# L-3/T-2 $\quad$ B. Sc. Engineering Examinations 2009-2010 

Sub : IPE 381 (Measurement and Quality Control)
Full Marks: 210
Time : 3 Hours
The figures in the margin indicate full marks.
USE SEPARATE SCRIPTS FOR EACH SECTION

## SECTION - A

There are FOUR questions in this Section. Answer any THREE.

1. (a) A die is loaded in such a way that, number $1,2,3$ are twice likely to occur than number $4,5,6$. If the die is rolled twice, what is the probability of getting 2 odd numbers or two even numbers?
(b) The total number of hours, measured in units of 100 hours, that a family runs vacuum cleaner over a period of one year is a continuous random yariable X that has the density function:
$F(x)=\left\{\begin{array}{lll}x & ; & 0<x 1 \\ 2-x & ; & 1 \leq x<2 \\ 0 & ; & \text { elsewhere }\end{array}\right.$
(i) Find the Cumulative Distribution Function $\mathrm{F}(\mathrm{x})$
(ii) $\operatorname{Draw} F(x)$ with respect to x .
(iii) Find the probability that over a period of one year, a family runs their vacuum cleaner less that 120 hours.
(c) Explain with neat sketch the working principle of an autocollimator and pivoted stylus to measure the diameter of a bore. Derive the expression for bore diameter and find the probable amount of error in calculation for,

$$
\begin{aligned}
& \mathrm{R}=50 \mathrm{~mm} \pm 0.01 \mathrm{~mm} \\
& \alpha=10^{\circ} \pm 0.01^{\prime} \\
& \beta=9^{\circ} \pm 0.1^{\prime}
\end{aligned}
$$

Where the symbols carry the usual meanings.
2. (a) The output voltage of certain electric circuit is specified to be 131 . If the voltage falls as low as 130 , serious consequences may result. In a given period, 40 independent readings on the voltage are to be taken. For testing $H_{0}: \mu \geq 131$ versus $H a: \mu=130$, Significance level, $\alpha$ is to be 0.05 . If the standard deviation, $\sigma=1.9$ volt for these circuit, calculate the probability of Type-I and Type-II Error.
(b) The following data show the frequency counts for 380 observations on the number of bacterial colonies within the field of a microscope.

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## Contd ... O. No. 2(b)

| Number of colonies per field | Frequency of observations |
| :---: | :---: |
| 0 | 56 |
| 1 | 104 |
| 2 | 80 |
| 3 | 62 |
| 4 | 42 |
| 5 | 27 |
| 6 | 9 |

Test the hypothesis that, the data fit the poisson distribution. Here $\lambda$ is the average number of colonies per field. Use Significance level, $\alpha=0.05$.
(c) What is a best size wire? What are the advantages of using best size wire to measure effective diameter of a screw thread? Derive the expression of effective diameter of a screw thread using best size wire.
3. (a) Define involute and cycloidal profile of gear? Derive expression for Involute function.
(b) What do you understand by interchangeable manufacturing and why is it important?
(c) What is the significance of Chebyshev's theorem in statistical application?
(d) Explain the following types of measurement errors that likely to creep in precision measurement:
(i) Contact point penetration
(ii) Effect of alignment
(iii) Error due to poor contact.
4. (a) What do you understand by Moment Generating Function? Derive the expression of Moment Generating Function for Binomial and Geometric distribution.
(b) With relevant sketch explain the following criteria to design a limit gauges:
(i) Allocation of tolerance.
(ii) Fixing gauge element with handles.
(c) What do you understand by kinematic accuracy of a gear? What is the basic difference between gear reproducing method and gear generating method? What are the sources of error in these two gear manufacturing method?
(d) Why a screw thread is more prone to error than a plain shaft? What problem may arise due to error in screw thread?

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## IPE 381

## SECTION - B

There are FOUR questions in this Section. Answer any THREE.
5. (a) "TQM reflects a different way of viewing the entire way of life of the people in the organization" - Do you agree with this statement? Justify your answer.
(b) Explain the stages of PDCA cycle which one must go through to get from 'problem faced' to 'problem solved'.
(c) How does the concept of 'zero defect' not economically beneficial according to Juran's Model? Is it possible to achieve minimum cost at the point of $100 \%$ good quality? Discuss briefly.
6. (a) How does BPR differ from TQM? What are the risks and barriers to BPR?
(b) The production of integrated circuits by etching them onto silicon wafers requires silicon wafers of consistent thickness. However their customer has raised questions about whether or not the process is capable of producing wafers within their specifications of $0.250 \mathrm{~mm} \pm 0.005$. Using the data provided in the Table- 1 ,
(i) Draw $\bar{X}-R$ chart to find out whether the process is in good control or not.
(ii) Calculate the process potential index and process performance index.
(iii) Interpret the indices.
(iv) Find out the total fraction of products not meeting specifications.
(v) Process Capability Ratio.

Table - 1: Silicon Wafer Thickness

| Subgroup | Thickness of silicon wafers for four observations |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 0.2500 | 0.2510 | 0.2490 | 0.2500 |
| 2 | 0.2510 | 0.2490 | 0.2490 | 0.2520 |
| 3 | 0.2510 | 0.2510 | 0.2490 | 0.2480 |
| 4 | 0.2490 | 0.2470 | 0.2520 | 0.2480 |
| 5 | 0.2500 | 0.2470 | 0.2500 | 0.2520 |
| 6 | 0.2510 | 0.2520 | 0.2490 | 0.2410 |
| 7 | 0.2510 | 0.2480 | 0.2500 | 0.2500 |
| 8 | 0.2500 | 0.2490 | 0.2490 | 0.2520 |
| 9 | 0.2500 | 0.2470 | 0.2500 | 0.2510 |
| 10 | 0.2480 | 0.2480 | 0.2510 | 0.2530 |
| 11 | 0.2500 | 0.2500 | 0.2500 | 0.2530 |
| 12 | 0.2510 | 0.2490 | 0.2510 | 0.2540 |
| 13 | 0.2500 | 0.2470 | 0.2500 | 0.2510 |
| 14 | 0.2500 | 0.2500 | 0.2490 | 0.2520 |
| 15 | 0.2500 | 0.2470 | 0.2500 | 0.2510 |

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7. (a) The basic QFD methodology involves four basic phases - Explain each phases with appropriate example.
(b) A company and its customer have agreed to follow a double sampling plan with the following parameters :
lot size $=3000$,
First sample size $=40, \quad$ Acceptance No. $=2$
Second sample size $=80, \quad$ Acceptance No. $=4$
For fraction non conforming value 0.05 ,
Find out the total probability of acceptance in the combined sample.
(c) 'Quality appraisal means quality evaluation' - Justify this statement.
8. (a) Which parameters of a gear is tested using Parkinson Gear Tester? Discuss the working principle of a Parkinson Gear Tester explaining how it is used to test the gear.
(b) Does tooth eccentricity effects pitch error in a gear? If yes, explain the effect from different point of gear performance.
(c) Explain how Barrel Tumbling is used for surface finish. What are the purposes of using it?

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## Standard Normal Distribution Table



