# Meta-Heuristic Approach to Supply Chain Optimization in an Integrated Hierarchical Production Planning System 

A thesis submitted to the Department of Industrial and Production Enginecring in partial fulfillment of the requirements for the degrec of

## DOCTOR OF PHILOSOPHY

by<br>Sultana Parvecn



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This thesis titled "Meta-Heuristic Approach to Supply Chain Optimization in an Integrated Hierarchical Production Planning System', submitted by Sultana Parveen, Roll No.: P04030801F, Session: April 2003, to the Deparment of Industrial and Production Enginecring. Bangladesh University of Engineering and Techoology, Dhaka 1000, Bangladesh, has been accepted as satisfactory in partial fulfillment of the requirements for the degree of Doctor of Philosophy on 07 March 2009.

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## List of Abbreviations

| AHP | Analytic Hierarchy Process |
| :---: | :---: |
| CLSP | Capacitated Lot-Sizing Problem |
| COP | Combinatorial Procedure |
| DISP | Dynamic Lot-Sizing Problem |
| DRP | Distribution Requirement Planning |
| EDD | Earliest Due Date |
| EOQ | Economic Order Quantity |
| FGSP | Flexible Job-Shop Scheduling Problem |
| GA | Genetic Algorithm |
| GPPB | Generalized Par Period Balancing |
| GSA | Genctic Algorithm With Search Area |
| LTC | Least Total Cost |
| LUC | Least Unil Cost |
| MCDM | Multi Criteria Decision Making |
| MOEA | Multi Objective Evolutionary Algorithm |
| MOGA | Multi Objective Genetic Algorithun |
| MOP | Multi Objective Problem |
| MPCS | Material Planning and Control Systeın |
| MPS | Master Production Scheduling |
| MRP | Material Requirements Planning |
| NPGA | Niched Parcto Genetic Algorithm |
| NPGA | Nondeterministic Polynomial |
| NSGA | Non Dominated Sorting Genetic Algorithon |
| POQ | Period Order Quantity |
| PPB | Part Period Balancing |
| ROR | Re-Order Point |
| SPT | Shortest Processing Time |

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## Abstract

The total supply chain of any cnterprise is composed of three main sections: backward linkage, forward linkage and inside value-chain. The backward linkage is a function of inward supply management, with its inherent uncertainty. The intemal value chain is basically a hybrid function of several materials management functions. The two most important of these functions are complex issues of uncertain inventory control and NP-hard type production scheduling problem. The forward side is composed of muli-variable interactive system, where variables interact with each other to control market demand. An internal material planning is one of the most complex tasks in an industry. Presence of a large number of variables, operating in uncerlain environment, is the main reason behind such complexity. As a result, optimization in a materials planning system requires a great deal of simplification. A material planning is thus suggested in several levels, starting from long-range aggregate planning, going through disaggregated Master Production Scheduling, individual component planning and finally ending to shop floor scheduling. Each individual level has its own form of complexity. The first level of complexily starts in converting an aggregate production planning system into disaggregated master production scheduling. The master production scheduling is essentially the output of aggregate planning where master production scheduling process drives the material requirements planning (MRP) system. The determination of net requirements is the core of MRP processing. Lot-sizing is a major aspect of the MRP process. A lot-sizing problem involves decisions to delermine the quantity and timing of production for $N$ different items over a horizon of $T$ periods. In the present work, it has been assumed that only onc machine of each type is available with a fixed capacity in cacl period. The objective is to minimize the sum of set-up and inventory carying costs for all items without incurring backlogs. In case of a single item production only an optimal solution algorithm exists. But for medium-size and multi-item problems, oplimal solution algorithms ate not available. It has been proved that even the iwo-item problem with constant capacity is NP-hand (Nondeterministic polynomial-hard). This has increased the importance of searching for good heuristic solutions. In the present research
work, heuristic methods have been developed and implemented to solve the multi-item, single level, limited capacity lol-sizing problem, bypassing parameters to the next step of planning.

Production scheduling is the most complex step in the hicrarchical production planning system. That is why the production scheduling problems have received ample attention from both rescarchers and practilioners, because an efficient production schedule can achieve reduction of production cost and inventory cost, increase in profit and increase in 'on-lime' delivery to customers. A Pareto-optimal algorithen is developed in this rescarch work for a scheduling problem on a single machine with periodic maintenance and non-preenptive jobs. In literature, most of the scheduling problems address only one objective function; while in the real world, such problems are always associated with more than one objective. In this work, both multi-objective functions and multi-maintenance periods arc considered for a single machine scheduling problem. On the other hand, periodic maintenance schedutes are also considered in the model. The objective of the model addressed in this work is to minimize the weighted function of the total job flow time, the maximum tardiness, and the machine idle time in a single machine environment. The parametric analysis of the trade-offs of all solutions with all possible weighted combination of the criteria has been carried out. A neighborhood search heuristic has been developed adso. The computational results have shown that the modified Parcto-optimal algorithm provides a better solution than the neighborhood search heuristic and this shows the efficiency of the modified Pareto-optimal algorithm.

For forward side optimization, distribution system parameters have been identified that affect subsequent marketing. The parameter of distribution for optimization has been sclected with Multi Criteria Decision Making (MCDM) technique. Finally a distribution plan has been optinized using optimization-based 'Transportation algorithm'.

## Chapter 1 Introduction

### 1.1 Background

The supply chain management is an integrated and coordinated process of planning, implementing and controlling eflicient and cost cffective flow and storage of goods, services and related information from the point of origin to the point of consumplion with the ultimate objective of confoming to customer requirements. It begins with raw materials acquisition, continues through internal value-chain operations and ends with distribution of linished goods.

The total supply chain is composed of three main stages: the backward linkage, internal valuc-chain and the forward linkage. The backward linkage is a function of supply management, cenicred on multiplicity of basically operations research-based 'Transportation problem'. The internal materials management is a typical example of NPhard (NP stands for Non-deteministic Polynomial, i.e. the problem cannot be solved optimally in polynomial time) type inventory control and production scheduling problem. The forward linkage is composed of multi-variable interactive system, where variables interact with each other to control market demand. In lact, the forward side again becomes an input to backward linkage, because the market demand again helps in creating aggregate demand. As such, it forms a loop of inlegrated "Production Planning Systern". However, this loop, as a 'system' has never been studied, although discrete studies on single elements have been reported.

Materials planning is one of the most complex tasks in an industry. Presence of a large number of variables, operating in uncertain environment, is the main reason behind such complexity. As a result, optimization in a materials planning system requires a great deal of simplification. Materials planning is thus suggested in several levels, starting from longrange aggregate plarning, going through disaggregated Master Production Schcduling,
individual component planning and finally ending to shop dloor scheduling. Each individual fevel has its own form of complexity. A large majority of these complex planning issues fall in the calegory of either sub-optimization or in totally infeasible solution spacc. Thus, optimization in a hierarchical materials planning is of high level of attention to the researchers, although results obtained so far is not considerable [1, 2]. The noted complexitics in four individual levels of hierarchical planning system are explained below.

The first level of complexity starts in converting an aggregate production planning system into disaggregated master production scheduling. Linearity of cost functions, non-lincarity of demand functions and other operating variables create this complexity. When resource (manpower, machine hours and inventory) availability and constraints are added to this, complexity increases several folds [3, 4]. As a result, the problem becomes a complex one, having conflicting constraints and thus, difficult to achicve objective. The master production scheduling is essentially the output of aggregate planning where master production scheduling process drives the material requirements planning (MRP) system. The determination of net requirements is the core of MRP processing. Iot-sizing is a significant aspect of the MRP process. Lot-sizes generally meet products requirements for one or more periods. Optimizing routines for lot-sizing problem have been shown to be all demanding from a computing stand point in both practical as well as rescarch environment. The multiitem capacitated lot-sizing problem is found to be NP-hard [4]. The problem is even harder from practical point of view, since optimal sotution methods have failed to solve all but very few problem. It has been found that most methods require extensive computational power. Thus their applicability is rather limited. So a heuristic method has been developed to solve the lol-siding problem, bypassing parameters to the next step of planning.

For the inulti-item capacitated lot-sizing problems, the various heuristics, which have been proposed over the years, are classified into a number of classes. Heuristics belonging to the period-by-period heuristic work from period 1 to period $H$. Consider a period $t$ in the process. One certainly has to produce max $\left\{0, d_{i, k}, l_{i,-1}\right\}$ for all products $;$ in order to avoid stock outs in the current period, where $d_{\mathrm{t}}$ is the demand for item $i$ in period $t$ and $I_{11}$ is the
inventory of item $i$ at the end of period $t$. Infeasibility occurs when the net demand in some period $f$, i.e. $\sum_{i=1}^{*} \max \left\{0, d_{u n}-I_{, t-1}\right\}$ may exceed available capacity. The lot-sizing problem now can be stated as

Minimize $Z(X)=\sum_{i=1}^{N} \sum_{j=1}^{H}\left(S_{i} \delta\left(x_{i t}\right)+h_{1} I_{n}\right)$
subject to $I_{y}=I_{1, y-1}+x_{1 j}-D_{u} \quad i=1,2, \ldots, N^{\prime}$ and $j=1,2, \ldots, H$

$$
\begin{array}{ll}
I_{10}=I_{t H}=0 & i=1,2, \ldots, N^{\prime} \\
\sum_{i=1}^{N_{i}} k_{i} x_{i j} \leq C_{i} & j=1, \ldots, H \\
0 \leq x_{i y} \leq x_{\max x} & i=1,2, \ldots, N^{\prime} \text { and } j=1,2, \ldots, H \\
I_{t j} \geq 0 & i=1,2, \ldots, N^{\prime} \text { and } j=1,2, \ldots, H
\end{array}
$$

where $N^{\prime}=$ number of total items afler meeting the maximum lot-size limitation

$$
=N+\sum_{t+1}^{N} n_{t}, \quad n_{j}=\left\lceil\frac{d_{\max \mathrm{t}}}{x_{\operatorname{muxa}}}\right\rceil-1 . \text { where }
$$

$d_{\text {mux } 1}=$ maximum periodic demand for the ith item.
$x_{\text {max } i}=$ the limited lot-size for item $i$ which cannot be exceeded in any period.
$N=$ The number of original item

Production scheduling is another complex step of hierarchical production planning system, which even in the simplest possible form, may become a difficult task with the possibility of multi-variables, containing constraints and somelimes, conflicting objectives [5]. Its integration can be ensured if a suitably selected planning variable can be passed from upper disaggregation model to this level. Its solvability in real-time is of prime imporance, which ultimately leads to undesirable NP-hardness. Scheduling is a subject in which problems look casy, if not trivial. lhey are, on the contrary, among the hardest in mathematics [6, 7]. According to Baker, "Scheduling is the allocation of resources over time to perform a collection of tasks". A production scheduling specifies the order of assigning of each job to the respective resource (i.e. machine) and also specifies the star and end time of each job in a manufacturing system. Scheduling is a decision-making task and the objective is to find an appropriate schedule in terms of certain performance criteria (for example, minimizing makespan or minimizing flow-time, minimizing tardiness, ctc.) [6]. Production scheduling
problem has received ample atcontion from both rescarchers and practitioners, because an efficient production schedule contributes to reduction of production cost and inventory cost, increase in profit and increase in 'on-time' delivery to customers. The theory of scheduling includes a varicty of techniques that are useliul in solving scheduling problens. Indeed, the scheduling field has become a focal point for the development, application and evaluation of combinatorial procedures (COP), simulation techniques, nework inethods and heuristic solution approaches. The selection of an appropriate technique depends on the complexity of the problem, nature of the model and the clwice of the criterion, as well as other lactors [8]. However, a Iocal search optimization technique or a heuristic can be used, in order to trade-off between time to solve a problem and accuracy of results. This research shows that Pareto optimal solution method provides better solution than even a neighborhood search technique. a local search teclnique. This research aims at applying Pareto optimal technique [9] to select the right schedule. Most studies on production scheduling aim to minimize makespan, that is, the total completion time of all jobs. The objective of this research, in case of scheduling, is to find trade-offs among total completion time $\sum C_{1}$, maximum lateness $L_{\max }$, and total machine idle time $I$, where $I=\sum_{|n|}^{k} f_{b r}, L_{m a x}=\max _{j}\left\{T_{j}\right\}$ and $T_{j}=$ $\max \left\{0, L_{j}\right\}$ for jobs $j, j=1,2, \ldots, n$ and batch $i$.

It must be acknowledged that optimization at an individual tevel may end up in a highly sub-optimized and even a non-optimized solution. While heuristics have been suggested by many to solve an independent planning level, solution to an integrated flow or hierarchical materials planning has never been reported so far [10, 11]. This necessitates an integrated solution al several levels of production planning with approprate heuristics, where production planning is a part of total product planning loop.

A limitation of curent rescarch on applying optimization lechnique is the selcetion of unjustilied objective function. Traditionally, it is assumed that a parameter needs to be optimized through right operations management technique [12-14]. However, there is no basis as to why a particular parameter is selected as the objective function. This research provides an idea that AHP can be used to justify selection of the right parameter as the
objective function of an optimization technique. The following Figure 1.1 shows the summary of the research:

Thus, this tesearch aims at optimizing materials planning system in the total supply chain which integrates different levels of planning system.


Figure 1.1 Itierarchical Production Planning and Distribution System

### 1.2 Objectives of the Research Work

The objectives of the research work have been defined as follows:

1. To configure aggregation-disaggregation of material planning system.
2. To develop mathematical models and heuristics for the optimication of aggregate planning, master production scheduling, material requirement planning through lotsizing technique.
3. To implement. simulate and run the heuristics to minimize the total cost.
4. To identify the production scheduling paranmers that affect subsequent planning steps.
5. To select the balancing paraneter i.e. total completion time, maximum lateness, machine idle time with MCDM (multi critcria decision making) technique.
6. To develop a Parcto optimal algorithm for minimizing total completion time, maximum lateness, and machine idle lime of a production scheduling system.
7. To implement, simulate and run the Parcto optimal algorithm.
8. To identily distribution system parameters that alfect subsequent marketing.
9. To select the parameter of distribution for optimization with MCDM technique.
10. To design and optimize downstream distribution plan, with selected variables.

### 1.3 Organization of the Thesis

This thesis is organized as follows. The second chapter deals basically with aggregate planning and master production scheduling which have been optimized through lot sizing optimization. This chapler also includes various lot sizing techniques, background of lot sizing problem, heuristic methods of solution of present real life lot sizing problem and computational resules and conclusion. The third chapter deals with production scheduling optimization. This chapler presents a deseription of the multi-criterion scheduling conecpt, Iiterature survey of production scheduling problem, a modified Pareto-optimal algorithm to solve multi-criterion scheduling problem, an algorithn for neighborhood scarch technique, problem settings for a single machine scheduling problems, compulational results of the modilied algorithm and the neighborhood search heuristic and finally the conclusion on the multi-criterion perspective of this problem under consideration. The fourth chapter concentrates on distribution planning optimization. This chapter includes introduction of distribution planning, its background, application of transportation-based optimization technique, analysis of computational results and conclusion. The fifth chapter consists of conclusions and recommendations for future.

# Chapter 2 <br> Aggregate Planning 

### 2.1 Introduction

Aggregate planning is one of the several important functions in a manufacturing organization of today and this would remain so in future. It is the age of manufacturing. The manufacturing industries are now facing a time of intense international competition, which will only become more severe in the days to come. Aggregate planning is also known by such names as production plarning, operation planning. It is an activity that considers the best use of production resources in order to satisly production goals over a certan period named the planning horizon. Production planning typically encompasses three time ranges for decision making: long-term, medium-term and shori-term. The long-term planning ustally focuses is on anticipating aggregate needs and involves such strategic decisions as product, equipment and process choices, facility location and design, and resource planning. Medium-term planuing deals with making decisions on material requirements planning (MRP) and establishing production quantities or lot sizing over the planning period, so as to optimize some perfonmance criteria such as minimicing overall costs, while meeting demand requirements and satislying existing capacity restrictions. The short-lem planning, on the other hand, focuses on day-to-day decision making on scheduling of operations such as job sequencing, controlling etc in a workshop. The rescarch work focuses mainly on medium-term production planning and especially on single-level tot sizing decisions. In the spectrum of production planning, aggregate planning is intermediate-range capacity planning that typically covers a time horizon of 2 to 12 months, although in some companics it may extend to as much as 18 months. It is particularly useful for organizations that experience seasonal or other fluctuations in demand or capacity. Aggregate planning begins with a forecast of aggregate demand for the intermediate range. This is followed by general plan to mect the demand by setting oulput, employment, and finished-goods inventory levels or scrvice capacitics. Managers might consider a number of plans, each of
which must be examined in the light of feasibility and cost. If a plan is reasonably good but has more weakness, it may be revised and improved. Conversely, a poor plan should be discarded and allernative plans be sought considered until an acceptable one is found out. The production plan is essentially the output of aggregate planning.

Aggregate planners are concemed with the quantity and the timing of expected demand. If total expected demand for the planning period is much dilferent from available capacity over that same period, the major approach of planners will be to try to achicve a balance by altering capacity, demand or both. On the other hand, cven if capacity and dernand are approximately equal for the planning horizon as a whole, planners may still be faced with the problem of dealing with uneven demand within the planning interval. In some periods, expected demand may exceed projected capacity, in others expected demand may be less than projected capacity, and in some periods the two may be equal. The lask of aggregate planners is to achicve rough equality of demand and capacity over the entire planning horizon. Moreover, planners are usually concerned with minimining the cost of aggregate plan. Effective aggregate planning requires good information. First, the available resources over the planning period must be known. Then, a forecast of expected demand must be available.

From forecasts and customer orders, production planning determines the requirement of human and material resources to produce efficiently the ouputs demanded. The goal is to eflectively allocate system capacity (plant, equipment, and manpower) over a designated time horizon.

Production plan indicates the organization's strategic position in response to the expected demand for its output. A good production plan with the optimal use of resources should yield such results as (i) be consistent with organizational policy, (ii) meet demand requirements, (iii) be within capacity constraints, and (iv) minimize costs. However, for a conslant demand for a product, the planning activity becomes trivial. But with a stochastic demand, the system must have a sound production planning; and the associated planing problem is said to be dyramic. Some major strategy variables associated with production
planning for stochastic demand are the production rate, the inventory level, the work force size, etc. These variables could be varied, modified or even kept fixed, or be nonexistent in a given organi/ation, depending on its peculiarities and policies.

### 2.2 Disaggregating the Aggregate Plan

For the production plan to be translated into meaningful terms for production, it is necessary to disaggregate the aggregate plan. The result of disaggregating the aggregate plan is a master schedule showing the quantity and timing of specific end items for a scheduled horizon. A master schedule shows the planned output for individual products rather than an entire product group, along with the timing of production.

### 2.2.1 Master Production Scheduling

Production planning is an input to the Master Production Scheduling (MPS), where the master production schedule is a staternent of what end items a company plans to produce by quantity and time period. MPS is a disaggregation and implementation ol the production plan. It translates the production plan into specific products or product modules and specilies the time period tor their completion. The master scledule is the hear of production planning and control. The master schedule bas three inputs: the beginning inventory, which is the actual quantity on hand from the preceding period; forccasts for each period of the schedule; and customer orders, which are quantitics already committed to customers. The master scheduling process uses this information on a period-by-period basis to determine the projected inventory, production requirements, and the resulting uncommitted inventory. The master production scheduling process drives the material requirements planning system.

### 2.2.2 Material Requirements Planning System

The intense global competition in manufacturing has thrown a strong challenge to the management to seek new and more effective ways of managing production to maintain or to achieve a compctitive edge. Therefore, many companics have to imptement computer-based production and inventory control systems. lhe most widely adapted systems are called material requirements planning (MRP) and manufacturing resouree planning.

MRP system is a computer-based information system that translates master schedule requirements for end items into time-phased requirements lor subassemblies, components, and raw materials. Hence, requirements for end items generate requirements for lower-level components, which are broken down by plarning periods so that ordering, fabrication, and assembly can be scheduled for timely completion of ond items while inventory levels are kept reasonably low. Material requirements planning is as much a philosophy as it is a technique, and as much an approach to scheduling as it is to inventory control. MRP begins with a schedule for finished goods that is converted into a schedule of requirements for the subassemblies, components parts, and raw materials needed to produce the finished items in the specified time frame.

The primary inputs of MRP are a bill of materials, which tells the composition of a finished product; a master schedule, which tells how much finished product is desired and when; and an inventory records file, which tells how mucl inventory is on hand or on order. The planner processes this intormation to determine the net requirements for each period of the planning horizon. The materials that a firm must actually acquire to meet the demand generated by the master schedule are the net material requirements. The determination of the net requirements is the core of MRP processing. So there are two major distinguishing teatures of MRP, (1) requirement for items controlled by MRP are calculated based on schedules for higher-levels items as opposed to being forecast, and (2) plans are time phased in the form of lot-sizing showing order teleases and reccipts by tine periods throughout some planning horizon. So lot-sizing is a significant aspect of the materials requirement planuing process and acts as a major component of a balanced MRP operation.

### 2.2.3 Lot-Sizing Problem

The determination of lot sizes in an MRP system is a complicated and difticult problem. Jot sizes are the product quanlities issued in the planned order receipt and planned order relcase sections of an MRP schedule. For products produced in-house, lot sizes are the production quantitics of batch sizes. For purchased products, these are the quantities ordered from the supplier. Lot sizes generally meet product requirements for one or more periods. Lot sizing decisions give rise to the problem of identilying when and how much of a product to produce such that setup, production and holding costs are minimiced, Making the right decisions in lot sizing will affect directly the system performance and its productivity, which are imporant for a manulacturing fim's ability to compete in the market. Therelore, developing and improving solution procedures for lot sizing problems is very imporant.

Most lot-sizing techniques deal with how to balance the setup or order costs and holding costs associated with meeling the net requirements gencrated by the MRP planning process. In the past few years there have been several activities in computer based production and inventory control dealing with how to select lot-sizes in the face of an cssentially deterministic but time-varying demand pattern. Presently, lot-sizing problem has taken its place as one of the most important functions in an industrial enterprise. However, optimizing routines for lot-sizing prohlems have been shown to be all too demanding from a computing standpoint in both practical as well as research enviromment. The present work would seek for an efficient means of obtaining an optimal multi-item lol-sizing solution to research problems. This would facilitate development of improved heuristics appropriate for practical settings. Research on the relevant fields has yielded several mathematical and heuristic policies which produce oplimal and near optimal results. The ever increasing importance ol this issue therefore calls for further research in this field.

The complexity of lot sizing problems depends on the features taken into account by the model. The following characteristics affect classifying, modeling and the complexity of lot sizing decisions.[15]

## Planning Horizon

The planning horizon is the time interval on which the master production schedule extends into the future. The planning horizon may be finite or infinite. A finite-planning horizon is uswally accompanjed by dynamic demand and an in finite planning horizon by stationary demand. In addition, the system can be observed continuously or at discrete time points, which then classifies it as a continuous or discrete-type system. In terms of time period terminology, lot sizing problems fall into the categories of cither big bucket or small bueket problems. Big bucket problems, are those where the time period is long enough to produce multiple items (in muliti-item problem cases), while for small bucket problems the time period is so shor that only onc item can be produced in each time period. Another variant of the planning horizon is a rolling horizon usually considered when there is uncertainty in data. Under this assumption, optimal approaches for cach horizon act as heuristics but cannot guarantee the optimal solution.

## Number of Levels

Production systems may be single-level or multi-level. In single-level systems, usually the linal product is simple. Raw materials, aher processing by a single operation such as forging or casting, are changed to final product. In other words, the end item is directly produced from raw materials or purchased materials with no intermediatc subassemblics. Product demands are assessed directly from customer orders or market forecasis. This kind of demand, as will be further discussed later, is known as independent demand. In multilevel systems, there is a parent-component relationship among the items. Raw materials after processing by several operations change to end products. The output of an operation (level) is input for another operation. Therefore, the demand at one level depends on the demand for its parents' level. This kind of demand is named dependent demand. Multi-level problems are more difficult to solve than single-level problems. Multi-level systens are further distinguished by the lype of product structure, which includes serial, assembly, disassembly and general or MRP syslems.

## Number of Products

The number of end items or final products in a production system is another important characteristic that affects the modeling and complexity of production planning problenss. There are two principal types of production system in terms of number of products. In single-item production planning there is only one end item (final product) for which the planning activity has to be organized, while in multi-item production planning, there are sevcral end items. The complexity of multi-item problems is much higher than that of single-item problems. van Hoesel and Wagelmans [16] provide theoretical results for the performance of algorithms for the single item capacitated lot sizing problem. (See also Section 4 of this paper.) Resources or capacities in a production system include manpower, equipment, machines, budget, etc. When there is no restriction on resources, the problem is said to be uncapacitated, and when capacity constraints are explicitly stated, the problem is named capacitated. Capacity restriction is important, and directly affects problem complexity. Problem solving will be more difficult when capacity constraints exist.

## Deterioration of Items

In the case that deterioration of items is possible, we encounter restrictions in the inventory holding time. This in turn is another characteristic which would affect problem complexity.

## Demand

Denand type is considered as an input to the model of the problem. Static demand means that its value does not change over time, it is stationary or even constant, while dynamic demand means that its value changes over time. If the value of demand is known in advance (static or dynamic), it is termed deterministic, but if it is not known exactly and the demand values occuring are based on some probabilities, then it is termed probabilistic. In independent demand cases, ал item's requirements do not depend on decisions regarding another item's lot size. This kind of demand can be seen in single-level production systems.

In multi-level lot sizing, where there is a parent-component relationship among the items, because the demand at one level depends on the demand for their parents (pervious level), it is called dependent. Problems with dynamic and dependent demands are much more complex than problems with static and/or independent demands. Also, problems with probabilistic demand will be more complex than problems with determinislic demand.

## Setup Structure

Selup structure is another imporiant characteristic that directly affects problem complexity. Setup costs and/or setup times, are usually modeled by introducing zero-one variables in the mathematical model of the problem and cause problem solving to be more di4cult. Usually, production changcover between different products can incur sctup time and setup cost. There are two types of sctup structure: simple setup structure and complex setup structure. If the setup time and cost in a period are independent ol the sequence and the decisions in previous periods, it is termed a simple setup structure, but when it is dependent on the sequence or previous periods, it is termed a complex setup. Three types of complex setups will now be described. First, if it is possible to continue the production run from the previous period into the current period without the need for an additional setup, thus reducing the setup cost and time, the structure is named setup carry-over. It can also be define a second type of complex setup, family or major sctup, caused by similarities in manufacturing process and design of a group of item(s). An item setup or minor setup also occurs when changing production among items within the same family. If there is sequencedependent setup, item setup cost and time depend on the production sequence; this is the third type of complex setup structure. It is obvious that the complex structures are more awkward in both modeling and solving the lot sizing problems.

## Inventory Shortage

Inventory shorage is another characteristic affecting modeling and complexity of problem solving. If shortage is allowed it means that it is possible to satisfy the demand of the current period in future periods (backlogging case), or it may be allowable for demand not to be satisfied at all (lost sales case). The combination of backlogging and lost sales is also possible. Problems with shortage are more difficult to solve than without shortage.

### 2.3 Literature Study

The imporance of lot-sizing in inventory management has been noteworlly over the years, since it is one of the basic features of the MRP. The MRP on the other hand, has the central importance in manufacturing resource planning and comprehensive MRP system. 'I his has been evident from elforts by researchers from amongest the academics and industrics yielding vast literatures containing abstract mathematical approach as well as highly pragmatic techniques. The literatures have been found places in a large numbers of journals. Section 2.3.1. presents some of the lot-sizing techniques and Section 2.3.2 summarizes the historical background study on the subject. Dixon-Silver heuristic used Silver-Meal heuristic and Wagner and Whitin algorithm. Section 2.3 rigorously describes these two heuristics, since the present work is fundamentally an extension of Dixon-Silver's work.

### 2.3.1 Lot-Sizing Techniques

The various approaches and techniques of lot-sizing as developed are presented below.

### 2.3.1.1 Period Order Quantity

The period order quantity ( POQ ) uses the same type of conomic reasoning as the EOQ (Economic Order Quantity which is for fixed demand or order), but determines the number of periods to be covered by each order rather than the number of units to order. This results
in a fixed order cycle as opposed to a fixed quantity as in EOQ. Total cost per period as a function of $t$, the cycle time in periods is given by

$$
C(t)=k / t+h(r t) / 2 .
$$

POQ is an improvement over EOQ as it eliminates remnants, and it perforns quite well if demand is relatively stable. However, like EOQ, it does not take full advantage of knowledge of future period-to-period variations in demand. Some other techniques described subsequently outperform POQ when variation in demand is significant [17].

### 2.3.1.1 Part-Period Algorithm

The part-period algorithm can determine order sizes under conditions of known, but varying, demand rates. While the algorithm does not ensure oplimality, it does approach optimal techniques. It equates the part-period value derived from order and holding costs to the generated part-period value. The generated part-period for an item is the number of parts held in inventory multiplied by the number of time periods over which the parts are held. In calculating the generated number of part-periods, it is assumed that no holding costs are incurred for itoms consumed in the period in which they arrive.

