 | Z | － | L | 9 | 21 | 81 | 81 | B1 | Til | 9 | 5 | $2 \cdot$ | 71 | t $\bar{i}$ | t | 11 | 9 | 15 | \％ | $\overline{\text { a }}+$ | 81 | 51 | 18 | ¢1 | 11 | $8{ }^{\text {c }}$ | 1 | ＋ | it | 00：21 |
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| Day | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 20 | 27 | 28 | 29 | 30 |
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| 700 | 122 | 118 | $0 \cdot$ | 85 | 70 | 80 | 714 | 78 | 77 | 76 | 76 | 26 | 76 | 76 | 7 m | 76 | 22 | 88 | 24 | 100 | 108 | 116 | 125 | 20 | 104 | 9 | 22 | 85 | 71 | 6-1 |
| 800 | 193 | 149 | . 136 | It2 | 91 | 98 | 100 | 102 | 105 | $10{ }^{\circ}$ | 107 | 107 | 107 | 107 | $10 \cdot$ | 107 | 121 | 135 | 149 | 163 | 16) | 163 | 163 | 159 | 177 | 162 | 146 | 131 | 101 | 106 |
| 009 | 279 | $17+$ | :52 | 1,3+ | (01) | 102 | 109 | 115 | 12? | t29) | 129 | 129 | 129 | 12) | 129 | 129 | 159 | 190 | 221 | 210 | 171 | 132 | 254 | 214 | 203 | 192 | fBt | 170 | 125 | 25 |
| 10-00 | 336 | 173 | 162 | $1+2$ | 119 | 113 | 12+ | 1,34 | 144 | 155 | 155 | 155 | 155 | 155 | 155 | 155 | 182 | 210 | 238 | 26.3 | 239 | 216 | 313 | 249 | 23 | 22 | 210 | 181 | 136 | 163 |
| 11:00 | 370 | (5) | 165 | 139 | 145 | 13.3 | 14) | 165 | 182 | 198 | 198 | 191 | 108 | 198 | 198 | 198 | 231 | 263 | 296 | 293 | 284 | 275 | 348 | $2{ }^{2}$ | 355 | 233 | 210 | 195 | 132 | 247 |
| 12:00 | 357 | 168. | 160 | 1,3,5 | 160 | 2 l 21 | 200 | 198 | 196 | 124 | 197 | 200 | 203 | 206 | 209 | 194 | 217 | 240 | 264 | 271 | 286 | 300 | 7 | 248 | 225 | 201 | 177 | 205 | 136 | 216 |
| 1300 | 22. | 162 | .152. | 127 | 125 | 167 | 186 | 185 | 185 | 184 | 190 | 197 | 203 | 309 | 215 | 184 | 202 | 221 | 239 | $25 t$ | 263 | 276 | 230 | 189 | 171 | 153 | 135 | 301 | 58 | 67 |
| 1400 | 203 | 138 | $\underline{126}$ | 113 | 99 | 155 | 159 | 164 | 169 | 174 | 16.3 | 152 | 141 | 130 | 120 | 133 | 147 | 160 | 174 | 175 | 190 | $20 \cdot 6$ | 199 | 160 | 142 | 124 | 106 | 139 | 148 | +39 |
| 1500 | 100 | 99 | 93 | 87 | 77 | 122 | 116 | 110 | 10. | 98 | 95 | 91 | 88 | 85 | 81 | ${ }^{5} 5$ | 90 | 94 | 98 | 112 | 112 | 113 | 85 | 8.3 | 80 | 26 | 73 | 78 | 92 | 92 |
| 16.60 | 34 | 37 | 40. | 35 | 31 | 31 | 31 | 30 | 30 | 30 | 30 | 30 | 29 | 29 | 29 | 29 | 29 | 30 | 30 | 30 | 31 | 32 | 9 | 19 | 20 | 22 | 24 | 21 | 31 | 24 |
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Yori: 2005 Month: December

| Day | 1 | 2 | 3 | 4 | 5 | 0 | 7 | 8 | 9 | 1 | 11 | 12 | 1.3 | $1+$ | 15 | 16 | 17 | 18 | 19 | 20 | $\underline{21}$ | 22 | 23 | $\underline{2+}$ | 25 | 26 | 27 | 28 | 21) | 30 | 31 |
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| 'linke |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | , | , | , | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  | , |  |  | 0 |
| 6.00 | 25 | 28 | 23. | 18 | 1. | 9 | 5 | 1 | 2 | 5 | 7 | 10. | 12 | 15 | 14 | 14 | 13 | 11 | 8 | 5 |  | 0 | 2 | 4 | 6 | 8 | 10 | 11 | 11 | 9 | 0 |
| 7:00 | 76 | 83 | 72 | 60 | 4 | 37 | 23 | 14 | 22 | 30 | 38 | 46 | 54 | 63 | 61 | 55 | 81 | 70 | 56 | 42 | 28 | 14 | 22 | 31 | 4 |  |  | , | 11 |  | 6 |
| 800 | 118 | 119 | 108 | 98 | 87 | 76 | 66 | 55 | 61 | 67 | 24 | 80 | R 0 | 22 | 88 | 76 | 172 | 14) | 126 | 102 | T4. | 5 |  |  | T | 48 | 5. | 6 | $7+$ | 66 | 58 |
| 9.00 | 166 | $1+1$ | 130 | t19 | 109 | 98 | 87 | 76 | 82 | 87 | 93 | 9 | 10.5 | 111 | 84 | 122 | 24 | , |  |  |  | 5 | 6 | 11 | 79 | 88 | 96 | 164 | 131 | 125 | $\underline{118}$ |
| 10000 | 195 | $t 57$ | 151 | 145 | 139 | 133 | 127 | 137 | 125 | 128 | 131 | 134 | 13 ? | 140 | $1{ }^{1}$ | t42 | 301 | 265 | 200 | 19 | 5 | 12 | , | 23 | 104 | 113 | 123 | 132 | 18 | 176 | 71 |
| 11-00 | 189 | 189 | 14: | 17.3 | 16. | 1.57 | 150 | 142 | 145 | 148 | [5u | 15.3 | 156 | 159 | 171 | 204 | 260 | 236 | 213. | 189 | 166 | 142 | 150 | 15 | 16 | 145 | [51 | 157 | 208 | 203 | 98 |
| 12.00 | 179 | 181 | 1901 | 199 | 2 nc | 216 | 225 | 234 | 218 | $2(1)$ | 187 | 172 | 156 | 140 | $23+$ | 21.3 | 328 | 309 | 290 | 271 | 253 | 234 | 225 | 216 | 208 | (9) | 181 | 189 | 22 | 216 | 208 |
| 13:00 | 164 | 175 | 176 | 1:8 | 1 BO | 182 | 183 | 185 | 180 | 17.5 | 170 | 164 | 159 | 154 | 185 | 220 | 315 | 289 | 263 | 23 | 211 | 185 | 183 | 182 | 180 | 178 | 176 | 175 | 77 | 22 | 2 |
| 14,00 | 147 | 1299 | 131 | 132 | 133 | 13+ | 136 | 137 | 135 | 1.33 | 131 | 129 | 12? | 125 | 137 | 168 | 316 | 192 | 178 | 16. | 151 | 137 | 1.6 | 134 | 33 | 3 | 13 | 179 | 135 | 万, | 182 |
| 1500 | 92 | 35 | 85 | 86 | 86 | 87 | $\mathrm{B}_{7}$ | 88 | 87 | B | B9 | $8+$ | S | 83 | 86 | 12 | 1016 | 105 | 1(w) | 96 | 92 | RR | 87 | 87 | B6 | 86 | 5 | 85 | 0 | 41 | 40 |
| LO 104 | 2 | 3-1 | 32. | 31 | 1 | 2 H | 27 | 25 | 25 | 25 | 23 | 25 | 21 | 24 | 15 | 31 | 2 k | 27 | 27 | 26 | 2 | 25 | 27 | \% | 30 | 31 | 32 | 34 | 38 | 47 | $4{ }^{2}$ |
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| 19:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | , | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |


| \％ | 08 | 82 | 0 E | $L Z$ | Iz | H2 | $\mathscr{F}$ | 62 | 15 | 52 | 15 | Giz | 6 | $1 \xi^{\prime}$ | Z\＆ | ゅ2 | L | 82 | R2 | を $\chi^{\prime}$ | Hz | iZ | （2） | sc | $\underline{z}$ | $t 2$ | $1 \varepsilon$ | $0 ¢$ | 08 | 12 | $02 \cdot 2$ |
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| $\bar{\square}$ | 65 | 65 | 65 | $5 ¢$ | ¢ | 59 | Z5 | 55 | 比 | 15 | IF） | ［ 3 | L5 | を | \％ | 碞 | 54 | 1） 5 | － 5 | と ${ }^{\text {d }}$ | L 5 | ＋s | 12 | 15 | CT | $\underline{5}$ | 19 | （11） | ［1］ | 117 | เห｜ |
| 8 ti | 䛧 | SH | 68 | $\overline{\text { I }}$ | 2， | ¢ ${ }^{4}$ | Hi | E\％ | 5 | 现 | $1 \mathrm{~K}^{\prime}$ | ＇940 | 9 R | r | 56 | 21 | 䛞 | H | 5 M | 51 | 59 | 14 | （x） | ＇ 2 | ¢12 | 11 K | 26 | 016 | It ${ }^{\text {r }}$ | Z | （以）に |
| $5{ }^{5}$ | 8B | ¢R | L8 | $L$ | －${ }^{\text {a }}$ | 18 | SL | \％ 8 | 10 | ［ | 巩 | \＆ | 9K | $z^{\prime}$ | tr | 12 | On | $\stackrel{\rightharpoonup}{\text { ch }}$ | ［ ${ }^{\text {\％}}$ | ＋fi | ¢ 2.4 | \％ | 65 | \＆ | （1） | 52 | （4） | 2 L | Hı | $1{ }_{1}$ |  |
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| 0. | 14 | ［ ${ }^{\text {L }}$ | t＋ | 5 | 4 | 臸 | 6 | 28 | to | I） | 59 | LL | $\underline{¢}_{5}$ | ［1 | ¢ ${ }^{\text {a }}$ | 49 | 4 | kL | 4 | $1{ }_{1}$ | 4 | 4 |  | － |  | （ | ， | \％ | 10 | （1） | M1－6 |
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| 59 | Ll | HL | t | 「 | ¢ | てL | кij | 111＇ | 26 | 为 | SL | 82 | IT | ＋ir | 5 | ＋41 | 1 |  |  |  |  |  | ， | L | 2 | 2 | th | $1 \times$ | 9 | 54 | 14，${ }^{1 / 2}$ |
| 69 | 26 | 2 | 6 | \％ | 4 | 61） | $\mathrm{B}^{\prime \prime}$ | H6 | 16 | โร | 做 | ki | G | ¢ | 18 |  |  |  |  |  |  |  |  |  |  |  | ¢ | 10n | \％ | C3 | （00．51 |
| W5 | 49 | $\bar{L}$ | ＋19 | 8 | 29 | ワ | 49 | EI＂ | \＆ 8 | 25 | $1 i$ | 4 | 51 | B2 | tr | ［ | （11） |  |  |  |  |  |  |  |  |  | 14 | 88 | 14 | \％ | （\％） $0^{\text {a }}$ |
| 95 | 17 | 62 | 们 | 6 | IS | 49 | 19 | L） | 9 | む5 | （1） | （） | $1{ }^{1}$ | ris | K1 | ग5 | 10 | 1 | 7 | 1 | S1 |  |  |  |  |  |  |  |  |  |  |
| 55 | 95 | $5{ }^{5}$ | $5{ }^{5 \prime}$ | 15 | 25 | 6 | 45 | Z） | L） | 15 | 25 | こ | נ1 | （i） | 19 | 15 | 65 |  | 哣 | 16 | 65 | 25 |  |  |  |  |  |  |  |  |  |
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| UT | Lt | 25 | ＋7 | H | 9 | $4{ }^{\circ}$ | d／5 | ts | $8{ }^{4}$ | \％ | St | 55 | 5 | 1／3 | 叶 | ¢ | 8 | 45 | 1 L | 4丕 | 们 | 6 | ¢ + | Ht | zc | ct | 4 | 15 | 15 | It |  |
| EE | 78 | 15 | Of | 行 | Lt | tr | LF | 1 F | PG | y | lt | ［¢ | （it | $1 \pm$ | 9 ${ }^{\circ}$ | 4 | ¢ | LS | 91 | LK | U12 | 己t | 48 | \＆ | $\stackrel{+}{+}$ | $11+$ | 15 | 29 | $\stackrel{5}{+}$ | 13 | －16 |
| 58 | 6 | P5 | $2 t$ | $1{ }^{10}$ | L5 | 5 | 6 | is | 59 | ${ }^{18}$ | 9 | Z5 | kt | （t） | 8 | Gt | Cf | 少 | 佔 | tr | zi | 少 | 65 | \％ | hir | 帅 | －5 | IIS | や | $\mathrm{NL}_{5}$ | （ki） 4 |
| \％ | 2 t | 2 | 「哵 | \＆t | （6） | 9 | 5 | 15 | E3 | 12 | $\bar{\square}$ | $t 5$ | Lt | しt | Ib | 41 | 4 | HS | 5 | 1 L | ＋i | 4 | EF | ¢15 | ZS | 15 | L5 | ¢ ${ }^{\text {c }}$ | \％ | It | फ， |
| 为 | Sp | GS | 6it | や | ¢5 | 隹 | 5 | 25 | － NS | 18 | せt | 54 | 壮 | （1） | 25 | Z + | （it | 15 | ds | \％ | 烟 | \＆t | サ | 4 | F | L | 115 | ¢¢ | 6 | \％$\dagger$ | （\％） |
| ¢ ${ }_{\text {d }}$ | ¢ 5 | G9 | ＋5 | $6{ }^{6}$ | 6 | 619 | （2） | 6 | リ | सह | こ） | リリ | 55 | $\ddagger$ | 116 | 保 | 1.5 |  | 21 | RL | ¢ $\dagger$ | ＋ | $51 \%$ | 45 | 45 | ＋9） | 113 | （\％） | （1） | 59 | ¢ ${ }_{\text {HI }}$ |
| 65 | 19 | 06 | 08 | ＋ | $\pm$ | Li | $2 i$ | （5） | $\pm L$ | 9 | リ | リ | H | fil | リ5 | 59 | 69 | ち！ | ${ }^{4} 5$ | H2 | 15 | 51 | 55 | 19 | 65 | IL | D 2 | Ci | 4 | 92 | 00 F |
| 67 | 67 | 2t | S） | 65 | 69 | ［4］ | 18 | 巾1 | こ¢ | 8 | ！ | 23 | E | $\mathrm{ch}^{\text {H }}$ | ヶ＇） | 29 | 6L | ［4］ | ＋ 1 | HL | 85 | M | 15 | 59 | て） | $0 \cdot$ | （\％ | － | 16 | E S | W） |
| －$t$ | 56 | ［8 | $t t$ | に | 12 | 58 | 57 | Z\％ | 88 | पリ | H2 | N8 | $6 L^{-}$ | ${ }^{1 / 1}$ | 16 | 49 | ¢ 8 | 54 | 18 | Cs | リリ | 2 | 59 | W | 0 | 54 | 58 | L 4 | \＆ 6 | ＋ 4 | D0＇z |
| $0{ }^{1}$ | I8 | 吅 | th | $\pm$ | 62 | L 4 | 18 | 68 | 故 | $t$ | 64 | 宕 | tH | 26 | $0{ }_{0}$ | 3 | 比 | 64 | 年 | 58 | I | 2 | （ 31 | 51 | Lí | 16 | 16 | ［G］ | 56 | 的 | 0.1 |
| 98 | LH | Í | 56 | 9） | 5 | 69 | 56 | 4.5 | Ck | F | 26 | 6 k | fís | 26 | 呩 | 18 | LK | E6 | E6 | 68 | 15 | M | $t$ | W） | ¢ $\mathrm{K}_{1}$ | $\underline{4}$ | \％ | 56 | 26 | 26 | （\％） |
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| I¢ | 0 0． | 62 | 87 | Lt | 92 | 52 | $\downarrow z$ | 亿z | CL | ［ 2 | （z | 65 | 81 | 21 | 91 | 5 I | － | ¢＇1 | ZI | II | 01 | © | R | 4 | 9 | 5 | $t$ | $\Sigma$ | $\Sigma$ | ［ | ${ }^{\text {frecl }}$ |

