HU Hutsofa Rom

L-2/T-1/ME

Date: 07/01/2013

BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA

L-2/T-1 B. Sc. Engineering Examinations 2011-2012

Sub: EEE 259 (Electrical and Electronic Technology)

Full Marks: 280

Time: 3 Hours

The figures in the margin indicate full marks.

USE SEPARATE SCRIPTS FOR EACH SECTION

SECTION - A

There are FOUR questions in this section. Answer any THREE.

1. (a) A three phase, Y connected, abc sequence voltage source is supplying a three phase load having impedance 12 + j9 Ω in each phase. If the line impedance is 0.06 + j0.12 Ω in each line connecting the source and load, determine line and phase currents, line and phase voltages both for source and load side. Given, the load is Y connected.

 $(30\frac{2}{3})$

(b) Make a free hand plot of signal vs. time of the following two signals:

(7)

(i) $x_1 = A_1 \sin \omega t$, (ii) $x_2 = A_2 \cos (\omega t - 60^\circ)$

 $(A_1 = 2A_2)$

From this plot determine which signal is leading with proper reasoning.

(c) Draw the vector diagram of the following signals:

(9)

(i) $x_1 = A_1 \sin(\omega t + 30^\circ)$,

(ii) $x_2 = A_2 \sin(\omega t - 30^\circ)$,

(iii) $x_3 = A_3 \sin (90^\circ - \omega t)$, (iv) $x_4 = x_1 + x_2 - x_3$

- (12)2. (a) Derive the approximate equivalent circuit referred to primary of a transformer.
 - (b) The equivalent circuit impedances of a 20 kVA, 4000/240 V, 60 Hz transformer are to be determined. The open circuit test and short circuit test were performed on the primary side of the transformer and the following data were taken:

 $(23\frac{2}{3})$

Open circuit test	Short circuit test
(on Primary)	(on Primary)
$V_{OC} = 4000 \text{ V}$	$V_{SC} = 489 \text{ V}$
$I_{OC} = 0.214 \text{ A}$	$I_{SC} = 2.5 A$
$P_{OC} = 400 \text{ W}$	$P_{SC} = 240 \text{ W}$

Find the impedances of the approximate equivalent circuit referred to the secondary side and sketch that circuit.

(c) Draw the phasor diagram of a transformer operating at a lagging power factor, unity power factor and a leading power factor. In which case the voltage regulation will be positive?

(11)

EEE 259 (ME)

3.	(a) Derive the equivalent circuit of a synchronous generator.	(12)
	(b) Show graphically, the open circuit and short circuit characteristics of a synchronous	`.
	generator. How can we determine the synchronous reactance at a given field current from	
	these characteristics?	(18)
	(c) A synchronous generator is supplying a load. A second is to be connected in parallel	
	with the first one. The generator has a no-load frequency of 61 Hz and a slope of	
	1 MW/Hz. The first load consumes a real power of 1000 kW at 0.8 pf lagging, while the	
	second load consumes a real power of 800 kW at 0.707 pf lagging.	$(16\frac{2}{3})$
	(i) Before the second load is connected, what is the operating frequency of the system?	
	(ii) After the second load is connected, what is the operating frequency of the system?	
4.	(a) Discuss armature current versus field current characteristics of a synchronous motor.	
	Why is it shaped like 'V'?	(15)
	(b) How is synchronous motor used for power factor correction?	(15)
	(c) Discuss the starting problems of a synchronous motor. How can we overcome these	
	problems?	$(16\frac{2}{3})$
	SECTION – B	•
	There are FOUR questions in this section. Answer any THREE.	
5.	(a) Discuss the current-voltage characteristics of the shunt, series, cumulatively	
	compounded and differentially compounded DC generators.	(20)
	(b) A 5-hp, 1500 rpm, 2-pole DC series motor is running at 3% less than the rated speed	
	supplying 2% more than the rated load. If induced voltage is 240 V, armature resistance	·
	is 10 Ω , field resistance is 2 Ω , then what is the input voltage? If the output torque is	
•	raised 5% due to increased load, while keeping the speed of rotation same as before,	
	determine the armature current assuming the same induced voltage as before.	$(26\frac{2}{3})$
6.	(a) A 480 V, 60 Hz, 50-hp, 3-φ induction motor is drawing 60 A at 0.85 pf lagging. The	
	stator copper losses are 2 kW, the rotor copper losses are 700 W, the friction and windage	
	losses are 600 W, the core losses are 1.8 kW and the stray losses are negligible. Find	
	(i) the air gap power; (ii) the output power and (iii) the efficiency of the motor.	$(24\frac{2}{3})$
	(b) Draw the torque-speed characteristics of an induction motor showing the starting	
	torque, pull-out torque and rated torque.	(12)
	(c) What is transducer? Classify transducers. What are primary and secondary	
	transducers? Give examples.	(10)

EE 259 (ME)

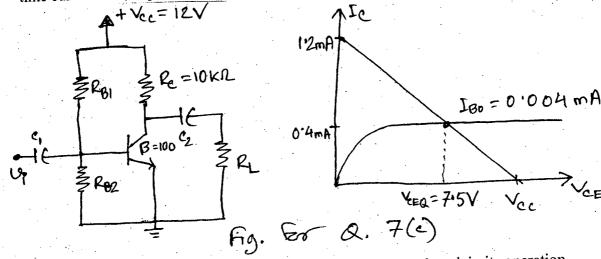
(a) What are the differences between voltage amplifiers and power amplifiers? Classify (10)power amplifiers.

(15)

(b) Briefly describe how a transistor can be used as an amplifier.

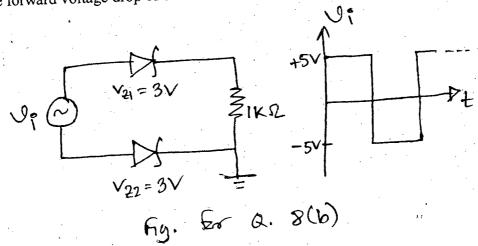
(c) For the circuit shown in Fig. for Q. 7(c), if an input signal v_i is applied such that the peak-to-peak variation of the base current is 0.01 mA, then draw the output voltage vs. time curve. Also, explain the slope of the curve.

 $(21\frac{2}{3})$

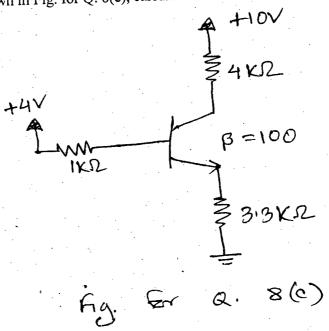


8. (a) Draw the circuit diagram of a full-wave bridge rectifier and explain its operation. (15)

(b) For the circuit shown in Fig. for Q. 8(b), plot the output voltage vs. time curve. (15)Assume forward voltage drop of each diode is 0.7 V.



(c) For the circuit shown in Fig. for Q. 8(c), calculate the base, emitter and collector currents. $(16\frac{2}{3})$



L-2/T-1/ME

Date: 24/12/2012

BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA

L-2/T-1 B. Sc. Engineering Examinations 2011-2012

Sub: HUM 303 (Principles of Accounting)

Full Marks: 210

Time: 3 Hours

The figures in the margin indicate full marks.

USE SEPARATE SCRIPTS FOR EACH SECTION

SECTION - A

		<u>SECTION</u>			7.44 A.
	There are FOU	${f R}$ questions in this s	section. Answer any	THREE.	•
l.,	(a) Explain the basic acco	ounting equation: As	ssets (A) = Liabilition	es (L) + Owner's Equity	(5)
	(OE) with examples.				(5)
	(b) What is trial balance?(c) Mr. Akhand and his	Describe the advant	ages and disadvanta	ges of trial balance. business on August 1,	(5)
	(c) Mr. Akhand and his 2012. The following trans	actions took place d	luring the first mont	h of operation:	(25)
	August 1 : Inves August 7 : Purch August 10 : Hired	sted Tk. 90,000 in ca hased office equipm I a managing direct	ash to start business. ent in cash amount for to manage the b	Tk. 120,000. usiness efficiency.	
	August 18 : Incur August 20 : Incur August 21 : Earn recei	rred advertising exported office rent in accept of the contract of the contrac	Tk. 20,000 per more anse on account as Tk. 10,00 selling the production account.	Tk. 5,000. 00. act, Tk. 10,000 is	
	August 25 · Paid	the amount due rela	n for his personal use ated to advertising e evious customer on	xpanse.	
		ployees' salaries exp	anse was due for Tk	. 4,000.	
	Requirement: Provide journal entries for	or above transaction	s.		
2	. (a) Discuss the objective	es and importance of	financial statement or principles to prov	s analysis. vide financial information	(3)
			•		(7)
	with examples briefly. (c) The following inform	ation taken from the	financial statements	of Eastern Housing Ltd.	(15)
		Net Sales	Tk. 50,000		
		Gross Profit	Tk. 12,500		•

110011011	
Net Sales	Tk. 50,000
Gross Profit	Tk. 12,500
Net Profit	Tk. 6,500
Owner's Equity:	
01. 01. 2011	Tk. 40,000
31. 12. 2011	Tk. 30,000
Total Assets:	
01. 01. 2011	Tk. 62,000
31. 12. 2011	Tk. 60,000

Contd ... Q. No. 2(c)

Required:

- (i) Calculate profit ratio
- (ii) Calculate Goss profit ratio
- (iii) Compute Return on Equity (ROE)
- (iv) Compute Return on Assets (ROA)
- (v) Compute Equity ratio
- (d) The following are selected items from a recent balance sheet of XYZ company:

Cash and Cash equivalents Tk. 6000 Short term investment Tk. 4000 Gross Accounts receivable Tk. 8000 Allowance for doubtful debt Tk. 1000 Merchandise inventory Tk. 4500 Prepaid expenses Tk. 4000 Accounts payable Tk. 8000 Notes payable Tk. 2000 Accured expenses Tk. 1200

Required: Compute (i) Current ratio, (ii) Quick ratio and (iii) Working capital amount.

3. Green View limited has the following information taken as trial balance on 31st December, 2011.

Name of Accounts	Debit (Tk.)	Credit (Tk.)
Cash	8,000	
Accounts Receivable	36,000	•
Allowance for uncollectible		4,800
Supplies	6,500	
Prepaid expense	8,000	
Inventory (01. 01. 2011)	94,000	· · · · · · · · · · · · · · · · · · ·
Office equipment	50,000	
Accumulated depreciation		
- Office equipment		10,000
Purchase	170,000	
Purchase Return		13,200
Sales Revenue		300,000
Sales Return	50,000	
Rent Expense	60,000	·
Salary Expense	49,000	
Accounts payable		25,000
Notes payable		8,000
Advertising Expense	28,000	
Capital		198,500
Total	559500	559500

(10)

Contd ... Q. No. 3

Information for Adjustments:

- (i) Estimated uncollectible account expense Tk. 2000
- (ii) Supplies consumed during the period Tk. 3000
- (iii) Prepaid expense is expired Tk. 2,200
- (iv) Inventory on December 31, 2011 is Tk. 85,000
- (v) Estimated depreciation for office equipment at the rate of 10% per year
- (vi) Interest expense is accrued Tk. 1500
- (vi) Advertising expense is accrued Tk. 5,000

Requirements:

(a) Show the necessary adjusting entries.

(15)

(b) Prepare adjusted trial balance.

(20)

4. The following is the trial balance of Tom Company as on 31st December, 2011.

	Debit (Tk.)	Credit (Tk.)
Sales revenue		50,000
Merchandise inventory (01. 01. 11)	6,000	
Purchase	24,000	
Purchase return		1,000
Sales discounts	2,500	
Accounts receivable	20,000	
Accounts payable		14,000
Capital	****	40,000
Drawings	10,000	
Salaries	8,000	
Supplies	3,000	
Delivery Van	20,000	
Cash	9,300	
Prepaid insurance	2,200	
Total	105,000	105,000

Other information:

- (i) Supplies used Tk. 1,200
- (ii) Depreciation on delivery Van is Tk. 2,000
- (iii) Merchandise inventory on 31st December, 2011 was Tk. 5,500
- (iv) Tk. 2,500 of accounts receivable was uncollectible
- (v) Salaries were accrued Tk. 4,000
- (vi) Insurance expense was Tk. 2,000

Required:

- (a) Prepare multiple income statement for the period ended on 31st December, 2011. (15)
- (b) Prepare statement of Owner's Equity and Balance Sheet as on 31st December, 2011. (20)

SECTION - B

There are FOUR questions in this section. Answer any THREE.

5. (a) What is meant by a product's CM ratio? How is this ratio useful in planning business operations?