To express order cost and holding cost in par-periods, it is necessary to divide the order cost by the holding cost per part per period. The order cost and holding cost part-periods are relerred to as the derived part-period value. The derived part-period value is the number of par-periods it takes to make order cost and holding cost cqual. A generated part-period value is obtained by accumulating part-periods over the demand time horizons for one or more periods. When the generated part-period value is first greater than the derived partperiod value, an order should be placed. The order quantity will be the accumulated demand up to the time period for the next order [17].

### 2.3.1.3 Lot-For-Lot

The simplest lot-sizing technique is lot-for-lot. $A$ lot is scheduled in each period in which a demand occurs lor a quantity equal to the net requirement.

Lot-for-lot ordering results in a zero inventory balance each period, but does involve many orders. It is most appropriate where the item has a large carying cost and a sinall ordering cost, such as large assembles with expensive components. Another situation where lot-forIot is appropriate is when demand is very sporadic and one or a few units are needed only occasionally. Lot-for-lot also provides a steadier flow of work than other lot-sicing techniques which produce fewer and larger orders [17].

### 2.3.2 Heuristic Techniques

The next three techniques are heuristics. They aim at providing a good, although not necessarily optimal solution with a rcasonable amount of computing. All the three techniques use stopping rules. That is, they start fron the first period and lest prospective orders covering the first period, then the first and second periods, then the first, second, and third periods, and so forth, until a stopping criterion is met. An order is scheduled covering demands in all periods up through the stopping period. Then the process is repeated starting at the next period afler the last stopping period.

## Least Unit Cost

The first of these rules is called least unit cost (LUC). The unit costs of orders covering successively greater numbers of periods are calculated. The unit cost for each prospective order is obtained by dividing the sum of the ordering and carrying costs by the number of units on the order. The first time cost per unil goes up, the prior period becomes the stopping period.

LUC is widely used in industry, and on the surface appears to be a reasonable approach to lot-sizing. However, closer analysis has raised some serious questions conceming the basic logic of the technique [17].

## Least Period Cost

The least period cost melhod [18] was developed by Siiver and Meal and is gencrally referred to as Silver-Mcal. This procedure secks to determine the total costs of ordering and carrying for lots covering successively greater numbers of periods into the future and to select the lot with the least total cost per period covered [17].

## Least Total Cost

The idea for the Least Total Cost (LTC) method (also called part-period-balancing), was developed by Matties and Mendoza. The concept stems from the fact that in the basic EOQ model, the inventory carrying cost is equal to the ordering cost at the optimum point. In the LTC procedure. lot-sizes covering successively greater numbers of periods into the fulure are lested until the largest lot is obtained for which the carrying cost is less than or equal to the ordering cost. The Authors presented this method to determine the lot for which the carrying cost was close to the ordering cost. This means that sometimes the carrying cost would be greater than the ordering cost. However, this is not the method presented by the original authors, and moreover it did not perform well because it has a bias toward orders that are too large [17].

## Look Ahead/Look Back

Look ahead/look back is a technique used to adjust a schedule of order already obtained by using some other technique. It was originally proposed as a relinement of LTC. However,

Iook ahead/look back can be applicd just as well to adjust schedules produced by other heuristics.

Look ahead/look back has the cffect of moving orders scheduled for periods of low demand into nearly periods of higher demand. This reduces the number of part-periods and, therefore, the carrying cost. Aucamp and l'ogarty have substantially improved and extended the technique. For one thing, their algorithm also takes into account the fact that if an order is moved forward or back to a period in which another order is scheduled, an ordering cost is saved. Their claim is that regardless of what schedule they start with, the end result is virtually optimal.

However, look ahead/look back is not widely used. The reasons are that adding this procedure makes lot-sizing more complex, adds to the amount of computation, and may only improve results marginally if a good lot-sizing procedure has been selected to arrive at the initial lot-sizes [17].

## Dynamic Lot-Sizing Problem

The dynamic lot-sizing problem (DLSP) has received considerable attention from both acadenics and industry during the past two decades. Specifically, the problem is that of determining lot-sizes for a single item when demand is deterministic and time varying. Time is discretized into periods (e.g. days, weeks and months) and production can be initiated only at the star of a period. Each time that production is initiated, a set-up cost is incurred. A holding cost is incurred for each unit of inventory that is carried from one period to the next. The objective is to minimize the total of set-up and holding costs, while ensuring that all demand is satislied on time. The dynamic demand, coordinated lot-size problem detemines the time-phased replenishment schedule (i.e., timing and order quantity) that minimizes the sum of inventory and ordering costs for a family of items. A joint shared fixed setup cost is incurred each time one or more items of the product family are replenished, and a minor setup cost is charged for cach item replenished. In addition, a
unit cost is applied to each item ordered. Demand is assumed to be deterministic but dynarnc over the planning horizon and must be met through current orders or inventory. Coordinated lot-size problems are ollen encountered in production, procurement, and transportation planning . The mathematical complexity of the coordinated lot-size problem is NP-complete indicating that it is unlikely that a polynomial bound algorithm will be discovered for its solution. For this reason, a significant literature base detailing alternative mathematical formulations and exact solution approaches for the problem is rapidly evolving in an effor to solve large industry problems.[19] This paper 120] considers the determination of lot sizes lor multiple products that can be jointly replenished. A fixed setup or order cost $\Lambda O$ (often referred to as a major set-up cost) is incurred whenever any product is ondered or produced, indeperdently of the number or type of products; and an cxtra cost Ai (usually relerred to as a minor or line set-up cost) is added if product is included in the joint order. The demand for each item is discrete, and varies in time, but is known over a given time horizon $H$. Lincar holding costs are charged on the end-pf-period inventorics and backlogging is nol permitted. The variable unit purchase cost for each product is constant throughout the horizon, so that the purchase cost of any item for total demand in the horizon is invariant of the replenishment policy. The problem is to determine a replenishment schedule for all items that minimizes the total set-up plus inventory holding cost over the horizon. Many dynamic programming solutions exist for this problem, but they are computationally complex. For example, when specialized to the multi-product dynamic lot-size problem Zangwill's method has a computational complexity that is exponential in the number of products, while Veinott's solutions are computationally exponential in the number of time periods. Other solutions that are computationally exponential in the number of products have also been proposed. However these solutions are of no use for practical prohlems, which usually involve many items and many time periods, so efforts have shifted to the development of heuristic solutions. Unfortunately, though these heuristics are relatively simple, when compared with the optimum dynamic programming solutions, they have two major disadvantages. First, they generally depend on the Wagner-Whitin dynamic progranming solution for the single-item dynamic lot-size
problem. Sccond, it is not known how good these heuristics are. Because a typical practical problem involves many items, and managers lind it difficult to understand dynarmic programming solutions, these heuristics are not desirable from a practical standpoint. A heuristic which overcomes these two problems has been given. This relies on a lower bound obtained from decomposing the problem into single-item problems. The decomposition gives an easily computed lower bound. The aim of this paper is (wo-fold: first, it gives two simple heuristics and determines their theoretical worst-case performances, and second it gives an improved version of the heuristic in Atkins and lyogun. All these heuristics are generalized versions of existing single-itern heuristics-the part period balancing (PPB1) heuristic and a variant of PPB1 denoted by PPB2, and the Silver- Meal (SM) heuristic. The generalized Silver-Meal heuristic was shown to perform very well on a wide set of problems. The par-period balancing heuristic is known to perlom well in practice and it is simple, but it has a worst-case performance of $1 / 3$. It will be shown that when this heuristic is generalized to the multi-product dynamic lot-size problem, the worst-case performance of the generalized heuristic cannot be less than $1 / 3$. The other heuristic, PPL2, which is a simple variant of the parl- period balancing heuristic, has a worst-case performance of $1 / 2$. It will be shown also that when this heuristic is generalized to the multiple product problem then the worst-case performance is preserved. The remainder of the paper is organized as follows. The second section gives a briel description of the problem and the lower bound. I he following section describes the two heuristics, the generalized PPB! (GPPBI) and the generalized PPB2 (GPPB2), and establishes their worst-case performances. Considerable recent attention has focused on the "Bullwhip Effect," a term coined by Proctor and Gamble. Dynamic programoning techniques applicd to stock mininization have also been used to quantily the Bullwhip Effect. The availability of an exact solution to the continuous differential inventory equations seemsto have been overlooked [21]. For example, when discussing equations withtime delays, none of the text books on dificrential equations or Laplace transforms point out that such equations can be solved exactly in terms of the Lambert Wfunction (Corless et al , 1996). This paper begins to address this omission. The aim is to solve exactly the equations for a model that has been shown to be practically
valuablc, and that has been sludicd in some delail, Only from analytucal solutions can the precise behavior of a model be carefully assessed over a wide range of conditions. This contributes valuable conceptual information to managers and expert system developers, who depend on behavioral heuristics. Thercfore, a goal of this paper [21] is to provide tools that help guide the exploration of the parameter space with numerical techniques. Since numerical treatments of unstable solutions require more care, such approaches should benelit.

Many optimal and heuristic techniques have been developed for variations of this problem,

## Single Item Uncapacitated Lot-Sizing Problem

First the concept of single item comes and there is no capacity restriction. Some of the most widely used heuristics for lot-sizing are: Silver-Meal heuristic [22], least unit cost heuristic [23]. These heuristics are nol directly applicable to the present work on scheduling problem. The reason is that these heuristics made the following assumptions:
(i) no capacity restrictions,
(ii) only one product to be produced, and
(iii) quantity produced to meet demand in only integer number of periods.

The effective use of the available capacity of plant could not be made in these heuristics. But when capacity constraint is realistically imposed in the scheduling problem, the available capacity use becomes necessary. This part of consideration is an important contribution to the present work.

The Silver-Meal heuristic calculates the lot size as the total demand for an integer number of periods that give the minimum total set-up and holding costs per unit time. The least urit cost heuristic calculates the lot-sizes in the same way as the Silver-Meal heuristic. But the exception is that, it minimizes the total costs per unit number of products produced rather than minimizing the total costs per unit time as is done in the Silver-Meal heuristic. For
muitiple products to be produced with no capacity constraints, the above heuristics can be applied to cach of the products independently.

## Multi Item Uncapacitated Lot-Sizing Problem

Frequently, multiple items are produced on a single machinc. This machine has finite capacity and it is usually loaded to or near capacity. Most of the existing methods for the multi-item dynamic lot-sizing problem implicitly assume that capacity is unlimited and hence their use will frequently result in excessive over or under loading in some periods. Therefore, in practice. planned lot-sizes may be split into smaller lots with some demand backlogged. This resulted to the orders are not being produced on time and the cconomics of scale of batch production is lost.

## Multi Item Capacitated Lot-Sizing Problem

The multi-item capacitated lot-sizing problem (CLSP) is found to be NP-hard when the single-item capacitated dynamic lol-sizing problem is already proven to be NP-hard [2428]. The problem is even harder from practical point of view, since optimal solution methods have failed to solve all but very small problems within reasonable computation times. Morcover, since very few workable techniques have been reported, methods to oblan optimum solutions could not be available casily. It has been found that most methods require extensive computational power, thus, their applicability is rather limited. As a consequance efforts are now being given to develop heuristics for the multi-item capacitated lot-siring problens. The various heuristics, which have heen proposed over the years, are classified into a number of classes. The first group of heuristics falling in a class could be called "common sense" heuristics. The heuristics belonging to this class can be found in Eisenhut [29], Lambrecht and Vanderveken [30], Dixon-Silver [31] etc. Many different variants have been proposed, for these common-sense heuristics, but they can basically be classified into two categories, such as
(i) the period-by-period heuristics, and
(ii) improvenent heuristics.
(i) Period by period heuristic: Heuristics belonging to the period-by-period heuristic work from period 1 to period $H$. Consider a period $t$ in the process. One cerlainly has to produce max $\left\{0, d_{i}, I_{, r-1}\right\}$ for all products $i$ in order to avoid stock outs in the current period, where $d_{i t}$ is the demand for item $i$ in period $t$ and $I_{i}$ is the inventory of item $i$ at the end of petiod $t$. The remaining capacity (if any) can be used to produce demand for some future period, in which case future sct-up costs may be saved at the expense of added inventory-holding costs. To indicate the viability of producing demand for a future period in the period under consideration, all heuristics use a priority index. The priority indices used by the heuristics are more sophisticated in that they try to capture the potential savings per time period and per unit demand. Although the exact Priority index may differ from heuristic to heuristic, they all proceed in the same way. Priority indices are calculated for all products and for all future periods. These priority indices are used to include future demands into the current production lot cither until no more with a positive index or until the capacity limit is hit.

Besides the difference in using priority index, the period-by-period heuristics also differ in the way in which they ensure feasibility. Infeasibility occurs when the net demand in some period $t$, i.e. $\sum_{i=1}^{n} \max \left\{0 . d_{1}-I_{t, t-1}\right\}$ may exceed available capacity. Two different approaches can be used to overcome this problem. The first one is the feedback mechanisin. When an infeasible period is encountered, demand with negative priority indices is shifted from the period to an earlicr period. A second approach, look ahcad mechanism, however, calculates a priority the required cumulative production up to period $t$ (for all $t$ ) such that no infeasibility will arise in period $(t+1)$. This pure single-pass heuristics require smaller computation time.
(ii) Improvements heuristics: The sccond category of heuristics called improvements heuristics start with a solution for the entire horizon and then try to improve this solution in cost ellective fashion by going through a set ol simple local improvement steps.

The second group of heuristics is all based on optimum seeking mathematical programming methods which are truncated in some way to reduce computational effort. The Mathematical-programming based heuristics are (i) Relaxation heuristies (ii) Dranch-and-Bound procedure (iii) Lincar programming based heuristics. Heuristics belonging to the class can be found in Wagner-Whitin's algorithm [28], Macs [32] Mixed-integerprogramming formulation etc. In Wagner-Whitin's algorithm capacity constraints are relaxed i,c. the capacity may be infinitc. So the problem decomposes into $N$ number of single-item uncapacitated dynamic lot sicing problems for which it provides an eflective method of solution. The first approach of this type is atributed to Newson (33). Starling from the Wagner-Whitin solutions for each product, the heuristic proceeds as follows.
(i) Select a period in which capacity is violated. For products with a set-up in that period, calculate the next best WW solution (i.c. the best solution for the problem where production in the violated period is foreed to zero).
(ii) Select the next best plan for the product yielding the smallest extra cost per unit capacity absorption, thereby releasing some capacity in the violated period.
(iii) The method proceeds in this way until all infeasibilities are removed.

The above approach has two drawbacks. Firstly, it may end up with no feasible solution at all, and secondly it restricts itself to WW schedules, whereas the optimal solution may not satisfy the WW condition $x_{H} I_{1},-1=0$ at all.

Mathernatical-programming based heuristics are not considered because these methods may not be very transparent to the casual user and these heuristics limit their regular use in industry.

## Wagner-Whitin Algorithm

l'he "square toot formula" for an cconomic lot-size under the assumption of a stcady-state demand rate is well known. The calculation is based on balancing of the costs of holding
inventory against the costs of placing an order. When the assumption of a steady-state demand rate is dropped, i.e., when the amounts demanded in each period are known but are different and furthermore, when inventory costs vary from period to period, the square root formula (applied to the overall average demand and costs) no longer assures a minimum cost solution.

The mathematical model may be viewed as a "one-way temporal leasibility" problem, in that it is feasible to order inventory in period $t$ for demand in period $t+k$ but not vice versa. This suggests that the sane model also permits an alternative intepretation as the following "one-way technological feasibility" problem.

## Mathematical Model

As in the standard lot sice formulation, one assumption is that the buying (or manufacturing) costs and selling price of the item are constant throughout all time periods, and consequently only the costs of inventory management are of concern. In the $t$-th period, $t=1,2, \ldots, H$, we let
$d_{t}=$ amount demanded,
$h_{s}=$ holding cost per unit of inventory carried forward to period $t+1$,
$S_{t}=$ ordering (or sct-up) cost,
$x_{t}=$ amount ordered (or manufactured or size of the lot), and
$c_{t}=$ unit variable cost, which can vary from period to period.
Let all period demands and costs are non-negative. The problem is to find a programme $x_{t} \geq 0, t=1,2, \ldots, I$, such that all demands are met at a minimum total cost; uny such program, will be termed optimal.

Of course one method of solving the optimization problem is to enumerate $2^{t /-1}$ combinations of either ordering or not ordering in each period (it has been assumed that an order is placed in the first period). A more efficient algorithm evolves from a dynamic programming characterization of an optinal policy.

Let / denote the inventory entering a period and $I_{0}$ initial inventory; for period $t$

$$
\begin{equation*}
I=I_{a}+\sum_{j=1}^{t-1} \mathbf{x}_{j}-\sum_{i=1}^{i-1} d_{j} \geq 0 \tag{2.1}
\end{equation*}
$$

The functional cquation representing the minimal cost policy for periods $t$ through $H$, given inconing inventory $l$, as

$$
\begin{aligned}
& f_{r}(l)=\min \left[h_{t-1} I+\square\left(x_{t}\right) s_{t}+f_{r+j}\left(I+x_{t}-d_{t}\right)\right] \\
& x_{t} \geq 0 \\
& I+x_{t} \geq d_{i}
\end{aligned}
$$

where

$$
\delta\left(x_{t}\right)= \begin{cases}0 & \text { if } x_{t}=0  \tag{2.3}\\ 1 & \text { if } x_{t}>0\end{cases}
$$

In period $H$

$$
\begin{align*}
& f_{H}(l)=\min \left[h_{H-1} I+\square\left(x_{H}\right) s_{H}\right] \\
& x_{H} \geq 0  \tag{2.4}\\
& I+x_{H} \geq d_{H}
\end{align*}
$$

Thercby obtaining an optimal solution as $I$ for period 1 is specilied. Assumption 2 below establishes that it is permissible to confine consideration to only $H+2-t, r>1$, values of $I$ at period $t$.

By taking cognizance of the special properties of the model, an allernative functional equation has been formulated which has the advantage of potentially requiring less than $H$ periods' data to obtain an optimal program; that is, it may be possible without any loss of optimality to narow the progran commitment to a shorter "planning horizon" than $I /$ periods on the sole basis of data for this horizon. Just as one may prove that in a linear programming model it suffices to investigate only basic sets of variables in search of an optimal solution, it is demonstrated that in the model an optimal solution exists among a very simple class of policies.

It is necessary to postulate that $d, \geq 0$ is demand in poriod 1 net of starting inventory. Then the fundamental proposition underlying the approach asserts that it is sulficient to consider prograns in which at period $t$ one does not both place an order and bring in inventory.

## Characteristics:

(1) There exists an optimal program such that $I_{x_{t}}=0$ for all $t$ (where $I$ is inventory entering period ().
(2) There exists an optimal program such that for all $t, x_{1}=0$ or $x_{i}=\sum_{j=t}^{k} d$, for some $k$ $t \leq k \leq N$.
(3) There exists an optimal program such that if $d_{t}$ is satisfied by some $x_{l^{* *}} t^{* *}<t^{*}$, then $d_{t}, t=t^{* *}+1, \ldots, t^{*}-1$, is also satisfied by $x_{f^{* *}}$.

For the particular cost structure assumed, it can be shown that an optimal policy has the propenty that $I_{t-\mu} x_{t}=0$, for $t=1,2, \ldots, H$. That is, the requirements in a period are satisfied either entirely from procurement in the period or enticly from procurenent in a prior period.

The property of an optimal solution stated above implies that we need consider only procurement programs where $x_{t}=0$, or $x_{i}=d_{t}+d_{t-t}^{+} .+d_{k}$, for some $k=t, t+1, \ldots, H$. To efficiently investigate such programs, the following algorithm can be used.

Let $F_{k}$ be the minimum cost program for periods $1,2, \ldots, k$, when $I_{k}=0$ is required. Let $j$ be the last period prior to $k$ having an ending inventory of zero. Thus $I_{j}=0, I_{k}=0$, and $I_{i}>0$, for $t=j+1 . j+2, \ldots, k-1$. Therefore, $x_{j+1}=d_{j+1}+d_{j}+2+\ldots+d_{k}$. Deline $M_{j k}$ to be the cost incurred in periods $j+1$ through $k$. It is

$$
M_{j k}=\mathbf{x}_{s, 1}+C_{i+1} x_{j+1}+\sum_{t=j+1}^{k-1} h_{t} I_{i} .
$$

Since

$$
\begin{aligned}
& I_{i}=x_{t+1}-\sum_{t=+1+1}^{1} d_{i}=\sum_{t=i+1}^{k} d_{i}, \text { for } j<t<k, \text { and } \\
& M_{j k}=x_{i+1}+C_{r+1} x_{i+1} \sum_{t=j+1}^{k-1} h_{t} \sum_{d=j+1}^{k} d_{i} .
\end{aligned}
$$

With this definition of $M_{k}$, we can write the following recursive equation for $F_{k}$.

$$
\begin{equation*}
F_{k}=\min \left[F_{j}+M M_{j k}\right], \quad k=1,2, \ldots, H \text { and } 0 \leq j<k, \tag{2.5}
\end{equation*}
$$

where $F_{o}=0$. The logic motivaling equation (2.5) is that for a $k$-pcriod horizon with zero initial and linal inventories and no shortages allowed. there will be some period where the last procurement is made. Call this period $j+1$, and by the property of an optimal solution, $I_{t}$ $=0$. Assume that we have found the optimal policy, and hence minimun cost $F_{t}$, for every $t$ $<k$, where assumption is $I_{t}=0$. Thus $F_{J}$ is known and $M_{f k}$ can be computed. The minimum cost for a $k$-period horizon results from selecting the optimal period for the last procurement. By trying all $j<k$, we can find the value of $j$, say $j_{k^{*}}$, which minimizes $F_{j}+M_{j k^{*}}$ Last procutement is in period $j_{k^{*+1}}$.

The procedure is to determinc in sequence the values $F_{6}, F_{2}, \ldots, F_{S}$. When $F_{H}$ is 1ound, having the minimum cost value for the $I /$-period horizon and $j_{H^{*}}$ can be used to work backward to extract the optimal lot sizes.

## Silver-Meal Heuristic Model

It is a simple heuristic method for selecting replenishment quantilics under conditions of deterministic time-varying demand where replenishment are restricted to the beginning by a period.

It has been wished to select the order quantity $Q$ so as to minimize the costs per unit time over the time period that $Q$ lasts. When there is restriction to replenishments at the beginning of a period the search is restricted to a set of $Q$ lasting for one, two, threc, etc., periods, i.c., searching is on a time variable $T$ which can take on the values of $1,2,3$, etc.

## Symbols

Suppose the following symbols have been destgned. $F(j)$ is the demand rate (assumed constant) during the $j$-th period (where period I is the period immediately following the present moment at which a replenishment decision has to be made).
$T=1,2,3, \ldots$ is the decision variable, the time duration that the curent replenishunent quantily is to last.
$R$ and $G(j)$ are quantities to be used in the algorithm,
$S$ is the ordering cost in the unit of currency,
$C$ is the unit variable cost in the unit of currency per picec,
$I$ is the inventory carrying charge expressed as a decimal fraction per period.
$M=\frac{S}{C I}$.

## Algorithrn

The algorithm is as follows:
Step 1: Initialization
Sel $T=1$,
$R=F(1)$, and
$G(1)=M$.
Step 2
Is $T^{2} F(T+1)>G(T)$ ?
No - go to Step 3
Yes - go to Step 4
Step 3
Set $T=T+1$
Evaluate $R=R+F(T)$, and
$G(T)=G(T-1)+(T-1) F(T)$
go to Step 2

Step 4: Calculation of replenishment quantity
$Q=$ current value of $R$ (because $R$ is defined in such a way that it has accumulated total demand through the end of period $\tau$ ).

$$
=\sum_{j \times 1}^{l} F(j)
$$

The most complicated operation in the algorithm is seen to be straight multiplication of two terms or the squaring of a number.

## Dixon-Silver Model

Onc elass of "common sense" heuristics considered here was initiated by Lisenlut [29] and could be called period-by-period heuristics. Eisenhuts procedure was later extended by Lambrecht and Vander Vaken [30], Dixon and Silver [131]. In Eisenhut heuristic there is no guarantee one will lind a feasible solution when only positive prionity indices are considered, the reason being, that net demand in some period $t$, i.e., $\sum_{t=1}^{N} \max \left\{0, d_{t t}-I_{1, t-1}\right\}$ may exceed available capacity.

Lambrecht and Vanderveken [28], Dixon and Silyer both are period-by-period beuristic and based on Wagner-Whitin condition. These period-by-period heuristics have the advantages that their computation time is low. Both heuristics use the priority index which is derived from the well-known Silyer-Meal heuristic for the single level uncapacitated dynamic lotsizing problem.

Lambrecht and Vanderveken use a feedback mechanism (Backtracking) when an infeasible period is encountered, i.e. they try to shill excess demand to leftover capacity in previous periods, taking into consideration setup and holding costs, until the infcasibility in period $t$ is removed.

Dixon and Silver, on the other hand, perform a priority (look ahead) computation of the cumulative production requirements up to period $t$ (for all $f$ ) such that no infeasibility will arise in period $(t+1)$.

From the comparison study of Maes and Van Wassenhove [32], backtracking procedure creates a lot of additional setups whereas in a look-aheal procedure demand wo be shifted to carlicr periods is incoporated in planned production lots. Indeed, when capacity constraints are tight it may not be possible to shif demand backwards such that it can be added to an already planned production lot. Instead demand may have to be split up and several extra selups may be necessary to fit everything. This explains why rather large dilferences between Dixon and Silver and the other heuristics occur. On the basis of the results of Maes and Van Wassenhove's [32] comparison study it can be concluded that a look ahead procedure such as the one used by Dixon-Silver[31] should be prelerred to a backtracking procedure used by Lambrecht and Vandervaken. However, when a strong trend in demand prevails, one should use a look-ahead procedure to cnswre feasibility rather than relying on a backtracking routine as in Lambrecht and Vandervaken. So a good heuristic should have a look ahead mechanism to ensure feasibility at the outset and period-by-period heuristic take advantage when capacities are tight and dilference in capacity absorption across products are large.

Considering these points as discussed above the Dixon and Silver heuristic is considered for further improvements in the present work.

Dixon-Silver model determines lot-sizes for a group of products that an produced at a single machine. It is assumed that the requirements for cach product are known period by period, out to the end of some common time horizon. For each product there is a fixed sctup cost incursed cach time production takes place. Unit production and holding costs arc assumed linear. The objective of the model is to determine lot-sises so that the total costs are minimized, with no back-logging and having capacity restriction.

The input to the model would include all the costs and product data for each item, such as inventery holding cost, setup cost, selup time, production rate or capacily absorption rate, safety stock, initial inventory and ending inventory. Forecasled demand would be given for cach item in each period. In addition, available capacity would be used period by period as input data. The mathematical model is presented below:

## Mathematical model

Minimize $Z(X)=\sum_{i=1}^{N} \sum_{j=1}^{n}\left(S_{r} \delta\left(x_{1}\right)+h_{i} i_{i j}\right)$
Subject to $I_{y}=I_{i, j-1}+x_{y}-D_{4} \quad i=1,2, \ldots, N$ and $j=1,2, \ldots, H$

$$
\begin{array}{ll}
I_{\Delta 0}=I_{\Delta H}=0 & i=1,2, \ldots, N \text { and } j=1,2, \ldots, H \\
\sum_{i=1}^{N} k_{r} x_{y} \leq C_{j} & j=1,2, \ldots, H \\
x_{y y}, I_{u} \geq 0 & i=1,2, \ldots, N \text { and } j=1,2, \ldots, H
\end{array}
$$

where $N=$ the number of items,
$H=$ the time horizon,
$D_{i j}=$ the given demand for item $i$ in period $j$,
$I_{i j}=$ the inventory of item $i$ at the end of period $j$ (aller period $j$ production and demand satis(lied),
$x_{i j}=$ the lot-size of item $i$ in period $j$,
$S_{1}=$ the sctup cost for item $i$,
$h_{\mathrm{s}}=$ the unit holding cost for item $i$,
$k_{1}=$ the capacity absorption rate for item $i$,
$C_{1}=$ the capacity in period $j$,
$\delta\left(x_{n}\right)= \begin{cases}1 & \text { if } x_{i j}>0 \\ 0 & \text { if } x_{y j}=0\end{cases}$
$\delta\left(\boldsymbol{r}_{n}\right)$ is a binary setup variable indicating whether a setup cost must be incured for item $i$ in period $j$ or not.

### 2.4 Development of the Model

This section deals with the moditication of the Dixon-Silver model with new parameters: setup time and limited lot-size per setup. The modified models are more attractive than the Dixon-Silver model since the sctup time and the limited lot-size per setup would be two impomant parameters from management point of view. In this regard two models have been
formulated. The model with sctup time, its heuristic method of solution has been presented in section 2.4.1. The model with the limited lot-size per setup, its beuristic method of solution, and sample output have been presented in Section 2.4.2.

### 2.4.1 Lot-Size Model with Setup Time

The lot-size model with selup time included is presented below showing the mathematical model, heuristic and sample calculations. The input to the model would include all the costs and product data for each item, such as inventory holding cost, setup cost, selup time, production rate or capacity absorption rate, safcty stock, initial inventory and ending inventory. Forecasted demand would be given for cach item in each period. In addition, available capacity would be used period by period as input data. The mathematical model is presented below.