| $z$ | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | 08 | 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 | . 0000 | . 0040 | . 0080 | . 0120 | . 0160 | . 0199 | . 0239 | . 0279 | . 0319 | . 0359 |
| 0.1 | . 0398 | . 0438 | . 0478 | . 0517 | . 0557 | . 0596 | . 0636 | . 0675 | . 0714 | . 0753 |
| 0.2 | . 0793 | . 0832 | . 0871 | . 0910 | . 0948 | . 0987 | . 1026 | . 1064 | . 1103 | . 1141 |
| 0.3 | . 1179 | . 1217 | . 1255 | . 1293 | . 1331 | . 1368 | . 1406 | . 1443 | . 1480 | . 1517 |
| 0.4 | . 1554 | . 1591 | . 1628 | . 1664 | . 1700 | . 1736 | . 1772 | . 1808 | . 1844 | . 1879 |
| 0.5 | . 1915 | . 1950 | . 1985 | . 2019 | . 2054 | . 2088 | . 2123 | . 2157 | . 2190 | . 2224 |
| 0.6 | . 2257 | . 2291 | . 2324 | . 2357 | . 2389 | . 2422 | . 2454 | . 2486 | . 2517 | . 2549 |
| 0.7 | . 2580 | . 2611 | . 2642 | . 2673 | . 2704 | . 2734 | . 2764 | . 2794 | . 2823 | . 2852 |
| 0.8 | . 2881 | . 2910 | . 2939 | . 2967 | . 2995 | . 3023 | . 3051 | . 3078 | . 3106 | . 3133 |
| 0.9 | . 3159 | . 3186 | . 3212 | . 3238 | . 3264 | . 3289 | . 3315 | . 3340 | . 3365 | . 3389 |
| 1.0 | . 3413 | . 3438 | . 3461 | . 3485 | . 3508 | . 3531 | . 3554 | . 3577 | . 3599 | . 3621 |
| 1.1 | . 3643 | . 3665 | . 3686 | . 3708 | . 3729 | . 3749 | . 3770 | . 3790 | . 3810 | 3830 |
| 1.2 | . 3849 | . 3869 | . 3888 | . 3907 | . 3925 | . 3944 | . 3962 | . 3980 | . 3997 | . 4015 |
| 1.3 | . 4032 | . 4049 | . 4066 | . 4082 | . 4099 | . 4115 | . 4131 | . 4147 | . 4162 | . 4177 |
| 1.4 | . 4192 | . 4207 | . 4222 | . 4236 | . 4251 | . 4265 | . 4279 | . 4292 | . 4306 | . 4319 |
| 1.5 | . 4332 | . 4345 | . 4357 | . 4370 | . 4382 | . 4394 | . 4406 | . 4418 | . 4429 | . 4441 |
| 1. | . 4452 | . 4463 | . 4474 | . 4484 | . 4495 | . 4505 | . 4515 | . 4525 | . 4535 | . 4545 |
| . 1.7 | . 4554 | . 4564 | . 4573 | . 4582 | . 4591 | . 4599 | . 4608 | . 4616 | . 4625 | 4633 |
| 1.8 | . 4641 | . 4649 | . 4656 | . 4664 | . 4671 | . 4678 | . 4686 | . 4693 | . 4699 | . 4706 |
| 1.9 | . 4713 | . 4719 | . 4726 | . 4732 | . 4738 | . 4744 | . 4750 | . 4756 | . 4761 | . 4767 |
| 2.0 | . 4772 | . 4778 | . 4783 | . 4788 | . 4793 | . 4798 | . 4803 | . 4808 | . 4812 | . 4817 |
| 2.1 | . 4821 | . 4826 | . 4830 | . 4834 | . 4838 | . 4842 | . 4846 | . 4850 | . 4854 | . 4857 |
| 2.2 | . 4861 | . 4864 | . 4868 | . 4871 | . 4875 | . 4878 | . 4881 | . 4884 | . 4887 | . 4890 |
| 2.3 | . 4893 | . 4896 | . 4898 | . 4901 | . 4904 | . 4906 | . 4909 | . 4911 | . 4913 | . 4916 |
| 2.4 | . 4918 | . 4920 | . 4922 | . 4925 | . 4927 | . 4929 | . 4931 | . 4932 | . 4934 | 4936 |
| 2.5 | . 4938 | . 4940 | . 4941 | . 4943 | . 4945 | . 4946 | . 4948 | . 4949 | . 4951 | . 4952 |
| 2.6 | . 4953 | . 4955 | . 4956 | . 4957 | . 4959 | . 4960 | . 4961 | . 4962 | . 4963 | 4964 |
| 2.7 | . 4965 | . 4966 | . 4967 | . 4968 | . 4969 | . 4970 | . 4971 | . 4972 | . 4973 | . 4974 |
| 2.8 | 4974 | . 4975 | . 4976 | . 4977 | . 4977 | . 4978 | . 4979 | . 4979 | . 4980 | . 4981 |
| 2.9 | . 4981 | . 4982 | . 4982 | . 4983 | 4984 | . 4984 | . 4985 | . 4985 | . 4986 | . 4986 |
| 3.0 | . 4987 | . 4987 | . 4987 | . 4988 | . 4988 | . 4989 | . 4989 | . 4989 | . 4990 | 4990 |
| 3.1 | . 4990 | . 4991 | . 4991 | . 4991 | . 4992 | . 4992 | 4992 | 4992 | 4993 | . 4993 |
| 3.2 | . 4993 | . 4993 | . 4994 | . 4994 | . 4994 | . 4994 | . 4994 | . 4995 | . 4995 | . 4995 |
| 3.3 | . 4995 | . 4995 | . 4995 | . 4996 | . 4996 | . 4996 | 4996 | . 4996 | . 4996 | . 4997 |
| 3.4 | . 4997 | . 4997 | . 4997 | . 4997 | . 4997 | . 4997 | . 4997 | . 4997 | . 4997 | . 4998 |
| 3.5 | . 4998 | . 4998 | . 4998 | . 4998 | . 4998 | . 4998 | . 4998 | . 4998 | 4998 | 4998 |

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Chi-Square Distribution Table


The shaded area is equal to $\alpha$ for $\chi^{2}=\chi_{\alpha}^{2}$

| $d f$ | $\chi_{.995}^{2}$ | $\chi^{2} 990$ | $\chi^{2}{ }_{975}$ | $\chi^{2}{ }^{2} 950$ | $\chi^{2}{ }^{2} 900$ | $\chi^{2}{ }_{100}$ | $\chi^{2} 050$ | $\chi^{2} .025$ | $\chi .010$ | $\chi^{2}{ }^{2} 05$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.000 | 0.000 | 0.001 | 0.004 | 0.016 | 2.706 | 3.841 | 5.024 | 6.635 | 7.879 |
| 2 | 0.010 | 0.020 | 0.051 | 0.103 | 0.211 | 4.605 | 5.991 | 7.378 | 9.210 | 10.597 |
| 3 | 0.072 | 0.115 | 0.216 | 0.352 | 0.584 | 6.251 | 7.815 | 9.348 | 11.345 | 12.838 |
| 4 | 0.207 | 0.297 | 0.484 | 0.711 | 1.064 | 7.779 | 9.488 | 11.143 | 13.277 | 14.860 |
| 5 | 0.412 | 0.554 | 0.831 | 1.145 | 1.610 | 9.236 | 11.070 | 12.833 | 15.086 | 16.750 |
| 6 | 0.676 | 0.872 | 1.237 | 1.635 | 2.204. | 10.645 | 12.592 | 14.449 | 16.812 | 18.548 |
| 7 | 0.989 | 1.239 | 1.690 | 2.167 | 2.833 | 12.017 | 14.067 | 16.013 | 18.475 | 20.278 |
| 8 | 1.344 | 1.646 | 2.180 | 2.733 | 3.490 | 13.362 | 15.507 | 17.535 | 20.090 | 21.955 |
| 9 | 1.735 | 2.088 | 2.700 | 3.325 | 4.168 | 14.684 | 16.919 | 19.023 | 21.666 | 23.589 |
| 10 | 2.156 | 2.558 | 3.247 | 3.940 | $4.865{ }^{\text {- }}$ | 15.987 | 18.307 | 20.483 | 23.209 | 25.188 |
| 11 | 2.603 | 3.053 | 3.816 | 4.575 | 5.578 | 17.275 | 19.675 | 21.920 | 24.725 | 26.757 |
| 12 | 3.074 | 3.571 | 4.404 | 5.226 | 6.304 | 18.549 | 21.026 | 23.337 | 26.217 | 28.300 |
| 13 | 3.565 | 4.107 | 5.009 | 5.892 | 7.042 | 19.812 | 22.362 | 24.736 | 27.688 | 29.819 |
| 14 | 4.075 | 4.660 | 5.629 | 6.571 | 7.790 | 21.064 | 23.685 | 26.119 | 29.141 | 31.319 |
| 15 | 4.601 | 5.229 | 6.262 | 7.261 | 8.547 | 22.307 | 24.996 | 27.488 | 30.578 | 32.801 |
| 16 | 5.142 | 5.812 | 6.908 | 7.962 | 9.312 | 23.542 | 26.296 | 28.845 | 32.000 | 34.267 |
| 17 | 5.697 | 6.408 | 7.564 | 8.672 | 10.085 | 24.769 | 27.587 | 30.191 | 33.409 | 35.718 |
| 18 | 6.265 | 7.015 | 8.231 | 9.390 | 10.865 | 25.989 | 28.869 | 31.526 | 34.805 | 37.156 |
| 19 | 6.844 | 7.633 | 8.907 | 10.117 | 11.651 | 27.204 | 30.144 | 32.852 | 36.191 | 38.582 |
| 20 | 7.434 | 8.260 | 9.591 | 10.851 | 12.443 | 28.412 | 31.410 | 34.170 | 37.566 | 39.997 |
| 21 | 8.034 | $8: 897$ | 10.283 | 11.591 | 13.240 | 29.615 | 32.671 | 35.479 | 38.932 | 41.401 |
| 22 | 8.643 | 9.542 | 10.982 | 12.338 | 14.041 | 30.813 | 33.924 | 36.781 | 40.289 | 42.796 |
| 23 | 9.260 | 10.196 | 11.689 | 13.091 | 14.848 | 32.007 | 35.172 | 38.076 | 41.638 | 44.181 |
| 24 | 9.886 | 10.856 | 12.401 | 13.848 | 15.659 | 33.196 | 36.415 | 39.364 | 42.980 | 45.559 |
| 25 | 10.520 | 11.524 | 13.120 | 14.611 | 16.473 | 34.382 | 37.652 | 40.646 | 44.314 | 46.928 |
| 26 | 11.160 | 12.198 | 13.844 | 15.379 | 17.292 | 35.563 | 38.885 | 41.923 | 45.642 | 48.290 |
| 27 | 11.808 | 12.879 | 14.573 | 16.151 | 18.114 | 36.741 | 40.113 | 43.195 | 46.963 | 49.645 |
| 28 | 12.461 | 13.565 | 15.308 | 16.928 | 18.939 | 37.916 | 41.337 | 44.461 | 48.278 | 50.993 |
| 29 | 13.121 | 14.256 | 16.047 | 17.708 | 19.768 | 39.087 | 42.557 | 45.722 | 49.588 | 52.336 |
| 30 | 13.787 | 14.953 | 16.791 | 18.493 | 20.599 | 40.256 | 43.773 | 46.979 | 50.892 | 53.672 |
| 40 | 20.707 | 22.164 | 24.433 | 26.509 | 29.051 | 51.805 | 55.758 | 59.342 | 63.691 | 66.766 |
| 50 | 27.991 | 29.707 | 32.357 | 34.764 | 37.689 | 63.167 | 67.505 | 71.420 | 76.154 | 79.490 |
| 60 | 35.534 | 37.485 | 40.482 | 43.188 | 46.459 | 74.397 | 79.082 | 83.298 | 88.379 100.425 | ${ }^{91.952}$ |
| 70 | 43.275 | 45.442 | 48.758 | 51.739 | 55.329 | 85.527 | 90.531 | 95.023 | 100.425 | 104.215 |
| 80 | 51.172 | 53.540 | 57.153 | 60.391 | 64.278 | 96.578 | 101.879 | 106.629 | 112.329 | 16.321 |
| 90 | 59.196 | 61.754 | 65.647 | 69.126 | 73.291 | 107.565 | 113.145 | 118.136 | 124.116 | 128.299 |
| 100 | 67.328 | 70.065 | 74.222 | 77.929 | 82.358 | 118.498 | 124.342 | 129.561 | 135.807 | 140.169 |