(5)

(b) Quality Products manufacture plastic football. The selling price is Tk. 37.50 per unit and variable cost is Tk. 22.50 per unit. Over the past year company sold 40,000 units of football, with the following results:

(30)

Sales (40,000 footballs)	Tk. 1,500,000
Less: Variable expenses	Tk. 900,000
Contribution Margin	Tk. 600,000
Less: Fixed expenses	Tk. 480,000
Net Operating Income	<u>Tk. 120,000</u>

Required:

- (i) Compute CM ratio and break -even point in units and sales Taka. Also compute degree of operating leverage of sales.
- (ii) The company estimates that, in the next year variable cost will increase by Tk. 3 per football. The selling price will remain constant at Tk. 37.50 per football. What will be the new CM ratio and the new break-even point in units and sales Taka.
- (iii) Refer to the data (ii) above if the expected change in variable costs take place how many footballs will have to be sold to earn the same net operating income (Tk. 120,000) as last year?
- (iv) Refer to the original data. Assume that will decrease variable cost by 40% but fixed cost will increase by 90%. What would be the new CM ratio and break-even point in units and sales Taka?
- (v) Refer to the data in (iv) above. Assume that in next year company will sell 50,000 units of football. Compute –

Contribution margin income statement and Margin of safety in units.

6. (a) Explain how fixed manufacturing overhead costs are shifted from one period to another under absorption costing.

(5)

(b) Advance Products Company manufactures and sells a single product. You have been given the following information:

(30)

<u>Particulars</u>	Amount (Tk.)
Variable cost per unit:	•
Direct materials	18
Direct labor	7
Variable manufacturing overhead	2
Variable selling and administrative	5
Fixed costs per year:	
Fixed manufacturing overhead	160,000
Fixed selling and administrative expense	110,000

Contd ... Q. No. 6(b)

During the year, the company produced 20,000 units and sold 16,000 units. The selling price of per unit is Tk. 50.

Required:

- (i) Compute the unit product cost under absorption costing and variable costing.
- (ii) Prepare income statement under both of the techniques.

7. (a) What are the purposes of cost allocation?

(5)

(b) Navana Company has two support departments – Administrative Services (AS) and Information Systems (IS) and two operating departments – Government Consulting (GOVT) and Corporate Consulting (CORP). For the first quarter of 2012, the following records are available

(30)

Navana Company For the first quarter, 2012

	Support Dept.		Operating Dept.		Total	
	AS	IS	GOVT	CORP		
Budgeted overhead before allocation	600,000	2,400,000	8,756,000	12,452,000	24,208,000	
Support work supplied by AS		25%	40%	35%	100%	
Support work supplied by IS	10%		30%	60%	100%	

Required:

Allocate the two support departments cost to the two operating departments by using

- (i) Direct method
- (ii) Step-down method
- (iii) Receiprocal method

8. (a) What are the objectives of cost accounting?

(5)

(b) Following information are available for Doel company at December 31, 2012.

(15)

Doel Company

December 31, 2012

Particulars	Beginning Inventory	Ending Inventory	
	Amount (Tk.)	Amount (Tk.)	
Raw material	3,200	2,500	
Work-in-process	1,350	1,700	
Finished goods	8,500	9,500	



 $(16\frac{2}{3})$

(15)

L-2/T-1/ME

Date: 31/12/2012

BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA L-2/T-1 B. Sc. Engineering Examinations 2011-2012

Sub: MATH 261 (Vector Calculus, Matrices, Laplace Transform and Series Solution)

Full Marks: 280

Time: 3 Hours

The figures in the margin indicate full marks.

Symbols used have their usual meaning.

USE SEPARATE SCRIPTS FOR EACH SECTION

SECTION - A

There are FOUR questions in this section. Answer any THREE.

1. (a) Find the value of k for which the following system of equations has non-trivial solutions. Also find the solutions.

> x + ky + 3z = 04x + 3y + kz = 02x + y + 2z = 0

(b) Examine the following system of vectors for linear dependence. If dependent, find the relation among them.

> $X_2 = (1, -1, 2, -1)$ and $X_3 = (3, 1, 0, 1)$. $X_1 = (1, 1, -1, 1),$

(c) Use Cayley-Hamilton theorem to find the inverse of the matrix (15)

 $\mathbf{A} = \begin{pmatrix} 1 & 2 & -2 \\ 1 & 1 & 1 \\ 1 & 3 & -1 \end{pmatrix}.$

2. (a) Find a matrix P which diagonalizes the matrix $A = \begin{pmatrix} 1 & 0 & -1 \\ 1 & 2 & 1 \\ 2 & 2 & 3 \end{pmatrix}$. Write down the

 $(23\frac{2}{3})$ diagonal form of A and also find A4.

(b) Express the following quadratic form as a sum of the squares and classify it as (23)definite, semi-definite or indefinite:

 $q = 4x_1^2 + 3x_2^2 - x_3^2 + 2x_2x_3 - 4x_3x_1 + 4x_1x_2.$

Also write down the equations of linear transformation and find a non-trivial set of values of x_1 , x_2 , x_3 which makes the form zero.

3. (a) Find $\underline{A} \times (\underline{\nabla} \times \underline{B})$ and $(\underline{A} \times \underline{\nabla}) \times \underline{B}$ at the point (1, -1, 2) if $\underline{A} = xz^2\hat{i} + 2y\hat{j} - 3xz\hat{k}$ and B = $3xz\hat{i} + 2yz\hat{j} - z^2\hat{k}$. (16)

(b) Show that curl (curl \underline{F}) = grad div $\underline{F} - \nabla^2 \underline{F}$ and hence show that $\nabla^2 \underline{F} = n(n+3) r^{n-2} \underline{r}$ $(20\frac{2}{3})$ where $\underline{F} = r^n \underline{r}$.

(c) Use Green's theorem to find the area bounded by the hypocycloid (10)

 $x^{\frac{2}{3}} + y^{\frac{2}{3}} = a^{\frac{2}{3}}$; a > 0.

MATH 261

4. (a) Show that (20)

$$\underline{F} = (6xyz + z^2)\hat{i} + 3x^2z\hat{j} + (3x^2y + 2xz)\hat{k}$$

is a conservative force field. Find the scalar potential of this field and the work done in moving an object in this field from the point (2, -2, 2) to (2, -1, 3).

(b) State Gauss's divergence theorem, Verify the theorem for

$$(26\frac{2}{3})$$

$$\underline{F} = 2x^2y\hat{i} - y^2\hat{j} + 4xz^2\hat{k}$$

taken over the region in the first octant bounded by $y^2 + z^2 = 9$ and x = 2.

SECTION - B

There are FOUR questions in this section. Answer any THREE.

5. (a) Solve the Bessel's differential equation (36)

$$x^{2}y'' + xy' + (x^{2} - n^{2})y = 0$$

by the method of Fröbenius.

(b) When n is positive integer, show that $J_{-n}(x) = (-1)^n J_n(x)$. (10²/₃)

6. Show that

(i)
$$\int_{0}^{x} x^{-n} J_{n+1}(x) dx = \frac{1}{2^{n} \underline{l} \underline{n}} - x^{-n} J_{n}(x).$$
 (16%)

(ii)
$$P_n(x) = \frac{1}{2^n \ln dx^n} (x^2 - 1)^n$$
. (20)

(iii)
$$P_{2n}(0) = (-1)^n \frac{1 \cdot 3 \cdot 5 \dots (2n-1)}{2 \cdot 4 \cdot 6 \dots 2n}$$
 (10)

7. (a) Show that
$$\int_{-1}^{1} P_{m}(x) P_{n}(x) dx = \begin{cases} 0 & \text{if } m \neq n \\ \frac{2}{2n+1} & \text{if } m = n \end{cases}$$
 (20)

(b) Evaluate
$$L\{J_o(at)\}$$
 and $L\{J_1(at)\}$. (14)

(c) Using Laplace transformation, show that
$$Si(\infty) = \frac{\pi}{2}$$
. (12½3)

8. (a) Using Laplace transformation, show that
$$J_0(t) = \frac{1}{\pi} \int_0^{\pi} \cos(t \cos \theta) d\theta$$
. (12%)

(b) Find (i)
$$L^{-1} \left\{ \frac{se^{-4\pi s/5}}{s^2 + 25} \right\}$$
 (ii) $L^{-1} \left\{ \frac{e^{4-3s}}{(s+4)^{5/2}} \right\}$. (14)

(c) Solve (using Laplace Transformation) (20)

$$Y''(t) - tY'(t) + Y(t) = 1$$
, $Y(0) = 1$, $Y'(0) = 2$.

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L-2/T-1/ME

Date: 17/12/2012

BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA

L-2/T-1 B. Sc. Engineering Examinations 2011-2012

Sub: ME 201 (Basic Thermodynamics)

Full Marks: 280

Time: 3 Hours

The figures in the margin indicate full marks.

USE SEPARATE SCRIPTS FOR EACH SECTION

SECTION - A

There are **FOUR** questions in this section. Answer any **THREE**. Steam table R-134a properties are supplied.

1.	(a) Briefly explain 'thermodynamic equilibrium' and 'quasi-static process'.	(10)
	(b) With a suitable diagram, show that work is a path function. Mention some similarities	
	between 'work' and 'heat'.	(15)
	(c) Draw a typical P-T diagram of a pure substance and label it. Briefly explain the	
	physical meanings of (i) critical point (ii) triple point.	(15)
	(d) One kg of air is compressed reversibly and isothermally from 0.1 MPa and 27 °C to	
	1.0 MPa. Assuming ideal gas, estimate work done and heat transfer during this process.	$(6\frac{2}{3})$
2.	(a) Using 'First Law of thermodynamics', show that internal energy is a thermodynamic	
2.	property. Briefly explain the physical meaning of 'internal energy and how it differs from	•
	'entropy'.	(10)
	(b) With schematic diagrams and proper assumptions, simplify the 1st Law of	
	thermodynamics for the following devices:	(15)
	(i) Nozzle	9
	(ii) Heat exchanger	
	(iii) Throttling device	•
	(c) Briefly explain Joule's free expansion experiment and show that, $u = f(T)$ for ideal gases.	(10)
	(d) Air initially at 1 bar and 27 °C is compressed in steady state to 5 bars and 177 °C. The	
	power input to the compressor is 5 kW and heat loss is 0.5 kW. If the changes in potential	
	and kinetic energies are neglected. Estimate mass flow rate of air.	$(11\frac{2}{3})$
3.	(a) Briefly present Kelvin-Planck (KP) and Clausius (C) statements of the second law of	
	thermodynamics. Show that, any violation of Clausius statement implies the violation of	
•	KP statement.	(10)
	(b) Show that, $\eta_{rev} > \eta_{irrev}$.	(10)
	(c) Distinguish between perpetual motion machine of 1st kind and 2nd kind.	(10)
	(d) Dry saturated steam at 10 MPa expands isothermally and reversibly to 1.0 MPa.	
	Calculate the heat supply and work done per kg of steam during the process.	(10)
	Contd P/2	

ME 201

Contd ... Q. No. 3

(e) Suppose that, 1 kg of saturated vapor at 100 °C is converted to saturated liquid at 100 °C in an isobaric process. If the surrounding air is at 300 K, estimate net change in entropy of the system plus surroundings.

 $(6\frac{2}{3})$

(5)

(5)

4. (a) Show that,
$$C_p - C_v = \frac{\beta^2}{kT}$$
. vT (15)

where kT = isothermal compressibility, and

 β = volume expansivity

- (b) Using the expression of 4(a), show that for ideal gas, $C_p C_v = R$.
- (c) What is the difference between saturated liquid and compressed liquid? **(5)**
- (d) A system undergoes a process between two states: first in a reversible manner and then in an irreversible manner. For which case is the entropy change greater? Why?

(5)

- (e) The entropy of hot water decreases as it cools. Is this a violation of increase of entropy principle?
- (f) An insulated rigid tank is divided into two equal parts by a membrane. Air is contained in one half and the other half is evacuated. The membrane is punctured and air quickly fills the entire volume. Explain the work done and entropy generation in the process.

 $(11\frac{2}{3})$

(10)

(30)

 $(6\frac{2}{3})$

SECTION - B

There are FOUR questions in this section. Answer any THREE. Make reasonable assumptions in case of any missing data. Symbols indicate their usual meaning.

5. (a) Write short note on Binary Vapor Power Cycle. Provide component-wise schematic and corresponding T-s diagram.

(b) A stream power plant operates on an ideal reheat-regenerative Rankine cycle with one reheater and one open feed water heater. Steam enters the HP turbine at 10 MPa and 600°C and leaves the LP turbine at 8 kPa. Steam is extracted from the turbine at 2.0 MPa and it is reheated to 550°C at a pressure 0.8 MPa. Water leaves the feed water heater as saturated liquid. Heat is transferred to the steam in the boiler at a rate of 630 MW. Determine (i) the mass flow rate of steam through the boiler, (ii) the net power output (iii) the thermal efficiency of the cycle.