## Mathematical model

Minimize $Z(X)=\sum_{i=1}^{N} \sum_{j=1}^{H}\left(S_{1} \delta\left(x_{i}\right)+h_{i} I_{y}\right)$
Subject to $I_{y}=I_{r, j-1}+x_{y}-D_{n} \quad i=1,2, \ldots, N$ and $j=1,2, \ldots, H$

$$
\begin{array}{ll}
I_{t 0}=I_{t j}=0 & t=1,2, \ldots, N \\
\sum_{i=1}^{U}\left[k_{t} x_{y}+S t_{d} \cdot \delta\left(x_{k j}\right)\right] \leq C, & j=1,2, \ldots, H \\
x_{f j}, I_{y j} \geq 0 & i=1,2, \ldots, N \text { and } j=1,2, \ldots, H
\end{array}
$$

where $S t_{1}=$ setup time for item $i$.

## Heuristic Method of Solution

Several methods have been proposed for a solution of the multi-itern constrained dynamic lot-sizing problem (DLSP). Most of these techniques have weakness or limitation that either they can not guarantec the generation of a feasible solution or become computationally prohibitive. It has been proved that even the single-item problem with constant capacity is

NP-hard [8-11]. That is, it is in a class of problems that are extremely difficult to solve in a reasonable amount of time. When the selup time would be included, the problem would become strictly NP-hard. Therefore, a simple heuristic has been developed which would guarantee a feasible solution. The heuristic method of solution is presented below in steps.

## Step 1 Creation of an equivalent demand matrix:

- Convert the initial demand matrix into cquivalent demand matrix with the use of initial inventory, ending inventory and salety stock.
- Use the initial inventory to satisly as much demand as possible in the first few periods. The net requirements will be that demand not satisfied by the initial inventory. During the calculation of the net demands, the amount of the safety stock should be maintained.

Let $\mathrm{Fin}=$ initial inventory for item $i$,
lend $=$ ending inventory for item $i$,
$^{2} e m_{t}=$ remaining initial inventory for item $i$, and
$S S_{i}=$ safety stock for item $i$.
$d_{y}=$ equivalent demand for product $i$ in period $j$.
Initially set $\mathrm{Irem}_{\mathrm{J}}=\mathrm{Kin}-S S_{1}$ and period $j=1$.
Then set $d_{\mathrm{t}}=\left\{\begin{array}{ll}0 & \text { if }^{0} \text { Irem }_{c}>D_{i j} \\ D_{y j}-\text { Irem }_{t} & \text { if } \text { Irem }_{\mathrm{r}} \leq D_{q}\end{array}\right.$.
Compute $^{\text {Irem }}=$ Irem $_{t}-D_{1 y}$.
Sct $j=j+1$ and recycle till $/$ Fem $m_{\mathrm{t}}>0$.

- Since the amount of the safety stock is always maintained, the demand in the last period $H$ would be partially satisfied by the safety stock of the period $H$-1. If ending inventory is desired, then the requirements in period $/ /$ should be increased by the desired ending inventory. Then

$$
d_{H H}=D_{d H}+\text { Iend }_{t}-S S_{r}
$$

- Compute the net demands for all $i=1,2, \ldots, N$.


## Step 2 Check the feasibility of the problem:

## Feasibility Condition:

$$
\begin{aligned}
\sum_{i=1}^{H} C R_{1} \leq & \sum_{i=1}^{H} C_{i} \\
\text { where } C R_{j} & =\sum_{i=1}^{N} k_{i} d_{i j} \\
C R_{j} & =\text { demand in terins of capacity unit for period } j_{1} \\
k_{i} & =\text { capacity absorption rate for product } i
\end{aligned}
$$

If the feasibility condition is not satisfied, the problem is infeasible i.e. all demands cannot be met with the available capacity.

## Step 3 Use the Dixon-Silver heuristic with inclusion of setup time [through steps 3.1 to 3.12]

## Step 3.1

- Start at period l, i.e. set $R=1[R=1,2, \ldots, H]$. When lot-sizing of period 1 is complete, then lot-sizing is started for period 2 up to period $H$.


## Step 3.2

- Initialize lot-size $x_{1 y}$, by equalizing to demand $d_{11}$, i.e.,

$$
x_{i f}=d_{n} \quad i=1,2, \ldots, N \text { and } j=1,2, \ldots, I / .
$$

## Step 3.3

- Initially set the value of the time supply to one i.e., $T_{\mathrm{t}}=1$, where $i=1,2, \ldots, N$.

Time supply $(T)$ denotes the integet number of period requirements that this lot will exactly salisfy.

## Step 3.4

- Produce $d_{A_{R}}>0$, in the lot-sizing period $R$, where $i=\mathrm{I}, 2, \ldots, N$.
- After producing $d_{i R}$ calculate remaining capacity in period $R$, denoted by $R C_{R}$, by

$$
R C_{R}=C_{R}-\sum_{r=1}^{N} k_{1} d_{J R} .
$$

- Let $\dot{I}_{i j}$ be the amount of inventory at the end of period $j$ for item $i$, resulting from only the currently scheduled production in period $R$. Initialize $i_{i j}$ with zero, i.e.,

$$
\dot{I}_{i j}^{\prime}=0, \quad i=1,2, \ldots, N \text { and } j=1,2, \ldots, H .
$$

## Step 3.5

- Let $A P_{j}$ be the amount of inventory (in capacity units) resulted from the production of period $R$ that will be used in period $j$. Then

$$
A P_{:}=\sum_{\mathrm{j}=1}^{N} k_{\mathrm{r}}\left(I_{1, j-1}^{\prime}-I_{\mathrm{r}, \mathrm{j}}^{\prime}\right) .
$$

- Let $C R_{j}$ be the total demand (in capacity units) in period $j$. Then

$$
C R_{1}=\sum_{t=1}^{N} k_{1} d_{u} .
$$

- The production plan for pcriod $R$ is feasible in and only if the following condition is satisfied for $t=2, \ldots, H$.

$$
\sum_{i=R+1}^{N+1-1} A P_{j} \geq \sum_{j=k+1}^{k+1-1}\left(C R_{j}-C_{j}+S t_{j}\right)
$$

- Determine the carliest period $t_{c}$ at which the above feasibility constraint is not satisfied, i.e.,

$$
t_{c}=\min \left\{t \mid \sum_{r=i l+1}^{k+r-1} A P,<\sum_{j=R+1}^{R+t-1}\left(C R,-C_{,}+S t,\right)\right\} .
$$

To remove inleasibility upto $t_{c}$, extra amount is to be produced with the use of remaining capacity $R C_{R}$ of period $R$. If there is no infeasibility, set $t_{c}=H+1$.

## Step 3.6

- Consider only iterns $i$ which have
(1) $T_{1}<t_{r}$,
(2) $R C_{R}$ is sufficient to produce $d_{i, R+Y_{1}}$, and
(3) $d_{i ; R+7,}>0$.

To decide the best item (from a cost standpoint) to be produced in period $R$, calculate the priority index $U_{r}$ for all of these items, where

$$
\begin{align*}
& U_{r^{\prime}}=\frac{A C\left(T_{r}\right)-A C\left(T_{r^{\prime}}+1\right)}{k_{r} d_{l^{\prime}, T_{1}+1}} \text {, and }  \tag{3.1}\\
& A C\left(T_{r^{\prime}}\right)=\left\{S_{r^{\prime}+H_{r}} \cdot \sum_{i=R}^{R+T_{i}^{\prime-1}}(j-R) d_{r^{\prime}}\right\} / T_{r^{\prime}}
\end{align*}
$$

Among these find the one, denoted by $i$, that has the largest $U_{t}$.

- $U_{\text {, }}$ is the marginal decrease in average costs per unit of capacity absorbed.
- $A C\left(T_{t}\right)$ is average cost per unit time of a lot of item $i$ which will satisfy $T_{i}$ periods' requirements. This is from the Silver-Meal model in which future selup cost may be saved at the expense of added inventory holding cost.


## Step 3.7

- Check the valuc of $U_{s}$.
(a) Ir Ui $>0$, then it is cconomic to produce ${ }^{d_{1, t}} t_{1}$ in period $R$.

Increase the value of iot-size $x_{k i}$ and inventory $i_{i j}$ by $d_{1, R+T_{i}}$. i.e.,

$$
\begin{aligned}
& x_{t+1}=x_{1 R}+d_{1, R+T_{1}} \\
& I_{y}^{\prime}=I_{v}^{\prime}+d_{1, R+r_{1}} \quad j=R+1, \ldots, R+T_{4} .
\end{aligned}
$$

Decrease the value of lot-size $x_{i, K+t_{l}}$, demand $d_{t, R+T_{l}}$ and remaining capacity $R C_{R}$ by $d_{i, H 1 T}$, i.c., set

$$
\begin{aligned}
& x_{i, R+Y_{1}}=x_{t, R+Z_{C}}-d_{1, R+7} \\
& d_{1, R+r_{1}}=d_{\mathrm{r}, k+l_{1}}-d_{\mathrm{r}, h r i_{1}}=0 \\
& R C_{H}=R C_{R}-d_{t, k+3,} .
\end{aligned}
$$

- Set $T_{\mathrm{r}}=T_{\mathrm{t}}+1$ and continue from Step 3.5 .
(b) If $U_{1} \leq 0$, then it is nol economic to increase $T_{1}$ of ainy item, because of the increase of the total cost.
- Check the value of $t_{c}$.
(i) If $t_{c}>H$, then no infeasibilities left and lot-sizing of the current period is complete. Go to Step 3.12.
(ii) If $t_{c}<H$, there are infeasibilities and production of one or more item is to be increased and it is done through Steps 3.8 to 3.11 .


## Step 3.8

- Calculate the value of $Q$, where

$$
Q=\max _{R+t_{c}-1 \leq t \leq H}\left[\sum_{j=R+1}^{\prime}\left(C R_{j}-\left(C_{i}-S t_{j}\right)-A P_{j}\right)\right] .
$$

- $Q$ is the amount of production still needed in the current period to eliminate infeasibilities in the later period because the available capacity is not sufficient to mect the demands of those periods.


## Step 3.9

- Consider only items $i$ for which
i. $T_{i}<t_{c}$, and
i. $d_{i, k+\}_{1}}>0$.

To decide the best item (from a cost standpoint) to be produced in period $R$, calculate the priority index $A_{\text {r }}$, for all of these items, where

$$
\Delta_{i^{\prime}}=\frac{A C\left(T_{i^{\prime}}+1\right)-A C\left(T_{1^{\prime}}\right)}{k_{i^{\prime}} d_{l^{\prime}, J_{i}^{\prime}=1}} .
$$

- Find the one, denoted by $i$, that has the smallest $\Delta_{1}$.


## Step 3.10

- Let $W=k_{1} d_{1, k+T_{1}}$.
- Compare the value of $Q$ with $W$.
(a) If $Q>W$,

Inerease the value of lot-sise $x_{i f}$, and inventory $\dot{I}_{i j}$ by $d_{, k+r_{1}}$, i.e.,

$$
\begin{aligned}
& x_{\mathrm{D} k}=x_{\Delta R}+d_{, R+r_{0}} \\
& I_{v}^{\prime}=I_{q}^{\prime}+d_{1, R+r_{i}} \quad j=R+I_{2}, \ldots, R+T_{i} .
\end{aligned}
$$

Decrease the value of lot-size $x_{1, R+7,}$, demand $d_{, R+\Gamma, ~}$, and remaining capacity $k C_{R}$ by $d_{, \mathcal{R}^{+}+T_{j}}$, i.e.,

$$
\begin{aligned}
& x_{i, \beta+L_{1}}=x_{i, R+L_{1}}-d_{, R+R+T_{1}} \\
& d_{1, R+\Gamma_{1}}=d_{1, R+C_{1}}-d_{, R+R+T_{2}}=0 \\
& R C_{R}=R C_{R}-d_{1, R+t_{1}} .
\end{aligned}
$$

$\operatorname{Set} Q=Q-W$ and $T_{4}=T_{i}+I$.
Continue from Step 3.9.
(b) If $Q \leq W$,

Sct $I Q=\left\lceil\frac{Q}{k_{r}}\right\rceil$.
Inercase the value of lot-sice $x_{J R}$ and inventory $I_{I I}$ by $I Q$, i.e.,

$$
\begin{aligned}
& x_{n}=x_{l R}+I Q \\
& I_{n}^{\prime}=I_{i n}^{\prime}+I Q .
\end{aligned}
$$

Decrease the value of lot-size $x_{1, k+2 ;}$; and demand $d_{i, N+3,1}$ by $I Q$, i.e.,

$$
\begin{aligned}
& x_{t, R+T_{1}}=x_{1, R+T_{1}^{\prime}}-I Q \\
& d_{1, R * T_{;}}=d_{t, R * J_{c}}-I Q .
\end{aligned}
$$

## Step 3.11

- Set $R=R+1$.
- Check the value of $R$.
(a) If $R<H$, then continue from Step 3.3.
(b) If $R>H$, lot-sizing is complete up to period $/ /$.


## Step 3.12

- Calculate the values of
i. Forecasted machine time required/period.
ii. Total expected setup cost.
iii. Total expected inventory holding cost.
iv. Tolal expected safety stock cost.
- Stop.


### 2.4.2 Model with the Limited Lot-Size Per Setup

The Iot-size model with the limited lot-size per setup is presented below slowing the mathematical model, heuristic and sample calculations. Like the previous model, the input would include all the cost and product data for each item, such as inventory holding cost, setup cost, the limited lot-size per setup, production rate or capacity absorption rate, salety stock, initial inventory and conding inventory. lorecasted demand would be given for each item in cach period. In addition, available capacity would be used period by period as input data. It is to be noted that Dixon-Silver heuristic allows only one setup for each item in each period. But the limitation on lot-size may need more than one setup in a particular period. So should this limitation be incoporated into Dixon-Silver heuristic, each time an item when processed in a now sctup is to be considered a new item. This may call for splitting an
item into several new items in a paricular period. However, the maximum number of the new splitted items will be restricted by the maximum periodical demand of the item. As for example, for the ith item if the maximum periodic demand and the limited lot-sise be respectively $d_{\max ,}$ and $x_{\text {max } 1,}$, the number of new items will be $n_{r}=\left\lceil\frac{d_{\text {max }},}{x_{\text {maxx }}}\right\rceil$. Thus the total number or new items will be $\sum_{i=1}^{N} n_{j}$, where
$N$ is the number of items. So after mecting the Iot-size dimitation, the total number of items to be considered in the model should be $N^{\prime}=N+\sum_{n=1}^{N} n_{1}$.

In view of the above discussions, the model may now be presented as follows.

## Mathematical Model

Minmize $Z(X)=\sum_{i=1}^{t i} \sum_{j=1}^{j f}\left(S \delta\left(x_{i j}\right)+h_{1} I_{n j}\right)$
Subject to $I_{i s}=I_{4,-1}+x_{i 4}-D_{i j} \quad i=1,2, \ldots, N^{\prime}$ and $j=1,2, \ldots, H$

$$
\begin{array}{ll}
I_{\mathrm{r} 0}=I_{\Delta H}=0 & i=1,2, \ldots, N^{\prime} \\
\sum_{i=1}^{N^{r}} k_{i} x_{v} \leq C_{j} & j=1, \ldots, H \\
0 \leq x_{u} \leq x_{\max \mathrm{r}} & i=1,2, \ldots, N^{\prime} \text { and } j=1,2, \ldots, H \\
I_{u} \geq 0 & i=1,2, \ldots, N^{\prime} \text { and } j=1,2, \ldots, H
\end{array}
$$

where $N^{\prime}=$ number of total items after meeting the maximum fol-si/e limitation

$$
=N+\sum^{\infty} n_{r}, \quad n_{1}=\left\lceil\frac{d_{\max \mathrm{r}}}{\mathbf{x}_{\max \mathrm{x}}}\right\rceil-1 . \text { where }
$$

$d_{\text {max } 1}=$ maximum periodic demand for the ith item.
$x_{\mathrm{max} t}=$ the limited lot-size for jtem i which camot be exceeded in any period.

## Heuristic Method of Solution

The original two-item problem with constant capacity is NP-hard. In the present work a new constraint on upper limit of the limited lot-size is considered. With this new constraint the problem is also NP-hard. Therefore, a simple heuristic has been developed which guarantecs a feasible solution.

## Step 1 Creation of an equivalent demand matrix:

- Using the same technique of Step 1 of Section 3.2.1, the given $N \times H$ demand Inatrix is converted into an equivalent $N \times H$ demand matrix with the use of initial inventory, ending inventory and safety slock.


## Step 2 Check the feasibility of the problem:

- The feasibility of the problem for $N$ ilems is checked using the sume formulas of Step 1 of Section 3.1.2.

Step 3 Convert the multi-setup problem into single setup problem [through steps 3.1 and 3.2]

## Step 3.1

- Find the maximum demand $d_{\text {max }}$, for each item $i$ by using the formula

$$
d_{\text {max } 1}=\max \left\{d_{i j} \mid j=1,2, \ldots, H\right\} .
$$

- Find the number ol new items $t_{t}$ to be considered to satisfy demand $d_{\max }$, by using the formula

$$
n_{i}=\left\lceil\frac{d_{\max i}}{x_{\operatorname{tax} / i}}\right\rceil-1
$$

Then the number of total items after limiting the lot-size is

$$
N^{\prime}=N+\sum_{i-1}^{*} n_{i} .
$$

Item $i$ is splited into $n_{t}+1$ items. Let the new items are $i_{0}, i_{1}, \ldots, i_{n_{i}}$.

Initially set $d_{\mathrm{cm} \mid f}=d_{y}$ and $l=0$.
Then set $d_{i, 5}=\left\{\begin{array}{ll}d_{\text {rim }} & \text { if } d_{\text {rem } 1,} \leq x_{\text {max }} . \\ x_{\text {max }} & \text { if } d_{\text {rem } 1 / 4}>x_{\text {max }}\end{array}\right.$.

Set $l=l+1$ and recycle up to $l=n_{l}$.

- Now the equivalent demand matrix $N \times H$ is converted into a new demand matrix $N^{\prime} \times H$


## Step 3.2

- Initialize the values of sctup cost, holding cost and capacity absorption rate for the $N$ new items from that of the $N$ items by using the formulas

$$
\begin{aligned}
& S_{t_{n}}=S_{\mathrm{r}_{2}}=\ldots-S_{1_{n}}=S_{i}, \\
& h_{\mathrm{r}_{11}}=h_{\mathrm{t}_{1}}=\ldots=h_{\mathrm{l}_{m}}=h_{t_{1}} \\
& k_{\mathrm{r}_{11}}=k_{\mathrm{r}_{1}}=\ldots=k_{1_{m}}=k_{r} .
\end{aligned}
$$

Step 4 Apply the Dixon-Silver heuristic with inclusion of the limited lot-size per setup |through Steps 4.1 to 4.13]

## Step 4.1

- Starl at period 1, i.e. set $R=1 \mid R=1,2, \ldots . ., H]$
- Ater completing the lot-sizing of period 1 , the lot-sizing ol period 2 is started.


## Step 4,2

- Initialize lot-size $x_{i j}$ by equalizing to demand $d_{y y}$, l.e.,

$$
x_{n}=d_{\eta} \quad i=1,2, \ldots, N^{\prime} \text { and } j=1,2, \ldots, h .
$$

- Calculate remaining allowable amount that can be produced by the following equation.

$$
x_{\mathrm{rcm} y}=x_{\max t}-x_{j} \quad i=1,2, \ldots, N^{\prime} \text { and } j=1,2, \ldots, H .
$$

where
$x_{\text {rem }}=$ remaining atlowable amount that can be produced if $x_{\text {Ij }}$ is produced at period $j$ for item $i$.

## Step 4.3

- Initially set the value of time supply to one i.e. $T_{i}=1$, where $i=1,2, \ldots, N^{\prime}$.
l'ine supply $T_{i}$ denote the integer number of periods requirements that this lot will exactly satisfy.


## Step 4.4

- For each item $i, i=1,2, \ldots, N^{\prime}$, produce $d_{i k}(>0)$ in the lot-sizing petiod $R$.
- After producing $d_{\mathrm{I}}$ calculate remaining capacity in period $R$, denoled by $R C_{\mu}$, hy

$$
R C_{k}=C_{k}-\sum_{i=1}^{N} k_{t} d_{i z}
$$

- Let $I_{7}^{\prime}$ be the amount of inventory al the cnd of period $j$ for item $i$, resulting from only the currently scheduled production in period $R$. Initialise $I_{\text {II }}^{\prime}$ with zero, i.e.,

$$
I_{y}^{\prime}=0, \quad i=1,2, \ldots, N^{\prime} \text { and } j=1,2, \ldots, H .
$$

## Step 4.5

- Let $A P_{j}$ be the amount of inventory (in capacity units) resulted from the production of period $R$ that will be used in period $j$. Then

$$
A P_{f}=\sum_{\mathrm{r}-1}^{N_{1}} k_{( }\left(l_{r, r-\mathrm{i}}^{\prime}-I_{t, j}^{\prime}\right) .
$$

- Let $C R$, be the total demand (in capacity units) in period $j$. Then

$$
C R_{r}=\sum_{t=1}^{w^{w}} k_{1} d_{v}
$$

- The production plan for period $R$ is feasible if and only if the following condition is satisfied for $t=2, \ldots, H$.

$$
\sum_{t-\beta=\beta=1}^{n+1-1} A P_{t} \geq \sum_{i=R^{2}+1}^{8+1-1}\left\{C R_{J}-C_{j}\right\} .
$$

- Detcrmine the earliest period $t_{c}$ at which the above feasibility constraint is not satisfied, i.c.,

$$
t_{c}=\min \left\{t \mid \sum_{j=\beta+1}^{k+t-1} A P,<\sum_{j=R+1}^{k+i-1}\left(C R,-C_{j}\right)\right\}
$$

To remove infcasibility uplo $t_{c}$, cxtra amount is to be produced with the use of remaining capacity $R C_{R}$ of period $R$.

If there is no infcasibility, set $t_{\mathrm{c}}=H+1$.

## Step 4.6

- Consider only items $i^{\prime}$ which have
(1) $T_{i}<t_{c}$,
(2) $R C_{R}$ is sufficient to produce $x_{\text {can }}$,
where $x_{\text {can }}=\min \left\{d_{t: R+1, r}, x_{\text {rem } r}\right\}$, and
(3) $x_{c a n}>0$.

By equation (1) find the item, denoted by $i$, that has the largest $U_{i}$.

## Step 4.7

- Check the value of $U_{i}$.
(a) If Ui $>0$, then it is economic to produce xcan in period $R$.

Increase the value of lot-size $x_{B R}$, inventory $I_{i j}^{\prime}$ and $x_{\text {rem }, R H 7,}$ by $x_{\text {com }}$ i.e., sct

$$
\begin{aligned}
& x_{r R}=x_{\Omega R}+x_{\text {can }} \\
& \dot{I_{y}}=i_{i}^{\prime}+x_{c R n} \quad j=R+1, \ldots, R+I_{i} \\
& x_{\mathrm{rem}, R \vdash r_{\mathrm{r}}}=x_{\mathrm{remm}, K^{+}+\mu}+x_{\mathrm{cam}} .
\end{aligned}
$$

Decrease the value of lot-sice $x_{i, R+1,}$, demand $d_{1, R+\Gamma_{1}}$, remaining capacity $R C_{R}$ and $x_{\text {ren }} / R$ by $x_{\text {can }}$,i.c., set

$$
x_{,, R+l_{,}}=x_{,, R+T_{1}}-x_{c a t h}
$$

$$
\begin{aligned}
& d_{\mathrm{r}, R+T_{1}}=d_{t, \beta+r_{r}}-x_{\text {cur }} \\
& R C_{R}=R C_{R}-x_{\text {can }} \\
& x_{\mathrm{rem}, R}=x_{\mathrm{rem}, R}-x_{\text {cour }} .
\end{aligned}
$$

- Set $T_{i}=T_{i}+1$ and continue from Step 4.5.
(b) If $U_{1} \leq 0$, then it is not economic to increase $T_{\text {, ol any itcm (total cost increases). }}$
- Check the value of $t_{c}$.
(i) If $t_{c}>H$, then no inleasibilities left and lot-sizing of the current period is complete. Go to Step 4.12.
(ii) If $t_{c}<H$, there are infeasibilitics and production or one or more iten is to be increased and it is done through Steps 4.8 to 4.11 .


## Step 4.8

- Calculate the value of $Q$, where

$$
Q=\max _{R_{1, t}-1 \leq t \leq H}\left[\sum_{j=R+1}^{\prime}\left(C R_{j}-C_{j}-A P_{j}\right)\right] .
$$

- $Q$ is the amount of production still needed in the current period to elininale infeasibilitics in the later period because the available capacity is not sufficient to meet the demands of those periods.


## Step 4.9

- Consider only items $i$ for which
i. $T<l_{1}$,
ii. $R C_{R}$ is sufficient to produce $x_{C, 3}$,

$$
\text { where } x_{c u n}=\min \left\{d_{i, k+f_{1},}, x_{n, y n+R}\right\} \text {, and }
$$

iii. $x_{\text {gan }}>0$.

To decide the best item (from a cost standpoint) to be produced in period $R$, calculate the priority index $\Delta_{r}$ for all of these items, where

$$
\mathrm{A}_{i}=\frac{A C\left(T_{i}+1\right)-A C\left(T_{i}\right)}{k_{r} d_{i} T_{i+1}} .
$$

- Armong these find the one, denoted by $i$, that has the smallest $\Delta_{1}$.


## Steps 4.10

- Let $W=k_{1} x_{\text {cap }}$.
- Compare the value of $Q$ with $W$.
(a) $\operatorname{If} Q>W$,

Increase the value of lot-size $x_{i j}$, inventory $l_{t}$ and $x_{\text {rem } r, h+i, i}$ by $x_{\text {can }}$, l.e., set

$$
\begin{aligned}
& x_{t i f}=x_{i d}+x_{c y m} \\
& I_{i j}^{\prime}=I_{y}^{\prime}+x_{d \omega T} \quad j=R+1, \ldots, R+T_{t} \\
& x_{\mathrm{rem}, ~, R+\pi}=x_{\mathrm{jcm} / R+T i}+x_{\mathrm{Cam}} .
\end{aligned}
$$

Decrease the value of lot-size $x_{t, j+7,}$, demand $d_{1, h+T,}$, remaining capacity $R C_{R}$ and $x_{\mathrm{rcm}}$ iR by $x_{\text {carr }}$ i.e., set

$$
\begin{aligned}
& x_{i, R+\gamma_{1}}=x_{d, R+T_{,}}, x_{c a n} \\
& d_{, R+T_{r}}=d_{1, R+T_{,}}, x_{c a n} \\
& R C_{R}=R C_{R}-x_{C A H} \\
& x_{\mathrm{rem} R R}=x_{\text {rem d }}-x_{\text {cur }} .
\end{aligned}
$$

Set $Q=Q-W$ and $T_{t}=T_{i}+1$, and continue from Step 4.9.
(b) If $Q \leq W$,

$$
\operatorname{Set} I Q=\left\lceil\frac{Q}{k_{1}}\right\rceil
$$

Increase the value of lot-size $x_{i n}$, inventory $I_{i /}$ and $\boldsymbol{r}_{\text {rem }} n_{i, R+T_{1}}$ by $I Q$, i.e., set

$$
\begin{aligned}
& x_{t R}=x_{i H}+I Q \\
& I_{H}^{\prime}=I_{i g}^{\prime}+I Q . \quad j=R+1, \ldots, R \mid \cdot T_{i}
\end{aligned}
$$

$x_{\text {rem } d, h+}+T_{i}=x_{\text {remin }, R \mid T_{\mathrm{r}}}+I Q$.

Decrease the value of lot-size $x_{1, R+\tau_{2}}$, demand $d_{t, k+i_{1}}$ and $x_{r e \pi / R}$ by $/ Q$, i.e., set

$$
\begin{aligned}
& x_{\mathrm{r}, R+r_{1}}=x_{\mathrm{r}, R \Omega U_{1}}-I Q \\
& d_{\mathrm{r}, R+T_{1}}=d_{\mathrm{r}, \mathrm{H}+\mathrm{T}_{1}}-I Q \\
& x_{\mathrm{r}: \mathrm{ma}, R}=x_{\mathrm{rcm} / R}-I Q
\end{aligned}
$$

## Step 4.11

- Set $R=R+1$.
- Check the value of $R$.
(a) If $R<H$, then continue from Step 4.3.
(b) If $R>H$, lot-sizing is complete up to period $/ I$ for $N^{\prime \prime}$ itens.


## Step 4.12

- Convert the $N^{\prime} \times H$ lot-sizing matrix into $N \times H$ Iot-sicing matrix by applying the formula

$$
x_{t-1}=\sum_{i-0}^{n_{1}} x_{i, t} .
$$

## Step 4.13

- Calculate the values of
i. Forecasted machine time tequited/period.
ii. Total expected selup cost.
iii. Total expected inventory holding cost.
iv. Total expected safety stock cost.
- Stop.


### 2.5 Computational Results with Real Life Data

The algorithm developed by Dixon and Silver [31] to generate feasible solution for multiitem single level capacitated tot-sizing problem was tested by a programming language in PC version. Thus a near optimal solution was obtained. The results are detailed in Section 2.5.1 below. This algorithm has been extended in the present work. The setup time and the upper limit on the lol-size have been included in the original algorithn. Thus the DixonSilver algorithm is separately extended with these two new parameters as deseribed in section 2.4. This section presents the results obtained from the modified models using a programming language in PC version. Section 2.5 .2 shows results with setup time consideration, and Section 2.5 .3 shows the results with upper bound on the limited lot-size.