Srouse

## Hourly Relative Humidity（\％）


Year． 2005 Month Februng

| Day | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 14 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 |
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| lume |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| U16） | 71 | 97. | ） | 88 | 咀 | 39 | （k） | ${ }_{3}$ | 85 | 87 | 9 | （W） | R ${ }_{\text {R }}$ | 48 | $6{ }^{6}$ | H9 | gut | 8.4 | प9\％ | d | 53 | 74 | 77 |  | 50 | 74 | 79 | ${ }_{7}$ |
| $1(x)$ | （1） | ＊$\times 1$ | 87 | ${ }^{\prime} 3$ | ${ }^{6} 3$ | 31 | 陦 | 75 | 76 | 77 | K－1 | P41 | 78 | 45 | （i） | ＊ | H7 | Rill | \％ | 89 | 5 | 37 | 70 | 75 | 57 | \％，9 | 67 | 71 |
| 200 | 4 | ${ }^{8}$ | 79 | Th | 77 | 64 | H2 | $\mathrm{Gi}^{1}$ | 6 | 倞 | 37 | 71 | 71 | 41 | 58 | ${ }_{3} 3$ | Rif | 76 | 8 | kH | 53 | 72 | 6 | 72 | $5 ¢$ | 43 | 55 | 13 |
| 3 chl | 65 | 36 | 70 | 73 | 72 | 54 | 39 | 59 | 54 | 54 | 711 | tis | 64 | 38 | 52 | 詸 | ． 1. | 72 | BI | kfi | 54 | 7 | 55 | ［19 | 54 | 57 | 41 | 55 |
| ＋ 4.14 F | （k） | 713 | 64 | （14 | ${ }_{6} 6$ | 47 | 73 | 52 | 5. | 54 | 62 | 5 | 59 | 12 | 4 | 74 | 75 | 67 | 74 | \％ | 48 | 61 | 4 | 6.3 | 49 | 45 | 3 | $4{ }^{4}$ |
| 5̧ M0 | 56 | 14 | 5） | 55 | 55 | 4.3 | 6s | 45 | 47 | 49 | 53 | 50 | 4 | 26 | 35 | （i） | （is | 62 | 74 | 75 | 43 | 51 | 12 | 58 | 45 | 33 | 32 | 37 |
| （6，0） | 51 | 5 s | 53 | 46 | ＋6 | 36 | 39 | 3 | 41 | ． 45 | 4.5 | $\pm+$ | 31 | 30 | 27 | 6 | $\mathrm{C}_{1}$ | 57. | 71 | 69 | 37 | 4 | 36 | 32 | 4 | 31 | 26 | 28 |
| 710 | 55 | 53 | 51） | 42 | 41 | t6． | 51 | 35 | 43 | 43 | 43 | 4 | 2 t | 19 | $2 i$ | （1） | 57 | 55 | 65 | 6.5 | 37 | 4 | ． 3 | 47 | 3R | 22 | 25 | 3 |
| 8 OCO | 59 | 47 | 47 | 4 | 3 | 35 | 43 | 12 | 45 | 4 | 12 | 35 | $2{ }^{2}$ | 18 | 25 | 37 | 52 | 57 | （i） | 6 | 34 | 34. | 33 | 43 | 37 | 24 | 24 | 27 |
| 9.10 | 62 | $4 ?$ | 4 | 37. | 31 | 35 | 35 | 21） | $4 \bar{i}$ | 3 R | 411 | 31 | 24 | 17 | 24 | 54 | 47 | 511 | 54 | 5R | $3{ }^{3}$ | 3.7 | 12 | 38 | 35 | 25 | 2. | 21 |
| 11）．143 | ${ }_{6} 15$ | 4i | 49 | －$n$ ． | 3.4 | 42 | －4 | 4 | 18 | 3） | 4 | $3{ }^{4}$ | ${ }^{11}$ | 21 | 27 | 56 | 5.2 | 5.3 | 57 | 59 | 42 | 4 | 34 | 39 | 34 | 27 | 24 | 25 |
| 11.00 | 6 F | 4 | 53 | 43 | $3{ }^{3} 4$ | $4)$ | 52 | 39 | 51 | 41 | 45 | 4 | 35 | 37 | 31 | 39 | 53 | 57. | 6 | $6 t$ | 4 | 44 | ${ }^{2}$ | 39 | 34 | 24 | 25 | 29 |
| $12 \times 1$ | 71 | 37 | 54 | $4{ }_{4}$ | 3） | 56 | 61 | 44 | 51 | 11 | 4.3 | 45 | 4 | 29 | 34 | 01 | 1.2 | （i） | 6.1 | 62 | 519 | 47 | $3{ }^{2}$ | 4） | 37 | 31） | 16 | 3.3 |
| 13，1／1］ | 74 | 5 R ． | （12 | 511 | 4） | （i） | 64 | 511 | $5{ }_{5}$ | 4 H | 5 | 4 A | 4. | 31 | 45 | 6 | cis | 6 | $\mathrm{Lff}_{1}$ | （19） | 32 | 51 | 4 H | 44 | 42 | 37 | ，${ }_{1}$ | 41 |
| 14．14i | W | ［ 2 | 17 | 55 | 59） | 63 | $6{ }_{6}$ | 514 | （0） | 35 | 65 | $5_{1} 1$ | A | 4 | 54 | 7.1 | 73 | 6） | 願 | 75 | 53 | 54 | 57 | 47 | 47 | 44 | 34 | 41 |
| 15，（x） | 8.5 | 4 | 71 | 5） | 6 | 67 | （i） | 6.2 | 63 | 12 | 73 | 5 | 49 | 3 | 0 | 79 | 7） | 31 | 73 | 82 | 55 | 54 | 1.7 | 31 | 52 | 51 | 34 | 54 |
| 1 ra （\％） | Rícin | 70 | 72 | （1） | 74 | 711 | 72 | 65 | fifi | ${ }_{6}$ | 72 | 5tr | 5 | 11 | 71 | k 2 | 81 | 77 | 73. | ${ }^{1} 3$ | 57 | 59 | 6 | 52 | 55 | 54 | ${ }_{4}{ }_{1}$ | 58 |
| 1700 | R 7 | 73 | 34 | $7{ }^{1}$ | 79. | 72 | 76 | 67 | 711 | 3.7 | 12 | （1） | 52 | 4 | 75 | Ri， | ${ }^{2} 4$ | 81 | 73 | R5 | 59 | 6 | 71 | 53 | 54 | $\underline{1}$ | 5. | 64 |
| 18（h） | 48 | 3 | 35 | 8. | R4 | 75 | 79 | 3 ll | 13 | 79 | 71 | 63 | 54 | ${ }^{517}$ | 79 | 苜 | ${ }^{16}$ | 85 | 73 | 46 | 61 | 62 | 73. | 54 | 4 | ${ }_{1} 1$ | 01 | 69 |
| 19.10 | $8)$ | 79 | 77 | 78 | 85 | 7 | 79 | 37 | 7 H | 79 | 73 | 6 K | 55 | 55 | 79 | H | 4 | k5 | 73 | ${ }^{48}$ | 64 | 65 | 75 | 54 | 仿 | 688 | 67 | 71 |
| 210 | ${ }^{3}$ | 43 | m 1 | R0） | 87 | 78 | 39 | 76 | R2 | 71 | 7 fm | 74 | 57 | （ 1 | Hir | ＊ | Kíd | \％if | $\cdots 1$ | ＊ | 67 | iris | 77 | 54 | 6： | 69 | 72 | 74 |
| 2109 | 91 | $\pm$ | K2 | H2 | ${ }_{\text {d }}$ | kill | 79 | 79 | $\mathrm{H}_{3}$ | 74 | 79 | 7 | 59 | 1.5 | ${ }_{\text {Kib }}$ | 39 | Bri | Ril | 85 | 91 | $7!1$ | 71 | \％ | 54 | 72 | 70 | 73 | 76 |
| 27（min | $(1)$ | 57 | 55 | 55 | 5） | 5.5 | 53 | 53 | 5 | 5 | 52. | 53 | 3 | 4 | 5.7 | 5） | 57 | 57 | 57 | 61 | 47 | 17 | 5 | 36 | 48 | 47 | 52 | 51 |
| 33： 21 | 30 | 2 | 27 | 27. | $21)$ | 27 | 36 | 26 | 29 | 24 | 26 | $2{ }^{2}$ | 20 | 22 | $2 ?$ | 30 | 27 | 29 | 28 | 31 | 23 | 24 | 26 | 18 | 24 | 23 | 24 | 25 |