(c) The plant engineer is thinking about discarding the condenser. He instead plans to pump water at atmospheric pressure to the boiler and expel steam out from the turbine at atmospheric pressure for he thinks of the condenser as a wastage of energy since it is only condensing steam and may be using a separate cooling tower for itself. However, you have reasons to believe that condenser is a necessary component for augmenting work output. Substantiate your reasoning with appropriate T-s diagram. What are the theoretical and practical limits of condenser pressure?

6. (a) For an air-standard ideal diesel cycle with compression ratio " r_c ", cut-off ratio " β ", and ratio of specific heats of air "k", show that the thermal efficiency,

(15)

$$\eta_{\text{th,diesel}} = 1 - (r_c)^{1-k} \left[\frac{\left(\beta^k - 1\right)}{k \left(\beta - 1\right)} \right]$$

(b) Calculate net work output per unit mass of air, back work ratio and thermal efficiency for a Brayton cycle with one stage reheating and one stage intercooling, where air enters the compressor at 300 K and 100 kPa, and enters the turbine at 1400 K and 1300 kPa. Turbines and compressors are isentropic. The regenerator effectiveness is 0.75. Take k =1.4 and $C_p = 1.005 \text{ kJ/kg-K}$.

(25)

(c) A simple gas turbine is working on the ideal Brayton cycle with a maximum cycle temperature T₃ and minimum cycle temperature T₁. Show that, pressure ratio (r_p) for maximum net work should be,

 $(5+1\frac{2}{3})$

$$r_{p} = \left(\frac{T_{3}}{T_{1}}\right)^{k/2(k-1)}$$

Will the cycle efficiency be maximum at this pressure ratio as well?

7. (a) List the deviations of vapor compression refrigeration cycle from the ideal one. Identify them on the P-h diagram.

 $(6\frac{2}{3})$

(b) The initial conditions for an air-standard ideal Otto cycle operating with a compression ratio of 8:1 are 0.95 bar and 17°C. At the beginning of the compression stroke, the cylinder volume is 2.20 L, and 3.60 kJ of heat is added during the heating process. Calculate the pressure and temperature at the end of each process of the cycle, and determine the thermal efficiency and the MEP.

(15)

(c) A commercial refrigerator with refrigerant R134a as the working fluid is used to keep the refrigerated space at 5°C by rejecting its waste heat to cooling water that enters the condenser at 17°C at a rate of 0.2 kg/s and leaves at 25°C. The refrigerant enters the condenser at 1.4 MPa and leaves at the same pressure at 42°C. The inlet state of the isentropic compressor is at 100 KPa and - 20°C. Determine (a) the quality of the refrigerant at the evaporator inlet, (b) the refrigeration load in tons, and (c) the COP of the refrigerator.

(25)

ME 201

8. (a) Define ton of refrigeration.

 $(1\frac{2}{3})$

(b) For a dry bulb temperature of 25°C and wet bulb temperature of 15°C, determine the absolute humidity (ω), relative humidity (ϕ), and mixture enthalpy (h) in kJ/kg of dry air at a pressure of 0.5 bar.

(15)

(c) A mixture consists of 19.23 percent carbon dioxide, 8.86 percent water vapor and 71.91 percent nitrogen by mass. The mixture is being maintained at 298 K and 1 bar where under ideal gas assumptions the enthalpies of the gases are known ($h_{CO_2} = 9364$ kJ/kmol, $h_{H_2O} = 9904$ kJ/kmol, $h_{N_2} = 8669$ kJ/kmol). Determine (a) the specific enthalpy of the mixture in kJ/kmol, and (b) apparent gas constant of the mixture in kJ/kg-K.

(15)

(d) Write down the stoichiometric combustion equation of n-Octane with air at 1 atm and 25°C and calculate the LHV and HHV of n-Octane for a complete combustion using data from the following table:

(15)

Substance	Formula	Δh_f^0 (MJ/kmol)	h _{fg} (MJ/kmol)
Oxygen	O) 1/2 (g)	0	
Nitrogen	N ₂ (g)	0	
Carbon dioxide	CO ₂ (g)	-393.52	
Water	H ₂ O (l)	-285.83	44.01
n-Octane	C ₈ H ₁₈ (g)	-208.45	41.46

Saturated Water, Pressure Table

A	Table C.2k	Saturated	i Water, Pres	sure Tab	le (Metric Units).			**** · · · · · · · · · · · · · · · · ·			
			Volum	ej m ^a ko	Energy	r, Kulrko, za ?		Entision ka/			445 TX (047) is	
	n Mos											
Ī												
	0.000611 0.0008	0.01	0.001000	206.1	0.0	2375.3	0,0	2501.3	2501.3	0.0000	9.1571	9.1571
- 1	0.0008	3.8	0.001000	159.7	16.8	2380.5	15.8	2492.5	2508.3	0:0575	9.0007	9.0582
	0.001	7.0	0.001000	129.2	29.3	2385.0	29.3	2484.9	2514.2	0,1059	8.8706	8.9765
8	0.0014		0.00 000 + 0.001001	1087	40.6	2000	40.6	24785	2519.1	0.1460	8 7609	8 9099
	00018.		0.001001	F 82.76	4 1 1	239 3	3039	9473	2523.4	£ 1807,	. 807304.	6 2 8 86 8 1
. 4	0.0018	15.8	0.001001	74.03	58.9 68.5	2394.7 2397.2	069	24002	, 2527,1	0210	8,84952)	\$\$\\$8.8\$\$*
	0.002	17.5	0.001001	67.00	73.5	2399.5	66.5 73.5	2464.0	2530.5	0.2367	8.5259	8.7626
.	0.003	24.1	0.001003	45.67	101.0	2408.5	101.0	2460.0 2444.5	2533.5	0.2606	8.4639	8:7245
	0.604	29.0	0.001004	34.86	214	2415.2	1214	2444.5 2430.0	2545.5 2 55 4.4	0.3544	8.224 0	8.5784
	0.006	7862	0.001006	25,74	15.6	24240		2468	2587.45	0.4225 		8,4754
	0008	1416	0.001008	7.18,10 ⁵ -	1739	2402.1	1739	2401	2577.0	0.5924	77,9104	8 0312
-	0.01	45.8	0.001010	14.67	191.8	2437.9	191.8	2392.8	2584.6	· 0.6491	7.5019	8,2295 8,1510
	0.012	49.4	0.001012	12.36	206.9	2442.7	206.9	2384.1	2591.0	0.6961	7.3910	8.0871
	0.014	52.6	0.001013	10.69	220.0	2446.9	220.0	2376.6	2596.6	0.7365	7.2968	8.0333
	0018	55.0	0.001016.	9488	231.5	2480.5	2016	2369.9	26014	O77/19	7.0:493.4	7.9868
	0018-55	451,888	10000	6,445	3.424.6	24598	2419	2362.9	28058	tetai	71426	Terday .
	0.02	60.1	2000007	7,849	2514)	£2458,7 i.,	, 251 4	23583	26007	0.8819.75	-70770	77.9090
	0.03	69.1	0.001022	5.229	289.2	2468.4	289.2	2336.1	2625.3	0.9439	6.8256	7.7695
	0.04 0.06	75.9	0.001026	3.993	. 317.5	2477.0	317.6	2319.1	2636.7	1.0260	6.6449	7.6709
	0.00	85.9 86.5	0.001033 0.001069	2.732	359.8	2489.6	359.8	2293.7	2653.5	1.1455	6.3873	7.5328
		906	-0.001043	(2.037) (1834)	8918	2498.6	200	274	#2005.7±10	12331	. 62923b 3	2464
	0.00	10483	0.001647	1428	495.2	2506.1	.4749	2258,1	2675.6-4	1,0020	4 6 05 / State	7.8602
No.	0.14	109.3	0,001051	1.237	458.2	. 2512.1 2517,3	. 409 J A	2244.2.1	2683.5	1,0610	-,5,907.0 ₇ ,-	7,2989
i	0.16	113.3	0.001054	1.091	475.2	2517.3 2521.8	458.4 475.2	2232.0	2690.4	1.4112	5.8360	7.2472
1	0.18	116.9	0.001058	0.9775	490.5	2525.9	475.3 490.7	2221.2	2696.5	1.4553	5.7472	7.2025
	· · · · · · · · · · · · · · · · · · ·				700.0	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	450.7	2211.1	2701.8	1.4948	5.6683	7.1631

acceptance of the	ACCUTE THE VERTICAL PROPERTY OF THE PARTY OF										
	er i la comp	, Yourn	oniiio	. LEner	y/ ka/ka	1000	Eritheoly, kur	1.		(1) <u>/28/7</u> (2011)	
Ď.	Māl 7. ie		1	Line	T		T.				
CONTRACT	namen karamarar										
0.2	120.2	0.001061	0.8857	504.5	2529.5	504.7	2201.9	2706.6	1.5305	5.5975	7.1280
0,3	133.5	0,001073	0.6058	561,1	2543.6	561.5	2163.8	2725;3	1,6722	5,3205	6.9927
0.4	143.6	0.001084 *	0.4625	604.3	2553.6	604.7	2133.8	2738.5	1,7770	5.1197	6.8967
08	3,4889.4	# 20.0014pt	0.3(57	669,9.1	2567A	670.6	20852	27668	3,9318	4.8293.4	8.7509
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4.1	70G	0.00127	0.00	7617	2583.6	7628	2015 37	2778		4 440 2	8 6 7 7
1.2	188.0	0.001139	0.1633	797.3	2588.8	798.6	1986,2	2784.8	2.2170	4.3072	6.5242
1,4	195.1	0.001149	0.1408	828.7	2592.8	830.3	1959.7	2790.0	2.2847	4.1854	6,4701
1.6	201.4	9.001159	0.1238	856.9	2596.0	858.8	1935.2	2794.0	2.3446	4.0780	6.4226
1.8	2012	0.00(168)	e garaga	82277	2598.4	884.81	1812.6	279715	2 8996	0.9816	6.8802
233	200	#100M77#	CD9968	7,8084	26063	9088	7/8077	72799.5	24.7/3	100	
	2,009	0.001216	0.08668	1004.8	2604)1	1008.4	1795.7	28041.	7.46	32.6	6.878
4	250,4	0.001252	0.04978	1082.3	2602.3	1087.3	1714.1	2801.4	2.7970	3.2739	6.0709
6	275.6	0.001319	0.03244	1205.4	2589.7	1213.3	1571.0:	2784.3	3.0273	2.8627	5.8900
8	295.1	0.001384	0.02352	1305.6	2569,8	1316.6	1441.4	2758.0	3.2075	2.5365	5,7440
	24 - 25 SQC 44 - 11	0.001485	0.02048	1850.6	95578-1	18693	1878 <i>8</i> :	274246-4	e 8 286 Sur	23916	28 d781
10	31435	0.0014523	0.01803	1893.0	2544.4	1407.6	1011	×27247;	100000	2,2546	5,6149
12	22.8	## 0.000527# A	F0,01926+-	#1472.B	251817.6	1491,3	11938	2684.0	0.4970 ***	18044	6,4933
14	336.8	0.001611	0.01149	1548.6	2476.8	1571.1	1066.5	2637.6	3.6240	1.7486	5.3726
16	847.4	0,001711	0.009307	1622.7	2431.8	1650:0	930.7	2580.7	3.7468	1.4996	5.2464
18	357.1	0,001840	0.007491	1698.9	2374.4	1732.0	777.2	2509:2	3.8722	1.2332	5.1054
20,000		0.00200	2005846	1785 6	22002	1826.9	589777	2410 0151	40146	0.9 (65)	4 9281
150	364 (452)	E 0.0031559	# OXX 155	202967	2029.6	2099.9	0.70700.144	20993	448054	0.0000	4.4305
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Saturated Water, Temperature Table