### 2.5.1 Results of a Multi-item Single Level Capacitated Lot-sizing Problem

The Dixon-Silver algorithm has been used with real life data. Data has been collected from a renowned fumiture company. The products are fixed chairs. Twelve models of fixed chairs have been considered here, and these models are given in Figure 2.1. It is assumed that the entire production to meet demands is done in the plant and no subcontracting is permissible. Moreover, a furher assumption is made that plant capacity could not be increased.


Figure 2.1 Twelve models of fixed chairs that have been considered as sample product.

## Product data

The relevant product data (e.g., holding cost, setup cost, production rate, safety stock, initial inventory and ending inventory) has been depieted in Table 2.1 . The problem size has been restrieted at 12 products and 12 time periods; each time period corresponds to a month.

Table 2.1 Relevant product data for the particular machine.

| $\begin{gathered} \text { Item } \\ \text { No } \\ \text { in } \end{gathered}$ | Holding Cost $\left(h_{i}\right)$ | Setup Cost (S) | Production Rate ( $1 / k_{1}$ ) | Safety Stock (SSi) | Initial lnventory $\left(i n_{j}\right)$ | Ending Inventory (fentif) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 01 | 12.0 | 200.0 | 6 | 50 | 150 | 90 |
| 02 | 12.0 | 3000 | 5 | 60 | 100 | 120 |
| 03 | 12.0 | 3000 | 5 | 50 | 150 | 120 |
| 04 | 12.0 | 250.0 | 7 | 100 | 200 | 220 |
| 05 | 12.0 | 300.0 | 10 | 130 | 250 | 220 |
| 06 | 12.0 | 300.0 | 9 | 150 | 250 | 200 |
| 07 | 12.0 | 250.0 | 8 | 100 | 100 | 200 |
| 08 | 12.0 | 200.0 | 8 | 60 | 250 | 200 |
| 09 | 12.0 | 200.0 | 7 | 100 | 400 | 500 |
| 10 | 12.0 | 200.0 | 7 | 150 | 220 | 210 |
| 11 | 12.0 | 250.0 | 8 | 90 | 130 | 130 |
| 12 | 12.0 | 200.0 | 12 | 70 | 200 | 100 |

## 2. Product demand plant capacity

Product demands are quite seasonal and the same scasonal indices are used for all the products. Forecasted demand and the capacity of the machine are shown in Table 2.2. It has been assumed that the capacity per month is the total number of hours available per month. In this problem, Period 1 corresponds to the month of January, Period 2 corresponds to the month of February. Thus the machine capacity in Period I is the total production hours in January. There is two shifts ( 8 hours in each shif) in the factory. There is one hour for rest, tea etc in each shilt. There is six working days in a week. To be on the safe side, it has been assumed that there is some overtime in some month for overproduction due to higher denand. Also there is some holidays in some month for different festival. As for example, the machine capacity in Pcriod 2 is $14 \mathrm{hr} \times 24$ days $=330$ hours. Similarly the machine capacity for the other periods has been calculated.

Table 2.2 Forecasted demand and capacity of the hypothetical machine.

| $\begin{gathered} \text { Item } \\ \text { No } \\ \hline \end{gathered}$ | Period |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 01 | 90 | 60 | 80 | 80 | 90 | 80 | 70 | 75 | 60 | 60 | 50 | 50 |
| 02 | 80 | 70 | 80 | 80 | 75 | 90 | 90 | 80 | 80 | 60 | 60 | 50 |
| 03 | 100 | 60 | 60 | 50 | 80 | 80 | 90 | 100 | 90 | 120 | 80 | 150 |
| 04 | 180 | 165 | 125 | 150 | 200 | 180 | 120 | 150 | 145 | 240 | 220 | 220 |
| 05 | 200 | 190 | 280 | 260 | 200 | 210 | 200 | 130 | 120 | 240 | 240 | 210 |
| 06 | 400 | 240 | 245 | 250 | 230 | 200 | 230 | 205 | 145 | 380 | 255 | 190 |
| 07 | 450 | 350 | 350 | 380 | 340 | 360 | 400 | 450 | 450 | 400 | 450 | 350 |
| 08 | 200 | 250 | 250 | 200 | 150 | 160 | 190 | 100 | 250 | 100 | 250 | 100 |
| 09 | 500 | 500 | 450 | 400 | 450 | 500 | 400 | 400 | 700 | 450 | 700 | 110 |
| 10 | 350 | 250 | 220 | 225 | 120 | 130 | 130 | 145 | 115 | 204 | 200 | 150 |
| 11 | 300 | 200 | 200 | 100 | 160 | 100 | 130 | 100 | 90 | 140 | 120 | 90 |
| 12 | 150 | 95 | 95 | 100 | 100 | 90 | 75 | 75 | 60 | 130 | 105 | 90 |
|  | Forecasted Machine Requirements (hours) |  |  |  |  |  |  |  |  |  |  |  |
|  | 370 | 330 | 370 | 350 | 370 | 350 | 370 | 370 | 350 | 300 | 350 | 300 |

## 3. Equivalent demand schedule

An equivalent demand schedule is generated such that starting and conding inventory are accommodated. In addition, demands are adjusted such that in the heuristic solution, the inventery at the end of any period never drops below the safety stock level. Table 2.3 depicts the equivalent demand alter considering initial inventory, ending inventory and safety stock.

Table 2.3 Equivalent demand with the use of initial inventory, ending inventory and safety stock.

| Item | Period |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 01 | 0 | 50 | 80 | 80 | 90 | 80 | 70 | 75 | 60 | 60 | 50 | 90 |
| 02 | 40 | 70 | 80 | 80 | 75 | 90 | 90 | 80 | 80 | 60 | 60 | 110 |
| 03 | 0 | 60 | 60 | 50 | 80 | 80 | 90 | 100 | 90 | 120 | 80 | 220 |
| 04 | 80 | 165 | 125 | 150 | 200 | 180 | 120 | 150 | 145 | 240 | 220 | 340 |
| 05 | 80 | 190 | 280 | 260 | 200 | 210 | 200 | 130 | 120 | 240 | 240 | 300 |
| 06 | 300 | 240 | 245 | 250 | 230 | 200 | 230 | 205 | 145 | 380 | 255 | 240 |
| 07 | 450 | 350 | 350 | 380 | 340 | 360 | 400 | 450 | 450 | 400 | 450 | 450 |
| 08 | 10 | 250 | 250 | 200 | 150 | 160 | 190 | 100 | 250 | 100 | 250 | 240 |
| 09 | 200 | 500 | 450 | 400 | 450 | 500 | 400 | 400 | 700 | 450 | 700 | 510 |
| 10 | 280 | 250 | 220 | 225 | 120 | 130 | 130 | 145 | 115 | 204 | 200 | 210 |
| 11 | 260 | 200 | 200 | 100 | 160 | 100 | 130 | 100 | 90 | 140 | 120 | 130 |
| 12 | 20 | 95 | 95 | 100 | 100 | 90 | 75 | 75 | 60 | 130 | 105 | 120 |
|  | Forecasted Machine Requirements (huurs) |  |  |  |  |  |  |  |  |  |  |  |
|  | 370 | 330 | 370 | 350 | 370 | 350 | 370 | 370 | 350 | 300 | 350 | 300 |

## 4. Results

Table 2.4 shows the final lot-sizes and forecasted machine hour requirements for each period, and lable 2.5 shows the inventories at the end of each period for all items.

Table 2.4 Final lot-si/es and forceasted machine time requirements for Dixon-Silver heuristic.

| $\begin{aligned} & \text { Item } \\ & \text { No } \end{aligned}$ | Period |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 01 | 0 | 50 | 80 | 80 | 90 | 80 | 70 | 135 | 60 | 50 | 90 | 0 |
| 02 | 40 | 70 | 80 | 80 | 75 | 90 | 122 | 188 | 0 | 60 | 110 | 0 |
| 03 | 0 | 60 | 60 | 50 | 80 | 80 | 90 | 195 | 115 | 80 | 220 | 0 |
| 04 | 80 | 165 | 125 | 150 | 200 | 180 | 120 | 295 | 240 | 220 | 0 | 340 |
| 05 | 80 | 190 | 280 | 260 | 200 | 210 | 200 | 130 | 120 | 240 | 240 | 300 |
| 06 | 300 | 240 | 245 | 250 | 230 | 200 | 230 | 205 | 145 | 380 | 255 | 240 |
| 07 | 450 | 350 | 350 | 380 | 340 | 360 | 400 | 450 | 450 | 400 | 450 | 450 |
| 08 | 10 | 250 | 250 | 200 | 150 | 160 | 190 | 100 | 350 | 0 | 250 | 240 |
| 09 | 200 | 500 | 450 | 400 | 450 | 500 | 400 | 400 | 843 | 309 | 698 | 510 |
| 10 | 280 | 250 | 220 | 225 | 120 | 130 | 130 | 260 | 204 | 200 | 145 | 65 |
| 11 | 260 | 200 | 200 | 100 | 160 | 100 | 130 | 190 | 0 | 260 | 0 | 130 |
| 12 | 20 | 95 | 95 | 100 | 100 | 90 | 75 | 75 | 60 | 130 | 105 | 120 |
|  | Forecasted Machine Requirements (hours) |  |  |  |  |  |  |  |  |  |  |  |
|  | 221.0 | 318.6 | 318.0 | 297.2 | 291.1 | 291.3 | 288.7 | 3700 | 350.0 | 300.0 | 350.0 | 300.0 |

Table 2.5 lnventories at the end of each period for all items.

| $\begin{aligned} & \hline \text { Ittun } \\ & \mathrm{Nop} \end{aligned}$ | Period |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 01 | 60 | 50 | 50 | 50 | 50 | 50 | 50 | 110 | 110 | 100 | 140 | 90 |
| 02 | 60 | 60 | 60 | 60 | 60 | 60 | 92 | 200 | 120 | 120 | 170 | 120 |
| 03 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 145 | 170 | 130 | 270 | 120 |
| 04 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 245 | 340 | 320 | 100 | 220 |
| 05 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 220 |
| 06 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 200 |
| 07 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 200 |
| 08 | 60 | 60 | 60 | 60 | 60 | 60 | 60 | 60 | 160 | 60 | 60 | 200 |
| 09 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 243 | 102 | 100 | 500 |
| 10 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 265 | 354 | 350 | 295 | 210 |
| 11 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 180 | 90 | 210 | 90 | 130 |
| 12 | 70 | 70 | 70 | 70 | 70 | 70 | 70 | 70 | 70 | 70 | 70 | 100 |

Other results are tabulated below:

| 'Total available machine time ( $\sum_{t=1}^{\prime \prime} C_{t}$ ) | ; 4180.0 hour |
| :---: | :---: |
| Total setup time ( $\sum_{n=1}^{N} n_{\mathrm{r}} S t_{t}$ ) where $n_{r}$ is the number of setup for item $i$. | : 0.0 hour |
| Total forecasted machinc time | : 3695.9 hour |
| Total inventory holduingcost, $C_{i n v}=\sum_{\pi-1}^{*} \sum_{*-1}^{\prime \prime}\left(I_{t \prime}-S S_{1}\right): \mathrm{Tk} .49,332.00$ |  |
| Total expected safety-stock cost, $C_{s 7}=\sum_{u=1}^{N} S S_{\text {, }}$ | : Tk. 159,840,00 |
| Total expected setup cost, $C_{\text {sel }}=\sum_{i=1}^{N} n_{i} S$, | Tk. 32,850.00 |
| Total expected cost ( $\left.C_{\text {dnv }}+C_{s s}+C_{s e r}\right)$ | : Tk. 242,022.00 |

### 2.5.2 Results of Multi-Item Single Level Capacitated Lot-Sizing Problem with Setup Time

In the real life problem in Section 2.5 .1 machine setup time to produce each product itern is included. Relevant product data including setup time for each iten has been presented in Table 2.6. In the present work setup time has been taken from the factory. Use of the set up time would obviously be a more realistic approach. Forecasted demands and capacities as presented in Table 2.2 are also used in the present case. The equivalent demands after considering initial inventory, ending inventory and safcty stock are also same as presented in Table 2.3. The extended heuristic algorithm as developed in section 2.4 has been applied to the problem. Table 2.7 shows the final lot-sizes and forecasted machine hour requirements for each period, and Table 2.8 shows the inventories at the end of each period for all items.

Table 2.6 Relevant product data for the extended heuristic with setup time.

| $\begin{gathered} \text { Item } \\ \text { No } \\ \text { (o) } \\ \hline \end{gathered}$ | Holding Cost (b) | Sctup Cost (S) | Setup Time ( $\left.\mathrm{S}_{\mathrm{t}_{2}}\right)$ | Production Rate $\left(1 / h_{0}\right)$ | Salely Stuck ( $\mathrm{SS}_{i}$ ) | $\begin{gathered} \text { Initial } \\ \text { Inventory } \\ \left(I n_{i}\right) \end{gathered}$ | Ending Inventory (lend) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 01 | 12.0 | 200.0 | 0.50 | 6 | 50 | 150 | 90 |
| 02 | 12.0 | 300.0 | 0.50 | 5 | 60 | 100 | 120 |
| 03 | 12.0 | 300.0 | 0.50 | 5 | 50 | 150 | 120 |
| 04 | 12.0 | 250.0 | 0.33 | 7 | 100 | 200 | 220 |
| 05 | 12.0 | 300.0 | 0.25 | 10 | 130 | 250 | 220 |
| 06 | 12.0 | 300.0 | 0.33 | 9 | 150 | 250 | 200 |
| 07 | 12.0 | 250.0 | 0.25 | 8 | 100 | 100 | 200 |
| 08 | 12.0 | 200.0 | 0.50 | 8 | 60 | 250 | 200 |
| 09 | 12.0 | 200.0 | 0.33 | 7 | 100 | 400 | 500 |
| 10 | 12.0 | 200.0 | 0.50 | 7 | 150 | 220 | 210 |
| 11 | 12.0 | 250.0 | 0.50 | 8 | 90 | 130 | 130 |
| 12 | 12.0 | 200.0 | 0.33 | 12 | 70 | 200 | 100 |

Table 2.7 Final lot-sizes and forecasted machine time requirements for the extended heuristic with setup time.

| $\begin{array}{\|c} \hline \text { Item } \\ \text { No } \\ \hline \end{array}$ | Period |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1. | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 01 | 0 | 50 | 80 | 80 | 90 | 80 | 70 | 135 | 60 | 50 | 90 | 0 |
| 02 | 40 | 70 | 80 | 80 | 75 | 90 | 170 | 140 | 0 | 170 | 0 | 0 |
| 03 | 0 | 60 | 60 | 50 | 80 | 80 | 163 | 218 | 99 | 0 | 220 | 0 |
| 04 | 80 | 165 | 125 | 150 | 200 | 180 | 120 | 295 | 240 | 220 | 0 | 340 |
| 05 | 80 | 190 | 280 | 260 | 200 | 210 | 200 | 130 | 120 | 240 | 240 | 300 |
| 06 | 300 | 240 | 245 | 250 | 230 | 200 | 230 | 205 | 145 | 380 | 255 | 240 |
| 07 | 450 | 350 | 350 | 380 | 340 | 360 | 400 | 450 | 450 | 400 | 450 | 450 |
| 08 | 10 | 250 | 250 | 200 | 150 | 160 | 190 | 100 | 350 | 0 | 250 | 240 |
| 09 | 200 | 500 | 450 | 400 | 450 | 500 | 400 | 400 | 825 | 325 | 700 | 510 |
| 10 | 280 | 250 | 220 | 225 | 120 | 130 | 130 | 260 | 204 | 200 | 175 | 35 |
| 11 | 260 | 200 | 200 | 100 | 160 | 100 | 130 | 190 | 0 | 159 | 101 | 130 |
| 12 | 20 | 95 | 95 | 100 | 100 | 90 | 75 | 75 | 60 | 130 | 105 | 120 |
|  | Forceasted Machine Requirements (hours) |  |  |  |  |  |  |  |  |  |  |  |
|  | 224.8 | 323.5 | 322.9 | 302.0 | 296.0 | 296.1 | 317.7 | 369.9 | 348.0 | 299.5 | 349.2 | 298.9 |

Table 2.8 Inventories for the heuristic with setup time.

| Itanl | Period |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{N} \mathbf{0}$ | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ | $\mathbf{1 0}$ | $\mathbf{1 1}$ | $\mathbf{1 2}$ |
| $\mathbf{0 1}$ | 60 | 50 | 50 | 50 | 50 | 50 | 50 | 110 | 110 | 100 | 140 | 90 |
| $\mathbf{0 2}$ | 60 | 60 | 60 | 60 | 60 | 60 | 140 | 200 | 120 | 230 | 170 | 120 |
| $\mathbf{0 3}$ | 50 | 50 | 50 | 50 | 50 | 50 | 123 | 241 | 250 | 130 | 270 | 120 |
| $\mathbf{0 4}$ | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 245 | 340 | 320 | 100 | 220 |
| $\mathbf{0 5}$ | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 220 |
| $\mathbf{0 6}$ | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 200 |
| $\mathbf{0 7}$ | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 200 |
| $\mathbf{0 8}$ | 60 | 60 | 60 | 60 | 60 | 60 | 60 | 60 | 160 | 60 | 60 | 200 |
| $\mathbf{0 9}$ | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 225 | 100 | 100 | 500 |
| $\mathbf{1 0}$ | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 265 | 354 | 350 | 325 | 210 |
| $\mathbf{1 1}$ | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 180 | 90 | 109 | 90 | 130 |
| $\mathbf{1 2}$ | 70 | 70 | 70 | 70 | 70 | 70 | 70 | 70 | 70 | 70 | 70 | 100 |

The following results have also been found aller applying the heuristic algorithm with setup time.

Table 2.9 Time and cost after applying the heuristic algorithm with setup time.


### 2.5.3 Results with the Limited Lot-Size per Setup

Kelevant product data including the limited lot-size per setup for cach item has been depicted in Table 2.10. The limited lot-size per setup for each item has been taken arbitrarily. The demands and capacitics are extracted from Table 2.2. The equivalent demands after considering initial inventory, ending inventory and safety stock are extracted From Table 2.3. To illustrate the algorithm a few sample calculations for the period 8 have been shown. Forecasted demand and capacity with limited lot size per setup are depicted in Iable 2.11.

Table 2.13 shows the final lot-sizes and forecasted machine hour requirements for each period, and Table 2.14 shows the inventories at the end of each period for all items.

Table 2.10 Relevant Product data for the heuristic with the limited lot-size per setup.

| Itemn <br> No | Holding <br> Cost | Setup <br> Cost | Maxinum <br> Lot-Size | Production <br> Rate | Safery <br> Stock | Initial <br> Inventory | Ending <br> Inventory |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{0 1}$ | 12.0 | 200.0 | 150 | 6 | 50 | 150 | 90 |
| $\mathbf{0 2}$ | 12.0 | 300.0 | 150 | 5 | 60 | 100 | 120 |
| 03 | 12.0 | 300.0 | 150 | 5 | 50 | 150 | 120 |
| $\mathbf{0 4}$ | 12.0 | 250.0 | 150 | 7 | 100 | 200 | 220 |
| $\mathbf{0 5}$ | 12.0 | 300.0 | 200 | 10 | 130 | 250 | 220 |
| 06 | 12.0 | 300.0 | 200 | 9 | 150 | 250 | 200 |
| $\mathbf{0 7}$ | 12.0 | 250.0 | 200 | 8 | 100 | 100 | 200 |
| $\mathbf{0 8}$ | 12.0 | 200.0 | 200 | 8 | 60 | 250 | 200 |
| $\mathbf{0 9}$ | 12.0 | 200.0 | 200 | 7 | 100 | 400 | 500 |
| $\mathbf{1 0}$ | 12.0 | 200.0 | 200 | 7 | 150 | 220 | 210 |
| $\mathbf{1 1}$ | 12.0 | 250.0 | 200 | 8 | 90 | 130 | 130 |
| $\mathbf{1 2}$ | 12.0 | 200.0 | 200 | 12 | 70 | 200 | 100 |

The maximum periodic demand for itcon 9 is

$$
\begin{aligned}
d_{\max 9} & =\max \left\{d_{1, j} \mid j=1,2, \ldots, H\right\} \\
& =\max \{200,500,450,400,450,500,400,400,700,450,700,510\} \\
& =700
\end{aligned}
$$

The limited lot-size for item 9 is $x_{\max }=200$.

Then the number of new items to $b c$ considered to satisfy demand $d_{\text {max }}$ is

$$
n_{1}=\left\lceil\frac{d_{\max 9}}{x_{\max 9}}\right\rceil-1=\left\lceil\frac{700}{200}\right\rceil-1=4-1=3
$$

Similarly, the number of new items to be considered to satisfy demands $d_{\text {max }}$ are

| $n_{1}$ | $n_{2}$ | $n_{3}$ | $n_{4}$ | $n_{5}$ | $n_{6}$ | $n_{7}$ | $n_{8}$ | $n_{9}$ | $n_{10}$ | $n_{11}$ | $n_{12}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 1 | 2 | 1 | 1 | 2 | 1 | 3 | 1 | 1 | 0 |

Then the number of total items alter limiting the lot-size is

$$
N^{\prime}=N+\sum_{-121}^{N} n_{t}=12+13=25
$$

Item 9 is spiitted into $n_{1}+1=4$ items. Let the new items are $9_{0}, 9_{1}, \ldots, 9_{3}$.
Continue the same calculation for other demands. From 'Iable 2.3, the new demand matrix for $N^{\prime}=25$ items can be obtained as shown in Table 2,11.

Table 2.11 Demand after considering limitation on the naximum allowable lot-size.

| $\begin{array}{\|c} \hline \text { Item } \\ \text { No } \\ \hline \end{array}$ | Period |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| $\mathrm{Ot}_{0}$ | 0 | 50 | 80 | 80 | 90 | 80 | 70 | 75 | 60 | 60 | 50 | 90 |
| 020 | 40 | 70 | 80 | 80 | 75 | 90 | 90 | 80 | 80 | 60 | 60 | 110 |
| ${ }^{03} 3_{0}$ | 0 | 60 | 60 | 50 | 80 | 80 | 90 | 100 | 90 | 120 | 80 | 150 |
| $0_{40}$ | 80 | 150 | 125 | 150 | 150 | 150 | 120 | 150 | 145 | 150 | 150 | 150 |
| $0_{0}$ | 80 | 190 | 200 | 200 | 200 | 200 | 200 | 130 | 120 | 200 | 200 | 200 |
| ${ }^{06} 0$ | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 145 | 200 | 200 | 200 |
| ${ }^{07} 0$ | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 |
| $08_{0}$ | 10 | 200 | 200 | 200 | 150 | 160 | 190 | 100 | 200 | 100 | 200 | 200 |
| $w_{0}$ | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 |
| 100 | 200 | 200 | 200 | 200 | 120 | 130 | 130 | 145 | 115 | 200 | 200 | 200 |
| $11_{0}$ | 200 | 200 | 200 | 100 | 160 | 100 | 130 | 100 | 90 | 140 | 120 | 130 |
| 120 | 20 | 95 | 95 | 100 | 100 | 90 | 75 | 75 | 60 | 130 | 105 | 120 |
| $0^{031}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 70 |
| $0^{04}$ | 0 | 15 | 0 | 0 | 50 | 30 | 0 | 0 | 0 | 90 | 70 | 150 |
| 042 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 40 |
| ${ }^{05} 1$ | 0 | 0 | 80 | 60 | 0 | 10 | 0 | 0 | 0 | 40 | 40 | 100 |
| 061 | 100 | 40 | 45 | 50 | 30 | 0 | 30 | 5 | 0 | 180 | 55 | 40 |
| ${ }^{87} 1$ | 200 | 150 | 150 | 180 | 140 | 160 | 200 | 200 | 200 | 200 | 200 | 200 |
| 072 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 50 | 50. | 0 | 50 | 50 |
| $\mathrm{OS}_{1}$ | 0 | 50 | 50 | 0 | 0 | 0 | 0 | 0 | 50 | 0 | 50 | 40 |
| ${ }^{09} 1$ | 0 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 |
| $0^{09}$ | 0 | 100 | 50 | 0 | 50 | 100 | 0 | 0 | 200 | 50 | 200 | 110 |
| 093 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 100 | 0 |
| $\mathrm{ta}_{1}$ | 80 | 50 | 20 | 25 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 10 |
| 111 | 60 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Initialice setup cost, holding cost and production cate for the ilems $9_{0}, 9_{1}, 9_{2}$ and $9_{3}$ from that of the item 9 as follows.

$$
\begin{aligned}
& S_{9_{0}}=S_{9_{1}}=S_{9_{2}}=S_{9_{3}}=S_{9}=200.0, \\
& h_{9_{0}}=h_{9_{1}}=h_{9_{2}}=h_{9_{3}}=h_{9}=12.0, \\
& k_{9_{0}}=k_{9_{1}}=k_{9_{2}}=k_{9_{3}}=k_{9}=1 / 7 .
\end{aligned}
$$

Similarly set the value of setup cost, holding cost and production rate for the $N^{\prime}=25$ new items from those of the $\mathrm{N}=12$ items.

| $\underset{\substack{\text { Item } \\ N_{0}}}{\substack{\text { n }}}$ | Holding Cost | Selup Cost | Production Rate |
| :---: | :---: | :---: | :---: |
| $0_{0}$ | 12.0 | 200,0 | 6 |
| $02_{0}$ | 12.0 | 300.0 | 5 |
| ${ }^{03} 0$ | 12.0 | 3000 | 5 |
| 040 | 12.0 | 250.0 | 7 |
| $0_{0}$ | 12.0 | 300.0 | 10 |
| $0_{0}$ | 12.0 | 300.0 | 9 |
| ${ }^{07} 0$ | 12.0 | 250.0 | 8 |
| ${ }^{08} 0$ | 12.0 | 200.0 | 8 |
| $0_{09}$ | 12.0 | 200.0 | 7 |
| $\mathrm{LO}_{0}$ | 12.0 | 200.0 | 7 |
| $\mathrm{ti}_{0}$ | 12.0 | 250.0 | 8 |
| 12.10 | 12.0 | 200.0 | 12 |
| ${ }^{03} 3_{1}$ | 12.0 | 300.0 | 5 |
| ${ }^{04} 1$ | 12.0 | 250.0 | 7 |
| $04_{2}$ | 12.0 | 250.0 |  |
| 051 | 12.0 | 300.0 | 10 |
| $0_{1}$ | 12.0 | 300.0 | 9 |
| ${ }^{07}{ }_{1}$ | 12.0 | 250.0 | 8 |
| $0^{07}$ | 12.0 | 250.0 | 8 |
| ${ }^{08} 1$ | 12.0 | 200.0 | 8 |
| $0_{09}$ | 12.0 | 200.0 | 7 |
| $0_{2}$ | 12.0 | 200.0 | 7 |
| 093 | 12.0 | 200.0 | 7 |
| ${ }^{10} 1$ | 12.0 | 200.0 | 7 |
| $11_{1}$ | 12.0 | 2500 | 8 |

Now apply the modified Dixon-Silver heuristic with the limited lot-size for 25 items. The lot sizes for the new items are shown in Table 2.12.

Table 2.12 Lot sizes for $N^{\prime}=25$ items.

| $\begin{array}{\|c} \hline \text { Item } \\ \text { No } \\ \hline \end{array}$ | Period |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11. | 12. |
| ${ }^{010}$ | 50 | 150 | 150 | 0 | 150 | 0 | 150 | 0 | 0 | 45 | 90 | 0 |
| $0^{0} 0$ | 110 | 150 | 150 | 0 | 150 | 0 | 45 | 0 | 150 | 50 | 110 | 0 |
| ${ }^{03} 3_{0}$ | 120 | 0 | 50 | 0 | 150 | 150 | 50 | 0 | 150 | 150 | 0 | 140 |
| $0^{04}$ | 150 | 150 | 150 | 55 | 150 | 150 | 150 | 120 | 150 | 150 | 150 | 145 |
| 050 | 200 | 200 | 200 | 70 | 200 | 200 | 200 | 130 | 200 | 200 | 200 | 120 |
| ${ }^{06} 0$ | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 145 |
| ${ }^{17} 7_{0}$ | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 |
| $\mathrm{08}_{0}$ | 10 | 200 | 200 | 200 | 200 | 200 | 200 | 0 | 200 | 100 | 200 | 200 |
| ${ }^{09} 0$ | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 |
| $10_{0}$ | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 40 | 0 | 200 | 200 |
| ${ }^{11} 0$ | 200 | 200 | 200 | 200 | 200 | 200 | 0 | 200 | 20 | 120 | 130 | 0 |
| $12_{0}$ | 200 | 110 | 0 | 200 | 0 | 200 | 0 | 0 | 200 | 35 | 120 | 200 |
| $0_{1}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 70 | 0 |
| $\mathrm{va}_{1}$ | 15 | 0 | 0 | 80 | 0 | 0 | 0 | 0 | 150 | 10 | 150 | 150 |
| 042 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 40 | 0 |
| $05_{1}$ | 0 | 140 | 0 | 0 | 10 | 0 | 0 | 0 | 80 | 0 | 100 | 0 |
| $0_{1}{ }_{1}$ | 200 | 0 | 35 | 0 | 30 | 35 | 0 | 0 | 200 | 75 | 0 | 0 |
| ${ }^{07}{ }_{1}$ | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 0 | 180 |
| 072 | 50 | 0 | 0 | 0 | 0 | 0 | 50 | 0 | 50 | 100 | 0 | 0 |
| ${ }^{08} 1$ | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 50 | 0 | 90 | 0 | 0 |
| ${ }^{09} 1$ | 0 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 200 |
| $09_{2}$ | 150 | 0 | 0 | 150 | 0 | 0 | 0 | 200 | 50 | 0 | 200 | 110 |
| 093 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 100 | 0 | 0 |
| ${ }^{10} 1$ | 175 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 10 | 0 |
| 111 | 60 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Convert the $N^{\prime} \times H$ lot-sizing matrix into $N \times H$ lot-sizing matrix by applying the fommula $x_{i, j}=\sum_{i=0}^{p} x_{t, i}$.