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Table B. Factors used in 3 $\sigma$ Quality Control Charts.

| Sample size $n$ | $\frac{\bar{X} \text { charts }}{\text { Factors for control }} \begin{aligned} & \text { limits } \end{aligned}$ |  |  | $S$ charts |  |  |  |  | $R$ charts |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\left.\begin{array}{c}\text { Factors } \\ \text { for central } \\ \text { line }\end{array}\right]$ | Factors for control limits |  |  |  | Factors <br> for central <br> line <br> $\mathrm{d}_{2}$ <br> 1 | Factors for control limits |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  | B | B5 | $\mathrm{B}_{6}$. |  | $\mathrm{d}_{3}$ | $\mathrm{D}_{1}$ | $\mathrm{D}_{2}$ | $\mathrm{D}_{3}$ | $\mathrm{D}_{4}$ |
|  | A | $\mathrm{A}_{2}$ | $\mathrm{A}_{3}$ |  |  | B ${ }^{\text {a }}$ | 0 | 2.606 | 1.128 | 0.853 | 0 | 3.686 | 0 | 3.267 |
| 2 | 2.121 | 1.880 | 2.659 | 0.7979 | 0 |  | 0 | 2.276 | 1.693 | 0.888 | 0 | 4.358 | 0 | 2.574 |
| 3 | 1.732 | 1.023 | 1.954 | 0.8862 | 0 | 2.266 | 0 | $\frac{2.276}{2.088}$ | 2.059 | 0.880 | 0 | 4.698 | 0 | 2.282 |
| 4 | 1.500 | 0.729 | 1.628 | 0.9213 | 0 | 2.266 | 0 | 1.964 | 2.326 | 0.864 | 0 | 4.918 | 0 | 2.114 |
| 5 | 1.342 | 0.577 | 1.427 | 0.9400 | 0 |  |  | 1.874 | 2.534 | 0.848 | 0 | 5.078 | 0 | 2.004 |
| 6 | 1.225 | 0.483 | 1.287 | 0.9515 | 0.030 |  |  | 1.806 | 2.704 | 0.833 | 0.204 | 5.204 | 0.076 | 1.924 |
| 7 | 1.134 | 0.419 | 1.182 | 0.9594 | 0.118 | 1.882 |  | 1.751 | 2.847 | 0.820 | 0.388 | 5.306 | 0.136 | 1.864 |
| 8 | 1.061 | 0.373 | 1.099 | 0.9650 | 0.185 |  |  | 1.707 | 2.970 | 0.808 | 0.547 | 5.393 | 0.184 | 1.816 |
| 9 | 1.000 | 0.337 | 1.032 | 0.9693 | 0.239 |  |  | 1.669 | 3.078 | 0.797 | 0.687 | 5.469 | 0.223 | 1.777 |
| 10 | 0.949 | 0.308 | 0.975 | 0.9727 | 0.284 | 1.71 |  | . 637 | 3.173 | 0.787 | 0.811 | 5.535 | 0.256 | 1.744 |
| 11 | 0.905 | 0.285 | 0.927 | 0.9754 | 0.321 |  |  | 1.610 | 3.258 | 0.778 | 0.922 | 5.594 | 0.283 | 1.717 |
| 12 | 0.866 | 0.266 | 0.886 | 0.9776 | 0.354 | 1.646 |  | 1.585 | 3.336 | 0.770 | 1.025 | 5.647 | 0.307 | 1.693 |
| 13 | 0.832 | 0.249 | 0.850 | 0.9794 | 0.382 |  |  | 1.563 | 3.407 | 0.763 | 1.118 | 5.696 | 0.328 | 1.672 |
| 14 | 0.802 | 0.235 | 0.817 | 0.9810 | 0.406 |  |  | 1.544 | 3.472 | 0.756 | 1.203 | 5.741 | 0.347 | 1.653 |
| 15 | 0.775 | 0.223 | 0.789 | 0.9823 | 0.428 | 1.572 | 0.440 | 1.526 | 3.532 | 0.750 | 1.282 | 5.782 | 0.363 | 1.637 |
| 16 | 0.750 | 0.212 | 0.763 | 0.9835 | 0.448 | 1.552 | 0.440 | 1.511 | 3.588 | 0.744 | 1.356 | 5.820 | 0.378 | 1.622 |
| 17 | 0.728 | 0.203 | 0.739 | 0.9845 | 0.466 | 1.534 | 0.475 | 1.496 | 3.640 | 0.739 | 1.424 | 5.856 | 0.391 | 1.608 |
| 18 | 0.707 | 0.194 | 0.718 | 0.9854 | 0.482 | 1.5 | 0.475 | 1.483 | 3.689 | 0.734 | 1.487 | 5.891 | 0.403 | 1.597 |
| 19 | 0.688 | 0.187 | 0.698 | 0.9862 | 0.497 | 1.503 | 0.490 | 1.470 | 3.735 | 0.729 | 1.549 | 5.921 | 0.415 | 1.585 |
| 20 | 0.671 | 0.180 | 0.680 | 0.9869 | 0.510 | 11.490 | 0.504 | . 470 | 3.778 | 0.724 | 1.605 | 5.951 | 0.425 | 1.575 |
| 21 | 0.655 | 0.173 | 0.663 | 0.9876 | 0.523 | 1.4 | 0.51 | 1.45 | 3.819 | 0.720 | 1.659 | 5.979 | 0.434 | 1.566 |
| 22 | 0.640 | 0.167 | 0.647 | 0.9882 | 0.534 |  | 0.528 | 1.438 | - 3.858 | 0.716 | 1.710 | 6.006 | 0.443 | 1.55 |
| 23 | 0.626 | 0.162 | 0.633 | 0.9887 | 0.545 | 年1.455 | 0.539 | 1.429 | - 3.895 | 0.712 | 1.759 | 6.031 | 0.451 | 1.548 |
| 24 | 0.612 | 0.157 | 0.619 | 0.9892 | 0.555 | 1.44 | 0.549 | 1.420 | - 3.931 | 0.708 | 1.806 | \|6.056 | 0.459 | 1.54 |
| 25 | 0.600 | - 0.153 | 0.606 | 0.9896 | 0.565 | 1.4 | 0.55 |  |  |  |  |  |  |  |

# BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA 

L-3/T-2 B. Sc. Engineering Examinations 2009-2010
Sub : ME 343 (Machine Design-II)

# Full Marks: 210 <br> Time : 3 Hours <br> The figures in the margin indicate full marks. <br> USE-SEPARATE SCRIPTS FOR EACH SECTION 

## SECTION - A

There are FOUR questions in this Section. Answer any THREE.
The students may use "Máchine Design Handbook-II". Assume reasonable value for missing data if there is any. The Symbols have their usual meanings.