Table	e C.1b Saturat	ed Water, Te	mperature	Table (Metric	: Units)						
			ne mas	i Kili	oy kuka .e		denticity, a			Elizaber (Mil	
7							1000				
SEE SALE	0.0000	13: 0.001000	206.1	0.0	2375.3	0.0	2501.3	2501,3	0.0000	9,1671	9.1571
0.	.000000 0:00070			8.4	2378.1	8.4	2496.6	2505.0	0.0305	9.0738	9.1043
5				21,0	2382.2	21:0	2489.5	2510.5	0.0761	8.9505	9.0266
0	0.0000	POCK PROPERTY OF THE PARTY OF T	AND CONTRACTOR PROPERTY AND CONTRACTOR OF CO	4. 7.0	anaga.	7 42	30.777	28197	34. O 1610	1.000	7 No. 18 3 146
, in					4,047,64		2465@	2500	10/2246		
3 5			27.0		2200		46.0	100	0.00		
25	PARTICIPATION PROPERTY OF THE PARTICIPATION OF THE		43.36	104.9	2409.8	104.9	2442.3	2547.2	0.3672	8,1916	8,5588
30			32.90	125.8	2416.6	125.8	2430.4	2556.2	0.4367	8.0174	8.4541
35	·	0.001006	25,22	146.7	2423.4	146.7	2418.6	2565.3	0.5051	7,8488	8.3539
F # 40	277 00075	d'Aksolie (de	1082	14075	2430.1	167.5	er (2400£	- VC 40 4.0	1572		1,2578
T 45	- COP		Ag (590)	984	2490.8	1684	22943	1,2583	(685)		
150	17-12-00120	10001012	120	7777090	13,2435	12,112,003	2,62,282,8	26921	OVICE	7,773	1,7004
55		0.001015	9.569	230.2	2450.1	230.2	2370.7	2600.9	0.7678	7.2243	7.9921
60	0.01994	0.001017	7,671	251.1	2456.6	251.1	2358.5	2609.6	0,8310	7.0794	7.9104
65	0.02503	0.001020		272.0	2463.1	272.0	2346.2	2618.2	0.8934	6.9384	7.8318
			1,17 18,042	202.03	724895	9.2330					
	100		r (e) A (e)		2015						
		7 70 0 102		3040	944) 2482(2)	244	2008.01	00510	10/4	6.4100	7.5453
85	0.05783			355.8	2488.4	355.9	2296.0 2283.2	-2651.9 2660.1	1.1344 1.1927	6.4109 6.2872	7.5455
90	0.07013			376.8	2494.5	376.9 397.9	2283.2	2668.1	1.2503	6.1664	7.4167
95	0.08455	The street of th	NAME OF THE PROPERTY OF THE PROPERTY OF	397.9	2500.6	397.9 34190	2210.2	2676.0	1,2003	0.1004	7.4107
		Principalities		* 0.0	-2306	i iran	7.7	4616			
		900000									
100	0.0701	0.001060	0,6685	546.0	2539.9	546.3	2174.2	2720.5	1,6348	5.3929	7.0277
130	0.2701	0.001070 0.001080			2559.9 2550.0	589.1	2174.2	2720,3	1,7395	5.1912	6.9307
140	0.3613 0.4758	0.001080			2559.5	632.2	2114.2	2746.4	1.8422	4.9965	6.8387
150	0.4756	0.001090	0.3920	001.7	2009.0	W2.2	2114.2	4140,4	1.0422	7.0300	- 0,000/

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		- Serialina	ini kiji 🖫 i	, resilien	(AU)		antielisy i ety			itiry/Ellig	
	er En Wee		7	10.00		A History					
160	0.6178	0.001102	0.3071	<i>≥</i> 874.9	2568.4	675.5	2082.6	2758.1	1.9431	4.6079	6.7510
1		0.001102	0.2428	718.3	2576.5	719.2	2049.5	2768.7		4.6249	6.6672
170	0.7916								2,0423		ī
180	1.002	0.001127	0.1941	762.1	2583.7	763.2	2015.0	2778.2	2.1400	4.4466	6.5866
444	12 OH	4 (10) (1	-0.665	906.2	(2500.0)	,9476	1976.8	44.64			0.000
200	1884		04274	850.6	2505.0	102	184.00	77.572			
			<i>0</i> 044 k	1997			T 194481.			3,844	
220	2.318	0.001190	0.08620	940.9	2602.4	943.6	1858.5	2802.1	2.5183	3,7686	6.2869
230	2.795	0.001209	0.07159	986.7	2603.9	990.1	1813.9	2804.0	2.6105	3,6050	6.2155
240	3,344	0.001229	0.05977	1033.2	2604.0.	1037:3	1766.5	2803.8	2.7021	3.4425	6.1446
200		0.022514	0.05010	1000.3	26024	1967	1464	284		32885	
x 260 s	also.		9.42	1,284,3		1944	1662.6	1270 d B			
7270 ts.	31.5495		10000569	P-11772	2590,715	-11846	10052	27/8974			#10 BO 10 P
280	6,411	0.001332	0.03017	1227.4	2586.1	1236.0	1543.6	2779.6	3.0674	2.7905	5.8579
290	7.436	0.001366	0.02557	1278.9	2576.0	1289.0	1477.2	2766.2	3.1600	2.6230	5.7830
300	8.580	0.001404	0.02168	1332.0	2563.0	1344,0	1405,0	2749.0	3.2540	2.4513	5.7053
38:0 at	9.866	0.00447	0.01835	1387.0 12	2546.4	14013	(- 1826 <i>)</i> (-	2727.574	3360	22709	45.623
0.00	14621177	Toportagina	0,014.00		728256	248176	1287	270017	344		
230	10,04	4,000 500	70,01500	1605/23#	24990	1525 3 75	11406	2668.9	er 3,6644	189117	* 5.9425 x
340	14.59	0.001638	0.01080	1570.3	2464.6	1594.2	1027.9	2622.1	3.6601	1.67 65	5.3366
350	16.51	0.001740	0.008815	1641.8	2418.5	1670.6	893.4	2564.0	3.7784	1.4338	5.2122
360	18.65	0.001892	0.006947	1725.2	2351.6	1760.5	720.7	- 2481.2	3,9154	1,1382	5.0536
270.	79-21-0 5	4- G 002216	0.004531	1944 0	22200	18906	442 2	23027-7		010476	100
34974 196	22.088	D000155	4,000,3185	2029.6	2029,6-1	20000	0.0	2009.3			4,430%

Tabl	e C.3b Sup	erheated V	Vater Vap	or (Metric l	Units) co	ntinued			·		٠.			•
								Temperatu	, evil					
	g Alpartage		20 1 1	100 L 1 100	(14 	1 450	500	560	600	850	700		D. San	and the same
19140509115	v. m²/kg	O CONTRACTOR OF THE CONTRACTOR	1114 0.1	1255 0.138	PERSONA DIN MANAGEMENT		MANAGER STATES		Dan Herivalah	and Established				900
	i/: k.lΩm		.,	1255 0.138 72.6 2859.		0.1635 3030.4	0.1757 3118.2	0,1877 3203.0	0.1996 3290.9	0.2114 3380.2	'0,2232' 3471.0	0.2350 3563.2	0.2467 3057.0	0.2700
2 (212	h, kJ/kg			23.5 3137.		3357.5	3467.6	3578.3	3690.1	3803.1	3917.5	4033.2	4150:4	3849.3 4389.4
PER	. s; بيا/kg ماريخ	TOCOTON PROPERTY OF THE PUBLISHED	 	672 6.957		7.2853	7:4325	7.5713	7.7032	7.8290	.7.9496°	8.0656	8.1774	8.3903
		Mary Property of the Control of the	建模型类型 地质	8114 0.090 500 2843	63 0.0990a 74 2032 7	01079	. 01182 3107.9	100	0.024	0190	0 1484	0.1583	0.641	7 0 798
30 (23)	12.6	非色型性 98世 和自由	NUMBER OF STREET	05+ 015	3230.8	3340	3456.6	3569	3285 D 3882 D	3798.5	34888 35 3917	40204 40202	41480	3846.5 4385.0
		ю	MONTHANN STATES OF	388 8743	erance checkens	/ 0842	72346	731SE	7,5020	7,6084	77860	72747	7 987	8 2008
	v,m³/kg ∴ u,kU/kg	• •		5884 0.066							0.1109:	0,1169	0.1229	D:1347
4 (250	h, kulingi		- '296	25.3 2826.0 30.7 3092.4		3010.1 3330.2	3099.5 3445.2	.3189.0 3559.7	3279.1 3874.4	3370.1 3789.8	3462.1 3905.9	3555.5	3650.1	3843.0
	s, kJ/kg	ю.		622: .6.582		63371	7.0908	7.2343	7,3698	7,4981	7.6206	4023.2 7.7381	4141.6 7.8511	4382.3 8.0655
			"我们就是我们的,我们就是我们的。"	3618 0.042	or south that the	A STATE OF THE STA	70000	STATE OF THE PROPERTY OF	0.06525	0.06942	#EF0.07352	007768	0.00	21270868
627			266 268	CHICAGO PARTICIPATION OF THE P	2892.8	2000	33822	3014	3266.9	33598	9552	\$647.6	39643 (4	3837.6
	18.074		40	CONTRACT BUILDING APPLICATIONS	March Market Street	03013 67201	6422.1 118881.1	3540.8 2296	36384 127 1685	3776.2 72938	0094.9 1062	40131 76433	413270	4375.3
	· v, m ⁸ /kig	are the Landing Charles	- 0.02	2425 0.0299			Section of the Sectio	ACREA 201 LAND ACREA TOLI	0.04845	0.05168	0.05481	0.05791	7.66756 0.06097	0.05702
8 (295.	u, KVkg		- 259			2966.7	3064.3	3159.8	3254.4	3319.0	3444.0	3539.6	3636.1	3832.1
1 .	° jr.kd/kg. s,kd/(kg⊹l	io	- 276 - 5.79	. , ,		3272.0 6:5559	3398.3 0.7248	3521.0 6:8786	3642.0 7:0214	3762.3 7.1553	3882.5	4002.9	4123,8	4368.3
70	THE VIEWS			0.022		0.02075	7 0 00270	0.07564	0.00837	0.04101	7:2821 0:04358	7,4027 0,048(1)	7.5182 0.04859	7.7359
1000		(Saltas)		2000	2802.4	2048.3	30458	201445	2417	7 33382	3-0454	المالحو	36290#	3828.3
	*** **** 9			2023	0096.6 919 - 62127	2246.6		- 4360.0	98263	3748.8	36/0.57	3992.8	ania.	480123
SHEET STATES	v, m³/kg	X. POLICE LA LA COMPANIA DE LA COMP		0.0172	and a district of the work	2,6 4197 0.02412	0.02680	47589 0.02929	6 9007 0.03164	7.04062 0.03390	7/1696	7 29 9	7,4086	7.6280
40,000	U. KUKU			. 2841.4	2795.3	2918.8	3026.6	3128.9	3228.7	3327.2	0.03610 3425.3	0.03824 3523.4	0.04034 3821.8	0.04447 3820.6
12 (324	n, iung		- `~			3208.2	3348.2	3480.3	3608.3	3734.0	3858.4	3982.3	4105.9	4354.2
TO SECURE	-8, kJ/jkg -K		echaniose-sc. Hall	5.7604	6:0754	5.3006	8:4879	6.6535	8,8045	6.9445	7.0757	7./1998	7.31.78	7.5390
								ne sur c						
	MPIT ATOM		e en	8 200	W.	600	-60	100	190	900	ed in	90.	60	1000
	v; m²/kg	0.01565	0.01845	0.02080	0.02293	0.02491	0.02680	0.02861	0.03037	:0.03210	0.03379	0.03546	0.03711	0.03875
15 (342,2	u.kl/kg	2740.7	2879.5	2996.5	3104.7	3208.6	3310:4	3410.9	3511.0	3611.0	3711.2	3811:9	3913.2	4015:4
	"h;k√kg' .sik√kg:K)	2975.4. 5.8819,	6156.2 6.1412	3308,5 .6.3451	3448,6 8.5207	3582.3 6.6784	3712.3; 6.8232;	3840.1 6.9580	3966.6	4092.4	4218.0	4343,8	4469.9	4590.6
			40.01210	100ja775	001656	001818	0.01969.4	0.9300	7.0848	7.2048 0.02385	7.3192 10.02516%	7.4288 0.02645	7.5340 0. 02771	7:8356 002897
20 (365 8	U, Crig	26 92	2806217	294,0	002	0174.C L	228) 65	03865	490.0	85927	0095	37974	80000	40031
	1000	2861	000 ; 1005	3238.2	30001	38316	3875:3 7.7	3809.1	8940.8	4089.8	41963	4526A	44226	#562.5
	v, m²/kg	0.00818	0.01104 •	6.1400 0.01305	8.035 6 0.01475	0.01607	6,6691	B 8002	60017	.7. 9 891.11.	2012	7.2839	14901	17.4903
22.088	u, ku/kg	2552.9	2772:1	2919.0	3043.9	0.01627 3159:1	0:01788 3269.1	0.01901 3376:1	.0.02029 3481-1	0.02152 3585.0	0.02272 3688.3	0.02389 3791.4	0:02506 3894:5	0.02619 3998:0
(374.196)	h, kuling	2733,7	3015.9	3207.2	2369.6	3518.4	3659.6	3796.0	3929.2	4060.3	4190.1	4319.1	4447,9	4576.6
52290900	s, kJ/(kg · K)	.5,4013	5:8072	6.0634	8.2670		6.5998	6.7437	6,8772	7.0024	7,1206	7,2330	7:3404	7.4436
	1000	20078 20078	2615.3	0.0068 2820 7	0.01017. 0.2003	001145 91 006 5345	001260 F	001366 333586	0.01468 3447.0	00 (562) 366 (8)	001655	001/45	0.018307	0.01820
	T.O.G	9310	1282137	308.0	276	942 g 🖑	Logic -	37457	3886	4024 3 P	4169.0	37885 42919	428	3978.8. 4534.7
	e you			1002	SHORTEN TO SOME THE PARTY	war to make a second	6 406 6	86614	6/030	68341	6.0566	7,0726	7 (825 -	7 28752
	v, m³/kg .u, kd/kg	0.00191 1654.5	0,00369; 2365.1	0.00562 2678.4			0,00906 3158.0	0.00994:	0.01076	0.01152.	0.01226	0.01296	0.01365	0.01432
40	h, kJ/kg	1930.8	2512.8	2903.3			3520.6	3283.6 3681.3	3402.9 3833.1	3517.9 3978.6	3629.8 4120:0	3739.4 4257:9	'3847.5' 4393.5'	3954.6 4527.6
	s, ku/kg·K)	4,1143	4.9487 Maria Salaman	5.4707	5:7793	6,0122	6 2063	6.3759	.6.6281	8.667.1	6.7957	6,8168	7.0291	7.1365
		7,00,63 1745.3	0.00208	0.00296		Mark Street Street Street		ETTERS AND PERSONS	0.00889/		0.00800 📝	0.00651	6 00900	0.00048
0		18434	2638	2360 5 2367 9	N. Karakaran J. P. Yang	266[7] - 3.] 31512 (3-47	3028 8 3 36 4 5	31772. 3808	3010.6 3128.8	2416	3516	3687.0	37650	3906.4
74.50	s Way Ki		40,77	4032171	CALLED TO A STATE OF THE STATE	CATALOGUE PARTICIONES DE	588381	The Part of the Control	THE REPORT OF THE PARTY OF THE	3969 () 6 4 1 8 x	4043.3 84523	41915 83814	48350 68012	4015.2
	v, m³/kg	0.00152	0.001.77	0.00219	0.00276	0.00339	0.00398	O TATOLOGY MANAGEMENT OF	MAN AN PARKAGE PARKET	0.00548	0.00591	0.00635	0.00871	0.00709
.80	u, kJ/kg h, kJ/kg	1887,0 1808.3	1944.9 2086.9	22 (8.9			• .				3497.3	3622.3	3742.1	3857.8
	s, kul/ikg · K)	-3:8338	4,2328	2393.9 4.8492			*** *			3803.8 6,2137	3970.1 6.3652	4127.9	4279.1	4425:2
		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				2,0000		ا عصوب	ימאניאה'	U _I E 131	03002	6.5026	6.6289	67459