As an example let us compute $x_{9,8}$.

$$
\begin{aligned}
x_{9,8} & =\sum_{l=0}^{n_{1}} x_{9_{i}, 8} \\
& =\sum_{l=0}^{3} x_{9_{t}, 8} \\
& =x_{9_{0,8}}+x_{9_{1}, 8}+x_{9_{2}, 8}+x_{9_{3}, 8} \\
& =200+200+200+100 \\
& =700 .
\end{aligned}
$$

Table 2.13 Final lot-sizes and forecasted machine time requirements for the heuristic with the limited lot-size per setup.

| $\begin{array}{\|c\|} \hline \text { Itrm } \\ \mathrm{No} \\ \hline \end{array}$ | Period |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 01 | 50 | 150 | 150 | 0 | 150 | 0 | 150 | 0 | 0 | 45 | 90 | 0 |
| 02 | 110 | 150 | 150 | 0 | 150 | 0 | 45 | 0 | 150 | 50 | 110 | 0 |
| 03 | 120 | 0 | 50 | 0 | 150 | 150 | 50 | 0 | 150 | 150 | 70 | 140 |
| 04 | 165 | 150 | 150 | 135 | 150 | 150 | 150 | 120 | 300 | 160 | 340 | 295 |
| 05 | 200 | 340 | 200 | 70 | 210 | 200 | 200 | 130 | 280 | 200 | 300 | 120 |
| 06 | 400 | 200 | 235 | 200 | 230 | 235 | 200 | 200 | 400 | 275 | 200 | 145 |
| 07 | 450 | 400 | 400 | 400 | 400 | 400 | 450 | 400 | 450 | 500 | 200 | 380 |
| 08 | 110 | 200 | 200 | 200 | 200 | 200 | 200 | 50 | 200 | 190 | 200 | 200 |
| 09 | 350 | 400 | 400 | 550 | 400 | 400 | 400 | 700 | 450 | 500 | 600 | 510 |
| 10 | 375 | 200 | 200 | 200 | 200 | 200 | 200 | 200 | 44 | 0 | 210 | 200 |
| 11 | 260 | 200 | 200 | 200 | 200 | 200 | 0 | 200 | 20 | 120 | 130 | 0 |
| 12 | 200 | 110 | 0 | 200 | 0 | 200 | 0 | 0 | 200 | 35 | 120 | 200 |
|  | Forecasted Machine Requirements (hours) |  |  |  |  |  |  |  |  |  |  |  |
|  | 365.1 | 327.5 | 318.3 | 272.3 | 338.7 | 299.9 | 274.6 | 262.2 | 346.3 | 296.5 | 343.8 | 288.8 |

Table 2.14 Inventories for the heuristic with the limited lot-size per sctup.

| Item | Period |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{N} \mathbf{0}$ | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ | $\mathbf{1 0}$ | $\mathbf{1 1}$ | $\mathbf{1 2}$ |
| $\mathbf{0 1}$ | $\mathbf{1 1 0}$ | 200 | 270 | 190 | 250 | 170 | 250 | 175 | 115 | 100 | 140 | 90 |
| $\mathbf{0 2}$ | 130 | 210 | 280 | 200 | 275 | 185 | 140 | 60 | 130 | 120 | 170 | 120 |
| $\mathbf{0 3}$ | 170 | 110 | 100 | 50 | 120 | 190 | 150 | 50 | 110 | 140 | 130 | 120 |
| $\mathbf{0 4}$ | 185 | 170 | 195 | 180 | 130 | 100 | 130 | 100 | 255 | 175 | 295 | 370 |
| $\mathbf{0 5}$ | 250 | 400 | 320 | 130 | 140 | 130 | 130 | 130 | 290 | 250 | 310 | 220 |
| $\mathbf{0 6}$ | 250 | 210 | 200 | 150 | 150 | 185 | 155 | 150 | 405 | 300 | 245 | 200 |
| $\mathbf{0 7}$ | 100 | 150 | 200 | 220 | 280 | 320 | 370 | 320 | 320 | 420 | 170 | 200 |
| $\mathbf{0 8}$ | 160 | 110 | 60 | 60 | 110 | 150 | 160 | 110 | 60 | 150 | 100 | 200 |
| $\mathbf{0 9}$ | 250 | 150 | 100 | 250 | 200 | 100 | 100 | 400 | 150 | 200 | 100 | 500 |
| $\mathbf{1 0}$ | 445 | 395 | 375 | 350 | 430 | 500 | 570 | 625 | 554 | 350 | 360 | 410 |
| $\mathbf{1 1}$ | 90 | 90 | 90 | 190 | 230 | 330 | 200 | 300 | 230 | 210 | 220 | 130 |
| $\mathbf{1 2}$ | 400 | 415 | 320 | 420 | 320 | 430 | 355 | 280 | 420 | 325 | 340 | 450 |

The following results have also been found after applying the heuristic algorithin with the limited lot-size per setup.


The results of three models have been summarized below.

| Parameter | Dixon \& Silver | With Set up <br> Time | With Limited <br> Lot-sise |
| :--- | ---: | ---: | ---: |
| Total available machine <br> time | 4180.0 hr | 4180.0 hr | 4180.0 hr |
| Total forecasted <br> machinc time | 3695.9 hr | 3748.4 hr | 3734.0 hr |
| Total Sct-up time <br> requirements | 0.0 hr | 52.5 hr | 0.0 hr |
| Total inventory holding <br> cost | Tk.49,332.00 | Tk.53,124.00 | Tk.227,208.00 |
| Total safety stock cost | Tk.159,840.00 | Tk.159,840.00 | Tk.159,840.00 |
| Total selup cost | Tk.32,850.00 | Tk.32,500.00 | Tk.44,350.00 |
| Total expected cost | Tk.242,022.00 | Tk.245,464.00 | Tk.431,398.00 |

The inclusion of setup time will result in machine occupation time to be increased. The consideration of set up time also led to increase in inventory holding cost. This increase in cost could be attributed to increased inventory held for meeting demand of the later period,

Effect of the limitation on the lot-size is dependent on the extent of reduction of the lot-size. It is obvious that the smaller the allowable lot-sice, the greater will be the number of setup which will eventually lead to more splitted items. This in tum led to the increase number of required setups.

Costs due to implementation of this restriction on lot-sice went up quite significantly. Further decrease in lot-size would obviously result in higher costs. But al the lower range of allowable lot-size, there has been a trend of slight increase in setup costs.

### 2.6 Conclusions

Lot-sizing problem has been recognized to be one of most important functions in industrial units. Thus efforts have been given to develop usable optimizing routines but within limited boundary conditions. Various models have been developed with restricted applications in real-life settings because of their demanding computational enormisty. Thus heuristic models have been evolved. These heuristics have given feasible solutions. The Dixon-Silver heuristic was used in the present work. The heuristic was extended to include two very important parameters such as, (i) plant or machine set up time and (ii) maximum limit of production lot-size from a machinc. From analysis and results, the present wotk has demonstrated that feasible solutions could be obtained with competitive computer usage. The results of the two heuristics developed in the present work, have been discussed in Section 2.5.

## Chapter 3 Scheduling

### 3.1 Introduction

Operations schedules are short-term plans designed to implement the master production schedule. Operations scheduling focuses on how best to use existing capacity, taking into account technical production constraints. Oficn scveral jobs must be processed at one or more workstations. Typically, a variety of tasks can be performed at cach workstation. If schedules are not carefully planned to avoid botllenecks, waiting lines may develop. In poorly scheduled job shops, it is not at all uncommon for jobs to wait for 95 percent of their total production cycle. This results in a long workllow cycle. A schedule is a timetable for performing activities, utilizing resources, or allocating facilities.

Most real-world scheduling problems are naturally multi-criterion. However, due to the lack of suitable solution techniques such problems are usually transformed into a singleobjective problem. A solution is called Pareto-optimal if it is not possible to decrease the value of one objective without increasing the value of the other [34]. The difficulty that arises with this approach is the rise of a set of Parcto-optimal solutions, instead of a single optimum solution.

A Pareto-optimal solution is developed in this research work for a scheduling problem on a single machine with periodic maintenance and non-preemplive jobs. In literature, most of the scheduling problems address only one objective function, while in the real world, such problems are always associated with more than one objective. In this research work, both multi-objective functions and multi-maintenance periods are considered for the machine scheduling problem. To avoid the complexities involved in solving an explicit multiobjective optimization problem, mulliple objective functions anc consolidated and transformed into a single objective function alter they are weighted and assigned proper weighting factors. In addition, periodic maintenance schedules are also considered in the model. The objective of the model addressed in this research work is to minimize the
weighted function of the total job flow time, the maximum tardiness, and the machine idle time in a single machine problem with periodic maintenance and non-preemptive jobs. An algorithm is developed to solve this multiple criterion problem and to construct the paretoset. The parametric analysis of the trade-offs of all solutions with all possible weighted combination of the criterions is analyzed. The result of a neighborhood search heuristic is also provided. Results are provided to explore the best schedule among all the Paretooptimal sets and to compare the result of the modified Parcto-optimal algorithm with the result of the neighborhood search heuristic.

### 3.2 Literature Study

Most real-world scheduling problems are naturally multi-criterion. However, due to the lack of suitable solution techniques such problems are usually transformed into a singleobjective problem. A solution is called Pareto-optimal if it is not possible to decrease the value of one objective without increasing the value of the other [34]. The difficulty that arises with this approach is the rise of a set of Pareto-optimal solutions, instead of a single optimum solution.

There are several approaches that deal with the multi-objective problems. Traditionally, the most common way is to combine the multiple criterions into a single scalar value by using weighted aggregating functions according to the preferences sel by the scheduler (or decision-makers) and then to find a compromise solution that reflects these preferences |35]. However, in many real scenarios involving multi-criterion scheduling problems, it is prefcrable to present a set of promising solutions to the decision-makers so that the most adequale schedule can be chosen. This has increased the interest in investigating the application of Pareto-optimization techniques to multi-criterion scheduling problems. The aim in Pareto-optimization is to find a sct of compromised solutions that represent a good approximation to the Pareto-optimality [34]. In recent years, several algorithms proposed for Parcto-optimization have been published because multi-objective optimization problems
exist in almost any domain [36, 37]. The job shop scheduling problem (JSP) with a single objective is a widely reseatched problem in the area of production scheduling. In a job shop, several jobs require scheduling, each with different processing times on different machines. Many applications of JSPs in industry have been discussed in the literature. Operations rescarch practitioners, production management experts, management scientists, mathematicians and computer scientists have discussed the scheduling theory. The solution procedure for solving the JSP diflers as the objective of the scheduling differs. Most of the rescarchers conceming the job shop scheduling problem have focused on developing scheduling algorithms for a single objective measure. Much work has been done to solve ISPs by using single objective meta-heuristic procedures like simulated annealing algorithm, genetic algorithm and tabu search algorithon. These algorithms are generic optimization algorithms, i.c. they are intended for use on a wide range of optimization problems [38]. The real-work scheduling problems are multi-objective in nature. In such cases, several objectives are considered simultancously when a schedule is generated. Simultancous consideration of several objectives during scheduling totally modilies the scheduling approach. A scheduler who improves the schedule with respect to one objective may want to know how the schedule performs with respect to the other objectives. Thus the goal is to generate a fcasible schedule that minimizes several objectives. This schedule is called a Pareto optimal solution. A single feasible schedule that minimizes several objectives may not exist. In other words, individual optimal solutions of cach objective are usually different. Under such situations, the scheduler may be interested in having a schedule with weighted combination of several scheduling objectives as the performance measure. It is possible that the weights of various objectives are known before scheduling. This approach [38] permits computing of a unique strict Parcto optimal solution. It is also possible that the decision maker wants to choose a Pareto optimal solution according to the prioritics cxisting at the time of decision making. In that case, a family of best trade-off schedules called the Pareto optimal set is to be found. The set of Pareto solutions is called the Pareto front. Therefore solving a multi-objective scheduling problem is a Parcto optimization problem. Generating the Parcto optimal sel for the scheduling problem can be
computationally expensive and is often infeasible, because of the complexity of the scheduling problem [38]. Moreover, when meta-heuristics are used, there is no gurantee that the Pareto set for a given multi-objective oplimization problem like multi-objective scheduling can be gencrated. However, a sel of non-dominated solutions can be generated close to the Pareto optimal set [38]. Many real-world optimization problems involve multiple (and ofien conflicting) objectives. These problems are relevant in a varicty of engincering disciplines, scientific lields, and various industrial applications. Unlike single objective optimization problens, where one attempts to find the best solution (global optimum), in multi objective optimization problems, there may not exist one solution that corresponds to the best with respect to all objectives. Solving a multi-objective optimization problem consists of generating the Pareto fronticr, the set of non-dominated solutions that represents the irade-off among the objective function values. Different approaches are used to approximate and generate such sets of Parcto optimal solutions. Some interactive approaches incorporate preferences into the optimization procedure to explore a specilic region of the solution space, while other approaches focus on generating diverse sets of Pareto optimal solutions. Such sets of Pareto optimal solutions can be extremely large. which motivates the need for post-optimality analysis for multi objective optinization problems. The area of post-optimality analysis addressed in this paper foctses on obtaining a preferred subset of solutions from a very large set of solutions with weeptable objective function values. The goal in obtaining large sets of Pareto optimal solutions is to provide the decision-maker with a diverse set of such solutions. Although obtaining diverse Parcto optimal solutions is imporant, it is oflen impractical for a human decision-maker to manually examine each such solution, and hence, efficiently identify a good subset of such solutions. Previous research in this area has focused on generalizing the representation of the full set of Pareto optimal solutions with a smaller subset [39]. Such procedures are not post-optimality analysis procedures, but rather, extensions to multi-objective optimization procedures, which are designed to generate diverse sels of Pareto optimal solutions. Another area of rescarch that incorporates preferences into the optimization procedures are interactive methods. These interactive methods provide a decision-maker with better control
over the optimization process, allowing them to explore specilic regions of the search space. However, solutions obtained are quite sensitive towards the prelerences of the decisionmaker. These approaches also require the decision-maker to have a thorough knowledge of the problern. This paper [39] analyzes a discrete optimization problem formulation for obtaining a preferred subset of Pareto optimal solutions from a larger sct. This formulation alleviates the sensitivity of value function approaches, while obtaining a desired size subsct of Pareto optimal solutions [39]. In recent years, several variations of multi objective cyolutionary algorithms (MOEAs) [40] have been developed to handle MOPs [35]. Many of the suggested MOEAs have been employed in a variety of real-world applications [40]. These next generation algorithms have been improved in three dimensions compared to the previous generation of MOEAs introduced in the 1990's, which include the first (origingl) version of the non dominated sorling genetic algorithm (NSGA) of Srinivas and Deb (1994), the niched Pareto genetic algorithm (NPGA) of Nafploitis ct al. (1994) and the multi objective genetic algorithm (MOGA) of Fonseca and Flemming (1993). First, the compulational complexity of the existing MOFAs has been reduced from $O(m N 3)$ of the lirst generation to $O(m N 2)$ of the second generation so that solving larger-sized problems is not as computationally burdensome. [40]. The $m$ and $N$ are the number of objectives and the population size, respectively. Second, some degree of elitism is incorporated in most MOEAs to ensure the propagation of good non dominated solutions for faster convergence. In expensive MOPs, 「ast convergence towards Pareto optimal solutions is a highly desired feature of any promising algorithm. Third, new diversification slrategies that are insensitive to the selection of the sharing factor have been employed. Given the variations of MOEAs, the idea of using dynamic population sizing has not been thoroughly investigated, and to date only a fow studics have exploted this idea. For example, Tan et al. (2001) introduced an increment in MOEA that uses dynamic population sizing based on the online discovered Parcto front and ats desired population distribution density [40]. In another study, Shen and Daskin (2005) suggest a MOEA-based heuristic approach for finding tradeoffs between customer service and cost in an integrated supply chain design using a dynamic population siaing scheme. However, they do not address how the growing poputation size is controlled.

The related work of Farina et al. (2004) addresses dynamic MOPs, where the optimication is time-dependent and the objective functions, the constraints and/or the parameters of the problem, not the MOEA, vary with time (i.e., at each iteration of the optimigation process). In this study [40], considering static MOPs, where optimization using FPGA is performed offline, and the characteristics of the MOP are not time-dependent. The majority of evolutionary multi objective optimization (EMO) studies that propose new MOEAs for solving MOPs evaluate the performance of those algorithms over a large number of generations (or solution evaluations). However, there is now a growing need for designing MOEAs capable of dealing with computationally- and/or linancially-expensiveMOPs. Litle work exists that considers expensive MOPs. Additionally, many real-world problems involve complicated, "black-box" objective functions that can make a large number of solutions evaluations computationally prohibitive [40]. Furlhermore, repeatedly evaluating such complicated objective functions can be demanding on resources. Specifically, the motivation comes from simulation-based optimization research. Computer simulation of real-world systems tends to involve the construction of complicated models that capture the complex, nonlinear interrelationships between independent and dependent variables and can repor the value of several system performance objectives simultancously. These models [40] are used to evaluate candidate system design solutions in search of the best solution (or set of solutions) according to several performance objectives.

A inulti-objective optimization algorithm capable of rapidly finding a diverse set of Pareto optimal solutions would be greatly benclicial in such a situation. The purpose of this research is to propose a multi-objective optimization methodology that finds evenlydistributed Parcto optimal solutions in a computationally-efficient manner. In addition to multiple objectives, periodic maintenance is also considered for this scheduling problem. An uncxpected breakdown will make the shop behavior hard to predict, and thereby will reduce the efficiency of the production system. Maintenance can reduce the breakdown rate with minor sacrifices in production [41].

In literature, there are several approaches for handling multi-criterion problems. Branch and Bound technique is one of those approaches that could obtain a better solution for such problems. Branch and bound technique explores all the possible enumerations to lind the best sequence with minimum value in $O\left(2^{\prime \prime}\right)$ time complexity [42]. Liao and Chen [41] address minimizing the maximun bardiness of jobs in a periodically maintained single machine problem. A branch and bound algorithm is developed to find the optimal solution, and a heuristic solution is also devised for handling the large problem. The larger is the neighborhood, the bether is the quality of the locally optimal solutions, and the greater is the accuracy of the final solution. At the same time, searching larger neighborhoods requires more time at each stage. Because of many runs of a neighborhood search algorithm, longer execution times per run lead to fewer runs within a specified time. For this reason, a larger neighborhood can produce a more effective heuristic algorithm only if the larger neighborhood can be searched in a very efficient manner. A surycy of large-scale neighborhood search algorithms can be found in Ahuja [43]. For the single-machine problem, Adiri [44] assumes two cases of a breakdown, that is, the resumable and nonresumable cases assuming that machine idle time is unknown and follow a probabilistic distribution pattern. Mosheiov [45] solves the minimization of total completion time for two-parallel-machine-scheduling problem by assuming cach machite is available in a specified interval. Lee [46] also studies in this area for other machine configurations including single and parallel machines.

Problem of scheduling on a single machine to minimize total weighted tardiness of jobs can be described as follows: there are $n$ jobs to be processed, each job has an integer processing time, a weight and a due date. The objective is to minimize the total weighted tardiness of jobs. The problem belongs to the class of NP-hard problems. Some new properties of the problem associated with the blocks have been presented and discussed. These properties allow any to propose a new fast local search procedure based on a 'I abu scarch approach with a specific neighborhood which employs blocks of jobs and a compound moves lechnique. A compound move consists in perfoming several moves simulianeously in a
single iteration of algorithm and allows any to accelerate the convergence to good solutions. In the algorithm [47], an idea has been used which decreases the complexity for the search of neighberhood from $\mathrm{O}\left(n_{3}\right)$ to $\mathrm{O}(n 2$ ). Additionally, the neighborhood is reduced by using some elimination criteria. The method presented in this paper [47] is deterministic one and has not any random element, as distinct from other eflective but non-detemninistic methods proposed for this problem, such as Tabu scarch of Crauwels, H. A. J., Potts, C. N., \& Van Wassenhove, L. N. (1998) Computational experiments on the benchunark instances from OR-Library (http://pcople.brunel.ac.uk/ mastijb/jeb/info.html) are presented and comparcd with the results yielded by the best algorithms discussed in the literature. These results show that the algorithm proposed allows us to obtain the best known results for the benchmarks in a shon time. The presented properties and ideas can be appled in any local scarch procedures [47].

In many manufacturing systems, jobs that are completed carly are held as linishedgoods inventory until their duc-dates, and hence one incurs carliness costs. Similarly, jobs that are completed after their due-dates incur penalty. The objective in such situations would, therefore, be to mect the due-dales of the respective jobs as closely as possible, and consequently minimize the sum of earliness and tardiness of jobs because earliness and tardiness of jobs greatly influence the perfornance of a schedule with respect to cost. In addition, a job incurs holding cost from the time of its arrival until its completion. Most studies on scheduling in such manufacturing systems assume unit earliness cost, unit tardiness cost and unit holding cost of a job. However, in reality such an assumption need not always hold and it is quite possible that there exist different costs of carliness, tardiness and holding for different jobs. In addition, most studies on job-shop scheduling assume that jobs are independent and that no assernbly operations cxist. The study [48] addresses the problem of scheduling in dynamic assembly job-shops (i.e. shops that manufacture multilevel jobs) with the consideration of jobs having dillerent carlincss, tardiness and holding costs. An attempt is made in this paper to present dispatching rules by incorporating the relative costs of earliness, tardiness and holding of jobs in the form of scalar weights. In the
first phase of the study, relative costs (or weights for) carlincss and tardiness of jobs are considered, and the dispatching rules are presented in order to minimize the sum of weighted earliness and weighted tardiness of jobs. In the second phase of the study, the objective considered is the minimization of the sum of weighted carliness, weighted tardiness and weighted flow time of jobs, and the dispatching rules are presented by incorporating the relative costs of carliness, tardiness and flow time of jobs. Simulation studics have been conducted separately for both phases of the current study, the perlomance of the scheduling rules have been observed independently, and the results of the simulation study have been reported. The proposed rules are found to be eflective in minimizing the mean and maximum values of the measures of performance [48].

This paper [49] studjes two models of two-stage processing with flow shop at the lirst stage followed by open shop at the second stage. The first model involves multiple machines at the first stage and two machines at the second stage, and the other involves multiple machines at both stages. In both models, the objective is to minimize the makespan. This problem is NP-complete, for which an efficient heuristic solution algorithm is constructed and its worst-case performance guatantec is analyzed for both models. An integer programming model and a branch and bound algorithm are proposed for model 1 and a lower bound is developed for model 2 as benchmarks for the heuristic algorithms. Computational experiences show that the heuristic algorithms consistently generate good schedule and the branch and bound algorithm is much efficient than the integerprogramming model.

This rescarch [50] presents an interesting scheduling problem common to freight consolidation terminals. 'This previously unstudied problern involves scheduling a set of inbound trailers to a fixed number of unload docks. The objective is to schedule the trailers to the unload docks to minimize the time span of the transfer operation. This study focuses on freight consolidation teminals in the parcel delivery industry. A simulation-based scheduling algorithen that uses a genetic algonithm to drive the search for new solutions is proposed. In addition to the introduction and discussion of the parcel hub seheduling
problem, the contribution of this rescarch is an approach that serves as the initial effor to solve this practical problem.

This work [51] presents the development and implementation of a production scheduling system for an electrical appliance manufacturer. Based on recent advances in optimizationbased scheduling approaches, two different software architectures based on two dillerent scheduling formulations, namely the RTN and the STN, are proposed to integrate information available in the different production units and stages with formal algorithmic tools. Optimization results indicate that signuficant coonomic benelits can be achicved (e.g. minimization of total operating costs) while ensuring full customer satisfaction as oposed to nomal practices followed in the company relying on human cxpertise. The work indicates that it is possible to solve real-life manufacturing problems using oplimizationbased approaches but the integration of information in a timely fashion seems to be a major factor in successfully implementing the system and fully realizing its benefits,

The paper [52] deals with the problen of finding a job sequence that minimizes the makespan in $m$-machine flow shops under the no-idle condition. This condition requires that each machine must process jobs without any interruption from the star of processing the first job to the completion of processing the last job. Since the problem is NP-hard, we propose a constructive heuristic for solving it that significantly outperforms heuristics known so far.

This paper $\{53\rceil$ considers the $n$-job, m-machine permutation flow shop with the objective of minimizing the mean flow time. Initial sequences that are structured to enhance the performance of local search lechniques are constructed from job rankings delivered by a trained neural network. The network's training is done by using data collected from optimal sequences obtained from solved examples of llow shop problems. Once trained, the neural network provides rankable measures that can be used to construct a sequence in which jobs are located as close as possible to the positions they would occupy in an optimal sequence. The contribution of these 'neural' sequences in improving the performance of some common local search techniques, such as adjacent pairwise interchange and Tabu search is
examined. Tests using initial sequences generated by different heuristics show that the sequences suggested by the ncural networks are more effective in directing neighborhood search methods to lower local optima.

This paper [54] deals with the production and preventive maintenance control problem for a multiple-machine manufucturing system. The objective of such a problem is to find the production and preventive maintenance rates for the machines so as to minimize the total cost of inventory/backlog, repair and preventive maintenance. A two-level hicrarchical control model is presented, and the structure of the control policy for both identical and non-identical manufacturing systems is described using parameters, refened to here as input factors. By combining analytical formalism with simulation-based statistical tools such as experimental design and response surface methodology, an approximation of the optimal control policies and values of input factors are determined. The results oblained extend those available in existing literalure to cover non-identical machine manufacturing systems. A numerical example and a sensitivity analysis are presented in order to illustrate the robustness of the proposed approach. The extension of the proposed production and preventive maintenance policies to cover large systems (multiple machines, multiple products) is discussed.

This paper [55] deals with the problem of sclecting and scheduling the orders to be processed by a manufacturing plant for immediate delivery to the customer site. Among the constraints to be considered are the limited production capacity, the available number of vehicles and the time windows within which orders must be served. At first the problem has been described as it occurs in praclice in some industrial cnvironnents, and then has been presented an integer progranming model that maximizes the profit due to the customer orders to be processed. A Tabu search-based solution procedure to solve this problem is developed and tested empirically with randomly generated problems. Comparisons with an exact procedure show that the method finds very good-quality solutions with small compulation requirements.

The genctic algorithm with scarch area adaptation (GSA) has a capacity for adapting to the structure of solution space and controlling the tradeoff balance between global and local searches, even if one does not adjust the parameters of the genetic algorithm (GA), such as crossover and/or mutation rates [56]. But, GSA needs the crossover opcrator that has ability for characteristic inheritance ratio control. In this paper, the modificd genetic algorithm has been proposed with search area alaptation (mGSA) for solving the Job-shop scheduling problem (ISP). Unlike GSA, the proposed method does not need such a crossover operator. To show the elfectiveness of the proposed method, numerical experiments have been conducted by using wo benchmark problems. It is shown that this method has better perfornance than cxisting Gas [56].

The effectiveness of the solution method based on simulated anncaling (SA) mainly depends on how to determine the SA-related parameters. A scheme as well as parameter values for defining an annealing schedule should be appropriately determined, since various schemes and their corresponding parameter values have a significant impact on the performance of SA algorithms. In this paper [57], based on robust design a now annealing parameter design method has been proposed for the mixed-model sequencing problem which is known to be NP -hard. To show the effectiveness of the proposed method, extensive computation experiments are conducted. It was found that the robust designed method oulperforms the SA algorithm.

One of the basic and significant problems [58], that a shop or a factory manager is encountered, is a suitable scheduling and sequencing of jobs on machincs. One type of scheduling problem is job shop scheduling. There are different machincs in a shop of which a job may require some or all these machines in some specific sequence. For solving this problem, the objective may be to minimize the makespan. After optimizing the makespan, the jobs sequencing must be carricd out for each machine. The above problem can be solved by a number of different methods such as branch and bound, cutting plane, heuristic methods, ctc. In recent years, rescarches have used genetic algorithms, simulated anncaling, and machine leaming methods for solving such problems. In this paper, a simulation model
is presented to work out job shop scheduling problems with the objective of minimizing makespan. The model has been coded by Visual SLAM which is a special simulation language. The structure of this language is based on the network modeling. Aller modeling the scheduling problem, the model is verified and validated. Then the computational results are presented and compared with other results repored in the literature. Finally, the model outpul is analyzed.