Hourly Relative Humidity（\％）

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| in | 5 | c |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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| © | $\bar{x}$ | $\because$ | 8 | ${ }_{6}$ | \％ | 5 | $\sim$ | n | 7 | ¢ | 8 | 二 | 단 | \％ |  | $F$ |  | $\sim$ | r | F－ | F | $\stackrel{7}{7}$ | 0 |  |
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| 97 | $\downarrow 2$ | $\downarrow 2$ | Gz | 12 | 9 | 82 | \％ | $L i$ | $\overline{s r}$ | （iz | 52 | 昭 | 0 | G | 位 | cz | 52 | Ö̇ | lit | Of | 6 | BZ | 42 | 82 | $8 \bar{L}$ | 现 | 04 | 52 | Lz | （0）U5̄ |
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| 58 | 115 | 5 | SL | ${ }^{\text {OH }}$ | $u$ | 4 | ZK | $u$ | 以 | z9 | $\dagger$ | －$\overline{\mathrm{c}}$ | ${ }^{10}$ | 外 | و | 5 | ＋19 | Hi | 15 | Li | 明 | ＋ | 昭 | ts | L | リ | 48 | Di | ＋ $\mathrm{H}_{1}$ | IkJIZ |
| 58 | K＇） | H | 5 | St | お | G | $6{ }^{6}$ | 12 | 19 | （1） | 14 | 6 |  | ¢R | ＋ | ti | 7） | I | 116 | 5 S | ＋ | 洝 | $\overbrace{}^{2}$ | Ik | ${ }_{4}$ | や | 㡎 | 9） | $L 8$ | D0＇61 |
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| 75 | \％ | ＋1 | 15 | 12 | ¢9 | 01 | 25 | Zs | $1+$ | CS | ¢ | WS | （ ${ }^{\prime \prime}$ | L＇ | \＄ | 109 | ${ }^{\prime \prime}$ | i | 81 | 4 | 29 | 45 | 55 | ＋5 | 45 | \％ | $\stackrel{L}{4}$ | （1） | 8 | （f）${ }^{\text {a }}$（ 1 |
| ${ }_{6}{ }^{\text {b }}$ | 69 | 95 | zs | 2 | （i） | 1）5 | † | \％ | Ot | zs | \％ 5 | 55 | \％9 | （1） | 1＋ | 9t | \％ | 6 | ！ | W | ¢5 | $\overline{\text { c }}$ | is | $\bar{\square}$ | z | $\stackrel{ }{+}$ | हो | $\stackrel{5}{9}$ | IIS | （m）： |
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Hourly Relative Humidity（\％）
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Hourly Relarive Humidity（\％）
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Hourly Relative Humidity（\％）

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| $\mathrm{Cl}_{1}$ | $\stackrel{3}{2}$ | \％ | $\bar{\sim}$ | W | $\pm$ | 인 | E | 5 | $\checkmark$ | － |  | C | 들 | 5 |  | 二 |  | \％ |  |  | 品 | F |  |  |
| ＋ | ¢ | 年 | 产 | \％ | F－ | ［ | E | $\bigcirc$ | 3 | $\pm$ | \％ |  | ${ }_{6}$ | 5 | \％ | ， |  | N |  |  | 5 | 5 | E |  |
| N | $\stackrel{\square}{\circ}$ | \＃ | 却 싱 | \％ | $\stackrel{1}{4}$ | $\cdots$ | 0 | 3 | 5 | 3 | 3 | 3 | 8 | F |  | $\pm$ |  | F | － |  | $\stackrel{\text { r }}{\sim}$ | $\stackrel{5}{5}$ | ＝ |  |
| N |  | 5 | 5 | 8 | $\underset{\sim}{0}$ | c | \％ | 간 | 1 | F | $\pm$ | $\stackrel{\sim}{5}$ | $\stackrel{1}{2}$ | $\bar{z}$ | 5 | ¢ | ！ | 8 | 줒 | \％ | $=$ | \＆ | 5 |  |
| त | 8 | \％ | \％ | S | F | \％ | F－ | $\stackrel{ }{2}$ | \％ | 5 | $\stackrel{\sim}{*}$ | T | 3 | $:$ | 8 | － | ＊ | 倖 | 츨 |  | $\equiv$ | \％ | E |  |
| － | $\pm$ | \％ | ，遠 | $\Rightarrow$ | F－ | $\stackrel{+}{*}$ | $\cdots$ | 2 | 只 | N | \％ | 5 | \％ | $\overline{\text { E }}$ | 家 | $\stackrel{1}{8}$ |  | $\cdots$ | H | E | N | $\bar{\square}$ | 今 |  |
| 3 | ㅊ | $:$ | ［ ${ }_{\text {a }}$ | \％ | ： | $\stackrel{-}{\text { F }}$ | $\stackrel{\square}{8}$ | 5 | 5 | $\pm$ | E | 장 | $今$ | F | ${ }^{2}$ | $\pm$ | $\Sigma$ | \％ | 5 | E | 8 | $\stackrel{3}{ }$ | H |  |
| 9 | S | C | \％ | $\pm$ | 2 | 12 | － | 今 | ¢ | C | T | $\because$ | $\pm$ | 3 | r |  | r | \％ | 5 | 찬 | ： | 號 | $\stackrel{3}{4}$ |  |
| $\stackrel{\sim}{-}$ | － | 完 | 찿 | $\stackrel{ }{\sim}$ | F－ | $\hat{3}$ | $\bigcirc$ | $\underline{=}$ | ＋ | 5 | E | 3 | 3 | F | － | $\cdots$ | x |  | \％ | \％ | 浐 | 줒 |  |  |