Superheated Water Vapour

Table C.	3b Superhea	ted Water	Vapor (N	letric Uni	ts)	,					****			e vantere pr
								lemperature (1						
	in e la	80	100	1801	200	280	200	3460	4.400	800	600	100	- M	100
	N. CONTACTOR STATEMENT		or ho	67.00	109.2	120.7	132.3	143.8.	155.9	178.4	201.5	224.6	247.6	270.7
:	v, m³/kg	74.52	86.08 2516.3	97.63 2588:3	2681.6	2736.2	2812.2	2889.8	2969.0	3132.3	3302.5	3479.7	3663.9	3855.1
0.002 (17.5)	u, kul/kg	2445.2 2594.3	2688,4	2783.6	2879,9	2977.8	3078.7	3177,4	3279.6	3489.1	3705.5	3928.8	4159.1	4396.5
	h, kuling s, kuling K)	8.9227	9.1936	9.4328	9.6479	9,8442	10.0251	10.1935	10,3513	10.8414	10.9044	11.1465.	11.9718	11,5832
	S. KUUU N	20787	34.42	23904	436647	174 20 37	1000 H	86.575fam	A2 18	(0138.	//B050	80.827	90.04	1082
	80 kWo	2447	2516.0	2588.1	20013-0	/ 2736 FT	28/2.2	2889,8	7.2089	31323(3)	3002.5	3479.6	70003 (7.4	38550
0.005 (32.0)	10.00	2603.6	2886.0	278331	2819935	v 2077.6	3076.6	3172	2708	J480 I	2,07 6 .4	3028.8	1000	4366.6
	'S KURDIKI'	8 4982	8.7699	e 8.00 6 7,	8294	9,4212	9,6022	9.7708.	20284	102165	19104816	107230	(OD-189)	11716031 64.14
A CONTRACTOR OF THE PARTY OF TH	v, m³/kg	14.87	17.20	19,51	21.83	24,14	26.45	28.75	31,06	35.68	· 40.29	44.81	49.53 3663.8	3855.0
oni us m	u, k1/kg	2443.9	2515.5	2587.9	2661.3	2736.0	2812.1	2889.7	2968.9	31323	3302.5	3479.6 3928.7	4159:1	4396.4
0.01 (45.5)	n ki/kġ	2592.6	2687.5	2783.0	2879.5	2977.3	3076.5	3177:2	3279:5; .9.6084	3489.0 9.8985	3705.4 10.1616	10,4037	10.6290	10.840
	s.kJ/kg·K)	8.1757	8.4487	8.6890.	8.9048	9:1010 7:12 05	9.2821 32.13.22	9.4506 66714724766	.9.6084	#.0900 #################################	2015	10.466	PSYM	17.07.17
	riming is		<u>8</u> 5864 e	0 /48 %	2860.0	2757	78 I 9	2889.5	200	31922	33024	9286	18618	9850
0021004	10 KVQ		20.45	78.3	287	2017.01	20783	31776	2701	3488.9	191653	89287	1591	400
			7 (39) 87	8.38787	8.5839	8.7807	8.96)9	9.1304	92884	9.5785.4	93477	100838	10,0091	10.5205
CHARLES EX	v: rit Aq		3.418	3.889	4.356	4.820	5.284	5.747	6.209	7,134	8.057	8,981	9.904	10.83
	iv: ku/kti		2511:6	2585.6	2659.8	2735:0	2811.3	2889.1	2968.4	3131,9	3302.2	3479.5	3003.7	3854.9
0.05 (31,3)	n, kJ/kg		2682.5	2780,1	2877.6	2976:0	3075.5	3176.4	3278.9	3488.6	3705.1	3928.5	4158.9	4396.3
	s, kd/ikg⋅K)	-	7.6955	7,9409	6.1588	6.3564	6.5380	8.7069	8.8650	9.1554	9,4185	9.6608	9,8861	10.0975
50000			2401	2778	108	44	31/24	7 4 IOS	344	5.095	25755	16415	igi.	779
	SALES OF THE		25096	2584.6	2660	T CTPA SE	2811.0	2888.8	2908.2	318184	30021	3419.4	. 00618 V1568	4382
	TrixUg		2680.0	2778.5	2816	2916.34	20750	0178	3278.6	4884	0704.9 2822	9928.4 + 95054		0.9422
	descriptions.		9575040	10 27820 61	8,0000	8 2001	63621	2 971	8 7094 3 103	3.565	4.028	4.490	4.952	5,414
	v, m /kg	-	1,896	1.938	2.172	2.406	2.639 2810.4	, 2.871 2893.4	.9.103 2967.8	3131.5	3301.9	3479.2	3063.5	3854:8
0.1.(99.6)	u, kd/kg	: · - ·	2506.6	2582:7	2658.0 2875.3	2733.7 2974.3	2810.4	3175.5	3278.1	3488:1	3704.7	3928:2	.4158.7	4396.1
3.1.4.2.0)	n, kulikg		2676.2 7.3622	2776.4 7.6142	2575.3 7.8351	8.0341	8.2165	8,3858	8.5442	8.6350	9.0984	9:3408	9:5660	9.7775
<u></u>	15, kJ/(kg⋅K)	<u></u>	1,3022	1.0145	7.00.11	U.A.A.T	5,2,100							

\$\begin{array}{c c c c c c c c c c c c c c c c c c c					•										
V, m²/kg 1,285 1,444 1,501 1,757 1,912 2,067 2,222 2,376 2,530 2,885 2,993 0,301 3,50 0,15 (111.4) 0, k/kg 2,579 \$\frac{2}{8}\$ 266 \$\frac{2}{2}\$ 2762 \$\frac{2}{2}\$ 2693,5 2697,7 2667,3 3048,4 3131,1 3215,6 3301/8 3470,D 3663,4 385,4 0,15 (111.4) 0, k/kg 2,579 \$\frac{2}{8}\$ 2872 \$\frac{2}{8}\$ 2972 7 3073,0 31745 32713 3081,7 3487,6 3951, 3704,3 3927,9 41595 4395 0,15 (111.4) 0, k/kg 2,772 \$\frac{2}{8}\$ 2872 \$\frac{2}{8}\$ 2972 7 3073,0 31745 32713 3081,7 3487,6 3951, 3704,3 3927,9 41595 4395 0,15 (111.4) 0, k/kg 2,772 \$\frac{2}{8}\$ 2872 \$\frac{2}{8}\$ 2972 7 3073,0 31745 32713 3081,7 3487,6 3951, 3704,3 3927,9 41595 4395 0,15 (111.4) 0,16 (1									emperature (
V, m²/kg 1,285 1,444 1,501 1,757 1,912 2,067 2,222 2,376 2,530 2,885 2,993 0,301 3,50 0,15 (111.4) 0, k/kg 2,579 \$\frac{2}{8}\$ 266 \$\frac{2}{2}\$ 2762 \$\frac{2}{2}\$ 2693,5 2697,7 2667,3 3048,4 3131,1 3215,6 3301/8 3470,D 3663,4 385,4 0,15 (111.4) 0, k/kg 2,579 \$\frac{2}{8}\$ 2872 \$\frac{2}{8}\$ 2972 7 3073,0 31745 32713 3081,7 3487,6 3951, 3704,3 3927,9 41595 4395 0,15 (111.4) 0, k/kg 2,772 \$\frac{2}{8}\$ 2872 \$\frac{2}{8}\$ 2972 7 3073,0 31745 32713 3081,7 3487,6 3951, 3704,3 3927,9 41595 4395 0,15 (111.4) 0, k/kg 2,772 \$\frac{2}{8}\$ 2872 \$\frac{2}{8}\$ 2972 7 3073,0 31745 32713 3081,7 3487,6 3951, 3704,3 3927,9 41595 4395 0,15 (111.4) 0,16 (1					1	300	360	400	12 60 77	600	860	600	700	2.600	1900
V, m'/mg					in the second second	SORETH HA	Karena			MAINTAN SHOW OF THE	PRINCIPAL AND	A CCC	Constitution and the constitut	2.201	
0.15 (111.4)															
6, kJ/rg 7, 74291 7, 6441 7, 8446 80.278. 8.1975 8.3562 8.5057 8.6473 8.7321 8.909 9,1533 9,3787 9,598 (7, 10)	0.157111.41		•	• •						•	• -				4395.9
1 1 1 1 1 1 1 1 1 1	0.10 (111.4)		•					-				•			
## 1													*****		
\$\begin{array}{c c c c c c c c c c c c c c c c c c c		AND THE RESERVE OF THE PARTY OF	and the second		plant in white the	Bulletin Market	a of distant	100	SECTION AND ADDRESS.	200	2 8 0 3 1 6 C 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ALL DATE OF STREET	用的机械介持在数据	C2:751-14-16-16-18	938546
1. 1. 1. 1. 1. 1. 1. 1.	02/1202	A STATE OF THE STATE OF	STATE OF THE SHAPE	建筑作业的通常从市区	4/01/2	20000	STATISTICAL PROPERTY.	SALID COLUMN		4 310000	377 37 ALLEN CO.	7:91436F5A714	and the second second	SV. A. P. Octob	4395.6
V, m²/q		350 VIDS - VIN SPORE		0.446.9360.645.069.44				A STATE OF THE PARTY OF	CLASS CONTRACTOR	MATCH STATE OF THE PARTY OF THE	Mary Control (St. August 1984)	邓州安全共和国和新疆			2404
V, m/kg		THE PROPERTY OF THE PERSONS	and stores and the same	PERSONAL PROPERTY.	MANAGE CONTRACTOR	Ship of the principle of	CANCED SHAME AND ASSESSED	CANAL THE PARTY.	STATE OF THE PARTY	destroyed to be desired at the last	AND ROLL WAS ARREST	CANAL SANCE THE FACE AND ADDRESS.	1 121	1 237	1.353
0.4 (145.6)		• •				-									3853.9
6. KUNG N 6.9307 7.1714 73797 7.5670 7.7350 7.8992 810-97 8.1921 8.3774 8.4566 8.6935 8.9253 8.13 5. KUNG N 6.9307 7.1714 73797 7.5670 7.7350 7.8992 810-97 8.1921 0.6638 0.6971 0.6638 0.772 0.6245 0.6245 0.6248 0.6971 0.6245	0.4 (143.6)								•					,	4395.1
5, KINGU N 63307 71772 7336 7433 7522 7523 7523 7523 7523 7523 7523 75		· •							•						9.1370
12 12 12 12 12 12 13 13	HATROPROVIDE PRODUCTION	.s, k.l/jkg K)	5.9307												0 0017
Page Fig. Page				STATE OF THE STATE		THE PROPERTY OF THE VIEW		A CANAL TO A CANAL OF THE ACT OF	THE TRUE STATE	公开设置的 对外的第四次	CATTON SOLVERSON		3.77	Charles to Contract	3853.3
V, m²/kg	06 (158 A)	A STATE OF THE STA		CARL STATE OF SHIPE OF		Mark Andrews	14147571451 437765	THE WAY COME			THE WAY AND THE	THE STATE OF THE STATE OF	3826.8	Victoria South	43944
V, m²/kg - 0.2608 0.2931 0.3241 0.3544 0.3843 0.4139 0.4433 0.4726 0.5018 0.5601 0.6181 0.67 0.6 (170.4) v, k,l/kg - 2633.6 2715.5 2797.1 2878.2 2959.7 3042.2 3125.9 3211.2 3297.8 3476.2 3661.1 385.0 0.6 (170.4) n, k,l/kg - 2839.2 2950.0 3056.4 3161.7 3267.1 3373.3 3480.6 3589.3 3699.4 3924.3 4155.7 436.6 4, k,l/kg, k) - 6,8167 7,0392 7,2336 7,4097 7,5723 7,7245 7,8680 8,0042 8,1341 8,3779 8,6041 8,81 4, k,l/kg, k) - 6,8167 7,0392 7,2336 7,4097 7,5723 7,7245 7,8680 8,0042 8,1341 8,3779 8,6041 8,81 4, k,l/kg, k) - 6,8167 7,0392 7,2336 7,4097 7,5723 7,7245 7,8680<				1075 D 2003 O 24 C 12 C		1 6 5 6 6 5 7 7 7 1 1 1 1	ALCOHOL:	77040	Transcription of the Con-		1571 1541 1713 1713 1810	THE BOOK OF THE STREET	85115	200	18,00
0.8 (170.4)				the transfer of the second	HAME OF STATE OF STATE OF	Paint the absent to the person of the	CELLARATEC, NACLACIA TONIA	0.3843	ASSESSMENT OF THE PROPERTY OF	ALEKAYAN METATIFOREN	ACCES ON THE PROPERTY OF	CONTRACTOR CONTRACTOR	Mary Cale Property	.0,6181	0.6761
0.6 (170.4)										3125.9	3211.2	3297.9	3476.2	3661.1	3852.8
\$, k, l/(k) - 6,8157 7,0092 7,2336 7,4097 7,5723 7,7245 7,8680 8,0042 8,1341 8,3779 8,6041 8,81	0.8 (170.4)	. •	_ ,						-		3589.3	3699.4	3924.3	4155,7	4393.6
0265 0265 0265 0266 0300 0307 0377 0377 0345 035 035 035 035 035 035 035 035 035 03			-						7:7245	7:8680	8.0042	8.1341	8.3779	8,6041	8,6161
2019 2708 2782 2815 2002 3176 2002 3176 2008 2786 3276 8800 380 3770 3770 3770 3770 3770 3770		and the second second second second		STEPHENSON STREET			02625	0.0066	0.3304	0.3541	403776	0 401 150	60478	0.49431	0.407
307.0 (201.0 (20				2621.9**	2709.8	2783.2	2875 2.2	W12937374	3040.2	9124.3	2008	3266.0	18475417	3860.5	3852.2
	1 (79.0)	a de la composição de la c		2827.9	11.00	005122	2.3167.12	3263.9	33707 ¹ /2	0478.4 is	35876	8697.9	3828) ()	21,416 4 .8	43020
E-FREEDOM TO THE TOTAL CONTROL OF THE TOTAL CONTROL		kula K		669482	6.0255	171,2971	7,3019-7	174636	7.6188	7.7600	7,8896	9.0298	8 2740	8505	87127
ν, π ² /kg – 0.1325 0.1520 0.1697 0.1866 0.2000 0.2192 0.2352 0.2510 0.2668 0.3292 0.329	CHRISTOPHINE		nerverskirkliker.	0.1325	0.1520	0.1697	0.1866	0.2030	0.2192	0.2352	0.2510	0.2658	0.2981	0.3292	0.3603
U, KJ/kg - 2598,1 2695.3 2783.1 2867.6 2951,3 3035.3 9120.3 3206.4 3293.9 3479.2 3658.7 3858	• • • •	• .			2695.3	- 2783.1	2867.6	2951,3	3035.3	3120,3	3206.4	3293.9	3473.2	3658:7	3850.8
1.5 (198.7) h, kulton - 2795.6 2920.2 5037.6 3147.4 3255.8 3564.1 3478.0 3582.9 3694.0 3582.9 4152.6 439	1.5 (198.3)		-			3037.6	3147.4	3255.8	3364,1	3473,0	3582.9	3694:0	3920.3	4152£	4391.2
						•				7.5706	7.7083	7.8393	(8.0846)	83118	8.5243