This paper [59] considers the problem of scheduling part families and jobs withn each part lamily in a flow shop manufacturing cell with sequence dependent family setups times where it is desired to minimize the makespan while processing parts (jobs) in each farnily together. Two evolutionary algorithms - a Genetic Agorithm and a Memetic Algorithn with local search - are proposed and empirically evaluated as to their effectivencss in finding optimal permutation schedules. The proposed algorithms use a compact represcntation for the solution and a hierarchically structured population where the number of possible neighborhoods is limited by dividing the population into clusters. In comparison to a Multi-Starl procedure, solutions obtained by the proposed evolutionary algorithms were very close to the lower bounds for all problem instances. Moreover, the comparison against the previous best algorithun, a heuristic named CMD, indicated a considerable performance improvement.

This paper 60 ] studies the single machine scheduling problem for the objective of minimizing the expected number of tardy jobs. Jobs have normally distributed processing times and a common deteministic due date. A new approach has been developed for this problem that generate near optimal solutions. The original stochastic problem is transformed into a non-lincar integer programming model and its relaxations. Computational study yalidates their effectiveness by comparison with optimal solutions.

This paper [61] considers the evaluation of the worst-case performance ratio between the best solution of the flow shop problem and the permutation flow shop with time delays considerations. It is observed that, even in the restricted case of two machines and unit execution time operations, the two models may generate different optimal values for the
makespan. More specifically, it is shown that, in the two-machine case, the performance ratio between the best permutation schedule and the best flow shop schedule is bounded by 2. When the operations of the $n$ jobs are restricled to be unil exceution time, this ratio is reduced to $(2-(3 / n+2)$ ) for the two-machine case, and is $m$ for the $n t$-machine case.

In this paper [62], tiltered and recovering bean search algorithms for the single machine earliness/tardiness scheduling problem with no idle time has been presented and compared them with existing neighborhood scarch and dispatch rule heuristics. Filtering procedures using both priority evaluation functions and problem-specific properties have been considered. The computational results show that the recovering beam search algorithms outperform their fillered counterpars, while the priority-based filtering procedure proves superior to the rules-based altemative. The best solutions are given by the neighborhood search algorithm, but this procedure is computationally intensive and can only be applied to small or medium size instances. The recovering beam search heuristic provides results that are close in solution quality and is significantly faster, so it can be used to solve even large problems.

Scheduling for the llexible job-shop [63] is very important in both lields of production management and combinatorial optimization. However, it is quite difficult to achicve an optimal solution to this problem with traditional optimization approaches owing to the high computational complexity. The combining of several optimization criteria induces additional complexity and new problems. Particle swarm optimization is an evolutionary computation technique mimicking the behavior of flying birds and their means of information exchange. It combines local search (by sell experience) and global scarch (by neighboring experience), possessing high search eliciency. Simulated annealing (SA) as a local search algorithm employs certain probability to avoid becoming trapped in a local optimum and has been proved to be effective for a varicty of situations, including scheduling and sequencing. By reasonably hybridizing these two methodologics, an easily implemented hybrid approach for the multi-objective flexible job-shop sebeduling problem (FJSP) has been developed. The results obtained from the computational study have shown
that the proposed algorithm is a viable and effective approach for the multi-objective FJSP, especially for problems on a large scale.

In this study, a modified Pareto-optinal algorithm (deternining the trade-offs between total completion time and maximum lateness) is developed for the multi-criterion scheduling problen with periodic maintenance. The specific problem considered in this paper is to minimize flow time, maximum lateness and machine idle time. These multiple objectives are transformed into a single objective function, cost function, by using an aggregate weighted sum method. All possible weight combinations are calculated for cach sequence of Pareto-optimal set to present different level of importance of each objective. On the other hand, to generate various scts of Pareto-optimal scquences from different maintenance plans, different values for both time interval between two maintenance periods and amount of time to perform maintenance are computed for the same instance. Various maintenance plans give more flexibility to the scheduler (or decision-maker) to make a decision according to both his preferences and maintenance necessity/availability. A neighborhood search heuristic is also applied to the same instance in order to compare it with the modificd algorithm.

### 3.3 Problem Description

There are $n$ independent non-preemptive jobs, that is, once a job is started it must be completed to process them on a single machine without interruption. Each job $j$ becomes available for processing at ready time zero and has a due date $d_{j}$, At every $T$ unit of time, the machine is seized to hold for maintenance. A number of jobs that are grouped together to fit in every $T$ amount of time is a batch. There could be machine idle time, $I_{b}$, before the maintenance starts afler the last job in a batch is completed. The maintenance period is $M$ which is also a fixed time. The total machine idle time is oblained by adding the idle time of all the batches.

The algorithm presented here for the problem combines all the criterions together in one schedule. The new approach starts with an initially obtained set of Parcto-optimal schedule
for llow time and maximum tardiness minimization problem. It then includes machine idle time $I$ and maintenance time $M$ in cach of these initially found sequences. Once the rescheduling of machine maintenance and ideness period of machine is completed, it then calculates the new values of flow time, matximum tardiness and machine idle time for which the assigned weights are $w_{4}, w_{2}$, and $w_{3}$, respectively. All possible weight combinations, satisfying $w_{I}+w_{2}+w_{3}=1$, are assigned for criterions in cach schedule of Pareto-optimal set. The minimum total cost among all the Parcto-optimal sequences according to certain weighted parameters gives the best sequence for the problem. It is clear that the problem is $N P$-hard since the problem that minimizes the maximum tardiness subject to periodic maintenance period and nonresumable jobs is $N P$-hard [41].

For two or more contradictory criterions, cach criterion corresponds to a different optimal solution, but none of these trade-off solutions is optimal with respect to all criterions [35]. Thus, multi-criterion optimization does not try to lind one optimal solution but a set of trade-off solutions. The fundamental difference is that multi-objectuve optimization deals with a set of Parcto-optimal solutions. The best schedule among the set that gives the most promising result for a particular set of weighted criterions is found.

## Notation

The following notations are used throughout this work:
$n \quad$ Number of jobs for processing at time zero
$J_{J} \quad$ Job number $j,(j=1,2, \ldots, n)$
$p_{J} \quad$ Processing time of job $j$
$p_{t r} \quad$ Processing time of job $j$ in batch $i$
$C_{j}$ Completion time of job $j$
d. Due date of job $j$
$L_{j} \quad$ Lateness of job $j$, where $L_{j}=C_{j}-d_{j}$
$T_{j} \quad$ Tardiness of job $j$, where $T_{j}=\max \left\{0 ; L_{r}\right\}, L_{\text {max }}=\max _{j}\left\{T_{j}\right\}$
$T \quad$ Time interval between two maintenance periods

M Amount of time to perform one maintenance
$I_{b} \quad$ Machine idle time in batch $i,(i=1,2, \ldots, r)$
I Total machine idle time of a schcdule
$T_{b} \quad$ Tolal processing time for scheduled jobs in batch $i,(i=1,2, \ldots, r)$
$m \quad$ Iteration number.

### 3.4 Pareto-Optimal Algorithm

When there are multiple objectives, the concept of Pareto-optimality plays a role in scheduling. A schedule is Parcto-optimal if it is impossible to improve on one of the objectives without making at least one other objective worse. The scheduler may want to view a set of Pareto-optimal schedules before deciding which schedule to select, when there are multiple objectives. In this paper, the algorithm of determining trade-offs between total completion time and maximum lateness, initially proposed by Pinedo [34], is modified and extended, which includes periodic maintenance, In addition to the total completion time and the maximum lateness, the machine idle time is also considered as the third objective. A set of Parcto-optimal schedules represent the trade-olfs between total completion time, maximum lateness and machine idle time.

There are many sequencing rules that can be appted to the jobs through the machines in a job shop according to the preferences. Two of those basic sequencing rules, shortest processing time (SPT) and earliest due date (EDD) are adapted in the modifice Parctooptimal algorithm. For explanatory convenience, we define two lerms that are needed in the algorithm. The machine idle time of a batch, $I_{b}$, is defined as the time by sublracting the total processing time for scheduled jobs in a batch, $\mathcal{T}_{b t}$, from the time interval between two maintenance periods $T$ (i.e., $I_{b r}=T-T_{b i}$ ). The total machine idle time of a schedule, $I$, is delined by summing all machine idle time of all batches (i.e., $I=\sum_{t=1}^{k} I_{b t}$ ).

Pareto-optimal algoritim determincs the trade-offs between total completion time and maximum lateness only as initially presented by Pinedo [34]. A third objective, machine
idle time, is added and the stated algorithm is modified and extended accordingly. The steps of the modified Pareto-optimal algorithm are outlined as follows:

## Algorithm 1: Modified Pareto-Optimal Algorithm

Step 1. Set $m=1$ (number of iteration)
a) Schedule the jobs by SPT rule and apply EDD rule to the jobs with same processing time as schedule $S_{S P T / E D D}$
b) Compute $L_{\text {inax }}(S P T / E D D)$
c) Go to Step 8 to find machine idle time in the schedule $S_{S P T / E D O}$ and the revised $S_{S P T / E D D}$ is now called $S^{*} S_{Y T F D D}$ when maintenance time is included.

Step 2. Sct $m=2$
a) First schedule the jobs by EDD rule, and apply SPT rule to the jobs with same due date, as schedulc $S_{\text {FMPSST }}$
b) Compute $L_{\text {max }}(E D D / S P T)$
c) Go to Step 8 to find machine idle time in the schedule $S_{E D D S P T}$ and, on inclusion of maintenance time the revised $S_{\text {EDDSST }}$ is called $S_{\text {EDDNOT }}$.

Step 3. Iteration $m=3$.
Sel $I_{\text {min }}=L_{\text {max }}(E D D)$ and $\bar{d}_{s}=d_{s}+L_{\text {max }}$.
Step 4. Set $k=n, J^{c}=\{1, \ldots, n\}, \tau=\sum_{\mathrm{j}=1}^{\mathrm{n}} p_{\mathrm{J}}$ and $\delta=\tau$.
Step 5. Find $j^{*}$ in $J^{c}$ such that
$\bar{d}_{J^{*}} \geq \tau$, and $p_{J^{*}} \geq p_{i}$ for all jobs $l$ in $J^{\prime}$ such that $\bar{d}_{t} \geq \tau$.
Put job $j^{*}$ in position $k$ of the sequence.
Step 6. If there is no job $\ell$ such that $\vec{d}_{\varepsilon}<\tau$ and $p_{t}>p_{i}$, go to Step 7.
Otherwise find $j^{\prime \prime}$ such that $\tau-\bar{d}_{j}=\min \left(\tau-\bar{d}_{f}\right)$
For all $\ell$ such that $\bar{d}_{1}<\tau$ and $p_{r}>p_{p_{\mu}}$, Set $\delta^{*}=\tau-d_{1+\cdots}$.
If $\delta^{* *}<\delta$, then $\delta=\delta^{* *}$.
Step 7 . Set $k \leftarrow k-1$, and $\tau \leftarrow \tau-p_{j}$. Upate the set as $J^{t}=J^{t}-j^{*}$.
If $k \geq 1$ go to $\operatorname{Stcp} 5$.

Step 8. Generate a batch by grouping a set of jobs such that $\sum_{i=1}^{n} p_{j} \leq T$
Repeal grouping of the remaining jobs to form other batches.
Set $b_{i}=$ number of batches in one schedule, where $i=1,2, \ldots, r$.
Find machine idle time for one batch $I_{h t}=T-\sum_{j=1}^{n} p_{p}$
lind machine idle time for one schedule, $I=\sum_{i=1}^{\mu} I_{b l}$
Revise the schedule by adding the amount of time to perform maintenance, $M$, to the end of each batch.
Compute $\sum_{j-1}^{n} C_{i}^{*}, \dot{L}_{\max }^{*}$, and $I^{*}$.
Step 9. Set $L_{\text {max }}=L_{\text {max }}+\delta$.
If $L_{\text {max }} \leq L_{\text {max }}(S P T / E D D)$, sct $m=m+1, \bar{d}_{j}=\bar{d}_{1}+\delta$, and go to Step 4.
Otherwise STOP.

In Step 1, the algorithm starts with sequencing the jobs in SPT order, If two jobs have the same processing time, the job with smaller due date is placed earlier. Then $L_{\text {stmax }}(S P T / E D D)$ is calculated for this generated SPT/EDD schedutc. This $L_{\max }(S P T / E D D)$ value indicates when to stop the iterations in the algorithan. For the schedule of SPT/EDD ( $S_{S / 7 / E D D}$ ), batches are generated by grouping scts of jobs according to $\sum_{j=1}^{n} p_{l} \leq T$.

The first Parcto-optimal schedule ( $S_{S P T E D D}$ ) is oblained afler adding the maintenance time to the generated batches in $S_{S P T / E D D}$. The second Pareto-optimal schedule ( $S_{\text {EDDSST }}^{*}$ ) is obtained in Step 2 which is similar to Step 1. The only difference is that instead of starting with SPT order, the procedure starts with EDD order and follows the same idea as in Step 1. In Step 3, due dates of the jobs anc increased by $L_{m a x}(E D D / S P T)$ for the next iteration. Step 4 calculates the total processing time for $n$ jobs and assigns that value to $d$. Step 5 gencrates a Pareto-optinal schedule that minimizes $\sum_{f=j}^{n} C$, in which job $k$ is scheduled last, if and only if
(i) $\bar{d}_{k} \geq \sum_{j=1}^{n} p_{j}$,
(ii) $j_{\star} \geq p_{t}$ for all jobs $\ell$ in $J^{\prime}$ such that $\bar{d}, \geq \sum_{r=1}^{n} p_{i}$.

Step 6 determines the minimum increment $\delta$ in the $L_{m a r}$ that would allow for a decrease in the minimum $\sum_{j=1}^{n} C_{l}$ from the new generated Parcto-optimal schedule. Maintenance time is included to the generated Parcto-optimal schedule affer fomming the batches in Step 8. Three objective valucs $\left(\sum_{i=1}^{n} C_{j}^{*}, L_{\text {max }}{ }^{,}, I_{m+}^{*}\right)$ are also calculated at this point for all the Parcto-optimal schedules with periodic maintenance.

### 3.5 Computational Results with Bench Mark Data

Consider a single-machine scheduling problem with nine jobs, as given in Table 3.1, which is taken from Liao and Chen [41]. The time interval between two consecutive maintenances, $T$, is 8 hours and the amount of time to perform one maintenance, $M$, is 2 hours. Now, all possible Pareto-optimal schedules are generated to determine average flow time of jobs, $\bar{F}$ $\left(=\sum_{j=1}^{q} C^{*}, / 9\right)$, job tardiness $L_{\text {max }}{ }^{*}$, and machine idle time $I^{*}$ for nine jobs.

Table 3.1 The processing time and due dates (in hour) for 9-job problem*

| Jobs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $P_{j}$ | 1 | 5 | 3 | 5 | 2 | 2 | 3 | 4 | 4 |
| $d_{1}$ | 1 | 13 | 2 | 30 | 10 | 13 | 20 | 12 | 14 |

* Lias and Chen (2003).

Step 1 . An initial optimal schedule $S_{(S \mu T / H D D)}:<1-5-6-3-7-8-9-2-4>$ is found by arranging jobs in SPT order and followed by $d_{[j]} \leq d_{[k]}$ if $P_{j}=P_{k}$ and job $j$ and $k$ are adjacent (see Table 3.2). The maximum lateness, $L_{\text {max }}(S P T / E D D)$, cquals to 11 corresponding to job 2. Now Step 8 is applied to find the machine idle time after the insertion of maintenance.

Table 3.2 Parcto-optimal schcđule, $S_{\left(S P_{j i L D D}\right)}$

| Jobs | 1 | 5 | 6 | 3 | 7 | 8 | 9 | 2 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $P_{j}$ | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 | 5 |
| $d_{1}$ | 1 | 10 | 13 | 2 | 20 | 12 | 14 | 13 | 30 |
| $C_{j}$ | 1 | 3 | 5 | 8 | 11 | 15 | 19 | 24 | 29 |
| $L_{3}$ | - | - | - | 6 | - | 3 | 5 | 11 | - |

Step 8. A maintenance of 2 hours is inscred into the optimal schedule ol Step 1 cvery 8 hours as shown in Table 3. Thus from the table, $L_{\text {mix }}{ }^{*}(S P T / E D D)=22, \sum C_{j}^{*}=1+3+5$ $+8+13+17+24+35+45=151$ and $I^{*}=0+1+4+3=8$ for the lirst Parcto-optimal schedule $S_{\left(S^{\prime} / L D m\right)}$ : <1-5-6-3-7-8-9-2-4 $>$. Another possible Pareto-schedule is now sought in Step 2.

Table 3.3 Revised schedule $S_{\text {cprong, }}$ by inserling maintenance and idle times

| Jobs | I | 5 | 6 | 3 | $I_{b 1}$ | $M_{1}$ | 7 | 8 | $I_{h 2}$ | $M_{2}$ | 9 | $I_{03}$ | $M_{3}$ | 2 | $I_{b 4}$ | $M_{4}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $P_{r}$ | 1 | 2 | 2 | 3 | $\underline{0}$ | 2 | 3 | 4 | $\underline{1}$ | 2 | 4 | 4 | 2 | 5 | $\underline{3}$ | 2 | 5 |
| $d_{j}$ | 1 | 10 | 13 | 2 | - | - | 20 | 12 | - | - | 14 | - | - | 13 | - | - | 30 |
| $C_{1}$ | 1 | 1 | 3 | 5 | 8 | 8 | 10 | 13 | 17 | 18 | 20 | 24 | 28 | 30 | 35 | 38 | 40 |

Step 2. Now instead of finding $S_{\text {[sprsiry }}$, another schedule , $S_{(x y s)}$, ipl) , is obtained by litst applying EDD rule followed by SPT for the jobs with same due dates (not the same processing time as in $S_{\text {spr }}$, msy $)$. These computational results using Table 3.1 are reported in Table 3.4.

Table 3.4 Second Parcto-optimal schedule, $S_{(\text {(LDD/SAM }}$

| Jobs | 1 | 3 | 5 | 8 | 6 | 2 | 9 | 7 | 4 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $p_{1}$ | 1 | 3 | 2 | 4 | 2 | 5 | 4 | 3 | 5 |
| $d_{1}$ | 1 | 2 | 10 | 12 | 13 | 13 | 14 | 20 | 30 |
| $C_{1}$ | 1 | 4 | 6 | 10 | 12 | 17 | 21 | 24 | 29 |
| $L_{r}$ | - | 2 | - | - | - | 4 | 7 | 4 | - |

This yields $S_{\text {bobospl }}:<1-3-5-8-6-2-9-7-4>$ and $L_{\max }(E D D / S P T)=7$. As in the previous iteration, maintenance and machine idle times are considered for this Parcto-schedule in the next step.

Step 8. As beforc, after inserting the maintenance time with appropriate idle time into Table 3.4, the revised schedule is shown in Table 5 in which $L_{\max }{ }^{*}\left(E D D S S^{\prime}\right)=20$ corresponding to job $9 ; \sum C_{j}^{*}=1+4+6 \div 14+16+25+34+37+45=182$, and $I^{*}=2+2+3+1=8$ for the second Pareto-oplimal schedule, $S_{\text {tom }}^{*}{ }^{\prime \prime}:=\langle 1-3-5-8-6-2-9-7-4\rangle$.

Table 3.5 Revised schedule $S_{(F H \mu / S P T)}$ for second Pareto schedule.

| Jobs | 1 | 3 | 5 | $I_{b 1}$ | $M_{1}$ | 8 | 6 | $I_{b 2}$ | $M_{2}$ | 2 | $I_{b j}$ | $M_{3}$ | 9 | 7 | $I_{b 4}$ | $M_{4}$ | 4 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $J_{r}$ | 1 | 3 | 2 | $\underline{2}$ | 2 | 4 | 2 | $\underline{2}$ | 2 | 5 | $\underline{3}$ | 2 | 4 | 3 | 1 | 2 | 5 |  |
| $d_{j}$ | 1 | 2 | 10 | - | - | 12 | 13 | - | - | 13 | - | - | 14 | 20 | - | - | 30 |  |
| $C_{j}$ | 1 | 1 | 4 | 6 | 8 | 10 | 14 | 16 | 18 | 20 | 25 | 28 | 30 | 34 | 37 | 38 | 40 | 45 |
| $L_{j}$ | - | 2 | - | - | - | 2 | 3 | - | - | 12 | - | - | 20 | 17 | - | - | 15 |  |

Step 3. $L_{\text {max }}=L_{\text {max }}(E D D / S P T)=7$ from Step 2 since $L_{\text {max }}(E D D / S P T) \leq L_{\text {max }}(S P T / E D D)$ always. Therefore the duc date is updated as $\bar{d}_{j}=d_{j}+7$ to get the third Pareto-optimal schedule according to $\bar{d}_{3}$. This is reported in Table 3.6.

Table 3.6 Updated $\bar{d}_{j}=d_{j}+7$ (in EDD order)

| Jobs | 1 | 3 | 5 | 8 | 6 | 2 | 9 | 7 | 4 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $d_{j}$ | 1 | 2 | 10 | 12 | 13 | 13 | 14 | 20 | 30 |
| $\bar{d}_{j}$ | 8 | 9 | 17 | 19 | 20 | 20 | 21 | 27 | 37 |

Step 4. Here, $f^{\prime}=\{1,2,3,4,5,6,7,8,9\}$, the tolal number of jobs, $k=\left|J^{\prime}\right|=9$, and total processing time of the remaining jobs, $\tau=\sum p_{s}=29$ and set $\delta=\tau=29$ (at the beginning). Step 5. $J_{t}$ satisfies condition $\bar{d}_{r} \geq t(=29)$ and the corresponding $f_{4}$ is 5. So $J_{4}$ is scheduled as the last job in the sequence, $S_{t} \ll \ldots \quad 4>$.

Slep 6. None of the remaining jobs satisfies the conditions $\bar{d}_{p}<\tau$ and $p_{\mathrm{r}}>p_{j}$.
Step 7. The set statistics is updated as $J^{t}=\{1,2,3,5,6,7,8,9\}, k=\left|J^{c}\right|=8$, and $\tau=29-5=$ 24.

Since the Steps 5 to 7 are repeated likewisc in order to get the third Pareto-optimal schedulc, the results of this repeated search are summarized in Table 3.7, and the last search results in $S_{f}:<1,5,6,3,8,2,9,7,4>$ which, in tum, yiedds the thind Pareto optimal schedule as in lable 3.8. The maximum lateness for the third Pareto-optimal sehedule is $L_{\text {tud }}\left(S_{1}\right)=7$.

Table 3.7 Repetition of Steps 5 through 7

| Job (i) | Processing lime $(P)$ | Schedule $(S)$ |  | $\delta$ | $\tau$ |
| :---: | :---: | :---: | ---: | :---: | :---: |
| 4 | 5 | $<\ldots$ | $4>$ | 29 | 24 |
| 7 | 3 | $<\ldots$ | $7,4>$ | 3 | 21 |
| 9 | 4 | $<\ldots$ | $9,7,4>$ | 1 | 17 |
| 2 | 5 | $<\ldots$ | $2,9,7,4>$ | 1 | 12 |
| 8 | 4 | $<\ldots$ | $8,2,9,7,4\rangle$ | 1 | 8 |
| 3 | 3 | $<\ldots$ | $3,8,2,9,7,4\rangle$ | 1 | 5 |
| 6 | 2 | $<\ldots, 6,3,8,2,9,7,4\rangle$ | 1 | 3 |  |
| 5 | 2 | $<\ldots, 6,3,8,2,9,7,4\rangle$ | 1 | 1 |  |
| 1 | 1 | $<1,5,6,3,8,2,9,7,4>$ | 1 | 0 |  |

Table 3.8 l'hird Pareto-optimal schedule, $S_{t}$

| Jobs | 1 | 5 | 6 | 3 | 8 | 2 | 9 | 7 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $p_{j}$ | 1 | 2 | 2 | 3 | 4 | 5 | 4 | 3 | 5 |
| $d_{3}$ | 1 | 10 | 13 | 2 | 12 | 13 | 14 | 20 | 30 |
| $C_{j}$ | 1 | 3 | 5 | 8 | 12 | 17 | 21 | 24 | 29 |
| $L_{j}$ | - | - | - | 6 | - | 4 | 7 | 4 | - |

Step 8. So for $\mathrm{S}^{*}$ : $<$ 1-5-6-3-8-2-9-7-4> in Table 8, insertion of both mantenance and machine idle times lead to $L_{\text {max }}{ }^{*}\left(S_{1}\right)=20, \sum C_{1}^{2}=1+3+5+8+14+25+34+37+45=172$, and $I^{*}=0+4+3+1=8$. The revised schedule is shown in Tablc 3.9.

Table 3.9 Revised schedule $S_{1}$

| Jobs | 1 | 5 | 6 | 3 | $I_{b 1}$ | $M_{1}$ | 8 | $I_{b 2}$ | $M_{2}$ | 2 | $I_{61}$ | $M_{3}$ | 9 | 7 | $I_{t 4}$ | $M_{4}$ | 4 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $p_{t}$ | 1 | 2 | 2 | 3 | 0 | 2 | 4 | 4 | 2 | 5 | 3 | 2 | 4 | 3 | $\underline{1}$ | 2 | 5 |  |
| $d_{,}$ | 1 | 10 | 13 | 2 | - | - | 12 | - | - | 13 | - | - | 14 | 20 | - | - | 30 |  |
| $C_{t}$ | 1 | 1 | 3 | 5 | 8 | 8 | 10 | 14 | 18 | 20 | 25 | 28 | 30 | 34 | 37 | 38 | 40 | 45 |
| $L_{1}$ | - | - | - | 6 | - | - | 2 | - | - | 12 | - | - | 20 | 17 | - | - | 15 |  |

Step 9. At this step, set $L_{\text {max }}=L_{\text {max }}+j=7+1=8$. Since $L_{\text {max }}=8<$ $L_{\text {nux }}(S P T / E D D)=11$, continue to the next iteration for another schedule. Table 3.10 summarizes the results of all the iterations to get a set of Parcto-optimal schedules.
rable 3.10 All the itcrations of the algorithm

| Iteration $\rightarrow$ | Schedule | Parcto-Optimal Sequence | $\sum_{j-1}^{\mathrm{n}} C_{j}, L_{\max } \cdot I_{\mathrm{m}}$ | Cursent $d_{s}+\delta$ | $\delta$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | SPT/EDD | $<1-5-6-3-7-8-9-2-4\rangle$ | 151, 22, 8 | $30,20,14,13,13,12,10,2,1$ | - |
| 2 | EDD/S ${ }^{\text {PT }}$ | $\langle 1-3-5-8-6-2-9-7-4\rangle$ | 182, 20, 8 | $30,20,14,13,13,12,10,2,1$ | 7 |
| 3 | $\mathrm{S}_{1}$ | $<1-5-6-3-8-2-9-7-4\rangle$ | 172, 20, 8 | 37, 27, 21, 20, 20, 19, 17, 9, 8 | 1 |
| 4 | $\mathrm{S}_{2}$ | <1-5-6-3-8-9-2-7-4> | 137, 12, 0 | 38,28,22, 21, 21, 20, 18, 10,9 | 2 |
| 5 | $\mathrm{S}_{3}$ | <1-5-6-3-7-8-2-9-4> | 151,20,8 | 40, 30, 24, 23, 23, 22, 20, 12,11 | 1 |
| 6 | $\mathrm{S}_{4}$ | $\langle 1-5-6 \times 3-7-8-9-2-4>$ | 151, 22,8 | $41,31,25,24,24,23,21,13,12$ | Stop |

Afier generating all possible Pareto-optimal schedules with respect to job completion time $\bar{F}^{+}$, job tardiness $L_{\text {max }}{ }^{*}$, and machine idle time $\dot{I}^{*}$ for nine jobs, the total weighted function, $c\left(\bar{F}^{*}, L_{\max }^{*}, \dot{H}^{*}\right)=w_{1}\left(\sum_{j=1}^{9} C_{1}^{*} / 9\right)+w_{2} L_{\max }^{*}+w_{3} I^{+}$, where $w_{1}=0.5, w_{2}=0.4, w_{3}=0.1$ (arbitrarily chosen) for 6 schedules is calculated [see Table 3.11]. The minimum-weighted schedule is $\left.S^{*}=S_{2}:<1-5-6-3-8-9-2-7-4\right\rangle$ corresponding to $c\left(\bar{F}^{*}, L_{\text {max }}, I^{*}\right)=12.411$.