1. A $50 \mathrm{~mm} \times 50 \mathrm{~mm}$ ring-oiled full sleeve bearing is lubricated with SAE 40 oil at an inlet temperature of $38^{\circ} \mathrm{C}$ and supports a radial load of 5 kN . The bearing has a journal speed of $1500 \mathrm{rev} / \mathrm{min}$ and a radial clearance of $50 \mu \mathrm{~m}$. The bearing is medium construction $(\mathrm{A}=20 \mathrm{dl})$ and operating in still air. Determine
(a) oil average temperature
(b) coefficient of friction
(c) magnitude of minimum oil film thickness
(d) total flow and side flow
(e) maximum oil film pressure
(f) frictional loss in bearing
(g) heat dissipation to the surroundings.
2. The worm in a worm gear set is coupled to an electric motor, which rotates at 1500 rpm and delivers 15 kW of power. Decide upon the module, face width, pitch circle diameter of the gear assuming normal pressure angle, $\phi_{n}=20^{\circ}$, velocity ratio, $\mathrm{m}_{\mathrm{w}}=25$, number of starts, $\mathrm{N}_{\mathrm{w}}=4$. Choose high test C.I for the worm and bronze for the gear. Consider the limiting endurance strength of bronze as 168 MPa .
3. A skip for a mine shaft weights 1 ton and is to lift a maximum load of 1.5 ton from a depth of 250 m . The maximum speed of $7.5 \mathrm{~m} / \mathrm{s}$ is to be attained in 6 s .
(a) What size of $6 \times 37$ IWRC, IPS rope and sheave should be used based on the design on static condition considering factor of safety of 7.0.
(b) Determine the factor of safety of the rope size in (a) on the basis of fatigue for indefinite life.
(c) Find also the size of the rope based on the design of fatigue condition for a definite life of 0.2 million cycle considering safety factor of 1.3.

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4. (a) A ground finished shaft with a sled runner keyway is subjected to a completely reversed bending moment of 3500 N.m. The shaft transmits 60 kW at 250 rpm . The material is AISI 4130 , WQT $540^{\circ} \mathrm{C}$. Consider fatigue strength reduction factor of 1.6 for the keyway and a reliability factor of 0.868 for $95 \%$ reliability. Choose safety factor of 1.3 based on DE-elliptical model. Determine the shaft diameter.
(b) A helical gear has 40 teeth and a pitch diameter of 260 mm . The gear has normal module of 6 and the pressure angle in the plane of rotation is $21.52^{\circ}$. The force normal to the tooth surface is 4 kN . Determine the power transmitted at 600 rpm and the virtual number of teeth.

## SECTION - B

There are FOUR questions in this Section. Answer any THREE.
5. The $20^{\circ}$ full-depth teeth for a pair of steel gears are to transmit 30 kW with 1000 rpm of the 20 teeth pinion: $\mathrm{mg}=3$, continuous service and indefinite life. The driven machine is an off and on reciprocating compressor. Determine the face width, module and the type of steel material with its heat treatment.
6. A coiled compression spring is to fit inside a cylinder 20 mm in diameter. For one position of the piston, the spring is to exert a pressure on the piston equivalent of 35 kPa of piston area and in this position the overall length of the spring must not exceed 60 mm . A pressure of 300 kPa on the piston is to compress the spring 20 mm from the position described above. Design a spring for medium service. Specify suitable material, number of total and active coils for squard and ground ends.
7. (a) A 2 m long cylindrical pressure vessel with inner diameter of 0.9 m is subjected to an internal gauge pressure of 1 MPa . The vessel operates at room temperature and curing residual stresses are neglected. The cylinder is made of $45^{\circ}$ graphite/epoxy lamine. Determine the thickness of the vessel and number of laminae using the information as follows:
(i) thickness of each lamine is 0.13 mm
(ii) fibre volume fraction of lamina is $70 \%$
(iii) factor of safety is 1.95
(iv) use Tsai- Hill failure criteria.
(b) A shaft rotating at 500 rpm have radial load of 1.5 kN is to be filled with ball bearing. The design life of the bearing is 20 hr with $0.5 \%$ probability of failure. Choose a bearing.
8. A 24 hr service centrifugal pump running at 350 rpm consumes 75 kW , is to be driven by a compensator started motor of 90 kW with 1400 rpm . The center distance between the pulleys is 1.0 m to 1.2 m . Determine the details of a multiple V-belt drive for this installation.

# BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA 

L-3/T-2 $\quad$ B. Sc. Engineering Examinations 2009-2010
Sub : ME 303 (Convection, Boiling, Condensation and Mass Transfer)
Full Marks: 210
Time: 3 Hours
The figures in the margin indicate full marks.

## USE SEPARATE SCRIPTS FOR EACH SECTION

## SECTION - A

There are FOUR questions in this Section. Answer any THREE.
Assume any missing data with reasonable accuracy.

1. (a) Name the factors that one should consider during design of a modern heat exchanger and discuss.
(b) A heat exchanger is to be designed to cool an ethyl alcohol solution from $75^{\circ} \mathrm{C}$ to 45
${ }^{\circ} \mathrm{C}$ with cooling water entering the tube at $15^{\circ} \mathrm{C}$. The overall heat transfer coefficient based on the outer tube surface area $u_{0}=500 \mathrm{~W} / \mathrm{m}^{2}{ }^{\circ} \mathrm{C}$. Making necessary assumptions calculate the heat transfer surface area for each of the following flow arrangements:
(i) parallel flow, shell and tube
(ii) counterflow, shell and tube
(iii) one shell pass two tube pass
(iv) cross-flow, both fluids unmixed

Assume the following information:
mass flow rate of ethyl alcohol: $8.7 \mathrm{~kg} / \mathrm{sec}$
specific heat of ethyl alcohol: $\quad 3840 \mathrm{~J} / \mathrm{kg}{ }^{\circ} \mathrm{C}$
mass flow rate of cooling water: $9.6 \mathrm{~kg} / \mathrm{sec}$
specific heat of water: $\quad 4180 \mathrm{~J} / \mathrm{kg}{ }^{\circ} \mathrm{C}$.
(c) Define effectiveness of heat exchanger. Discuss the application of $\varepsilon$-NTU method for heat exchanger analysis.
2. (a) Distinguish between film-wise and drop-wise condensation. In which case you will expect more heat-flux and why?
(b) Calculate the average heat transfer coefficient for film-wise condensation of Pure steam at atmospheric pressure for
(i) a vertical surface of 1.5 meter in length.
(ii) the outside-surface of a vertical tube of 1.5 cm OD and 1.5 meter in length.
(iii) the outside surface of a horizontal tube 1.5 cm OD and 1.5 meter in length.
(iv) Discuss your findings that you have obtained.

In all cases, assume that the surface temperatures are constant at $30^{\circ} \mathrm{C}$ below the saturation temperature. The following properties of the condensate may be assumed:

$$
\begin{array}{ll}
k_{e}=0.64 \mathrm{w} / \mathrm{m}^{\circ} \mathrm{C} & \rho_{e}=995 \mathrm{~kg} / \mathrm{m}^{3} \quad h_{f g}=2400 \mathrm{~kJ} / \mathrm{kg} \\
\rho_{v} \approx 0 & \mu_{\mathrm{e}}=0.562 \times 10^{-3} \mathrm{~kg} / \mathrm{m}-\mathrm{sec}
\end{array}
$$

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3. (a) Give a neat sketch of a typical Pool boiling curve for a tube surface in a Pool of water at atmospheric pressure. Describe the influence of different factors affecting the nucleate boiling heat transfer.
(b) Make differences between nucleate and film boiling. Why does radiation heat transfer play a significant role in film boiling heat transfer?
(c) How is heat transfer coefficient in forced-convection boiling calculated? Describe.
4. (a) Define mass transfer coefficient. 'In equimolar counter diffusion of two gases the partial pressure gradients must be equal in magnitude but opposite in direction.' Explain.
(b) Dry air at atmospheric pressure blows across a thermometer which is enclosed in a dampened cover. The thermometer reads a temperature of $t_{w}$. Using the relation between heat and mass transfer derive an expression for determination of the temperature of the dry air.
(c) Write short notes on any three of the followings:
(i) Boundary layer film thickness in condensation (ii) Shell and tube heat exchanger condensation (iii) Critical heat flux (iv) Boiling heat transfer at low gravity (v) Fouling of heat exchanger (vi) Isothermal evaporation of water from a surface.