Saturated R134a Vapour

Table C.7c	Saturated Re	frigerant-134a	Temperatu	re Table (Met	ric Units)					
	Constitution .	Specific Vol	une zn /kg:	33,50 m	ternal Energy kul/1	and the	Enthelp	y ku kacasa	entropy	J(140 - 17)
Temp. CT		Sat Liguid V	Sat Vapor Va	Set Liquid u	Bat Vepor U.Y	Bet Liquid by	Even in	Sat Vapor h,	Set Liquid ey	Sat Vapor s
	0.054.04	0.000 705 5	0.3569	-0.04	204.45	0.00	222.88	222.88	0.0000	0.9560
-40 00	0.051 64 0.063 32	0.000 703 5	0.3303	4.68	206.73	4:73	220.67	225.40	0.0201	0.9506
-36 -32	0.003 52	0.000 717 2	0.2451	9.47	209,01	9.52	218.37	227.90	0.0401	0.9456
9 28	0.000 06.	6000 723 3	0.2052	8 8 4 7 14,317 150	211.20 70	4 37 y > 10	2160UF 14	230,38	0.0000	STED OF THE
30	0 101 99	0.000 720 5	0.1882	16.75	212.43	1883	214.80	231.62	0.0699	*,08390
- 34	24 Dr (1 80)	d.000,729.6×	0.1728	7 3 19 21	213,579	19.29	213 57 115	232.85	0.0796	0.9370
-22	0.121 92	0.000 732 8	0.1590	21,68	214,70	.21,77	212,32	234.08	0.0897	0.9351
-20	0.132 09	0.000 736 1	0.1464	24.17	215.84	24.26	211.05	235.31	0.0996	0.9332
-18	0.144 83	0,000 739 5	0,1350	26.67	216.07	26,77	209.76	236.53	0.1004	0.9315
12.00	0.157,48	0.000,742 6	0.1247.345	2038	218 1012		208.45	7,237,74	Ø1102	0.9298
127	0.188 40 0	0,000 749 8	0. 068	84.25	#220.38	25 64 39	205,772	240,15	r 13386	0.9267
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	· 0.20704	0.000 756.0	0.0919	39.38	A 222,60 Pr	30.54	203.00	in 242.54 mil	0.1583	
4	0.252 74	0.000 764 4	0.0794	44.56	224.84	44.75	200.15	244.90	0.1777	0.9213
0	0.292 82	0.000 772 1	0.0689	49.79	227.06	50.02	197.21	247.23	0.1070	0.9190
4	0.337 65	0.000 780 1	0.0600	55.08	229,27	55.35	194.19	248.53	0.2162	0.9169
A TOTAL	70.387.50.	0.000,788 4	0.0525	80.435	231.46	4 (60.13.)	180.07	,(521/BO)	0.2354	0.9150
120	0,442,04	4-0,000 797 1	0.0460353	65.83	33303/	20048	., /187.85	264 03	(0.2546	小。(08)33
107.3	0.504 (6	0.000.0003	0.0405	'E 1/120'	7 235 78	71.99	184.52	256 32 19 0	V02735	0.9102
20	0.571 60	0.000 815 7	0.0358	76.80	237.91	77.26	181.09	258.36 260.45	0.2924 0.3113	0.9089
24:	0.845 86	0.000 825 7	0.0317	82.37	240.01	82,90	177.55 175.73	260.45 261.48	0.3208	0.9069
26	0.685 30	0.000 830 9	0.0298	85.18	241.05	85.75		201.40	0.3206	0.0016
77 - 28	7 072676	0,000,836.2	0.0281	88400	E_2/242.08	3 488.0 1	173.89 1 172.00	263.50	03396	0.9070
30,	0770 06	0.000 841.7	0.0265	90.84	.j. 243.10	13.5 191A9	170.00° A	261.48	0.84901	0.9064
** + 100 ±	Q 615 28	0.000,047.3	0.0250	(20 00 m)	24408	9439	168.14	265.45	0.3584	0.9058
34	0.862 47	0.000 853 0	0.0236	96.68	245,12 246,11	97.31 100.25	169,15	266.40	0.3678	0.9053
38	0.911 68	0.000 859 0	0.0223	9 9 .47 102.38	240.11	103.21	164.12	267.33	0.3772	0.9047
38	0.962 98	0,000 865 1	0.0210	10530	7 248.06	108.19	163-05	268.24	10.3866	0.9041
300	1,016#	0.000 871,4 32	0.0199	108.25	249.02	109/19	159.94	259.14	0.3980	0.0036
	1,072.0	0.000 878 0 0.000 884 7	0,0188	100 20	249.56	3 (H12/22 4	1357.79 W	21001	0.4054	3. no 9030 ⁻² .
(44)	× 1129 9	Martin A. Charles Valley Valley Valley	0.0177 0.01	117.22	251.79	118.35	153,33	271.68	0.4243	0.9017
48	1,252 6	0,000 898,9 0,000 914 2	0.015 9 0.0142	123.31	253.55	124.58	148.68	273.24	0.4432	0.9004
• 52	1,385 1 1,527 8	0.000 914 2	0.0142	129.51	255.23	130.93	143.75	274.68	0.4622	0.8990
56	7.327 8 7.4 38 (3	0000 049 8		135.82	256.817	0.11.07.12 FA	138.62	275.00	6-0.4814.HE	0.8973
	2:1162	00010027	0.0086	152.22	2280.15	454.34	124.00	218.43	0,5302	ىد 0.8918 o
200	28324	0.001 076.6	0.0084	169.86	262.14-3	3 0172.71 C	106.41	279 12	00.5814 26	0.8627
90	3,243 5	0.001 194 9	0.0046	189.82	261.34	193.69	82.63	276.32	0.6380	0.8655
100	3.974 2	0.001 544 5	0,0027	218.60	248,49	224.74	34.40	259.13	0.7196	0.8117

Table C.7d Saturated Refrigerant-134a Pressure Table (Metric Units)												
***	14.46	- Specific Volu			rnal Energy k	July 1	Enthele	Y KUKOT	Entropy k	(Katio =		
Press. MPs P	Temp. 'C.	Sat. Liquid V	Sat, Vapor	Set Liquid	Sat. Vapor	Set Uguld hi	Evap hij	Set Vepor	St.V. quid	Say Vapo		
0.06	-37.07	0.000 709 7	0.3100	3.41	206.12	3.46	221.27	224.72	Q.0147	0.9520		
0.08	-31.21	0.000 718 4	0.2366	10.41	209.46	10.47	217.92	228.39	0.0440	0.9447		
0.10	-26.43	0.000 725 8	0.1917	16.22	212.18	16.29	215,06	231.35	0.0678	0.9395		
7 1 10 12 m	#22.08 VIII	70.000732.37	0.01614	2) 23	214.50	21.32	., 212.54	233,86	, ".TD.0879" 5	30,93545		
8 0.14 5 0ff6 +6	718.80 15°	0,000 738 1 6,000 743 5	***0)395	25.06*** 29.66	21650	29.78	210,27, 208,187,	237.97	0.1065	0.9322 40.9295		
0.18	-12.73	0.000 748 5	0.1098	33.31	219.94	33.45	206.26	239.71	0.1352	0.9273		
0.20	-10.09	0.000 753 2	0.0993	36.69	221.43	36.84	204,46	241.30	0.1481	0.9253		
0.24	-5.37	0.000 761 8	0.0834	42.77	224.07	42.95	201,14	244.09	0.1710	0.9222		
0.82 0.82		0,000,789.7 0,000,777.0 0,000,783.91	0.0719 0.0832.6 0.0564	48.18 63.06	226 36 228 40 230 28	48.69 53.31, 57.82	198,13±/ 195,35 192,76	248.52 248.66 260.58	0,1917 \$ 0,2089 \$ 0,2251	5 0.9197. 4 0.9177 ~0.9160		
0.4	8.93	0.000 790 4	0.0509	61.69	231.97	62.00	190.32	252.32	0.2399	0.9145		
0.5	15.74	0.000 805 6	0.0409	70.93	235:64	71,33	184.74	256.07	0.2723	0.9117		
0.6	21.58	0.000 819 6	0.0341	78.99	238.74	79.48	179,71	259.19	0.2999	0.9097		
07(0.8)	26 72 81 33 85 53 7	0.000 832 8 0.000 845 (C	0.0292 0.0265 0.0226	.86.19 .792,75 .98.79	241.42 243.78 245.88	86.78 93.42 99.56	175.07 170.78 4.5.166.62	261.85 _{//} - 264.15 266.18	0.3242 0.3459 : \ 0.3658; \	0.9080 0.9066 0.9054		
1.0	39.39	0.000 869 5	0.0202	104.42	247.77	105.29	162.68	267.97	0.3838	0.9043		
1.2	46.32	0.000 892 8	0.0166	114.69	261.03	115.76	155.23	270.99	0.4164	0.9023		
1.4	52.43	0.000 915 9	0,0140	123.98	253.74	125.26	148.14.	273.40	0.4453	0.9003		
207	57.02 62.01 62.40	0.000.639.2 0.000.963 1 10 0.000.987.8 1	0.0121 0.01084 40.0084	132.52 PM 140.49 148.02	256,00 257,68 259,41	134,02 142,22 149,90	2 (41.91 27.34.80 127.95 ar	managed of a residence of the same	04714 04954 06178	0.8982 0.5959 0.8934		
2.5	77.59	0.001 056 2	0.0069	165.48	261.84	168.12	111.06	279.17	0.5687	0.8854		
3.0	86.22	0:001 141 6	0.0053	181.88	262.16	185.30	92.71	278.01	0.0158	0.8735		