Table 3.11 A Parcto-Optimal Set

| Itcration, m | Schedule | Pareto-Optimal Sequence | $\sum_{j=1}^{9} C_{j}^{*}, L_{\text {man }}{ }^{*}, I_{m p}^{*}$ | $c\left(\bar{F}^{*}, L_{\operatorname{axax}}{ }^{*}, I^{*}\right)$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | SPT/EDD | $\langle 1-5-6-3-7-8-9-2-4\rangle$ | 151, 22, 8 | 17.989 |
| 2 | EDD/SPT | <1-3-5-8-6-2-9-7-4> | 182, 20, 8 | 18.91 t |
| 3 | $\mathrm{S}_{1}$ | $<1-5-6-3-8-2-9-7-4>$ | 172,20,8 | 18.356 |
| 4 | $\mathrm{S}_{2}$ | <1-5-6-3-8-9-2-7-4> | 137, 12, 0 | 12.411* |
| 5 | $\mathrm{S}_{3}$ | $<1-5-6-3-7-8-2-9-4>$ | 151,20,8 | 17.189 |
| 6 | $\mathrm{S}_{4}$ | $<1-5-6-3-7.8-9-2-4\rangle$ | 151, 22, 8 | I7.989 |

[^0]
### 3.6 Neighborhood Search Algorithm

As a second approach to the multi-criterion scheduling problem, a neighborhood scarch technique is considered. Many discrete optimization problems of practical interest cannot be solved optimally in the reasonable time. A practical approach to these problems is to use heuristics which do not guarantee the optimality of the solution, but near-optimal solutions can be obtained in a tolerable time limit. Neighborhood search starts with a feasible schedule and iteratively tries to improve the solution. At cach stage, it searches the "ncighborhood" of the current solution to find an improved solution. The search terminates when it finds a solution that is at least as good as any of its neighbors; such a solution is called a locally optimal solution. Typically, multiple runs of the neighborhood scarch are performed with different starting schedules called seeds, and the best locally optimal solution is selected. A comprehensive discussion of neighborhood search can be found in Ehrgott and Klamroth [64].
$A$ method of taking one sequence as a seed and systematically crating a collection of related sequences is the generating mechanism. In this work, the single adjacent pairwise interchange opetation serves as a generating mechanism for the example. The neighborhood of the seed scquence is a list of $(n-1)=9-1=8$, distinct sequences for this particular generating mechanism. The single adjacent painvise interchange is $O\left(n^{2}\right)$ in size (Baker, 1998). The search is illustrated on the numerical example. The performance measure of all the neighborhood sequences that is evaluated with respect to the initial seed is the weighted function. The same weight combinations, as given earlier, are used to evaluate the objectives (See Tables 3.12, 3.13 and 3.14). The following steps of neighborhood search, initially presented by Baker [42], are applicd to the numerical example.

## Algorithm 2: Neighborhood Search

Step 1.Obtain a sequence to be an initial seed and evaluate it with respect to the perfomance measure.

Step 2. Generate and evaluate all the sequences in the neighborhood of the seed. If none ol the sequences is better than the seed with respect to the perlonnance measure, stop. Otherwise proceed.

Step 3. Select one of the sequences in the neighborhood that improved the performance measure. Let this sequence be the now seed. Return to Step 2.

The single adjacent pairwise interchange mechanism is applied to the initial seeds, and the performance measure (weighted function) of each seed is compared with the perfornance measure of its neighborhood. Instead of generating all the sequences in the neighborhood of the seed, when a neighborhood gives an improved performance measure, the search stops, and that sequence becomes the new seed for the next stage. When a search of the new neighborhood produces no improvement, the search procedure leminates. The details of three seeds with their neighborhood sequences and their performance measures are presented in Tables 3.12, 3.13, and 3.14.

Table 3.12 Solution with a given initial seed, S: <1-2-3-4-5-6-7-8-9>

|  | Schedule | $\sum_{j=1}^{9} C_{r}, I_{\operatorname{mock}}, I_{a A}$ | $0.5 \bar{F}^{2}+0.4 L_{\max }{ }^{*}+0.11^{2}$ |
| :---: | :---: | :---: | :---: |
| Stage 1 |  |  |  |
| Seed: | 1-2-3-4-5-6-7-8-9 | 183, 24, 3 | 20.067 |
| Neighborhood: | 2-1-3-4-5-6-7-8-9 | 187, 24, 3 | 20.289 |
|  | 1-3-2-4-5-6-7-8-9 | 231,34, 11 | 27.533 |
|  | 1-2-4-3-5-6-7-8-9 | 185,24,3 | 20.178 |
|  | 1-2-3-5-4-6-7-8-9 | 201, 30, 7 | 23.867 |
|  | 1-2-3-4-6-5-7-8-9 | 183, 24, 3 | 20.067 |
|  | 1-2-3-4-5-7-6-8-9 | 184, 24, 3 | 21.122 |
|  | 1-2-3-4-5-6-8-7-9 | 182, 23, 2 | 19.511* sclection |
| Stage 2 |  |  |  |
| New Sced: | 1-2-3-4-5-6-8-7-9 | 182, 23, 2 | 19.511 |
| Neighborhood: | 2-1-3-4-5-6-8-7-9 | 186, 23, 2 | 19.733 |
|  | 1-3-2-4-5-6-8-7-9 | 230, 33, 10 | 26.978 |
|  | 1-2-4-3-5-6-8-7-9 | 184, 23, 2 | 19.622 |
|  | 1-2-3-5-4-6-8-7-9 | 202, 30, 7 | 23.922 |
|  | 1-2-3-4-6-5-8-7-9 | 182, 23, 2 | 19.511 |
|  | 1-2-3-4-5-8-6-7-9 | 184, 23, 2 | 19.622 |
|  | 1-2-3-4-5-6-7-8-9 | 183, 24, 3 | 20.067 |
|  | 1-2-3-4-5-6-8-9-7 | 183, 20, 2 | 18.367* sclection |
| Stage 3 |  |  |  |
| New Seed: | 1-2-3-4-5-6-8-9-7 | 183, 20, 2 | 18.367* selection |
| Neighbortood: | 2-1-3-4-5-6-8-9-7 | 187, 20, 2 | 18.589 |
|  | 1-3-2-4-5-6-8-9-7 | 240, 30, 10 | 26.333 |
|  | 1-2-4-3-5-6-8-9-7 | 185,20,2 | 18.478 |
|  | 1-2-3-5-4-6-8-9-7 | 202, 24, 6 | 21.422 |
|  | 1-2-3-4-6-5-8-9-7 | 183, 20, 2 | 18.367* selection |
|  | 1-2-3-4-5-8-6-9-7 | 185, 20, 2 | 18.478 |
|  | 1-2-3-4-5-6-9-8-7 | 183, 22, 2 | 19.167 |
|  | 1-2-3-4-5-6-8-7-9 | 182, 23, 2 | 19.511 |

Search terminates with weighted functional value $=18.367$

To compare the modified Pareto-optimal algorithm with the neighborhood search heuristic in case of bench mark data, the same instance with parameters $T=8, M=2, w_{1}=0.5, w_{2}=$ 0.4 and $w_{3}=0.1$ is used. The neighborhood scarch heuristic gives the best near-optimal schedule as $S$ : <I-5-6-3-7-2-8-9-4> with the mimimum weighted function equals to 18.367. On the other hand, the modified Pareto-optimal algorithm gives the best neat-optimal schedule as $\mathrm{S}:<1-5-6-3-8-9-2-7-4\rangle$ with the minimum weighted function equals to 12.410 . It can be coneluded that the modified Pareto-optimal algorithm provides a better result than the neighborhood scarch heuristic for this instance.

### 3.7 Computational Results with Real Life Data

Consider a single-machine scheduling problem with twelve jobs, as given in Figure 2.1, which is taken from a fumiture company. The time interval between two consecutive maintenances, $T$, is 25 hours and the amount of time to perform one maintenance, $M$, is 4 hours. Now, all possible Pareto-optimal schedules are generated to determine average flow time of jobs, $\bar{F}^{*}\left(=\sum_{j=1}^{y} C_{j}^{*} / 12\right)$, job tardiness $L_{m a x}$, and machine idle time $I^{*}$ for nine jobs.

Table 3.13 The processing time and due dates (in minute) for 12-job problen*

| Jobs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $p$, | 10 | 12 | 12 | 9 | 6 | 5 | 7 | 7 | 8 | 8 | 7 | 5 |
| $d$, | 30 | 85 | 70 | 55 | 15 | 10 | 20 | 25 | 20 | 45 | 50 | 25 |

Step 1. An initial optimal schedule $S_{\left(S m^{\prime} / t i 00\right)}:<6-12-5-7-8-11-9-10-4-1-3-2>$ is found by arranging jobs in SPI order and followed by $d_{[j]} \leq d_{[k]}$ il $P_{1}=P_{k}$ and job $j$ and $k$ are adjacent (sce Table 3.14). The maximum lateness, $L_{\text {mux }}(S P T / E D D)$, equals to 42 corresponding to job 1 . Now Step 8 is applicd to find the machine idle time after the insertion of inaintenance.

Table 3.14 Pareto-optinal schedule, $S_{\left(s N^{\prime} /(m) m\right)}$

| Jobs | 6 | 12 | 5 | 7 | 8 | 11 | 9 | 10 | 4 | 1 | 3 | 2 |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $P_{1}$ | 5 | 5 | 6 | 7 | 7 | 7 | 8 | 8 | 9 | 10 | 12 | 12 |
| $d_{5}$ | 10 | 25 | 15 | 20 | 25 | 50 | 20 | 45 | 55 | 30 | 70 | 85 |
| $C_{1}$ | 5 | 10 | 16 | 23 | 30 | 37 | 45 | 53 | 62 | 72 | 84 | 96 |
| $L_{s}$ | 0 | 0 | 1 | 3 | 5 | 0 | 25 | 8 | 7 | 42 | 14 | 11 |

Step 8. A maintenance of 4 hours is inserted into the optimal schedule of Step 1 every 25 hours as shown in Table 3.15 Thus from the table, $L_{\text {nax }}{ }^{\prime}(S P T / E D D)=67, \sum C_{f}^{*}=5+10$ $+16 \div 23+36+43+51+66+75+97+109+128=659$ and $I^{*}=2+3+8+3=16$ for
the lirst Parcto-optimal schedule $S_{\left(\mathrm{w}^{\prime} / \boldsymbol{m}_{1}\right)}:<6-12-5-7-8-11-9-10-4-1-3-2>$. The Cost $=$ 55.86. Another possible Pareto-schedule is now sought in Step 2.

Table 3.15 Revised schedule $S_{\text {sprptop }}$ by inserting maintenance and idle times

| Jobs | 6 | 12 | 5 | 7 | $I_{b 1}$ | $M_{1}$ | 8 | 11 | 9 | $I_{b 2}$ | $M_{2}$ | 10 | 4 | $I_{b 3}$ | $M_{3}$ | 1 | 3 | $I_{b 4}$ | $M_{4}$ | 2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $p_{j}$ | 5 | 5 | 6 | 7 | 2 | 4 | 7 | 7 | 8 | 3 | 4 | 8 | 9 | 8 | 4 | 10 | 12 | 3 | 4 | 12 |
| $d_{1}$ | 10 | 25 | 15 | 20 | - | - | 25 | 50 | 20 | - | - | 45 | 55 | - | - | 30 | 70 | - | - | 85 |
| $C_{1}$ | -5 | 10 | 16 | 23 | 25 | 29 | 36 | 43 | 51 | 54 | 58 | 66 | 75 | 83 | 87 | 97 | 109 | 112 | 116 | 128 |
| $L_{j}$ | - | - | 1 | 3 | - | - | 11 | - | 31 | - | - | 21 | 20 | - | - | 67 | 39 | - | - | 43 |

 applying EDD rule followed by SPT for the jobs with same due dates (not the same processing time as in $S_{\text {(arm mon }}$ ). These computational results using Table 3.13 are reported in Table 3.16.

Table 3.16 Second Pareto-optimal schedule, $S_{\left(f, p o s, s^{p}\right)}$

| Jobs | 6 | 5 | 7 | 9 | 12 | 8 | 1 | 10 | 11 | 4 | 3 | 2 |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $p_{,}$ | 5 | 6 | 7 | 8 | 5 | 7 | 10 | 8 | 7 | 9 | 12 | 12 |
| $d_{1}$ | 10 | 15 | 20 | 20 | 25 | 25 | 30 | 45 | 50 | 55 | 70 | 85 |
| $C_{,}$ | 5 | 11 | 18 | 26 | 31 | 38 | 48 | 56 | 63 | 72 | 84 | 96 |
| $L_{,}$ | 0 | 0 | 0 | 6 | 6 | 13 | 18 | 11 | 13 | 17 | 14 | 11 |

 previous iteration, maintenance and machine idle times are considered for this Paretoschedule in the next step.

Step 8. As before, afict insering the maintenance time with appropriate ide time into Table 3.16, the revised schedule is shown in Table 3.17 in which $L_{\text {max }}{ }^{*}(E D D S P T)=43$
corresponding to job $2 ; \sum C_{i}^{*}=5+11+18+37+42+49+68+76+83+96+108+128$ $=721$, and $I^{*}=7+5+0+4=16$ for the second Pareto-optimal schedule, $S_{\text {HRDNSTI }}$ : $<6-5$ -7-9-12-8-1-10-11-4-3-2>. The Cost $=48.84$

I able 3.17 Revised schedule $S_{\left(10, s^{\prime} P^{\prime \prime}\right)}$ for second Parcto schedule.

| Jobs | 6 | 5 | 7 | $I_{61}$ | M1 | 9 | 12 | 8 | $I_{62}$ | $M_{2}$ | 1 | 10 |  | $I_{b 3}$ | $M$ | 4 | 3 | $I_{b 4}$ | M4 | 2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P, | 5 | 6 | 7 | 7 | 4 | 8 | 5 | 7 | 5 | 4 | 10 | 8 | 7 | 0 | 4 | 9 | 12 | 4 | 4 | 12 |
| $d$, | 10 | 15 | 20 | - |  | 20 | 25 | 25 | - |  | 30 | 45 | 50 | - |  | 55 | 70 |  |  | 85 |
| $C^{\prime}$ | 5 | 11 | 18 | 25 | 29 | 37 | 42 | 49 | 54 | 58 | 68 | 76 | 83 | 83 | 87 | 96 | 108 | 112 | 16 | 128 |
| $I_{3}$ | - | - | - | - | - | 17 | 17 | 24 | - | - | 38 | 31 | 33 | - | - | 4 | 38 | - | - | 43 |

Step 3. $L_{\text {max }}=I_{\text {mux }}(E D D / S P T)=18$ from $\operatorname{Stcp} 2$ since $L_{\text {max }}(E D D / S P T)$ $\leq L_{\text {prax }}(S P T / E D D)$ always. Therefore the due date is updated as $\bar{d}_{j}=d_{t}+18$ to get the third Parcto-optimal schedule according to $\bar{d}_{3}$. This is reported in Table 3.18 .

Table 3.18 Updated $\bar{d}_{1}=d_{1}+18$ (in EDD onder)

| Jobs | 6 | 5 | 7 | 9 | 12 | 8 | 1 | 10 | 11 | 4 | 3 | 2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $d$, | 10 | 15 | 20 | 20 | 25 | 25 | 30 | 45 | 50 | 55 | 70 | 85 |
| $\bar{d}$, | 28 | 33 | 38 | 38 | 43 | 43 | 48 | 63 | 68 | 73 | 88 | 103 |

Step 4. Here, $J^{c}=\{1,2,3,4,5,6,7,8,9,10,11, I 2\}$, the total number of jobs, $k=\left|J^{c}\right|=12$, and total processing time of the remaining jobs, $\tau=\sum p_{j}=96$ and sct $\delta=\tau=96$ (at the beginning).

Step 5. $J_{2}$ satislies condition $\bar{d}_{j^{*}} \geq \tau(=96)$ and the corresponding $p_{2}$ is 5 . So $J_{2}$ is scheduled as the last job in the sequence, $S_{j:<}$... $2>$.

Step 6. None of the remaining jobs satisfics the conditions $\bar{d}_{i}<\tau$ and $p_{,}>p_{j *}$.

Step 7. The set statistics is updated as $J^{c}=\{1,3,4,5,6,7,8,9,10,11,12\}, k=\left|J^{c}\right|=11$, and $t=$ $96-12=84$

Since the Steps 5 to 7 are repeated likewise in order to get the third Pareto-optimal schedule, the results of this repeated scarch are summarized in Table 3.19, and the last search results in $S_{f}:<6,12,5,7,8,9,1,11,10,4,3,2>$ which, in turn, yields the third Pareto optimal sehedule as in Table 3.20. The maximum lateness for the third Pareto-optimal schedule is $L_{\max }\left(S_{1}\right)=18$.

Table 3.19 Repetition of Steps 5 through 7

| Job <br> (j) | Processing Time ( $P_{j}$ ) | Schedule (6) | $\delta$ | $t$ |
| :---: | :---: | :---: | :---: | :---: |
| 2 | 12 | <.........................2> | 96 | 96 |
| 3 | 12 | <.......................3,2> | 96 | 84 |
| 4 | 9 | <......................4,3,2> | 96 | 72 |
| 10 | 8 | $\langle\ldots . . . . . . . . . . . . . .10,4,3,2\rangle$ | 24 | 63 |
| 11 | 7 | < $\ldots \ldots \ldots \ldots \ldots . . .11,10,4,3,2\rangle$ | 15 | 55 |
| 1 | 10 | < $\ldots \ldots \ldots \ldots . .1,11,10,4,3,2>$ | 7 | 48 |
| 9 | 8 | <, ..........9, 1, 11, $10,4,3,2>$ | 7 | 38 |
| 8 | 7 | $<\ldots \ldots . . . .8,9,1,11,10,4,3,2\rangle$ | 7 | 30 |
| 7 | 7 | < $\ldots \ldots . . .7,8,9,1,11,10,4,3,2>$ | 7 | 23 |
| 5 | 6 | < $\ldots . .55,7,8,9,1,11,10,4,3,2>$ | 7 | 16 |
| 12 | 5 | $<\ldots 12,5,7,8,9,1,11,10,4,3,2\rangle$ | 7 | 10 |
| 6 | 5 | $<6,12,5,7,8,9,1,11,10,4,3,2\rangle$ | 7 | 5 |

Table 3.20 Third Pareto-optimal schedule, $S_{1}$

| Jobs | 6 | 12 | 5 | 7 | 8 | 9 | 1 | 11 | 10 | 4 | 3 | 2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $p_{3}$ | 5 | 5 | 6 | 7 | 7 | 8 | 10 | 7 | 8 | 9 | 12 | 12 |
| $d_{j}$ | 10 | 25 | 15 | 20 | 25 | 20 | 30 | 50 | 45 | 55 | 70 | 85 |
| $C_{,}$ | 5 | 10 | 16 | 23 | 30 | 38 | 48 | 55 | 63 | 72 | 84 | 96 |
| $L_{j}$ | 0 | 0 | 1 | 3 | 5 | 18 | 18 | 5 | 18 | 17 | 14 | 11 |

Step 8. So for $\mathrm{S}^{*}$ : $<6$-12-5-7-8-9-1-11-10-4-3-2 $>$ in Table 3.21, insertion of both maittenance and machine idle times lead to $L_{\text {max }}{ }^{*}\left(S_{1}\right)=29, \sum C_{j}^{*}=5+10+16+23+36+$ $44+54+65+73+82+99+111=618$, and $I^{*}=2+0+1=3$. The Cost $=37.65$. The revised schedule is shown in Table 3.21.

Table 3.21 Revised schedule $S_{1}$

| Jobs | 6 | 12 | 5 | 7 | $I_{61}$ | $M_{1}$ | 8 | 9 | 1 | $I_{62}$ | $M_{2}$ | 11 | 10 | 4 | $I_{53}$ | $M_{3}$ | 3 | 2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $p_{1}$ | 5 | 5 | 6 | 7 | 2 | 4 | 7 | 8 | 10 | - | 4 | 7 | 8 | 9 | 1 | 4 | 12 | 12 |
| $d_{j}$ | 28 | 43 | 33 | 38 | - | - | 43 | 38 | 48 | - | - | 68 | 63 | 73 | - | - | 88 | 103 |
| $C_{5}$ | 5 | 5 | 10 | 16 | 23 | 25 | 29 | 36 44 54 54 58 65 73 82 83 87 99 | 111 |  |  |  |  |  |  |  |  |  |
| $L_{J}$ | - | - | 1 | 3 | - | - | 11 | 24 | 24 | - | - | 15 | 28 | 27 |  | - | 29 | 26 |

Step 9. At this step, set $L_{\text {max }}=L_{\max }+\delta=18+7=25$. Since $L_{\operatorname{mux}}=25<L_{\max }(S P T / E D D)=$ 42, continue to the next iteration for another schedule.

Table 3.22 Repetition of Steps 5 through 7

| Job (j) | Processing Time $\left(P_{j}\right)$ | Schedule (S) | $\delta$ | $\tau$ |
| :---: | :---: | :---: | :---: | :---: |
| 2 | 12 | <.........................2> | 96 | 96 |
| 3 | 12 | <.......... ..............3,2> | 96 | 84 |
| 4 | 9 | <......................4,3,2> | 96 | 72 |
| 10 | 8 | <.., ..............10,4,3,2> | 17 | 63 |
| 1 | 10 | <...............1,10,4,3,2> | 8 | 55 |
| 9 | 8 | < $\ldots . \ldots \ldots \ldots . . . .9,1,10,4,3,2\rangle$ | 8 | 45 |
| 11 | 7 | <,..........11,9,1,10,4,3,2> | 8 | 37 |
| 8 | 7 | < $\ldots \ldots . \ldots . .8,11,9,1,10,4,3,2>$ | 8 | 30 |
| 7 | 7 | < $\ldots \ldots \ldots . .7,8,11,9,1,10,4,3,2>$ | 8 | 23 |
| 5 | 6 | $<\ldots \ldots .5,7,8,11,9,1,10,4,3,2>$ | 8 | 16 |
| 12 | 5 | <...12,5,7,8,11,9,1,10,4,3,2> | 8 | 10 |
| 6 | 5 | $:\langle 6,12,5,7,8,11,9,1,10,4,3,2\rangle$ | 8 | 5 |

Fourh Pareto-optimal schedule, $S_{2}$ by inscrting maintenance and idle time:
Table 3.23 Revised schedule $S_{2}$

| Jobs | 6 | 12 | 5 | 7 | $I_{61}$ | $M_{1}$ | 8 | 11 | 9 | $J_{\text {b } 2}$ | $M_{2}$ | 1 |  |  | $I_{6} 3$ | N |  | 4 | 3 |  | $M_{4}$ | 2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $p_{\text {j }}$ | 5 | 5 | 6 | 7 | 2 | 4 | 7 | 7 | 8 | 3 | 4 | 10 |  |  | 7 |  |  | 9 | 12 | 4 | 4 | 12 |
| d) | 35 | 50 | 40 | 45 | - |  | 50 | 75 | 45 |  |  | 55 |  | 0 |  |  |  | 80 | 95 |  |  | 110 |
| $C^{\prime}$ | 5 | 10 | 16 | 23 | 25 | 29 | 36 | 43 | 51 | 54 | 58 | 68 |  | 6 | 83 | 87 |  | 96 | 108 |  | 116 | 128 |
| L, | - |  | 1 | 3 | - | - | 11 | - | 31 | - | - | 38 |  | 1 | - |  |  | 41 | 38 |  | - | 43 |

So for $\mathrm{S}_{2}{ }_{2}$ : <6-12-5-7-8-11-9-1-10-4-3-2> in Table 3.23, insertion of both maintenance and machine idle times lead to $L_{\max }{ }^{*}\left(S_{2}\right)=43, \sum C_{j}{ }^{*}=5+10+16+23+36+43+51+68$ $+76+96+108+128=660$, and $I^{*}=2+3+7+4=16$. The Cost $=46.30$.

At this step, set $L_{\max }=L_{\max }+\delta=25+8=33$. Since $L_{\max }=33<L_{\operatorname{mux}}(S P T / E D D)=42$, continue to the next iteration for another schedule.
lable 3.24 Repetition of Steps 5 through 7

| $\begin{aligned} & \text { Job } \\ & \text { (i) } \end{aligned}$ | Processing Time $\left(P_{i}\right)$ | Schedule (S) | $\delta$ | $\tau$ |
| :---: | :---: | :---: | :---: | :---: |
| 2 | 12 | <............... .........2> | 96 | 96 |
| 3 | 12 | <.......................3,2> | 96 | 84 |
| 4 | 9 | <.....................4,3,2> | 96 | 72 |
| 1 | 10 | <........ . ...........1,4,3,2> | 9 | 63 |
| 10 | 8 | $\langle\ldots \ldots \ldots \ldots \ldots \ldots . .10,1,4,3,2\rangle$ | 9 | 53 |
| 9 | 8 | <...............9,10,1,4,3,2> | 9 | 45 |
| 11 | 7 | < $\ldots . . . . . . . . .11,9,10,1,4,3,2\rangle$ | 9 | 37 |
| 8 | 7 | $\langle\ldots \ldots \ldots . .8,11,9,10,1,4,3,2\rangle$ | 9 | 30 |
| 7 | 7 | <,........7,8, $11,9,10,1,4,3,2>$ | 9 | 23 |
| 5 | 6 | $\langle\ldots \ldots . .5,7,8,11,9,10,1,4,3,2\rangle$ | 9 | 16 |
| 12 | 5 | < $\ldots .12,5,7,8,11,9,10,1,4,3,2>$ | 9 | 10 |
| 6 | 5 | : $\langle 6,12,5,7,8,11,9,10,1,4,3,2\rangle$ | 9 | 5 |

Fiflh Pareto-optimal schedule, $S_{3}$ by inserting maintenance and idle time:
Table 3.25 Revised schedule $S_{3}$

| Jobs | 6 | 12 | 5 | 7 | $I_{b 1}$ | $M$ | 8 | 11 | 9 | $l_{b 2}$ |  | 10 | 1 | $I_{63}$ | $M_{3}$ | 4 | 3 |  | $M_{4}$ | 2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $p$, | 5 | 5 | 6 | 7 | 2 | 4 | 7 | 7 | 8 | 3 | 4 | 8 | 10. | 7 | 4 | 9 | 12 | 4 | 4 | 12 |
| $d$ | 43 | 58 | 48 | 53 | - |  | 58 | 83 | 53 | - |  | 78 | 63 | - |  | 88 | 103 | * |  | 118 |
| $C^{\prime}$ | 5 | 10 | 16 | 23 | 25 | 29 | 36 | 43 | 51 | 54 | 58 | 66 | 76 | 83 | 87 | 96 | 108 |  |  | 128 |
| $L$, | - | - | 1 | 3 | - |  | 11 | - | 31 | - |  | 21 | 46 | - |  | 41 | 38 | - | - | 43 |

So for $\mathrm{S}^{* 3}$ : $\langle 6-12-5-7-8-1$ 1-9-10-1-4-3-2 $\rangle$ in Table 325, insertion of both mantenance and machine idle times lead to $L_{\max }{ }^{*}\left(S_{3}\right)=43, \sum C_{1}^{*}=5+10+16+23+36+43+51+66+$ $76+96+108+128=658$, and $I^{*}=2+3+7+4=16$. The $\operatorname{Cost}=47.42$.

Al this step, sct $L_{\max }=L_{\max }+\delta=33+9=42$. Since $L_{\max }=L_{\text {pax }}(S P T / E D D)=42$, So, Slop

Table 3.26 Repetition of Steps 5 through 7

| Job <br> (j) | Processing Time $\left(P_{j}\right)$ | Schedulc (S) | $\delta$ | $\tau$ |
| :---: | :---: | :---: | :---: | :---: |
| 2 | 12 | <.......................2> | 96 | 96 |
| 3 | 12 | <........................3,2> | 96 | 84 |
| 1 | 10 | < ................. ....4,3,2> | 96 | 72 |
| 4 | 9 | <...................1,4,3,2> | 9 | 63 |
| 10 | 8 | < ................10, 1,4,3,2> | 9 | 53 |
| 9 | 8 | <..............9,10,1,4,3,2> | 9 | 45 |
| 11 | 7 | < $\ldots . . . . . . . . .11,9,10,1,4,3,2>$ | 9 | 37 |
| 8 | 7 | $<\ldots \ldots . . . .8,8,11,9,10,1,4,3,2\rangle$ | 9 | 30 |
| 7 | 7 | <,.......7, $7,11,9,10,1,4,3,2\rangle$ | 9 | 23 |
| 5 | 6 | < $\ldots \ldots . .5,7,8,11,9,10,1,4,3,2\rangle$ | 9 | 16 |
| 12 | 5 | < $\ldots .12,5,7,8,11,9,10,1,4,3,2\rangle$ | 9 | 10 |
| 6 | 5 | : $\langle 6,12,5,7,8,11,9,10,1,4,3,2\rangle$ | 9 | 5 |

Sixth Pareto-optimal schedule, $S_{\uparrow}$ by inserting maintenance and idle time;
Table 3.27 Revised schedule $S_{4}$

| Jobs | 6 | 12 | 5 | 7 | $I_{b i}$ | $M_{1}$ | 8 | 11 | 9 | $I_{b 2}$ | $M_{2}$ | 10 | 4 | $I_{b 3}$ | $M_{3}$ | 1 | 3 | $I_{b 4}$ | $M_{4}$ | 2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $p_{1}$ | 5 | 5 | 6 | 7 | 2 | 4 | 7 | 7 | 8 | 3 | 4 | 8 | 9 | 8 | 4 | 10 | 12 | 3 | 4 | 12 |
| $d_{1}$ | 52 | 67 | 57 | 62 | - | - | 67 | 92 | 62 | - | - | 87 | 97 | - | - | 72 | 112 | - | - | 127 |
| $C_{1}$ | -5 | 10 | 16 | 23 | 25 | 29 | 36 | 43 | 51 | 54 | 58 | 66 | 75 | 83 | 87 | 97 | 109 | 112 | 116 | 128 |
| $L_{j}$ | - | - | 1 | 3 | - | - | 11 | - | 31 | - | - | 21 | 20 | - | - | 67 | 39 | - | - | 43 |

So for $\mathrm{S}_{4}^{*}$ : $\langle 6$-12-5-7-8-11-9-10-4-1-3-2 $\rangle$ in Table 3.27, insertion of both maintenance and machine ide times lead to $L_{\max }{ }^{*}\left(S_{4}\right)=43, \sum C_{j}{ }^{\prime}=5+10+16+23+36+43+51+66$ $+75+97+109+128=659$, and $\Gamma^{*}=2+3+8+3=16$. The Cost $=55.86$.