| $\because$ | ${ }^{*}$ | 三 | 숮 | 2 | \％ | 7 | $F$ | F | 9 | 장 | $\cdots$ | F－ | 듣 | F－ | $\cdots$ | ＝ | \％ | ${ }^{\text {r }}$ | \％ | B | 8 | ᄃ |  |  |
| $\cdots$ | \％ | 5 | 惹 | $\because$ | $\pm$ | $\pm$ | $\stackrel{3}{3}$ | 込 | 출 | 9 | $\stackrel{\rightharpoonup}{x}$ | \％ | 完 | \％ | 5 | 5 | － | a | E | $\stackrel{1}{ }$ | 秥 | 2 |  |  |
| $\pm$ | $=$ | ¢ | 2 | t | ct | 5 | \％ | 梁 | $\geqslant$ | F | 조 | 프즈N | I | N | $\pm$ | ＇ | a | x | － | 자즐 | 줒 | \％ | 3 | 5 |
| m | \％ | 2 | 5 | $z$ | $\pm$ | $\stackrel{*}{\circ}$ | \＆ | 5 | $\stackrel{\square}{5}$ | 5 | F－ | 5 | 5 | 5 | $\because$ | － | \＆ | $=$ | 0 | 8 | 5 | E | ＇s | ¢ |
| $\stackrel{\sim}{7}$ | $\stackrel{\text { ¢ }}{ }$ | 5 | ${ }_{\sim}^{2}$ | E | \％ | I－ | \％ | N | － | \％ | $\therefore$ | 2 | $\overline{\bar{x}}$ | 号 | \％ | ） | ¢ | \％ | 「 | 号 | ${ }_{5}$ | $\stackrel{\square}{8}$ | $\pm$ | $\overline{\text { a }}$ |
| $=$ | $\stackrel{\sim}{*}$ | $\Sigma$ | $\equiv$ | 줓 | 三 | \％ | 等 | 二 | 10 | ${ }^{\text {c }}$ | $\bar{x}$ | ${ }^{\prime}$ | 號 | $\pm$ | 5 | \％ | 三 | E | 5 | 笖 | N | $\stackrel{1}{ }$ | ＝ | m |
| 9 | 空 | \％ | 5 | \％ | \％ | 玉 | \％ | F－ | 空 | $\overline{\bar{s}}$ | $7{ }^{2}$ | F－ | $\mathrm{i}^{\mathrm{n}}$ | F－ | 촐 | x | x | ＇${ }^{\text {r }}$ | ${ }_{\infty}$ | ¢ | c | $3{ }^{2}$ | 二 |  |
| 9 | ${ }_{5}$ | 古 | \％ | 2 | $\sim$ | F | C | f： | F | ${ }^{1}$ | 찿 | r $=$ | \％ | F | $\stackrel{\sim}{2}$ | 気 | $\overline{\bar{x}}$ | 実 | 玉 | 每 | \％ | $x$ | ［ | ${ }_{5}$ |
| $\infty$ | 5 | N | r＝ | $\stackrel{7}{7}$ | \％ | 6 | S | $\pm$ | \＃ | $\cdots$ | 5 | 5 | 5 | $\stackrel{5}{0}$ | ¢ | 1 | $1 \sim$ | $\cdots$ | F－ | $\stackrel{\square}{\text { F }}$ | s， | \％ | n | $\mathrm{Fi}_{1}$ |
| m－ | 3 | $\overrightarrow{\mathbf{x}}$ | $\overline{\text { c }}$ | \％ | $\stackrel{\sim}{\sim}$ | 3 | 5 | 5 | $E$ | E | 5 | $\checkmark$ | 5 | 寺 | C | F | F－ | \％ | F－ | 장 | § | $\vec{\square}$ | $\stackrel{\rightharpoonup}{\sim}$ | F |
| $\checkmark$ | 3 | $\cdots$ | \％ | R | $\mathrm{r}^{2}$ | 준 | S | \％ |  | 7 | T | $\stackrel{4}{5}$ | 2 | $\stackrel{5}{5}$ | in | \％ | \％ | P－ | E | $\stackrel{+}{-}$ | 去 | § | छ | F |
| ＇ | $\stackrel{5}{5}$ | $\stackrel{ }{5}$ | 9 | E | 边 | 2 | ${ }_{\sim}^{x}$ | \％ |  | F＝ | F | ＝ | 「 | $\cdots$ | ${ }^{\text {\％}}$ | 5 | ㅊ | 딜 | － | （ | ［ | $\pm$ | $\because$ | ＋ |
| ＊ | ＊ | 8 | $E$ | $\bar{\square}$ | $\overline{7}$ | \％ | \％ | 춫 | 8 | 劲 | 新 | $\stackrel{*}{x}$ | \％ | 5 | 江 | 「 ${ }^{\text {r }}$ | \％ | 告 | $\stackrel{1}{2}$ | 宗 | 3 | \％ | 5 | \％ |
| $\cdots$ | \％ | S | 8 | $\stackrel{\sim}{2}$ | $\stackrel{1}{\sim}$ | 잦 | 号 | 客 | 院 | 8 | 安 | $\underset{\sim}{2}$ | 자ㅈㅏㅜ | 2 | $\bar{\square}$ | $\stackrel{\square}{5}$ | ： | $\stackrel{\text { H }}{\text { ¢ }}$ | $\mathfrak{N}$ | $\stackrel{7}{7}$ | $\stackrel{ }{-}$ | 8 | こ | 二 |
| N | 5 | 囦 | 弾 | \％ | 축 | \％ | ${ }_{5}{ }^{2}$ | ${ }^{-1}$ | 部 | 筀 | 3 | $\overline{2}$ | 湥 | $\stackrel{3}{\circ}$ | $\stackrel{ }{2}$ | 8 | こ | 5 | 5 | 5 | 5 | 2 | ＇s） | F |
| － | 잉 | 2 | \％ | 管 | 5 | E | 思 | E | 5 | \％ | 7 | 寺 | $\stackrel{8}{2}$ | 존 | N | 关 | d | 2 | 5 | \％ | \％ | 8 | 5 | － |
| Э |  | S | 気 | 㲾 | 令 |  | 8 | 浸 | $\stackrel{\text { ¢ }}{ }$ | 줄 | 蔁 | 新 | $\frac{3}{2}$ | $\stackrel{8}{8}$ | $\stackrel{5}{7}$ | 동 | $\underset{=}{E}$ | 클 | 8 | $\underset{\substack{c \\ \hline \\ \hline}}{ }$ | 室 | 涍 |  |  |