## SECTION - B

There are FOUR questions in this Section. Answer any THREE.
Symbols have their usual meaning. Assume reasonable values for missing data, if any.
5. (a) What do you mean by the hydrodynamic and the thermal boundary layer over a flat plate? Show different regions in those boundary layers with their velocity and temperature profiles.
(b) Using dimensional analysis, show that for forced convection heat transfer over a flat plate, $N u=f(\mathrm{Re}, \mathrm{Pr})$.
(c) A flat plate 1 m wide and 1.5 m long, is maintained at $90^{\circ} \mathrm{C}$ in air with free stream temperature of $10^{\circ} \mathrm{C}$ flowing along 1.5 m side of the plate. Determine the velocity of the air required to have a rate of heat dissipation of 3.75 kW . Following correlations may be used:

$$
\begin{align*}
& N u_{L}=0.664 \operatorname{Re}^{1 / 2} \operatorname{Pr}^{1 / 3} \ldots . . . . . . . . . . . . . . . . . . . . . . . ~ f o r ~ l a m i n a r ~ f l o w ~  \tag{18}\\
& N u_{L}=\left[0.036 \operatorname{Re}^{0.8}-836\right] \operatorname{Pr}^{1 / 3} \ldots . . . . . . . . . . . . \text { for turbulent flow. }
\end{align*}
$$

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## ME 303

6. (a) Define developing flow and fully developed flow inside a circular pipe. What is entry zone?
(b) For a forced convection case inside a tube prove that $s t=\frac{f}{8}$.
(c) Wate flows with a mean velocity of $2 \mathrm{~m} / \mathrm{s}$ inside a circular pipe of inside diameter of 50 mm . The pipe wall is maintained at a uniform temperature of $100^{\circ} \mathrm{C}$. At a location where the flow is hydrodynamically and thermally developed, the bulk mean temperature is $60^{\circ} \mathrm{C}$. Calculate the heat transfer coefficient by using:

Gnielinsky Correlation:

$$
N u_{D}=\frac{(f / 2)\left(\operatorname{Re}_{D}-1000\right) \operatorname{Pr}}{1+12.7(f / 2)^{1 / 2}\left(\operatorname{Pr}^{2 / 3}-1\right)}
$$

Assume, the friction factor, $f=0.0205$. Take properties at bulk mean temperature.
7. (a) Draw the temperature and the velocity distribution in the vicinity of a heated flat plate placed vertically in still air.
(b) Define Grashof number. Explain its physical significance.
(c) A vertical plate of height 5 m and width 1.5 m has one of its surfaces insulated. The other surface is maintained at a uniform temperature of 400 K . This surface is exposed to quiescent atmospheric air at 300 K . Calculate the total rate of heat loss from the plate.

For natural convection over a vertical flat surface:

$$
\begin{array}{ll}
\overline{N u_{L}}=0.68+\frac{0.670 R a_{L}^{1 / 4}}{\left[1+(0.492 / \operatorname{Pr})^{3 / 16}\right]^{1 / 9}} ; & \text { for } R a_{L} \leq 10^{9} \\
\overline{N u_{L}}=\left\{0.825+\frac{0.387 R a_{L}^{1 / 6}}{\left[1+(0.492 / \operatorname{Pr})^{3 / 16}\right]^{3 / 27}}\right\} ; & \text { for } 10^{9}<R a_{L}<10^{12}
\end{array}
$$

8. (a) Explain the physical significance of the Reynolds number and the Rayleigh number in relation to the forced and free convection heat transfer.
(b) Derive the two-dimensional, steady state energy equation in Cartesian coordinate system. Under what condition does energy equation reduce to a simple conduction equation?
(c) Explain the physical significance of Nusselt number and Prandtl number in relation to heat transfer.



Figure 8.12 Correction factor to counterflow LMTD for heat exchanger with one shell pass and two, or a multiple of two, tube passes. (Courtesy of the Tubular Exchange Manufacturers Association.)


Figure 8.15 Correction factor to counterflow LMTD for a cross-flow heat exchanger with both fluids unmixed and one tube pass. [Extracted from R. A. Bowman, A. C. Mueller, and W. M. Nagel (7); with permission of the publishers, the American Society of Mechanical Engineers.)

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Figure 8.13 Correction factor to counterflow LMTD for heat exchanger with two shell passes and a multiple of two tube passes. (Courtesy of the Tubular Exchange Manufacturers Association.)


Figure 8.14 Correction factor to counterflow LMTD for cross-flow heat exchangers with the fluid on the shell side mixed, the other fluid unmixed, and one tube pass. [Extracted from R. A. Bowman, A. C. Mueller, and W. M. Nagel (7), with permission of the publishers, the American Society of Mechanical Engineers.]

## 410 <br> Condensation and boiling heat transfer

The heat-transfer coefficient is now written
or

$$
h d x\left(T_{w}-T_{g}\right)=-k d x \frac{T_{g}-T_{w}}{\delta}
$$

$$
h=\frac{k}{\delta}
$$

so that

$$
\begin{equation*}
h_{x}=\left[\frac{\rho\left(\rho-\rho_{v}\right) g h_{f f} k^{3}}{4 \mu x\left(T_{y}-T_{w}\right)}\right]^{1 / 4} \tag{9-7}
\end{equation*}
$$

Expressed in dimensionless form in terms of the Nusselt number, this is

$$
\begin{equation*}
\mathrm{Nu}_{x}=\frac{h x}{k}=\left[\frac{\rho\left(\rho-\rho_{\nu}\right) g h_{f_{0}} x^{3}}{4 \mu k\left(T_{g}-T_{w}\right)}\right]^{1 / 4} \tag{9-8}
\end{equation*}
$$

The average value of the heat-transfer coefficient is obtained by integrating over the length of the plate:
or

$$
\begin{align*}
& \bar{h}=\frac{1}{L} \int_{0}^{L} h_{x} d x=\frac{1}{3} h_{x=L}  \tag{9-9}\\
& \bar{h}=0.943\left[\frac{\rho\left(\rho-\rho_{c}\right) g h_{f g} k_{f}^{3}}{L u_{f}\left(T_{u}-T_{w}\right)}\right]^{1 / 4} \tag{9-10}
\end{align*}
$$

More refined analyses of film condensation are presented in detail by Rohsenow [37]. The most significant refinements take into account a nonlinear temperature profile in the film and modifications to the energy balance to include additional energy to cool the film below the saturation temperature. Both effects can be handled by replacing $h_{f g}$ with $h_{f o}^{\prime}$, defined by

$$
\begin{equation*}
h_{f g}^{\prime}=h_{f b}+0.68 c\left(T_{s}-T_{w}\right) \tag{9-11}
\end{equation*}
$$

where $c$ is the specific heat of the liquid. Otherwise, properties in Eqs. (9-7) and ( $9-10$ ) should be evaluated at the film temperature

$$
T_{f}=\frac{T_{g}+T_{w}}{2}
$$

With these substitutions Eq. (9-10) may be used for vertical plates and cylinders and fluids with $\operatorname{Pr}>0.5$ and $c T / h_{f g} \leq 1.0$.
For laminar film condensation on horizontal tubes Nusselt obtained the relation

$$
\begin{equation*}
\hbar=0.725\left[\frac{\rho\left(\rho-\rho_{v}\right) g h_{f g} k_{\xi}}{\mu_{f} d\left(T_{u}-T_{w}\right)}\right]^{1 / 4} \tag{9-12}
\end{equation*}
$$

where $d$ is the diameter of the tube. When condensation occurs on a horizontal tube bank with $n$ tubes placed directly over one another in the vertical direction, the heat-transfer coefficient may be calculated by replacing the diameter in Eq. (9-12) with $n d$.
When a plate on which condensation occurs is sufficiently large or there is a sufficient amount of condensate flow, turbulence may appear in the