Superheated R134a Vapour

ſ	Table C.8	b Superheate	ed Refrigeran	t-134a Vapo	r (Metric Ur	nits)			
120		Vinyako	VPV/SG	n Wika Til	W/(kg K)	eventadie	sullajkaj si	20 F2/3 G14"	e ka//kgabij
	770		OOEMRATT	(e) 57.67 (e)		e e		(a) (20 (4) (b)	
ľ	Sat.	0.31003	206:12	224.72	0:9520	0/19170	212.18	231.35	0.9395
	-20	0.33536	217.86	237.98	1.0062	0.19770	216.77	236.54	0.9602
٠ [_	-10	0:34992	224.97	245.96	1.0371	0.20686	224.01	244.70	0.9918
Š		0.3643374	26224	254.10	1.0675	0.21687	+4231,432	252.99	1.0227
1	100 44	X 0 37661 !	239 697	262 41		0.224733 0.23345	288,96	28143 270 02	1,0561
Įž,	30	0.40688	255:12	279.53	1.1657	0:24216	246.67 254.54	278.76	1.1122
	40.	0.42091	263.10	288:35	1:1844	0.25076	262.58	287.66	1.1411
	50	0.43487	271.25	297.34	1.2126	0.25930	270.79	296.72	1.1696
1	7.0	044879	279'68	308/51	9,2405	Giže779	279183	305/94	J. 1977
ř	70 et	\$646266 F	288.081/	G 5/84W #760	11,086164	1027823	287.70	4,315/02/34	-19254
i	9Ó	0.47650	296//5	025.94	2954	J/0/28464	7129830	11024.67.25	1,2528
. 3		0.49031	305.58 0 34 MPa (7)	335.00	1.3224	0:29302	305.27 ₩ 0 18 MPa (7)	334.57	1.2799
1	Sat.	0.13945	216.52	236.04	d Dagg	0.10023	NATIONAL ATTACACISM DESCRIPTION		PROFESSION STATE OF THE PROPERTY OF THE PROPER
1	–10	0.14549	223.03	243.40	0.9322 0.9606	0.10983 0.11135	.219.94 222.02	239,71 242.06	0.9273 0.9362
ļ	0	0.15219	230.55	251.86	0.9922	0.11678	229.67	250.69	0.9684
I	W-1045	0.15875	238/21	260 43 0	HI 0280	546H2207	207.44	259.41	
1	201	rom8520 at #	v 246 ot 234	280 161 6 F	10532	CO 12728	7245 33	268.23	1,0304
	#160 V	0,17065/	263196	4277,97	1.0828	i0/13236/it/	269,38	277.17	1.0604
١.	40	0.17783	262.06	286.96	1:1120	0.13730	261,53	286.24	1.0898
1	50 60	0.18404 0.19020	270.32 278.74	298.09 305.37	1,1407	0.14222	269.85	295,46	1.1187
, g	767	W046436	Parado	305.37	1.1690	0.14710 0.16193	278.31 286.837	304.79 314.28	1.1472
	166	0 20241	296 06	62439 IV	1 2244	0 15672	295.71	d23.02	1 2030
1	190	0.20846	1,303,967	334 14	m 25 6	0.16146	-304.63	333.70 m	1,2600
777	100	0.21449	314.01	344.04	1.2785	0.16622	313.72	343.63	1,2573
蓝		areni de Re	/0,20 MPB //	###10.08°S)			=024 MPa (7	Lie-537 Ok	
	Sat.	0.09933	221,43	241.30	0.9253	0.08343	224.07	244.09	0.9222
1	-10	0.09938	221.50	241.38	0.9256		- .	- <u>-</u> .	-
200	o D	0.10438	229.23	250.10	0.9582	0.08574	228.31	248.89	0.9399
	201	9.19826	237.05	268.89	0.0898 (f) 1.0208	006993 006999	238 28 2	257.64 266.85	(J.972) 7.0034
	30.	To order	1253 D6	276 77 1	9 6668	o ogzed	252 45	25.06	
	40	0.12311	261.26	285.88	1.0804	0.10181	260.72	286.16	1.0637
1.	50)	0.12758	269.61	295.12	1.1094	0.10562	269.12	294.47	1.0930
100	60 ************************************	0.13201	278:10	304.50	1.1380	0.10937	277.67	303.91	1,1218
		013636	2867747	614 02 - 323 68	1,1661	0.11907.0	7286.36	19.639	1116016
	er eon	0.4504	30447	44426	1 1939	81,574	532.79		1,1780
-	100	0.14932	313.57	343.43	1.2483	0.12398	313.27	343.03	1.2326
8		, P	oza Wza ch	that the college of t				(=248 C)	
-	Sat.	0.07193	226.38	246.52	0.9187	0.06322	228.43	248.66	0.9177
	O.	0.07240	227.37	247.64.	0.9238	· · · · · · · · · · · · · · · · · · ·	'		÷
	10	0.07613	235.44	256.76	0.9566	0.06576	234.61	255.65	0.9427
	20	140167/97/24/34	248/59/7	-266'91	0/9883/ 6/55	006901	242187	264'66	100749
) a	inese Openies	0,08320	4251/88/A	275 12 4	10192	0,07214	251/19	. 276 28	1,0085

	<i>y</i>					······································			
<i>M</i> e	C.8b Su	perheate	d Refrigerant	-134a Vapor	(Metric Unit	s) continue			
/ATE	Σ'n	% of E	υkl/kg ₹	hku/kg 📑 🛊 i	ω/ka/k)	v m³/kg	ijkJ/kg , j	OF ECHINARY PARK PARK THE ST. BASINESS	N(RB K)
· // 90	0.0	3393	299:37	326.52	1.0940	0.02980	298.46	325.28	1.0819
100	0.0	3519	308:93	337.08	1.1227	0:03095	308.11	335.98	1.1109
110	0.0	3642	318,57	347.71	1.1508	0.03207	317.82	346.68	1.1392
133120	动机体的生物和产品的产品。	8762±	328,31	35840,	1784 74	0.03316	327.62	357.47	11670 11943
130		3881	(338)14 (1) F	369 19 7 27	1.2055	0.03423	337 52 347 51	368.33 379/27/	
341149)	ANY CONTRACTOR OF THE PROPERTY	3997	348.09	380,07 (1) 391.05	1.2584	(0.03529)	357,61	390.31	1.2475
150		4113	358.15 368.32	402.14	1.2843	0.03736	367.82		1.2735
160		4227 4340	378.61	413.33	1.3098	0.03838	378.14	412.68	1.2992
200		44521	1889.02	424.63	A 33518 A	0.039397/4	988.57	424.0271	1 3245
			o MPa (7 ₈₈	CARRICLES CONTRACTOR STATES AND THE		CO TO A SENSON PROPERTY OF THE	1.20 MP# (7.	24832°C	
	ON BEOM	CHARLEST ALL PROPERTY OF THE STREET	AND AND THE PERSON OF THE PERSON OF STREET	bilings on year eviza. A strange of the transfer page 12	0.9043	0.01663	251.03	270.99	0.9023
Sat.		2020 2029	<i>247.7</i> 7 248.39	268.68	0.9066	0.01003	201.00	_	_
4.0 50		2029 2171	258.48	280.19	0.9428	0.01712	254.98	275.52	0,9164
500		23012	268:35	291367	0.9768	0.01635	265.42/15-120	287:44	0.9527
70	the Salvair of the Park	2423	278 110 22	302 34	9100d3	0.01947	276.69	298 96	0.9868
80	A DESCRIPTION OF THE PARTY OF T	2538	287.82	313120	0405	0.02051	285.62	310.24	1,0192
90	0.0	2649	297.53	324.01	1.0707	0:02150	295.59	321.39	1.0503
100	0.0	2755	307:27	334.82	1.1000	0.02244	305.54	332.47	1.0804
110	· · · · · · · · · · · · · · · · · · ·	2858	317:06	345:65	1.1286	0.02335	.315.50	343.52 354 58	1.1096
120		2959]	326/03/	356162	a 1 567	0.02423	825.514.) 335.68	365.68	1/1660
1300		3058	336 88 33 34 34 34 34 34 34 34 34 34 34 34 34	367 46 - 378 46 - 378	1184) 1211)	0.02592	34573	976 83 V	H#1933
150		3154 3250	357.06	389.56	1.2376	0.02674	355.95	388:04	1.2201
160		3344	367.31	400.74	1.2638	0.02754	366.27	399.33	1.2465
170		3436	377.66	412.02	1.2895	0.02834	376.69	410.70	1.2724
27,180)	10(214) 0.0	352867	"388/J2(" - V	428,401	10149	0.02912	367,23	42216	0893 (
		HOUSE PIL	1140 MP. (T.	, = 52.40°C)##		a a toward a	1.60 MPa (7.2	J-Greiz-en	
Sat.		1405	253.74	273.40	0.9003	0.01208	256.00	275.33	0.8982
60		1495	262.17	283:10	0.9297	0.01233	258.48	278.20 ⁻	0.9069
70		1603	272.87	295.31	0.9658	0.01340	269.89	291.33 .	0.9457
W. 601	N 0 7 6 0	1701	7283/29 3 1-1-1	307,10,75,5%	0.9997 - 4 4	0.01436	280.78	303,74	0,5813%
90	- 15 G-0 O	1792	293 55 gra	318,63	1,0319	0.015215	291/39[1	316.72	1.0148
20100		1878	303.73	390:05()	9.0628	0.01601	(90) 84 22	327,46	10467
110		1960	313.88	.341.32	1.0927	0.01677 ´ 0.01750 .	312.20 322.53	339.04 350.53	1,0773 1,1069
120		2039	324.05 334:25	352.59 363.86	1,1218 1:1501	0:01/30	332.87	361.99	1.1357
130		2115 2189	334.25 1344.60	375453	3617777	0.01887	343 242 0	373 44	H 638
150		2202-	354 82	366.49	1 2048 7	0.01953=7.4	353.667	384 91/11	1 1912
160	THE REPORT OF THE PARTY OF THE	2333	365 22	397.80	1 2315	0,02017	364 150	395 #3	12181
170	at hit he that "A man and a factor of them of a	2403	375.71	409.36	1.2576	0.02080	374.71.	407.99	1.2445
180		2472	386.29	420.90	1.2834	0.02142	385.35	419.62	1.2704
190		2541°	396.96	and the second s	1.3088	0.02203	396.08	431.33	1.2960 1.3212
200	***********	2608:	7,407,73 H = 1	444,24	1,3338	0.02263/245	A06 905 %	(377) (I) (Carry)	**************************************