Hourly Relative Humidity（\％）

Yeas 20015 Monds：2ugust

| Day | 1 | 2 | 3 | 4 | 5 | U | 7 | 8 | 9 | 114 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 11） | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | ． 30 | 31 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tinue |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $0 \times 0$ | B7 | 87 | 84 | ＊1． | 911 | 92 | HK | 122 | 12 | 浐 | 上5 | 06 | 05 |  | 犋 | 93 | 1） | り5 | 23 | 模 | 122 | 94 | 外 | 973 | 91 | 的 | 92 | 92 | 9 | 92 | 92 |
| 101 | 43 | Mis | 84 | 阶 | 47 | 91 | k7 | $\mathrm{R}_{\mathrm{c}}^{4}$ | リ4 | 45 | 35 | 明 | 21 | 94 | 絈 | 92 | NG | $9+$ | 4 | ${ }_{4}$ | 21 | リ3 | 8 k | 91 | H5 | 90 | R7 | 納 | 83 | 87 | R？ |
| 20 M | 7 R | 86 | （4） | 旺。 | 83 | $\mathrm{ki}^{1}$ ） | 47 | H3 | 95 | 頻 | 95 | 9 | 48 | 9 | R3 | 91 | \％ 4 | 94 | 45 | － | 919 | 93 | 陈 | RM） | H8 | Kis | R1 | 84 | \％ | R2 | h3 |
| 500 | 74 | 85 | 71 | R． | \＄ | M | 碞 | 79 | แ | 95 | 05 | 87 | H4 | 9 t | K1 | 121. | 75 | 03 | ${ }_{1} 1$ | 76 | ${ }_{6}$ | 52 | ${ }_{3}{ }_{4}$ | K7 | 46 | 83 | 7 m | 级 | 00 | 77 | 7 H |
| 4 | （1） | 78 | 73 | His | 77 | 85 | n 1 | 35 | 97 | 93 | 91 | 34 | \％ 2 | \％${ }_{6}$ | 71 | N2 | 72 | 91 | 42． | 73 | $\mathrm{H}_{4}$ | 87 | 82 | R5 | 85 | 79 | 35 | 75 | 68 | 74 | RO |
| 51 ln | 65 | $7(1$ | $\mathrm{S}_{1}$ | 3， | 73 | 81 | 37 | （0） | 6 | 92 | 87 | \＄2 | 79 | KS | 34 | 7.4 | 71 | B ${ }_{\text {H }}$ | ${ }^{1}$ | 71 | 3 | 8 | R1 | R 4 | 8， 4 | 74 | 74 | 71 | 6 B | 74 | 82 |
| 616 | 60 | 63 | 67 | $7{ }^{7}$ | 711 | 78 | 72 | y | 犗 | 91 | K． | 73 | 37 | H 2 | $7{ }_{7}$ | 6it | 67 | KG | 43 | （i，${ }_{\text {c }}$ | 75 | 77 | 7 | ${ }^{4} 2$ | 83 | 7 J | 3.7 | 64） | 67 | 67 | R4 |
| 7.06 | 5\％ | 62 | ［i］ | 73 | 72 | 77 | 311 | \％ | （9） | 53 | 74 | 74 | 75 | 3 H | is | 73 | 67 | $\mathrm{Ki}_{1}$ | 81 | $7 \%$ | 77 | $\mathrm{H}_{2}$ | 77 | 沙 | 83 | 6 H | 58 | 6.4 | 67 | Gu | 82 |
| $\mathrm{H}_{5}(\mathrm{X})$ | 57 | 67 | tir | 71. | 73 | 77 | 6） | 91 | H 2 | $\mathrm{Hi4}$ | 7.4 | 72 | 73 | 75 | 75 | 4 | 6,7 | $\mathrm{Kl}_{1}$ | 7 K | ［ 41 | 79 | k7 | 75 | 75 | ${ }^{\text {盐 }}$ | $\mathrm{f}_{6} 7$ | N2 | 63 | 6.7 | 6.4 | 39 |
| 9） $0^{0}$ | 55 | （1） | 6i | 61） | 75 | 76 | 67 | 197 | 75 | 41 | （t） | 1,9 | 71 | 71 | 74 | $k 7$ | 63 | 78 | 76 | リ2 | R1 | 22 | 71 | 72 | 79 | 1,5 | 87 | $6[$ | 67 | 63 | 77 |
| 10（b） | 58. | 0.5 | 6 R | 73 | ［4） | 77 | ＋1 | 124 | 73 | 4］ | 71 | 75 | 71 | 7.3 | 73 | $\mathrm{H}_{3}$ | ［ition | 76 | 76 | 水 | 8.8 | $\mathrm{KH}{ }^{\text {\％}}$ | 36 | 75 | ＊ | 71 | 85 | 64 | 6 | 66 | 76 |
| 11.00 | 61 | GS | 6 R | 只5． | 88 | 719 | 75 | リ2 | 7） | ＊2 | 77 | \％ 21 | 72 | $7+$ | 72 | Kll | 隹 | 73 | 75 | 87 | R $\mathrm{R}_{6}$ | H＋ | 78 | 79 | R2 | 36 | 82 | 67 | 70 | （1） | 76 |
| 12.000 | 64 | 12 | （1） | 93 | 物 | 刮 | 79 | $8{ }^{4}$ | 81 | स2 | 74 | $\mathrm{Mf}_{1}$ | 37 | 76 | 71 | 36 | 69 | 71 | 7.2 | 85 | K＇） | H | 81 | 32 | $\mathrm{R}_{3}$ | ${ }^{1} 2$ | W | －70 | 72 | 72 | 75 |
| 13.14 | 们 | 72 | 71 | 92. | 刮 | 22 | 83 | c） | 85 | Hif | $31)$ | Rif | 75 | 74 | 31 | 77 | 11 | 74 | 76 | $8{ }^{\text {dfi }}$ | Dir | 4.7 | 84 | R7 | H．${ }^{\text {a }}$ | $\underline{4}$ | B2 | 74 | 75 | 75 | ， 1 |
| 14－00 | 71 | 7.3 | 73 | 91 | Hi） | 85 | H | 9 | R8． | 911 | X 4 | K7 | 7 C | R1 | 37 | 77 | 74 | 73 | 76 | R ${ }_{\text {R }}$ | i） | 为 | 㬉 | 91 | 83 | 87 | H． 4 | 78 | 77 | 79 | B4 |
| 15100 | 71 | 7.7 | 75 | fiv． | H9） | 87 | ＇＊1． | 91 | 92 | 14 | S | 4， 7 | 81 | $\mathrm{H}_{3}$ | 911） | 7 T | $7 \mathrm{~F}_{1}$ | Rin | 77 | 阿 | 92 | 89 | 40） | 吅 | H3， | 89 | R ${ }_{4}$ | H2 | 8 g | 82 | k ${ }^{\text {d }}$ |
| $16.1 \times 1$ | 75 | 74 | 711 | Ki） | （4） | k7 | 01 | 92 | 02 | 94 | \％ | 49 | ${ }_{3} 3$ | $\mathrm{H}_{4}$ | 81 | ${ }_{4} 1$ | 79 | H2 | 719 | $\mathrm{H}^{\prime \prime}$ | 11 | on | 榢 | ？ | 35 | （3） | k7 | 的 | 43 | 84 | HH |
| 17 Ol | 77 | 75 | R3 | H | 91 | KK | 91 | Q2 | 92 | 15 | 41 | （91） | ＊S | $\mathrm{HCH}_{1}$ | 82 | 83 | R C | Y5 | 8 t | D19 | 89 | \％ | 91 | 25 | ¢ | （ $\times 1$ | RM | 45 | 86 | 87 | H2， |
| LSint | 74． | 76 | K＇ | 895 | 92 | $\mathrm{HiS}_{4}$ | 122 | 93 | 灶 | リ5 | 923 | 92 | R 7 | 47 | H3 | R5 | 炜 | － $\mathrm{H}_{7}$ | $\mathrm{R3}$ | 219 | 縑 | 91 | 21 | 15 | 00 | M | $\mathrm{H}^{\prime}{ }^{\prime}$ | 88 | 89 | 陣） | R7 |
| ［1）${ }_{\text {ch }}$ | 81 | R＇ | 48 | \＄9 | 23 |  | リ1 | 43 | 壮 | 95 | 97 | ． 92 | K） | 87 | $\mathrm{HF}_{6}$ | K7 | ¢4 | ${ }^{87}$ | H． | 10 | R9 | 91 | 21 | 4.7 | 91 | 21 | 45 | 留 | （0） | H7 | 98 |
|  | K2 2 | ¢7 | ［14． | 吅 | り3 | ［40 | 91 | 92 | 53 | 95 | 94 | 93 |  | ד | $x_{1}$ | K\％ | ${ }_{4}$ | 8 R | $\mathrm{K}_{1} 1$ | J！ | 少 | 911 | 21 | 92 | 92？ | 21 | 919 | 29 | F 5 | 枵 | 90 |
| $21-1 \times 1$ | 8.4 | 20 | （9） | Kh | 明 4 | 48 | ¢ ${ }^{\text {c }}$ | 92 | 93 | 25 | 15 | 93 | ［4 | Ki | 23 | ，2110 | $\mathrm{H}_{2}$ | $\mathrm{HR}_{\mathrm{H}}$ | 87 | ¢1 | 22 | ㅂㅣㅏ | ［12 | － $\mathbf{K}_{1}$ | 93 | 42 | 9 | 9 | R2 | 90 | 72 |
| $22.1 \times 1$ | 54 | （il） | 59 | 5リ | （ 1.3 | 59 | （al | 61 | 6.2 | 41 | （i） | ［1］ | is | 5 K | 121 | fill | 53 | 51 | 58 | （ k ） | 4.1 | （ | （1） | 硕 | 6 | S， 1 | （0） | 61 | 50 | （1） | 61 |
| 230\％ | 2 d | 30 | ¢ | 29 | 31 | $2)$ | आ | 31 | 31 | 32 | 12 | 11 | 29 | 2） | 31 | 30 | $\underline{27}$ | 21 | 29 | ＊） | 31 | 3.3 | 31 | ． 3 | 31 | 31 | 30 | 30 | 31 | 30 | 31 |