Table A. 4 Thermophysical Properties of Gases at Atmospheric Pressure ${ }^{a}$

| $T$ (K) | $\underset{\left(\mathbf{k g} / \mathrm{m}^{3}\right)}{\rho}$ | $\stackrel{c_{\boldsymbol{p}}}{(\mathbf{k} \mathbf{J} / \mathbf{g} \cdot \mathbf{K})}$ | $\begin{gathered} \boldsymbol{\mu} \cdot \mathbf{1 0} \\ \left(\mathbf{N} \cdot \mathrm{s} / \mathrm{m}^{\mathbf{2}}\right) \end{gathered}$ | $\begin{aligned} & \nu \cdot 10^{6} \\ & \left(\mathrm{~m}^{2} / \mathrm{s}\right) \end{aligned}$ | $\begin{gathered} k \cdot 10^{3} \\ (\mathrm{~W} / \mathrm{m} \cdot \mathrm{~K}) \end{gathered}$ | $\begin{aligned} & \alpha \cdot 10^{6} \\ & \left(\mathbf{m}^{2} / \mathrm{s}\right) \end{aligned}$ | Pr |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Air |  |  |  |  |  |  |  |
| 100 | 3.5562 | 1.032 | 71.1 | 2.00 | 9.34 | 2.54 | 0.786 |
| 150 | 2.3364 | 1.012 | 103.4 | 4.426 | 13.8 | 5.84 | 0.758 |
| 200 | 1.7458 | 1.007 | 132.5 | 7.590 | 18.1 | 10.3 | 0.737 |
| 250 | 1.3947 | 1.006 | 159.6 | 11.44 | $22: 3$ | 15.9 | 0.720 |
| 300 | 1.1614 . | 1.007 | 184.6 | 15.89 | 26.3 | 22.5 | 0.707 |
| 350 | 0.9950 | 1.009 | 208.2 | 20.92 | 30.0 | 29.9 | 0.700 |
| 400 | 0.8711 | 1.014 | 230.1 | 26.41 | -: 33.8 | 38.3 | 0.690 |
| 450 | 0.7740 | 1.021 | 250.7 | 32.39 | 37.3 | 47.2 | 0.686 |
| 500 | 0.6964 | 1.030 | 270.1 | 38.79 | 40.7 | 56.7 | 0.684 |
| 550 | 0.6329 | 1.040 | 288.4 | 45.57 | 43.9 | 66.7 | 0.683 |
| 600 | 0.5804 | 1.051 | 305.8 | 52.69 | 46.9 | 76.9 | 0.685 |
| 650 | 0.5356 | 1.063 | 322.5 | 60.21 | 49.7 | 87.3 | 0.690 |
| 700 | 0.4975 | 1.075 | 338.8 | 68.10 | 52.4 | 98.0 | 0.695 |
| 750 | 0.4643 | 1.087 | 354.6 | 76.37 | 54.9 | 109 | 0.702 |
| 800 | 0.4354 | 1.099 | 369.8 | 84.93 | 57.3 | 120. | 0.709 |
| 850 | 0.4097 | $1: 110$ | 384.3 | 93.80 | 59.6 | 131 | 0.716 |
| 900 | 0.3868 | 1.121 | 398.1 | 102.9 | 62.0 | 143 | 0.720 |
| 950 | 0.3666 | 1.131 | 411.3 | 112.2 | 64.3 | 155 | 0.723 |
| 1000 | 0.3482 | 1.141 | 424.4 | 121.9 | 66.7 | 168 | 0.726 |
| 1100 | 0.3166 | 1.159 | 449.0 | 141.8 | 71.5 | 195 | 0.728 |
| 1200 | 0.2902 | 1.175 | 473.0 | 162.9 | 76.3 | 224 | 0.728 |
| 1300 | 0.2679 | 1.189 | 496.0 | 185.1 | 82 | 238 | 0.719 |
| 1400 | 0.2488 | 1.207 | 530 | 213 | 91 | 303 | 0.703 |
| 1500 | 0.2322 | 1.230 | 557 | 240 | 100 | 350 | 0.685 |
| 1600 | 0.2177 | 1.248 | 584 | 268 | 106 | 390 | 0.688 |
| 1700 | 0.2049 | 1.267 | 611 | 298 | 113 | 435 | 0.685 |
| 1800 | 0.1935 | 1.286 | 637 | 329 | 120 | 482 | 0.683 |
| 1900 | 0.1833 | 1.307 | 663 | 362 | 128 | 534 | 0.677 |
| 2000 | 0.1741 | 1.337 | 689 | 396 | 137 | 589 | 0.672 |
| 2100 | 0.1658 | 1.372 | 715 | 431 | 147 | 646 | 0.667 |
| 2200 | 0.1582 | 1.417 | 740 | 468 | 160 | 714 | 0.655 |
| 2300 | 0.1513 | 1.478 | 766 | 506 | 175 | 783 | 0.647 |
| 2400 | 0.1448 | 1.558 | 792 | 547 | 196 | 869 | 0.630 |
| 2500 | 0.1389 | 1.665 | 818 | 589 | 222 | 960 | 0.613 |
| 3000 | 0.1135 | 2.726 | 955 | 841 | 486 | 1570 | 0.536 |

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Table A. 6 Thermophysical Properties of Saturated Water ${ }^{\text {a }}$

| Temperature, $T$ (K) | Pressure, <br> $P$ (bars) $^{b}$ | Specific <br> Volume $\left(\mathrm{m}^{3} / \mathrm{kg}\right)$ |  | Heat of Vaporization, $\boldsymbol{h}_{\mathrm{f}}$ ( $\mathrm{kJ} / \mathrm{kg}$ ) | $\begin{gathered} \text { Specific } \\ \text { Heat } \\ (\mathbf{k J} / \mathbf{k g} \cdot \mathbf{K}) \\ \hline \end{gathered}$ |  | Viscosity <br> ( $\mathrm{N} \cdot \mathrm{s} / \mathrm{m}^{2}$ ) |  | $\begin{aligned} & \text { Thermal } \\ & \text { Conductivity } \\ & (\mathbf{W} / \mathbf{m} \cdot K) \end{aligned}$ |  | Prandtl Number |  | Surface <br> Tension, $\begin{gathered} \sigma_{f} \cdot \mathbf{1 0}^{3} \\ (\mathrm{~N} / \mathrm{m}) \end{gathered}$ | Expansion Coefficient, $\beta_{f} \cdot 10^{6}$ ( $\mathrm{K}^{-1}$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\overline{v_{f} \cdot 10^{3}}$ | $v_{g}$ |  | $c_{p, j}$ | $c_{p, g}$ | $\mu_{f} \cdot 10^{6}$ | $\mu_{g} \cdot 10^{6}$ | $k_{f} \cdot 10^{3}$ | $k_{g} \cdot 10^{3}$ | $\boldsymbol{P r}_{\text {f }}$ | Pr ${ }_{8}$ |  |  |
| 273.15 | 0.00611 | 1.000 | 206.3 | 2502 | 4.217 | 1.854 | 1750 | 8.02 | 569 | 18.2 | 12.99 | 0.815 | 75.5 | -68.05 |
| 275 | 0:00697 | 1.000 | 181.7 | 2497 | 4.211 | 1.855 | 1652 | 8.09 | 574 | 18.3 | 12.22 | 0.817 | 75.3 | -32.74 |
| 280 | 0.00990 | 1.000 | 130.4 | 2485 | 4.198 | 1.858 | 1422 | 8.29 | 582 | 18.6 | 10.26 | 0.825 | 74.8 | 46.04 |
| 285 | 0.01387 | 1.000 | 99.4 | 2473 | 4.189 | 1.861 | 1225 | 8.49 | 590 | 18.9 | 8.81 | 0.833 | 74.3 | 114.1 |
| 290 | 0.01917 | 1.001 | 69.7 | 2461 | 4.184 | 1.864 | 1080 | 8.69 | 598 | 19.3 | 7.56 | 0.841 | 73.7 | 174.0 |
|  |  |  |  |  | , |  |  |  |  |  |  |  |  |  |
| 295 | 0.02617 | 1.002 | 51.94 | 2449 | 4.181 | 1.868 | 959 | 8.89 | 606 | 19.5 | 6.62 | 0.849 | 72.7 | 227.5 |
| 300 | 0.03531 | 1.003 | 39.13 | 2438 | 4.179 | 1.872 | 855 | 9.09 | 613 | 19.6 | 5.83 | 0.857 | 71.7 | 276.1 |
| 305 | 0.04712 | 1.005 | 29.74 | 2426 | 4.178 | 1.877 | 769 | 9.29 | 620 | 20.1 | 5.20 | 0.865 | 70.9 | 320.6 |
| 310 | 0.06221 | 1.007 | 22.93 | 2414 | 4.178 | 1.882 | 695 | 9.49 | 628 | 20.4 | 4.62 | 0.873 | 70.0 | 361.9 |
| 315 | 0.08132 | 1.009 | 17.82 | 2402 | 4.179 | 1.888 | 631 | 9.69 | 634 | 20.7 | 4.16 | 0.883 | 69.2 | 400.4 |
| 320 | 0.1053 | 1.011 | 13.98 | 2390 | 4.180 | 1.895 | 577 | 9.89 | 640 | 21.0 | 3.77 | 0:894 | 68.3 | 436.7 |
| 325 | 0.1351 | 1.013 | 11.06 | 2378 | 4.182 | 1.903 | 528 | 10.09 | 645 | 21.3 | 3.42 | 0.901 | 67.5 | 471.2 |
| 330 | 0.1719 | 1.016 | 8.82 | 2366 | 4.184 | 1.911 | 489 | 10.29 | 650 | 21.7 | 3.15 | 0.908 | 66.6 | 504.0 |
| 335 | 0.2167 | 1.018 | 7.09 | 2354 | 4.186 | 1.920 | 453 | 10.49 | 656 | 22.0 | 2.88 | 0.916 | 65.8 | 535.5 |
| 340 | 0.2713 | 1.021 | 5.74 | 2342 | 4.188 | 1.930 | 420 | 10.69 | 660 | 22.3 | 2.66 | 0.925 | 64.9 | 566.0 |
| 345 | 0.3372 | 1.024 | 4.683 | 2329 | 4.191 | 1.941 | 389 | 10.89 | 668 | 22.6 | 2.45 | 0.933 | 64.1 | 595.4 |
| 350 | 0.4163 | 1.027 | 3.846 | 2317 | 4.195 | 1.954 | 365 | 11.09 | 668 | 23.0 | 2.29 | 0.942 | 63.2 | 624.2 |
| 355 | 0.5100 | 1.030 | 3.180 | 2304 | 4.199 | 1.968 | 343 | 11.29 | 671 | 23.3 | 2.14 | 0.951 | 62.3 | 652.3 |
| 360 | 0.6209 | 1.034 | 2.645 | 2291 | 4.203 | 1.983 | 324 | 11.49 | 674 | 23.7 | 2.02 | 0.960 | 61.4 | 697.9 |
| 365 | 0.7514 | 1.038 | 2.212 | 2278 | 4.209 | 1.999 | 306 | 11.69 | 677 | 24.1 | 1.91 | 0.969 | 60.5 | 707.1 |
| 370 | 0.9040 | 1.041 | 1.861 | 2265 | 4.214 | 2.017 | 289 | 11.89 | 679 | 24.5 | 1.80 | 0.978 | 59.5 | 728.7 |
| 373.15 | 1.0133 | 1.044 | 1.679 | 2257 | 4.217 | 2.029 | 279 | 12.02 | 680 | 24.8 | 1.76 | 0.984 | 58.9 | 750.1 |
| 375 | 1.0815 | 1.045 | 1.574 | 2252 | 4.220 | 2.036 | 274 | 12.09 | 681 | 24.9 | 1.70 | 0.987 | 58.6 | 761 |
| 380 | 1.2869 | 1.049 | 1.337 | 2239 | 4.226 | 2.057 | 260 | 12.29 | 683 | 25.4 | 1.61 | 0.999 | 57.6 | 788 |
| 385 | 1.5233 | 1.053 | 1.142 | 2225 | 4.232 | 2.080 | 248 | 12.49 | 685 | 25.8 | 1.53 | 1.004 | 56.6 | 814 |