. 7	Table C.8b	Superheated	l Refrigerant	-134a Vapor	(Metric Unit	s) continue	d:		
	7.6	nicker occupante programme and the state of	NUMBER OF THE PROPERTY OF THE	CONTRACTOR STATE OF CONTRACTOR CO	kJ/(kg K)/.	MINERAL PROPERTY OF THE PROPER	u ku/ke/ tale	n ko/kg/line k	J/(Kg K)
Paris.	40	0.08660	260.17	284.42	1.0494	0.07518	259,61	283.67	1.0367
	50		268.64	293:81	1.0789	0:07815	268.14	293.15	1,0665
1	60	0.09319	277.23	303.32	1.1079	0.08106	276.79	302.72	1.0957
70	2.70	0.096417	265.96	(312 95 (73) 37	3191364 PA	0.08392	285.56	612 417	1/1243
23	9.80	0.00000	294 82 2 34 34 4	322 75 44 1	11644	0.08674	294/46	322:22/*******	101525
	00.4	0.10275	303.83	332.60	H1920:	O.08953	303.60	332/15	13802
	100	0.10587	312.98	342.62	1.2193	0.09229	312.68	342.21	1.2076
	110	0.10897	322:27	352.78	1.2461	0:09503	322.00	352.40	1.2345
١	120	0.11205	331:71	363.08	1:2727	0.09774	331.45	362.73	1.2611
		er Pe	0.40 MPa (7.			<i></i>	Sale parion sub-lines at passe previous asserts	n=15.74°C)	
	Sat.	0.05089	231,97	252.32	0.9145	0.04086	235.64	256:07	0.9117
	10	0.05119	232:87	253.35	0.9182	•	****		
	20	0.05397	241:37	262.96	0.9515	0.04188	239.40		0.9264
	9.30 -1.	0.05862: 11-14	240 80% vc 10	272:54 70 2. 1	0.89374	0 04416 3 0 04633 4 7 5	248.20 256.997	280 16 17 17 17 17 17 17 17 17 17 17 17 17 17	0.6597.1
	140	0.05917	25847-1960	20170	1.D148	0.04642+**	265 83	290 04	1 0220
200	60	0.06164 0.06405	275.89	301.51	1.0748	0.05043	274.73	299.95	1.0531
	70	0.06641	284.75	311.32	1:1038	0.05240	283.72	309.92	1,0825
	80	0.06873	293.73	321.23	1:1322	0.05432	292.80	319.96	1.1114.
	18.90VET VII	0.07102	302.84	331.25	1/1602/50	0.05620	302.00 1/2	330-105-228	397.4
	1007	0.07327.4	31207	341:38 (4)	1.1878	0.05805	(311,61)-752-7	-340.33	1 1875
	110.55	d107550.32°#	321/44	351-64	1 2149	0.05988	320,74 2 (1)	350.68	171049
1000	120	0.07771	330,94	362.03	1.2417	0.06168	330.30	361.14	1.2218
	130	0.07991	340.58	372.54	1.2681	0.06347	339.98	371.72	1.2484
200	140	0.08208	350:35	383.18	1.2941	0.06524	349.79	382.42	1.2746
2			0.60 MPA((7			TATAL STREET, COLUMN STREET, S	0:70 MP= (7.	er er bei geschafte aus an er autrikkeine kaal ben kokula bakta.	
	Sat.	0.03408	238.74	259.19	0.9097	0.02918	241.42		0.9080
1	30	0.03581	246.41	267.89	0.9388	0.02979	244.51		0.9197
986	40	0.03774	255.45 264 48:	278.09 288.23	0.9719 510037	0.03157 0.03324	253.83 263.08		0.9339
拉	200	CO395875 7 CO4134	7735a 1785	298 35	1,0346	0 03482	272.31	206 60	10182
	345 T P) 11	onana a a	282.66 July 1	308 482 117	3 0645	003634, 51	281.57	THE RESERVE OF THE PROPERTY OF THE PARTY OF	10487.7
783	80	0.04469	291.86	318.67	1.0938	0.03781	290.88	317:35	1.0784
	90	0.04631	301.14	328.93	1.1225	0.03924	300.27	327.74	1.1074
1	100	0.04790	310.53	339.27	1.1505	0.04064	309.74	338.19	1.1358
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L-2/T-1/ME

Date: 19/11/2012

BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA

L-2/T-1 B. Sc. Engineering Examinations 2011-2012

Sub: ME 241 (Engineering Mechanics)

Full Marks: 280

Time: 3 Hours

USE SEPARATE SCRIPTS FOR EACH SECTION

The figures in the margin indicate full marks.

SECTION - A

There are **FOUR** questions in this Section. Answer any **THREE**. Symbols indicate their usual meaning. Assume any missing data.

- (a) The slider block A, as shown in Fig. 1(a), starts from rest and moves to the left with a constant acceleration. Knowing that the velocity of block B is 304.8 mm/s after moving 609.6 mm, determine (i) the acceleration of A and B, (ii) the velocity and (23)position of A after 5 s. (b) Two wires AC and BC are tied together at C to a sphere which revolves at a constant speed v in the horizontal circle as shown in Fig. 1(b). Determine the range of values of v (23%)for which both wires remain taut. (a) The 3-kg collar is initially at rest and is acted upon by the force Q which varies as shown in Fig. 2(a). Knowing that $\mu_k = 0.25$, determine the velocity of the collar at (i) t=1 s, (ii) t=2 s. Solve the problem using the principle of impulse and momentum. (23)(b) A 1.4-kg collar is attached to a spring and slides without friction along a circular rod which lies in a vertical plane as shown in Fig. 2(b). The spring has a constant k = 25N/mm and is undeformed when the collar is at B. Knowing the collar passes through point D with a speed of 1 m/s, determine the speed of the collar as it passes through (23%)(i) point C, (ii) point B. (a) A rectangular plate is supported by two 150-mm links as shown in Fig. 3(a). Knowing that at the instant shown the angular velocity of link AB is 4 rad/s clockwise, determine (i) the angular velocity of the plate, (ii) the velocity of the center of the plate. (23)(b) End A of rod AB, as shown in Fig. 3(b), moves to the right with a constant velocity of 2 m/s. For the position shown, determine (i) the angular acceleration of rod AB, (23%)(ii) the acceleration of the midpoint G of rod AB. (a) The double pulley shown in Fig. 4(a) has a total mass of 6 kg and a centroidal radius of gyration of 135 mm. Five collars (weights), each of mass 1.2 kg, are attached to cords
- 4. (a) The double pulley shown in Fig. 4(a) has a total mass of 6 kg and a centroidal radius of gyration of 135 mm. Five collars (weights), each of mass 1.2 kg, are attached to cords A and B as shown in the figure. When the system is at rest and in equilibrium, one collar is removed from cord B. Neglecting friction, determine (i) the angular acceleration of the pulley, (ii) the velocity of cord A at t = 2 s.

Contd P/2

(23)

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(b) The 9-kg rod AB is attached by pins to two 6-kg uniform disks as shown in Fig. 4(b). The assembly rolls without sliding on a horizontal surface. If the assembly is released from rest when $\theta = 60^{\circ}$, determine the angular velocity of the disks when $\theta = 90^{\circ}$.

(23%)

(20)

(26%)

(23)

(23%)

(23)

(23%)

(23)

(23%)

SECTION - B

There are FOUR questions in this Section. Answer any THREE.

5. (a) A 450-kg crate is to be supported by the rope-and pulley arrangement as shown in Fig. 5(a). Determine the magnitude and direction of the force F which should be exerted on the free end of the rope.

(b) Determine the polar moment of inertia of the shaded area as shown in Fig. 5(b) with respect to the centroid of the area.

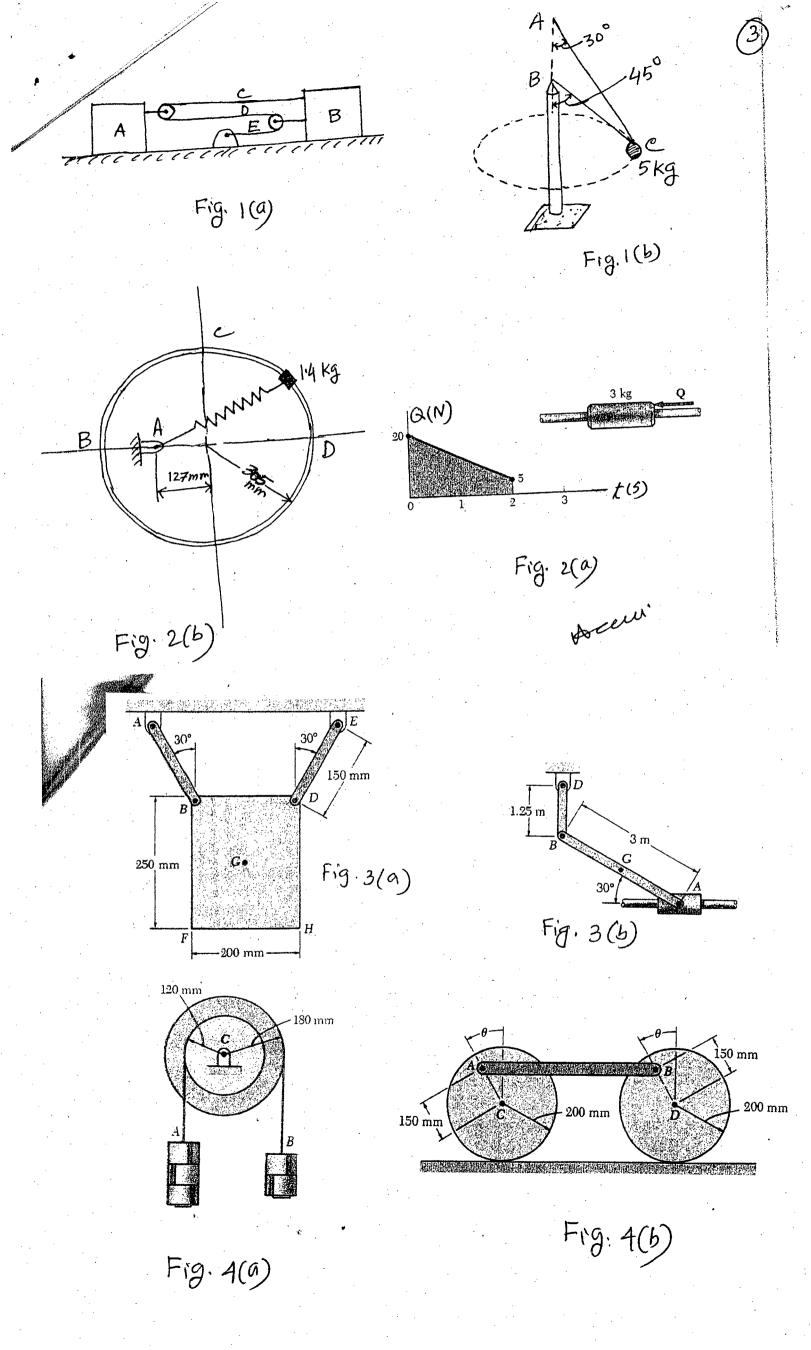
6. (a) The frame ACD is hinged at A and D and supported by a cable which passes through a ring at B and is attached to hooks at G and H as shown in Fig. 6(a). Knowing that the tension in the cable is 1125 N, determine the moment about the diagonal AD of the force exerted on the frame by portion BH of the cable.

(b) One end of rod AB rests in the corner A and the other is attached to cord BD as shown in Fig. 6(b). If the rod supports 200-N load at its midpoint C, find the reaction at A and the tension in the cord.

7. (a) Determine the distance h for which the centroid of the shaded area as shown in Fig. 7(a) is as high above line BB' as possible when k = 0.10.

(b) Determine the force in members FH and GH of the truss as shown in Fig. 7(b) when P = 35 kN.

8. (a) The frame as shown in Fig. 8(a) is loaded by a clockwise couple of magnitude 150
N-m applied at point A. Determine the components of the reactions at D and E.
(b) A cord is attached to and partially wound around a cylinder of weight W and radius r which rests on an incline as sown in Fig. 8(b). Knowing that θ = 30°, find (i) the tension in the cord, (ii) the smallest value of the coefficient of static friction between the cylinder and the incline for which equilibrium is maintained.





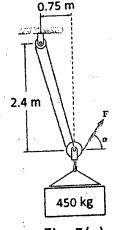


Fig. 5(a)

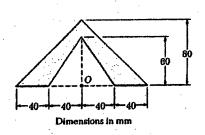


Fig. 5(b)

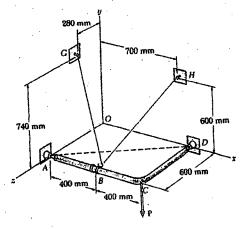


Fig. 6(a)

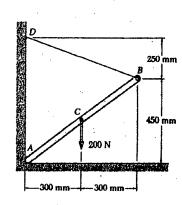


Fig. 6(b)

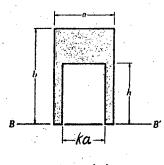


Fig. 7(a)

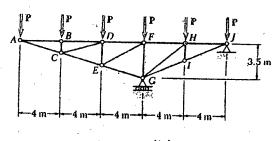


Fig. 7(b)

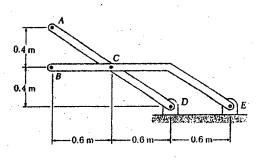


Fig. 8(a)

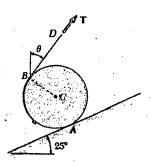


Fig. 8(b)