Hourly Relative Humidity（\％）

| Year． 2005 Mombl september |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dar | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 17 | 13 | 14 | 15 | 16 | 17 | 28 | 15 | 20 | 21 | 22 | 33 | 24 | 25 | 26 | 27 | 28 | 21） | 30 |
| Time |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| OWh | 97 | 95 | 9f1 | 20 | 93 | 97 | 122 | 98 | 97 | 94 | $2 \%$ | ${ }^{1} 3$ | 8.3 | \％ | 45 | 79 | $\mathrm{K}_{3}$ | 77 | H7 | \％ | 25 | 93 | ． 25 | $9:$ | 5 | $\%_{1}$ | 97 | 45 | 2¢ | A8 |
| 1－（k） | ，${ }^{1}$ | R9 | Ru | 4 | KR | R 7 | 8 ra | 92 | 93 | 2） | ＊ 4 | 77 | （2） | R 5 | 88 | 7 K | 限 | 74 | R4， | 14. | \％ | E7 | 91 | 姩 | 93 | ， | 91 | 42 | 92 | 85 |
| ？ 2 （k） | R3 | R3． | A． 5 | 79 | R．4． | 38 | \＄11 | W7 | RH． | H7 | 85. | 72 | 7 F | 7） | 84） | 7 k | 7 H | Cis | 71 | リ1 | \％ 5 | R1 | 67 | 外 | K1） | R4 | H＋ | 78 | 89 | B3 |
| 301 | 36 | 37 | 79 | 73 | －${ }^{\text {il }}$ | 6 | 74 | － HL | $\mathrm{K}_{4}$ | ， 3 | ${ }_{4}$ | fit | 75 | 34 | 73 | 77 | 75 | C | 只 | 49） | 8＊ 1 | 75 | 3.3 | 水 | R斤 | 78. | 77 | 75 | 85 | ［m |
| 4．（M） | 37 | 71 | 75 | 7 | k3 | ${ }^{1} 5$ | 42 | 77 | K］ | 77 | $7{ }^{7}$ | 估 | （6） | 511 | （6） | －72 | 72 | $\underline{62}$ | 6.4 | 49 | 76 | 74 | 81 | 93 | R？ | 76 | 34 | 71 | 枵 | 7 |
| 5． ¢ $_{\text {H }}$ | 77 | $\mathrm{c}_{1}$ | 74 | 俔 | s7 | 62 | $\mathrm{M}_{1}$ | 34. | 79 | 71 | 74 | 62 | （i） | 66 | 65 | fí | （6） | ¢， 1 | 6 | \％ | 7. | 71 | 79 | k） | \％ | 73 | 72 | $6{ }_{6}$ | Rk | 71 |
| （fill | 7 k | 63 | U， | Gí | 41 | $5 y$ | 144 | 311 | 76 | －6．4 | 71 | 住 | 57 | $\underline{6}$ | f．1 | ${ }_{6} 1$ | 66 | 5） | ${ }_{6} 1$ | 9 | （i） | （i） | 7 | R 4 | 75 | 71 | 69 | 64 | BP | $\mathrm{fi}_{7} 7$ |
| 7 lm | R2 | 69 | 6 | cis | 91. | 57 | 94 | ${ }_{6} 1$ | 7.3 | 1.3 | 67 | 6 | 118 | 62 | C．1） | （i） | 65 | 5\％ | 6.3 | 92 | 6.8 | 76 | 78 | Br－ | 78 | 6 k | 69 | 70 | kS | 77 |
| $8.0)$ | R＇5 | 3 | ¢19 | 71 | 91 | 54 | 1／N | 4.65 | $0{ }^{0}$ | 6. | （1） | f，ut | 12 | 63 | 5！ | 59 | 64 | Sti | 1.5 | $1{ }^{1}$ | $6{ }_{6}$ | 83 | 7 R | R4 | $4]$ | 6ris | 62 | 7 | $k 1$ | 86 |
| 9 9（3） | 49 | 74 | 12 | 73 | 9 t | 53 | 98 | 62 | $6 \square_{1}$ | ［i2． | （1） | （11） | 6.5 | 6．3． | 58 | 58 | 6.3 | 55 | 67 | 名 | 1.5 | 9） | 79 | $\mathrm{K}_{4}$ | 84 | 6.3 | 69 | $\mathrm{B}_{3}$ | 77 | 56 |
| 10：00 | 8 | 35 | 6i4 | 74 | \％ | 54 | ${ }^{58}$ | $6{ }_{6}$ | 67 | 6.4 | 6,2 | 15 | 75 | 64 | 6.2 | 61 | 6 | 59 | 67 | 26 | 68 | 49 | $\mathrm{B}_{4}$ | hS | $\mathrm{Hf}_{6}$ | 68 | 77 | R5 | 74 | 96 |
| 11 （x） | ${ }_{2} 2$ | $7{ }^{7}$ | （ $6_{6}$ | 74 | － | 16 | 97 | A 11 | ［i8） | 67 | 64 | （1） | R5 | 74 | 6.5 | 63 | fin | 6.2 | 67 | 15 | 72 | 87 | 911 | 85 | 88 | 74 | R5 | R | \％ | 97 |
| 1201 | 71 | 77 | 6 R | 75 | 47 | 7.3 | 97 | 74 | （1） | 69 | 85 | 74 | 25 | 79 | （1） | fit | 71 | （ris | 67 | 95 | 75 | 的 | 95 | $\mathrm{Hf}_{1}$ | 0 | 79 | 93 | \％88 | 79 | 97 |
| （3）（4） | 43 | 79 | 72 | 37 | m9 | 75. | 9 | 77. | 73 | 77 | 71 | 75 | 111 | 处． | 72 | $\mathrm{CaH}^{2}$ | 74 | （6） | 71 | \％ | 77 | R3 | リ5 | 49 | $x$ | $\mathrm{H}_{3}$ | 27. | 48 | 81 | 97 |
| 1＋10） | 8 k | ． 1 | 75 | \％ | （） | 76 | $\%$ | 79 | 7 H | 85 | 75 | 75 | 47 | kt | 74 | G） | 76 | 7，${ }^{3}$ | 74 | \％ | Pal | к） | リ4 | 91 | K1 | 4 | 2） 3. | ＊ 9 | ${ }_{3} 3$ | 2 |
| 15，14， | 92 | $\mathrm{H}_{3} 3$ | 79 | k 2 | 92 | 78 | 45 | R2 | K11 | 21 | ＊111． | 76 | ${ }^{3}$ | k 2 | 77 | 71 | 79 | \％ | 78 | 97 | $\mathrm{H}_{3}$ | 91 | 54 | 94. | Rip | 42 | 93 | 89 | ${ }^{2} 5$ | リf |
| 16．（0） | 听 | 45 | B1． | K2． | 13. | ${ }_{31}$ | 95 | K？ | H2 | 12 | ${ }_{8}$ | 78. | 84 | $\mathrm{Hfi}_{1}$ | （1） | 74 | 71 | 37 | 时． | 2 | ${ }^{14}$ | 91 | 94 | 95 | ${ }^{2}$ | $\mathrm{y}_{2}$ | 0.3 | 81 | ${ }^{\text {en }}$ | 72 |
| 17．（\％） | 91 | kR | 64 | 8,3 | 94 | 84， | \％ | $1{ }^{1} 1$ | 37 | 42 | ${ }_{4}$ | 79 | $H_{1}$ | k＇） | 83 | 7 | 74 | 38 | 91 | 2 | ${ }^{4} 5$ | 9 | 94 | リ | 1.1 | 93 | 42 | Bk | $6{ }_{6}$ | 46 |
| ［3，46） | 93 | 2， 1 | Hí | 83 | 95 | k7 | $\square_{6}$ | 126 | 85 | 93 | 92 | 81 | $k 7$ | 43 | 拓 | Pa1． | 79 | 79 | 97 | 訾 | $8{ }^{4}$ | 91 | 24 | リ 3 | 22 | 93 | 92 | kin | 89 | 96 |
| 1910） | $9+$ |  | 4 | \＄8 | 95 | 8i4 | $1{ }_{1}$ | 96 | 87 | 94 | 22 | 12 | к） | 9．3 | RT | R17 | $7{ }^{7}$ | 81 | 97 | 45 | 桇 | 91 | $1{ }_{4}$ | 17 | ． 92 | 24 | 92 | R9 | 5i） | 96 |
| 200 | 9， 4 | 89 | 87 | R5 | 95. | x） | 95 | 97 | kis | 194 | 92 | 12 | 归 | 93 | R） | 41 | H1．） | k2 | － 91 | 14 | ${ }_{\text {Hik }}$ | 9 | 0.3 | 96 | 93 | 94 | 22 | 13 | 910 | \％ 6 |
| 2 t | 05 | 89 | $\mathrm{k}_{7}$ | $\mathrm{BH}_{5}$ | 05 | T0． | 95 | 27 | ） | 15 | 22 | 83 | 92 | 93. | 12 | $\cdots 1$ | （1） | R．t | \％ | 牰 | R＇） | 91 | 明 | 96 | 94 | 195 | 22 | 92 | 919 | $\%$ |
| 22：14．18 | 13 | 51）． | 5i | 57 | 6 | （ $\times 1$ | 63 | $4_{1}$ | fil | $(3)$ | 41 | 5 | 61 | 1.2 | $(11)$ | 54. | 51 | 50 | $\mathrm{f}_{1}$ | 63 | 51 | ［1． | ${ }_{6} 1$ | 6 | 6，3 | $6{ }^{6}$ | 4 | 61 | 60 | 6,4 |
| $\underline{23.109}$ | 32 | 30 | 29 | 29 | 32 | 3 | 32 | 32 | 30 | 32 | 31 | 23 | 31 | 31 | 3 | 27 | 27 | 28 | 32 | 31 | 30 | 30 | 31 | 32 | 31 | 32 | 31 | 31 | 30 | 32 |