|  |  |  |  |  |  |  |  | 12.69 | 686 | 26.3 | 1.47 | 1.013 | 55.6 | 841 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 390 | 1.794 | 1.058 | 0.980 | 2212 | 4.239 | 2.104 | 237 | 12.69 | 686 | 26.3 | 1.47 | 1.013 | 5.6 | 84 |
| 400 | 2.455 | 1.067 | 0.731 | 2183 | 4.256 | 2.158 | 217 | 13.05 | 688 | 27.2 | 1.34 | 1.033 | 3.6 | 896 |
| 410 | 3.302 | 1.077 | 0.553 | 2153 | 4.278 | 2.221 | 200 | 13.42 | 688 | 28.2 | 1.24 | 1.054 | 51.5 | 52 |
| 420 | 4.370 | 1.088 | 0.425 | 2123 | 4.302 | 2.291 | 185 | 13.79 | 688 | 29.8 | 1.16 | 1.075 | 49.4 | 1010 |
| 430 | 5.699 | 1.099 | 0.331 | 2091 | 4.331 | 2.369 | 173. | 14.14 | 685 | 30.4 | 1.09 | 1.10 | 47.2 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 440 | 7.333 | 1.110 | . 0.261 | 2059 | 4.36 | 2.46 | 162 | 14.50 | 682 | 31.7 | . 1.04 | 1.12 | 45.1 |  |
| 450 | 9.319 | 1.123 | 0.208 | 2024 | 4.40 | 2.56 | 152 | 14.85 | 678 | 33.1 | 0.99 | 1.14 | 42.9 |  |
| 460 | 11.71 | 1.137 | 0.167 | 1989 | 4.44 | 2.68 | 143 | 15.19 | 673 | 34.6 | 0.95 | 1.17 | 40.7 |  |
| 470 | 14.55 | 1.152 | 0.136 | 1951 | 4.48 | 2.79 | 136 | 15.54 | 667 | 36.3 | 0.92 | 1.20 | 38.5 |  |
| 480 | 17.90 | 1.167 | 0.111 | 1912 | 4.53 | 2.94 | 129 | 15.88 | 660 | 38.1 | 0.89 | 1.23 | 36.2 |  |
| 490 | 21.83 | 1.184 | 0.0922 | 1870 | 4.59 | 3.10 | 124 | 16.23 | 651 | 40.1 | 0.87 | 1.25 | 33.9 | - |
| 500 | 26.40 | 1.203 | 0.0766 | 1825 | 4.66 | 3.27 | 118 | 16.59 | 642 | 42.3 | 0.86 | 1.28 | 31.6 | - |
| 510 | 31.66 | 1.222 | 0.0631 | 1779 | 4.74 | 3.47 | 113 | 16.95 | 631 | 44.7 | 0.85 | 1.31 | 29.3 | - |
| 520 | . 37.70 | 1.244 | 0.0525 | 1730 | 4.84 | 3.70 | 108 | 17.33 | 621 | 47.5 | 0.84 | 1.35 | 26.9 | - |
| 530 | 44.58 | 1.268 | 0.0445 | 1679 | 4.95 | 3.96 | 104 | 17.72 | 608 | 50.6 | 0.85 | 1.39 | 24.5 | - |
| 540 | 52.38 | 1.294 | 0.0375 | 1622 | 5.08 | 4.27 | 101 | 18.1 | 594 | 54.0 | 0.86 | 1.43 | 22.1 | - |
| 550 | 61.19 | 1.323 | 0.0317 | 1564 | 5.24 | 4.64 | 97 | 18.6 | 580 | 58.3 | 0.87 | 1.47 | 19.7 | - |
| 560 | 71.08 | 1.355 | 0.0269 | 1499 | 5.43 | 5.09 | 94 | 19.1 | 563 | 63.7 | 0.90 | 1.52 | 17.3 | - |
| 570 | 82.16 | 1.392 | 0.0228 | 1429 | 5.68 | 5.67 | 91 | 19.7 | 548 | 76.7 | 0.94 | 1.59 | 15.0 | - |
| 580 | 94.51 | 1.433 | 0.0193 | 1353 | 6.00 | 6.40 | 88 | 20.4 | 528 | 76.7 | 0.99 | 1.68 | 12.8 | - |
| 590 | 108.3 | 1.482 | 0.0163 | 1274 | 6.41 | 7.35 | 84 | 21.5 | 513 | 84.1 | 1.05 | 1.84 | 10.5 | - |
| 600. | 123.5 | 1.541 | 0.0137 | 1176 | 7.00 | 8.75 | 81 | 22.7 | 497 | 92.9 | 1.14 | 2.15 | 8.4 | - |
| 610 | 137.3 | 1.612 | 0.0115 | 1068 | 7.85 | 11.1 | 77 | 24.1 | 467 | 103 | 1.30 | 2.60 | 6.3 | - |
| 620 | 159.1 | 1.705 | 0.0094 | 941 | 9.35 | 15.4 | 72 | 25.9 | 444 | 114 | 1.52 | 3.46 | 4.5 | - |
| 625 | 169.1 | 1.778 | 0.0085 | 858 | 10.6 | 18.3 | 70 | 27.0 | 430 | 121 | 1.65 | 4.20 | 3.5 | - |
| 630 | 179.7 | 1.856 | 0.0075 | 781 | 12.6 | 22.1 | 67 | 28.0 | 412 | 130 | 2.0 | 4.8 | 2.6 | - |
| 630 635 | 190.9 | 1.935 | 0.0066 | 683 | 16.4 | 27.6 | 64 | 30.0 | 392 | 141 | 2.7 | 6.0 | 1.5 | - |
| 640 | $202.7{ }^{\text {\% }}$ | 2.075 | 0.0057 | 560 | 26 | 42 | 59 | 32.0 | 367 | 155 | 4.2 | 9.6 | 0.8 | - |
| 645 | 215.2 | 2.351 | 0.0045 | 361 | 90 | - | 54 | 37.0 | 331 | 178 | 12 | $26^{\circ}$ | 0.1 | - |
| $647.3^{\text {c }}$ | 221.2 | 3.170 | 0.0032 | 0 | $\infty$ | $\infty$ | 45 | 45.0 | 238 | 238 | $\infty$ | $\infty$ | 0.0 | - |

[^0]${ }^{\text {c Critical temperature }}$

Date : 18/07/2011
BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA
L-3/T-2 B. Sc. Engineering Examinations 2009-2010
Sub: ME 323 (Fluid Mechanics II)
Full Marks : 210
Time : 3 Hours
USE SEPARATE SCRIPTS FOR EACH SECTION

## SECTION - A

There are FOUR questions in this Section. Answer any THREE.
The questions are of equal value.
Assume reasonable data if necessary.