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| 会 | S | $\stackrel{1}{2}$ | $\stackrel{\sim}{\sim}$ | $\cdots$ | cin | ¢ | $\stackrel{+}{7}$ | ¢ | 子 | \％ | N | F | $\stackrel{\square}{5}$ | $\stackrel{\sim}{5}$ | 5 | 즌 | 灾 | 交 | 「－ | 웡 | $\stackrel{\sim}{2}$ | $\stackrel{1}{2}$ | $=$ |
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| 9 | $\stackrel{\square}{\square}$ | $\pm$ | P | $\sim$ | 8 | 0 | $=$ | 式 | Fi， | 午 | 等 | N | ＋ | in | ${ }_{5}$ | E | d | E | 3 | $\bar{F}$ | $\cdots$ | $\cdots$ | $\overline{7}$ |
| $\stackrel{1}{2}$ | 交 | － | $\stackrel{4}{\square}$ | 존 | E＊ | ～ | F | 자자N | 0 | 嫁 | ${ }_{9}$ | 5 | is | 5 | ［2 | 3 | $\stackrel{\rightharpoonup}{2}$ | N | 走 | 気 | 交 | 法 | 伥 |
| － | ～A | 管 | Nㅣㄷ | 등 |  | $\stackrel{4}{4}$ | $\pm$ | 筞 | $\stackrel{\sim}{2}$ | ＋ | ～ | 上 | $\bar{F}$ | \％ | \＃ | 耑 | \％ | $\stackrel{\square}{4}$ | 空 | S | 二 | $\overline{5}$ | $\cdots$ |
| ㄷ | $\stackrel{8}{8}$ |  | 3 | 永 8 | ＋ 7 | \％ | 水 | $\stackrel{\sim}{\sim}$ | $\sim$ | F | 잔 | s | $\pm$ | $\underset{\sim}{2}$ | $\infty$ | I | $\pm$ | $\sim$ | 2 | 年 | $\stackrel{\square}{\square}$ | \％ | ลิ |
| $=$ | $\sim$ | 3 | ${ }^{3}$ | 5 | 砍 | \％ | 조 | $\geqslant$ | $\stackrel{\sim}{*}$ | 寺 | $\stackrel{\square}{\circ}$ | 9 | $\cdots$ | N | － | $\underset{\sim}{2}$ | $\widetilde{8}$ | 17 | 「 | 줒 | $\hat{\square}$ | $E$ | 9 |
| $\infty$ | 先 | 5 | $\stackrel{*}{*}$ | $\stackrel{\sim}{2}$ | 37 | $\stackrel{\sim}{m}$ | 좆N | ミ | \＃ | $\underset{\sim}{7}$ |  | 5 | $\stackrel{\sim}{c}$ | $\cdots$ | 7 | $\geqslant$ | $\stackrel{4}{2}$ | 3 | ${ }^{\text {r }}$ | 촟 | $\pm$ | 5 | 家 |
| r | 云 | $\stackrel{*}{*}$ | $\cdots$ | 令 | （ ${ }^{\text {in }}$ | 7 | $\cdots$ | 장 | 5 | 拄 | 놀 | 奚 | 3 | $\cdots$ | $\stackrel{1}{6}$ | F－ | 晏 | \％ | 좆 | \％ | \％ | n | 三 |
| $\stackrel{+}{4}$ | 宗 | \％ | N | 空 |  | 7 | － | 4 | $\cdots$ | nir | T | ＋ | f． | $F$ | 3 | $\stackrel{\sim}{2}$ | ＊ | ¢ | \＃ | $\stackrel{7}{2}$ | $\underset{\sim}{x}$ | 3 | ลे |
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| 寸 | 7 | 7 | F | 9 | 吕 | 8 | 5 | n | ＋ | 念 | $\pm$ | \％ | $F$ | c | F－ | \％980 | \＃ | 3 | 二 | 完 | 会 | \％ | $\hat{\text { הे }}$ |
| en | 5 | ： | 조 | $\cdots$ | $\stackrel{\square}{7}$ 会会 | $\pi$ | 字 | 南 | 示 | 守 | n | 寝 | N | ＊ | 2 | F－ | 家 | 9 | in | $\cdots$ | 会 | ㄹ | $\underset{1}{1}$ |
| $\cdots$ | 3 | 「 | \％ | 앙 | E 9 | 7 | 于 | 守 | 7 | in | 令 | 5 | $\cdots$ | \％ | $\stackrel{*}{2}$ | 7 | 豆 | $\bar{x}$ | \％ | ${ }^{2}$ | 立 | $\stackrel{*}{*}$ | 令 |
| $\cdots$ | 8 | \％ | 30 | N | \＄ | 「 | H0 | 7 | $\stackrel{+}{7}$ | N | ${ }_{6}$ | \％ | $\cdots$ | ミ | 0 | $\pm$ | 옫 | 좆 | 三 | $\Sigma$ | $\stackrel{\sim}{2}$ | c | $\vec{\square}$ |
| 呺 | $\stackrel{3}{5}$ | 完 | 崈 | $\hat{S}_{\text {S }}$ |  | $3$ | $\underset{\vec{i}}{\vec{k}}$ | 氠 | 空 | 8 |  |  | 家 | 荃 | ํㅡํ | $8$ | － | 苞 | 家 | 空 | 家 | $\underset{\sim}{2}$ | \％ |

## APPENDIX E+ Hembly Cow Coret (\%)

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## 14burty Oland Cower (50)


APPENDIX F: Daily Total SunShine Hours
Daily Total SunShine Hours

| Year 2005 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Day | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |  |  |  |  |  |
| Mronth |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2. |  | 25 | 26 | 27 | 28 | 29 | 30 | 31 |
| Tanuary | 73 | 3.8 | 5.1 | 1.4 | 6.7 | 8.2 | 8.2 | 8.0 | 77 | 8.1 | 0.0 | 87 | 7.5 | 81 | 6.7 | 7.3 | 5.2 | 3.9 | 49 | R 5 | 80 | 28 | 00 | 6 | 89 | 7 |  |  |  |  |  |
| Felruact | 0.8 | 9.0 | 8.4 | 8.9 | 76 | 5.2 | 7.2 | 80 | 8.6 | 8.6 | 9.1 | 2.4 | 0.6 | 97 | 07 | 83 | 68 |  |  |  |  |  |  |  |  |  |  | 4.2 | 40 | 8.3 | 84 |
| March | 9.8 | 2.5 | 92 | 9.6 | 9.0 | 8.8 | 7.9 | 58 | 26 | 88 | 01 |  |  | -3 |  |  | 6.8 | 8.4 | 3.6 | 4.8 | 0.9 | 5.0 | 8. | 8.8 | 9.5 | 9.8 | 95 | 2.2 |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  | 01 | 0.0 | 8.8 | 8.3 | 3.5 | 9.3 | 8.2 | 2.1 | 5.2 | 9.2 | 90 | 6.8 | 2.6 | 0.9 | 8.5 | 8.3 | 2.3 | 8.3 | 7.1 | 5.2 | 27 |
| $\therefore$ April | 7.5 | 9.0 | 8.2 | 9.9 | 2.3 | 9.7 | 86 | 9.0 | 6.7 | 82 | 7.7 | 6 H | 9.8 | 9.4 | 9.6 | 8.5 | 8.6 | 10.0 | 75 | 3.0 | 10.5 | B6 | 8.8 | 0.1 | 7.1 | 7.5 | 8.6 | 8.8 | 6.4 | 8.1 |  |
| Mar | 7.6 | 44 | 10.9 | 56 | 59 | 9.4 | 10 B | 6.8 | 4.5 | $9+$ | 8.2 | 96 | 9.3 | 8.7 | 72 | 9.2 | 7.4 | R 3 | 3.9 | 9.4 | 5.8 | 1.6 | 3.2 | 5.1 | 7.2 | 10.0 | 96 | 9.4 | 92 | 11.3 | 11.1 |
| Juse | 9.1 | 77 | 9.5 | 7.9 | 76 | 9.4 | 8.1 | 6.4 | 8.4 | 37 | 18 | 3.1 | 0.6 | 1.0 | 02 | 00 | 0.3 | 39 | 2.0 | 1.8 | 1.5 | 0.0 | 0.3 | 2.4 | 0 t | 1.6 | 0.4 | 0.0 | 00 | 0.0 |  |
| Iuks | 0.6 | 0.0 | 0.0 | 01 | 0.4 | 8.8 | 105 | 7.6 | 4.7 | 0.6 | 0.2 | 15 | 0.0 | 1.4 | 0.0 | 0.5 | 8.9 | 3.6 | 45 | 1.9 | 4.6 | 0.1 | 3.4 | 8.3 | 10.0 | 67 | 7.1 | 7.3 | 2.1 | 7.3 | 9.6 |
| dugust | 8.8 | 6.0 | 6.9 | 2.8 | 3.6 | 1.0 | 3.3 | 0.2 | 1.0 | 0.0 | 32 | 1.7 | 2.9 | 1.8 | 3.9 | 34 | 9.5 | 3.3 | 16 | 3.9 | 2.6 | 2.6 | 0.7 | 0.4 | 0.7 | '6.1 | 4.2 | 9.0 | 5.6 | 1.8 | 4.7 |
| September | 2.7 | 5.4 | 6.4 | 3.2 | 0.0 | 7.8 | 1.2 | 7.2 | 48 | 5.3 | 77 | t0. 1 | 4.0 | 4.7 | 2.7 | 97 | 4.4 | 102 | 78 | 0.0 | 5.1 | 5.0 | 23 | 2.1 | 0.0 | 5.3 | 3.4 | 2.7 | 4.3 | 2.6 |  |
| October | 00 | 0.0 | 30 | 1.5 | 7.1 | 96 | 6.7 | 29 | 92 | 8.5 | 35 | 3.4 | 6.0 | 9.4 | 2.9 | 39 | 1.8 | 6.8 | 18 | 0.0 | 0.0 | 0.0 | 00 | 1.9 | 0.0 | 7.1 | 7.6 | 0.8 | 7.6 | 9.6 |  |
| November | 55 | 9.7 | 95 | 9.6 | 2.6 | BR | 8.3 | 00 | 5.1 | 7.6 | 9.3 | 9.3 | 9.1 | 84 | 7.7 | 8.6 | 8.2 | 84 | 6.6 | 3.9 | 2.0 | 3.8 | 09 | 0.2 | 3.2 | 14.0 | 7.2 | 8.2 | 82 | . 2 | 2, 8 |
| December | 7.7 | 8.3 | K. 1 | 4.5 | 82 | 7.9 | 8.2 | K0 | 8.0 | 8.6 | 8.4 | 8.6 | 87 | 8.5 | 8.2 | 7.4 | 0.8 | 27 | 7.3 | 8.3 | 7.3 | 0.0 | 5.2 | 8.0 | 8.3 | 71 |  | 8.2 |  | 75 |  |


[^0]:    Ruandel 14.05 .07
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    Dr. Amalesh Chandra Mandala
    Professor
    Department of Mechanical Engineering
    Bangladesh University of Engineering \& Technology

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[^7]:    Year. 2005 Montly. Octohet