1. (a) Write the advantages and disadvantages of dimensional analysis. Explain Buckingham $\pi$-theorem.
(b) The discharge over a prototype open channel is $200 \mathrm{~m}^{3} / \mathrm{s}$. Calculate the corresponding discharge over a 1:30 scale ratio model.
2. (a) Discuss the significance of Mach number in the fluid flow. Deduce an equation for the maximum discharge through a converging nozzle.
(b) An aircraft is flying at a speed of $1200 \mathrm{~km} / \mathrm{h}$ through air of temperature $26^{\circ} \mathrm{C}$ and at a pressure of 101.3 kPa absolute. Calculate the rise in temperature at the nose of the aircraft. Take $R=287 \mathrm{~J} / \mathrm{kg} \mathrm{K}$ and $\mathrm{k}=1.4$.
3. (a) Find the area-velocity relationship for compressible and incompressible flows. Explain the effects of variation of cross-sectional area on subsonic, sonic and supersonic flows.
(b) In the down stream of a normal shock wave in air the pressure, temperature and velocity are 252 kPa absolute, $102^{\circ} \mathrm{C}$ and $182 \mathrm{~m} / \mathrm{s}$. respectively. Find the pressure, temperature and density in the upstream of the shock wave. Take $\mathrm{k}=1.4$ and $R=287 \mathrm{~J} / \mathrm{kg} \mathrm{K}$
4. (a) Explain boundary layer with diagram. Find the equations of momentum thickness and energy thickness.
(b) Describe the different types of similarities which may exist between a model and a prototype.

## ME 323

## SECTION - B

There are FOUR questions in this Section. Answer any THREE. The figures in the margin indicate full marks.
Assume reasonable data if necessary. Moody diagram is supplied.
5. (a) For laminar flow in pipe, prove that the friction factor, $f=\frac{64}{\mathrm{Re}}$, where Re is the Reynolds number.
(b) A certain fluid of specific gravity 1.5 and dynamic viscosity $0.8 \mathrm{~N}-\mathrm{s} / \mathrm{m}^{2}$ is flowing through a pipe of diameter 110 mm . If the wall shear stress is $210 \mathrm{~N} / \mathrm{m}^{2}$, find the discharge and velocity at a radius of 40 mm from the pipe surface.
6. (a) What is minor losses and why is it so called? Derive an equation for the loss of head due to friction in pipes for turbulent flow.
(b) Petroleum oil is flowing through an inclined galvanized pipe at the rate of $0.25 \mathrm{~m}^{3} / \mathrm{s}$. At point (1) pressure is 2500 kPa and at point (2) pressure is atmospheric as shown in Fig. for Q. No. 6(b). Neglecting minor losses, find the diameter of the pipe. Specific gravity of petroleum oil is 0.75 and its absolute viscosity is $2.9 \times 10^{-4} \mathrm{~N}-\mathrm{s} / \mathrm{m}^{2}$.

7. (a) What is the difference between open channel flow and pipe flow? Prove that for the most economical trapezoidal open channel the angle of sloping side is $60^{\circ}$ and the length of the sloping side is equal to the width of the trapezoidal section at the bottom.
(b) Water is flowing through a circular open channel having a bed slope of 1 in 8500 . the flow rate of water is $0.5 \mathrm{~m}^{3} / \mathrm{s}$ and the depth of water in the channel is 0.85 times the diameter. Calculate the diameter of the channel if the Manning's constant $\mathrm{n}=0.016$.
8. (a) State Chezy's formula for open channel flow. Give the derivation of this formula mentioning the assumption.
(b) What is specific energy in open channel flow? Explain the physical significance of it.
(c) Explain the critical depth in reference to open channel flow.
ME $323 \quad=3=$

Fig Moody diagram

|  |  |
| :--- | :---: |
| Riveted steel | $\epsilon . \mathrm{mm}$ |
| Concrete | $0.9-9$. |
| Wood stave | $0.3-3$. |
| Cast iron | $0.18-0.9$ |
| Galvanized iron | 0.25 |
| Asphalted cast iron | 0.15 |
| Commercial steel or | 0.12 |
| wrought iron | 0.046 |
| Drawn tubing | 0.0015 |

# BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA 

L-3/T-2 $\quad$ B. Sc. Engineering Examinations 2009-2010
Sub : IPE 331 (Production Process)
Full Marks: 280
Time : 3 Hours
The figures in the margin indicate full marks.
USE SEPARATE SCRIPTS FOR EACH SECTION

## SECTION - A

There are FOUR questions in this Section. Answer any THREE.

1. (a) What are some of the materials used in making casting patterns? What features should be considered when selecting a pattern materials.
(b) With the help of diagram discuss the following
i) Die casting and
(ii) Centrifugal casting
(c) What features can be incorporated into the gating system to aid in trapping dross and mold material that is flowing with the molten metal?
(d) What are some of the general defects encountered in casting process? How might defective castings be repaired to permit successful use in their intended application?
2. (a) What is the difference between open die and impression die forging? Why is open-die forging not a practical technique for large scale production of identical products? Explain.
(b) With the help of diagram describe the following cold working of metals.
i) Roll forging
ii) Heading and
iii) Radial forging
(c) With the help of suitable diagram, discuss the terminology of an impression die forging.
(d) What are some of the attractive features of the extrusion process? What is the primary shape limitation of the extrusion process?
3. (a) Explain why and how continuous and discontinuous chips are formed. Discuss why Built-up-Edge (BUE) on a cutting tool is undesirable.
(b) Prove by Master line Method for a single point cutting tool.
i) $\tan \gamma_{y}=\tan \gamma_{0} \operatorname{Cos} \varphi+\tan \lambda \operatorname{Sin} \varphi$.
ii) $\operatorname{Cot} \alpha_{x}=\operatorname{Cot} \alpha_{0} \operatorname{Cos} \varphi+\tan \lambda \operatorname{Sin} \varphi$

Where the notation s indicate their usual meaning.

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## IPE 331

## Contd ... Q. No. 3

(c) The geometry of a cutting tool used for an operation is given by $0^{\circ}, 9^{\circ}, 6^{\circ}, 6^{\circ}, 7^{\circ}, 60^{\circ}$, 1 (mm). Calculate
i) Side rake angle ii) back rake angle and iii) maximum rake angle
4. (a) With the help of Earnest and Merchant theory, Show that $P_{z}=2 \gamma_{s} S_{0}$ t $\operatorname{Cot} \beta$
(b) During a metal cutting test under orthogonal conditions in a lathe with tool of rake angle $20^{\circ}$ and main cutting edge angle $60^{\circ}$, with a depth of cut of 3 mm and feed rate of $0.38 \mathrm{~mm} / \mathrm{rev}$, the following data was recorded.

Average chip thickness $=0.89$
Feed force $=835 \mathrm{~N}$
Main cutting force $=1570 \mathrm{~N}$
Calculate the following
i) Coefficient of friction at the chip tool interface
ii) Shear plane angle and
iii) Shear stress at the shear plane
(c) With the help of diagram, define the following terms in cold working of metals.
i) Dimpling ii) Beading and iii) Ironing
(d) List some operations that can be classified as bending. Use sketches and explain design functions of the products.

## SECTION - B

There are FOUR questions in this Section. Answer any THREE.
5. (a) Briefly describe the application of any three work holding devices used in a lathe machine.
(b) In Fig. 5(b) a component to be machined from a stock of C40 steel, 40 mm in diameter and 75 mm long is shown. Calculate the machining time required for completing the part with carbide tool. The available spindle speeds are $70,110,176,280$, $440,700,1100,1760$ and 2800 . Use a cutting speed of $135 \mathrm{~m} / \mathrm{min}$, feed rate of $0.38 \mathrm{~mm} / \mathrm{rev}$ and maximum depth of cut is 2 mm .


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## IPE 331

## Contd ... Q. No. 5

(c) What is centreless grinding? Describe with necessary sketches.
(d) What is meant by grain size, grade and structure of a grinding wheel?
6. (a) Differentiate helical and plain milling cutter used in horizontal milling machine.
(b) Calculate the indexing requirement for 167 divisions on a milling machine equipped with a differential indexing head. The index plates available are,

Plate $1: 15,16,17,18,19,20$ holes
Plate $2: 21,23,27,29,31,33$ holes
Plate $3: 37,39,41,43,47,49$ holes
The change gear set available is $24,24,28,32,40,44,48,56,64,72,86,100$.
(c) Explain the need for a clapper box in a mechanical shaper. Give the advantages and disadvantages of a hydraulic shaper as compared to a mechanical shaper.
7. (a Write down the sequence of operation required to obtain a hole that is accurate as to size and aligned on center. Briefly describe each operation.
(b) Classify different types of drills used in drill press.
(c) Why inadequate joint penetration and slag inclusions are occurred in welds and how these defects can be removed/controlled?
8. (a) Write down some advantages, disadvantages and practical applications of welding.
(b) With necessary sketches describe briefly the working principle of
(i) Resistance spot welding.
(ii) Thermit welding.
(c) Compare shielded metal are welding with the other are welding processes.


[^0]:    ${ }^{a}$ Adapted from Reference 19.
    ${ }^{b_{1}}$ bar $=10^{5} \mathrm{~N} / \mathrm{m}^{2}$.