Table 3.28 All the itcrations of the algorithm

| Iteration $m$ | Scheduie | Pareto-Optima! Sequence | $\begin{aligned} & \sum_{j=1}^{12} C_{j}^{\prime} \\ & L_{\max }^{\prime}, I_{m}^{\prime} \end{aligned}$ | Current $d_{j}+\delta$ | $\delta$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | SPTIEDD | <6-2-5-7-7-11-9-10-4-1-3-2> | 659, 67, 16 | 10, 25, 15, 20, 25, 50, 20, 45, 55, 30, 70, 85 | - |
| 2 | ECDSPT |  | F2, 1, 43, i6 | 10, 15, 20, 20, 25, 25, $00.45,50,55,70,85$ | 18 |
| 3 | S, | < $6-12-5-7-8 \cdot 9-1-11-10-4-3-2\rangle$ | 618.29, 3 | 28, 43, $33,38,43,38,48,68,63,73,88,103$ | 7 |
| 4 | $S_{7}$ | < 6-12-5-7-8-11-9-1-10-4.3-2> | 660, 43, 16 | 35, 50, 40, 45, 50, 75, 45, 55, 70, 80, 95, 110 | 8 |
| 5 | S 3 | < $6-12-5-7 \cdot 8 \cdot 11-9 \cdot 10 \cdot 1-43-2>$ | 658,46, 16 | 43, 58, 48, 53, 58, 83, 53, 78,63, 88, 103, 118 | 9 |
| 6 | Ss | $\langle 6-12-5-7-8-11-9-10-4-1-3-2\rangle$ | 659,67, 16 | $52,67,57,62,67,92,62,87,97,72,112,127$ | Stop |

Alter generating all possible Pareto-oplimal schedules with respect to job completion time $\bar{F}^{*}$, job tardiness $L_{\text {mata }}{ }^{*}$, and machine idle time $I^{*}$ for twelve jobs, the total weighted function, $c\left(\bar{F}^{*}, L_{\text {mas }}{ }^{2}, I^{2}\right)=w_{1}\left(\sum_{i=1}^{12} C_{i}^{2} / 12\right)+w_{2} L_{\text {llax }}+w_{3} I^{*}$, where $w_{l}=0.5, w_{2}=0.4, w_{3}=0.1$ (arbitrarily chosen) for 6 schedules is calculated [sce Table 3.28]. The minimum-weighted schedule is $S^{*}=S_{l}:<6-12-5-7-8-9-1-11-10-4-3-2>$ corresponding to $c\left(\bar{F}^{*}, L_{\max }, I^{*}\right)=$ 37.65.

Table 3.29 A Pareto-Optimal Set

| Iterallon <br> m | Schedule | Pareto-Opplimal Sequence | $\sum_{j=1}^{12} C_{j}{ }^{\prime}, L_{\text {max }}{ }^{\text {a }}$, $I_{\text {mit }}$ | $c\left(\bar{F}^{*}, L_{\text {max }}{ }^{*}, I^{*}\right)$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | SPT/EDD | <6-12-5-7-8-11-9-10-4-1-3-2> | 659, 67, 16 | 55.86 |
| 2 | EDDISPT | <6-5-7-9-12-8-1-10-11-4-3-2> | 721, 43, 16 | 48.84 |
| 3 | $\mathrm{s}_{1}$ | < 6-12-5-7-8-9-1-11-10-4-3.2> | 618, 29, 3 | 37.65 |
| 4 | $S_{2}$ | <6-12-5-7-8-11-9-1-10-4-3-2 > | $660,43,16$ | 46.30 |
| 5 | $\mathrm{S}_{3}$ | <6-12-5-7-8-11-9-10-1-4-3-2> | $658,46,16$ | 47.42 |
| 6 | $S_{4}$ | <6-12-5-7-8-11-9-10-4-1-3-2> | 659, 67, 16 | 55.86 |

[^1]
### 3.8 Neighborhood Scarch Algorithm

As a second approach to the multi-criterion scheduling problem, a neighborhood scarch technique is considered. Many discrete optimization problerns of practical interest cannot be solved optimally in the reasonable time. A practical approach to these problems is to use heuristics which do not guarantee the optimality of the solution, but near-optimal solutions can be obtained in a tolerable time limit. Neighborhood search starts with a feasible schedule and iteratively trics to improve the solution. At each stage, it scarches the "neighborhood" of the current solution to find an improved solution. The search terminates when it finds a solution that is at least as good as any of its neighbors; such a solution is called a locally optimal solution. A method of taking one sequence as a seed and systematically creating a collection of related sequences is the generating mechanism. In this work, the single adjacent pairwise interchange operation serves as a generating mechanism for the example. The neighborhood of the seed sequence is a list of $(n-1)=12-1$ $=11$, distinct sequences for this paricular generating mechanism. The single adjacent pairwise interchange mechanism is applied to the initial seed, and the performance measure (weighted function) of each seed is compared with the pertomance measure of its neighborhood. Instead of generating all the sequences in the neighborhood of the seed, when a neighborhood gives an improved perfomance measure, the search stops, and that sequence becomes the new seed for the next stage. When a search of the new neighborhood produces no improvement, the search procedure terminates. The delails of the secd with their neighborhood sequences and their perfonnance measures are presented in Tables 3,30. Search terminates with weighted functional value $=68.917$

Table 3.30 Solution with a given initial seed, $S:\langle 1-2-3-4-5-6-7-8-9-10-11-12\rangle$

|  | Schedule | $\sum_{j=1}^{12} C^{\prime}{ }^{\prime}$ | $L_{\text {max }}$ | $I_{\text {m }}$ | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Stage 1 |  |  |  |  |
| Seed: Neighborhood: | $\begin{aligned} & <1-2-3-4-5-6 \cdot 7 \cdot 8-9-10-11-12> \\ & <2-1-3-4-5-6 \cdot 7-8-9-10-11-12> \\ & \langle 1 \cdot 3-2-4-5-6 \cdot 7-7-9-10-11-12> \\ & <1-2-4-3-5-6-7-8-9-10-11-12> \end{aligned}$ | $\begin{aligned} & 844 \\ & 846 \\ & 844 \\ & 841 \end{aligned}$ | $\begin{aligned} & 96 \\ & 96 \\ & 96 \\ & 96 \\ & \hline \end{aligned}$ | $\begin{aligned} & 9 \\ & 9 \\ & 9 \\ & 9 \\ & \hline \end{aligned}$ | $\begin{array}{r} 74.467 \\ 74.550 \\ 74.467 \\ 74.342^{*} \\ \hline \end{array}$ |
| Stage 2 |  |  |  |  |  |
| New Seed: Neighbohood: | $\begin{aligned} & <1-2-4-3-5-6-7-8-9-10-11-12> \\ & <2-1-4-3-5-6-7-8-9-10-11-12> \\ & <1-4-2-3-5-6-7-8 \cdot 9-10-11-12> \\ & <1-2-3-4-5-6-7-8-9-10-1112> \\ & <1-2-4-5-3-6-7-8-9-10-1112> \\ & <1-2-4-3-6-5-7-8-9-10-11-12> \end{aligned}$ | $\begin{aligned} & \hline 841 \\ & 843 \\ & 844 \\ & 844 \\ & 898 \\ & 840 \end{aligned}$ | 96 96 96 96 103 96 | $\begin{gathered} \hline 9 \\ 9 \\ 9 \\ 9 \\ 16 \\ 9 \\ \hline \end{gathered}$ | $\begin{gathered} 74.342 \\ 74.425 \\ 74.467 \\ 74.467 \\ 80.217 \\ 74.300 * \end{gathered}$ |
| Stage 3 |  |  |  |  |  |
| New Seed: Neighborhood: | <1-2-4-3-6-5-7-8-9-10-11-12> <2-1-4-3-6-5-7-8-9-10-11-12> <1-4.2-3-6-5-7-8-9-10-11-12> <1-2-3-4-6-5-7-8-9-10-11-12> <1-2-4-6-3-5-7-8-9-10-11-12> <1-2-4-3-5-6-7-8-9-10-11-12> <1-2-4-3-6-7-5-8-9-10-11-12> <1-2-4-3-6-5-8-7-9-10-11-12> <1-2-4-3-6-5-7-9-8-10-11-12> <1-2-4-3-6-5-7-8-10-9-11-12> <1-2-4-3-6-5-7-8-9-11-10-12> | $\begin{aligned} & 840 \\ & 842 \\ & 843 \\ & 843 \\ & 899 \\ & 841 \\ & 841 \\ & 840 \\ & 880 \\ & 840 \\ & 899 \end{aligned}$ | $\begin{gathered} \hline 96 \\ 96 \\ 96 \\ 96 \\ 103 \\ 96 \\ 96 \\ 96 \\ 103 \\ 96 \\ 96 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 16 \\ 9 \\ 9 \\ 9 \\ 9 \\ 16 \\ 9 \\ 9 \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 74.300 \\ & 74.383 \\ & 74.425 \\ & 74.425 \\ & 80.258 \\ & 74.342 \\ & 74.342 \\ & 74300 \\ & 79.717 \\ & 74.300 \\ & 74.258{ }^{*} \\ & \hline \end{aligned}$ |
| Stage 4 |  |  |  |  |  |
| New Seed: Neighborhood | <1-2-4-3-6-5-7-8-9-11-10-12> <2-14-3-6-5.7-8-9-11-10-12> <1-4-2-3-6-5-7-8-9-11-10-12> <1-2;-4-6-5-7-8-9-11-10-12> <1-2-4-6-3-5-7-8-9-11-10-12> <1-2-4-3-5-6-7-8-9-11-10-12> <1-2-4-3-6.7-5-8-9-11-10-12> <1-2-4-3-6-5-8-7-9-11-10-12> <1-2-4-3-6-5-7-9-8-11-10-12> <1-2-4-3-6-5.7-8-11-9-10-12> | 839 841 842 842 900 840 840 839 887 838 | $\begin{gathered} \hline 96 \\ 96 \\ 96 \\ 96 \\ 104 \\ 96 \\ 96 \\ 96 \\ 104 \\ 96 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 9 \\ 9 \\ 9 \\ 9 \\ 17 \\ 9 \\ 9 \\ 9 \\ 17 \\ 9 \\ \hline \end{gathered}$ | 74258 <br> 74.342 <br> 74.383 <br> 74.383 <br> 80.800 <br> 74.3010 <br> 74.300 <br> 74.258 <br> 80.258 <br> 74.217 * |
| Stage 5 |  |  |  |  |  |
| New Seed: Neighborhood: | $\begin{aligned} & <1-2-4-3-6-5 \cdot 7-8-11-9-10-12> \\ & <2-1-4-3-6-5 \cdot 7-8-11-9-10-12> \\ & <1-4-2-3-6-5-7-8-11-9-10-12> \\ & <1-2-3-4-6-5-7-8-11-9-10-12> \\ & <1-2-4-6-3-5-7-8-11-9-10-12> \\ & \langle 1-2-4-3-5-6-7-8-11-9-10-12> \end{aligned}$ | $\begin{aligned} & 838 \\ & 840 \\ & 841 \\ & 841 \\ & 899 \\ & 839 \end{aligned}$ | $\begin{aligned} & \hline 96 \\ & 96 \\ & 96 \\ & 96 \\ & 104 \\ & 96 \end{aligned}$ | 9 9 9 9 17 9 | $\begin{aligned} & 74.217 \\ & 74.300 \\ & 74.342 \\ & 74.342 \\ & 80.758 \\ & 74.258 \end{aligned}$ |



To compare the modified Pareto-optimal algorithm with the neighborhood search heuristic in case of real life data, the same instance with parameters $T=25, M=4, w_{t}=0.5, w_{2}=0.4$ and $w_{3}=0.1$ is used. The neighborhood search heuristic gives the best near-optimal schedule as $\mathrm{S}:<1-2-4 \cdot 3-6-5 \cdot 7-11-6-9-12-10\rangle$ with the mininum weighted function equals to 68.917. On the other hand, the modified Pareto-optimal algorithm gives the best nearoptimal schedule as $\mathrm{S}:<6-12-5-7-8-9-1-11-10-4-3-2\rangle$ with the minimum weighted function equals to 37.65. It can be concluded that the modified Pareto-optimal algorithm provides a better result than the neighborhood search heuristic for this instance.

The same inslance shown in the example of real life data is repeated for nineteen levels of $T$ $(12,13, \ldots, 30)$ and five levels of $M(4,5,6,7,8)$ to show the performance of various sets of Pareto-optimal schedules for different maintenance plans. Table 3.31 shows the costs of Pareto-optimal algorithm and neighborhood search method for a paricular weight combination and Table 3.32 shows for the all possible weight combinations. In both cases

Pareto-optimal algorithm gives better results than that of neighborhood search method. Also these have been shown in Figures 3.1, .., 3.10.

As the time to petform maintenance, $M$ increascs, both the completion time and the maximum lateness increases too. On the other hand, as the time interval between two maintenance periods, $T$ changes, all three objectives are changing as well because of forming different batches.

Table 3.31 Pareto vs Neighborhood: Costs from One Weight Combination ( $w_{1}=0.5, w_{2}$ $=0.4, w_{3}=0.1$ )

| M | T | Parcto | Neighborhood |
| :---: | :---: | :---: | :---: |
| 4 | 12 | 67.22 | 83.38 |
|  | 13 | 72.34 | 79.62 |
|  | 14 | 65.20 | 75.56 |
|  | 15 | 58.85 | 80.57 |
|  | 16 | 6064 | 85.59 |
|  | 17 | 53.04 | 90.61 |
|  | 18 | 56.29 | 72.57 |
|  | 19 | 60.42 | 70.07 |
|  | 20 | 48.65 | 71.34 |
|  | 21 | 51.98 | 69.61 |
|  | 22 | 55.40 | 67.72 |
|  | 23 | 40.88 | 66.33 |
|  | 24 | 43.59 | 68.97 |
|  | 25 | 37.65 | 68.92 |
|  | 26 | 39.73 | 61.70 |
|  | 27 | 41.86 | 63.03 |
|  | 28 | 43.98 | 57.16 |
|  | 29 | 46.11 | 63.04 |
|  | 30 | 38.21 | 60.82 |
|  | 12 | 72,82 | 89.28 |
|  | 13 | 77.86 | 84.82 |
|  | 14 | 70.02 | 79.88 |
|  | 15 | 63.11 | 84.89 |
|  | 16 | 64.73 | 89.91 |
|  | 17 | 56.61 | 94.93 |
|  | 18 | 59.82 | 75.82 |
| 5 | 19 | 63.94 | 73.40 |




| M | T | Pareto | Neighborhood |
| :---: | :---: | :---: | :---: |
| 7 | 22 | 64.15 | 75.65 |
|  | 23 | 47.81 | 73.06 |
|  | 24 | 50.43 | 76.10 |
|  | 25 | 43.13 | 75.39 |
|  | 26 | 45.21 | 67.80 |
|  | 27 | 47.33 | 69.13 |
|  | 28 | 49.46 | 61.72 |
|  | 29 | 51.58 | 68.77 |
|  | 30 | 42.51 | 65.34 |
| 8 | 12 | 89.62 | 119.15 |
|  | 13 | 94.41 | 100.79 |
|  | 14 | 84.50 | 92.83 |
|  | 15 | 75.88 | 97.84 |
|  | 16 | 77.01 | 103.26 |
|  | 17 | 67.31 | 108.68 |
|  | 18 | 70.39 | 85.57 |
|  | 19 | 74.52 | 83.40 |
|  | 20 | 60.32 | 82.91 |
|  | 21 | 63.65 | 82.28 |
|  | 22 | 67.07 | 78.29 |
|  | 23 | 50.03 | 75.70 |
|  | 24 | 52.74 | 78.74 |
|  | 25 | 44.95 | 77.95 |
|  | 26 | 47.03 | 69.83 |
|  | 27 | 49.16 | 71.17 |
|  | 28 | 51.28 | 63.23 |
|  | 29 | 53.41 | 70.68 |
|  | 30 | 44.21 | 67.25 |

Table 3.32: Pareto vs Neighborhood: Costs from all Weight combinations ( $w_{1}=0.1$ to 0.8 , $w_{2}=0.1$ to $0.8, w_{3}=0.1$ to 0.8 , and $\left.w_{1}+w_{2}+w_{3}=1.0\right)$



Pareio Optimal: Coste from One Weight Combination (wi=0.5, w2=0.4, w $3=0.1$ )


Figure 3.1 Pareto Optinal: Costs from One Weight Combination.

Neighborhood Search: Costs from One Woight Combination (w1=0.5, w2=0.4, $w 3=0.1$ )


Figure 3.2 Neighborhood Search: Costs from One Weight Combination

## Pareto vs Neighborhood: Costs from One Weight Combination

 ( $\mathbf{w} 1=0.5, \mathrm{w} 2=0.4, \mathrm{w} 3=0.1$ ), and Maintenance Time $\mathrm{M}=4$
ligure 3.3 Pareto vs Neighborhood: Costs from One Weight Combination

Pareto vs Neighborhood: Cosis from One Weight Combination ( $\mathbf{w} 1=0.5, w_{2}=0.4, w^{3}=0.1$ ), and Maintenance Time $M=6$


Figure 3.4 Pareto vs Neighborhood: Costs from One Weight Combination

## Pareto vs Neighborhood: Costs from One Weight Combination

 ( $\mathbf{w} t=0.5, \mathrm{w} 2=0.4, \mathrm{w} 3=0.1$ ), and Maintenance Time $\mathrm{M}=8$

Figure 3.5 Pareto vs Neighborhood: Costs from One Weight Combination


Figure 3.6 Pareto Optimal: Costs from All Weight Combinations

Neighborhood Search: Costs from All Weight Combinations ( $w 1=0.1$ to $0.8, w 2=0.1$ to $0.8, w 3=0.1$ to 0.8 , and $w 1+w 2+w 3=1.0$ )


Figure 3.7 Neighborhood Search: Costs from All Weight Combinations


Figure 3.8 Parelo vs Neighborhood: Costs from all Weight combinations.

Pareto vs Neighborhood: Costs from All Weight Combinations ( $w 1=0.1$ to $0.8, w 2=0.1$ to $0.8, w 3=0.1$ to 0.8 , and $w i+w 2+w 3=1.0$ ), and Waintenance Time $\mathrm{M}=6$


Figure 3.9 Pareto vs Neighborhood: Costs from all Weight combinations.

Pareto vs Neighborbood: Costs from All Weight Combinations ( $w 1=0.1$ to $0.8, w 2=0.1$ to $0.8, w^{3}=0.1$ to 0.8 , and $w 1+w 2+w 3=1.0$ ), and Maintenance Time $\mathrm{M}=8$


Figure 3.10 Parcto vs Neighborhood: Costs from all Weight combinations.

Various maintenance plans give more flexibility to the scheduler (or decision-maker) to make a decision according to the prelerence and available maintenance altematives. Moreover, to transform multiple objectives into a single objective optimization problem, a weighted combination is considered. The weights may be time or situation dependent and sum of the weights must be equal to 1 . Typically, a sclueduler may not know the exact weights and may want to perform a parametric analysis to get a feeling for the trade-offs. In this work, all possible weight combinations of three objectives are perlormed to calculate the weighted function. lhese possible combinations for each schedule of Pareto-optimal set are also presented. The reason of presenting all the possible weight-combinations is that the imporance level of each objective can be diflerent according to the scheduler. These results are summarized in Appendix A. Appendix A provides cost of Pareto-optimal schedules which is dependent on total completion time, maximum Jaleness, and machine idle time for each combination of $T$ and $M$ for the all possible weight combinations. Table 3.29 only provides Pareto-optimal schedules with one possible weight combination (i.c., $w_{1}=0.5, w_{2}=$ $0.4, w_{3}=0.1$ ), while Appendix A provides information on the all possible weight combinations of thre objectives $\left(\bar{F}^{*}, L_{\text {max }}{ }^{*}, I^{*}\right)$. Also the sum of the costs of each Paretooptimal schedule for all the weight combinations is calculated in order to give an overall result of certain Pareto-optimal schedule. A schedule with the minimum sum of the costs is the best schedule within the set of Pareto-optimal schedules for a certain maintenance plan. Table 3.33 presents the sum of the costs of each Pareto-optimal schedule for all the weight combinations according to a certain maintenance plan. It also provides the Pareto-optimal schedule which gives the minimum cost for each maintenance plan. $A$ decision maker can decide which Parcto-optimal schedule and which combination ol weights he/she wants to use according to an available maintenance plan (i.c., $T$ and $M$ values). It can be concluded that the objective $c\left(\bar{F}^{*}, L_{\text {nux }}{ }^{*}, I^{*}\right)$ is depended on $T$ and $M$, and his shows the importance of a good mantenance plan. The minimum cost is 1002.00 for $\mathrm{T}=25$ and for $\mathrm{M}=4$.

Table 3.33 Summary of performance measures for all different alternative parameters

| T | M | SPT/EDD | SPT/EDI | S[1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I2 | 4 | 2709.00 | 2014.00 | 2457.00 | 2457.00 | 2517.00 | 2709.00 |
|  | 5 | 2860.00 | 2170.00 | 2632.00 | 2632.00 | 2656.00 | 2860.00 |
|  | 6 | 3011.00 | 2326.00 | 2807.00 | 2807.00 | 2807.00 | 3011.00 |
|  | 7 | 3162.00 | 2482.00 | 2982.00 | 2982.00 | 2982.00 | 3162.00 |
|  | 8 | 3313.00 | 2638.00 | 3157.00 | 3157.00 | 3157.00 | 3313.00 |
| 13 | 4 | 2473.00 | 2264.00 | 2245.00 | 2245,00 | 2269.00 | 2473.00 |
|  | 5 | 2603.00 | 2419.00 | 2399.00 | 2399.00 | 2399.00 | 2603.00 |
|  | 6 | 2733.00 | 2574.00 | 2553.00 | 2553.00 | 2553.00 | 2733.00 |
|  | 7 | 2863.00 | 2729.00 | 2707.00 | 2707.00 | 2707.00 | 2863.00 |
|  | 8 | 2993.00 | 2884.00 | 2861.00 | 2861.00 | 2861.00 | 2993.00 |
| 14 | 4 | 2208.00 | 2527.00 | 2507.00 | 2004.00 | 2004.00 | 2208.00 |
|  | 5 | 2319.00 | 2682.00 | 2661.00 | 2139.00 | 2139.00 | 2319.00 |
|  | 6 | 2430.00 | 2837.00 | 2815.00 | 2274.00 | 2274.00 | 2430.00 |
|  | 7 | 2541.00 | 2992.00 | 2969.00 | 2409.00 | 2409.00 | 2541.00 |
|  | 8 | 2652.00 | 3147.00 | 3123.00 | 2544.00 | 2544.00 | 2652.00 |
| 15 | 4 | 2415.00 | 1758.00 | 1758.00 | 2235.00 | 2235.00 | 2415.00 |
|  | 5 | 2526.00 | 1877.00 | 1877.00 | 2370.00 | 2370.00 | 2526.00 |
|  | 6 | 2637.00 | 1996.00 | 1996.00 | 2505.00 | 2505.00 | 2637.00 |
|  | 7 | 2748.00 | 2115.00 | 2115.00 | 2640,00 | 2640.00 | 2748.00 |
|  | 8 | 2859.00 | 2234.00 | 2234.00 | 2775.00 | 2775.00 | 2859.00 |
| 16 | 4 | 2041.00 | 1961.00 | 1925.00 | 1885.00 | 1885.00 | 2041.00 |
|  | 5 | 2132.00 | 2080.00 | 2042.00 | 2000.00 | 2000.00 | 2132.00 |
|  | 6 | 2223.00 | 2199.00 | 2159.00 | 2115.00 | 2115.00 | 2223.00 |
|  | 7 | 2314.00 | 2318.00 | 2276.00 | 2230.00 | 2230.00 | 2314.00 |
|  | 8 | 2405.00 | 2437.00 | 2393.00 | 2345.00 | 2345.00 | 2405.00 |
| 17 | 4 | 1684.00 | 2164.00 | 1597.00 | 1573.00 | 2084.00 | 1684.00 |
|  | 5 | 1759.00 | 2283.00 | 1698.00 | 1673.00 | 2199.00 | 1759.00 |
|  | 6 | 1834.00 | 2402.00 | 1799.00 | 1773.00 | 2314.00 | 1834.00 |
|  | 7 | 1909.00 | 2521.00 | 1900.00 | 1873.00 | 2429.00 | 1909.00 |
|  | 8 | 1984.00 | 2640.00 | 2001.00 | 1973.00 | 2544.00 | 1984.00 |
| 18 | 4 | 1831.00 | 1725.00 | 1723.00 | 1725.00 | 1723.00 | 1831.00 |
|  | 5 | 1906.00 | 1824.00 | 1822.00 | 1824.00 | 1822.00 | 1906.00 |
|  | 6 | 1981.00 | 1923.00 | 1921.00 | 1923.00 | 1921.00 | 1981.00 |
|  | 7 | 2056.00 | 2022.00 | 2020.00 | 2022.00 | 2020.00 | 2056.00 |
|  | 8 | 2131.00 | 2121.00 | 2119.00 | 2121.00 | 2119.00 | 2131.00 |
| 19 | 4 | 1978.00 | 1896.00 | 1894.00 | 1896.00 | 1894.00 | 1978.00 |
|  | 5 | 2053.00 | 1995.00 | 1993.00 | I995.00 | 1993.00 | 2053.00 |
|  | 6 | 2128.00 | 2094.00 | 2092.00 | 2094.00 | 2092.00 | 2128.00 |
|  | 7 | 2203.00 | 2193.00 | 2191.00 | 2193.00 | 2191.00 | 2203.00 |
|  | 8 | 2290.00 | 2292.00 | 2290.00 | 2292.00 | 2290.00 | 2290.00 |
| 20 | 4 | 2125.00 | 1434.00 | 2065.00 | 2067.00 | 2065.00 | 2125.00 |
|  | 5 | 2200.00 | 1516.00 | 2164.00 | 2166.00 | 2164.00 | 2200.00 |
|  | 6 | 2275.00 | 1598.00 | 2263.00 | 2265.00 | 2263.00 | 2275.00 |
|  | 7 | 2362.00 | 1680.00 | 2362.00 | 2364.00 | 2362.00 | 2362.00 |
|  | 8 | 2461.00 | 1762.00 | 2461.00 | 2463.00 | 2461.00 | 2461.00 |
| 21 | 4 | 1719.00 | 1576.00 | 1667.00 | 1574.00 | 1612.00 | 1719.00 |
|  | 5 | 1777.00 | 1658.00 | 1740.00 | 1656.00 | 1670.00 | 1777.00 |
|  | 6 | 1835.00 | 1740.00 | 1813.00 | 1738,00 | 1740.00 | 1835.00 |



* Mitiomum sum of the cost for each maintenance plan


### 3.9 Conclusion

A multi-criterion non-preemptive scheduling that reduces the total cost of the problem is considered in this sludy. Three criterions are considered; reduction of flow time, maximum tardiness, and machine idle time in a periodically maintained single machine problcm. The trade-olfs betwen the flow time and maximum tardiness is comparatively simple, but the trade-ofl between minimum flow time, maximum tardiness and machine idle time is a complex problem. In this study a new kind of approach that allows the use of weighted aggregation of the criterions is presented. The new approach started with an initially obtained set of Pareto-optimal schedule for flow time and maximum Lardness minimization problem. It then introduces machine idle time and maintenance time in each of these initially found sequences. Once the rescheduling of machine maintenance and idleness period of machine is completed, it then calculates the new values of flow time, maximum tardiness and machine idle time. All possible weight combinations for the criterions are computed. The search for the minimum total cost among all the Parcto-optimal schedules with the assigned weights on crterions is obtained. Finally, a promising sequence is chosen that gives the minimum total cost for a particular set of weights on the criterions.

A modified Pareto-oplimal algorithm for such technique has been devised and several properties associated with problem have also been investigated. An algorithm for neighborhood search technique has been proposed to provide the near-optimal solution for the problem. The performance of the modified Pareto-optimal algorithm has been cvaluated by comparing its solution with the solutions derived by the neighborhood scarch heuristic. Results have shown that the modified Pareto-optimal algorithm provides a better solution than the neighborhood scarch heuristic, and this shows the efficiency of the modified Parcto-optimal algorithin

## Chapter 4 Distribution

### 4.1 Introduction

Supply-chain management seeks to synchronize a firm's processes and those of its suppliers to match the flow of matcrials, services, and information with customer demand. Supplychain management has strategic implications because the supply system can be used to achieve important competitive priorities. It also involves the coordination of key processes in the firm stech as order placement, order fulfillment, and purchasing, which are supported by marketing, finance, engineering, infomation systems, operations and logistics.

Successful supply-chain management requires a high degree of lurctional and organizational integration. The interconnected set of linkages between suppliers of matcrials and services that spans the transfomation of raw materials into products and services and delivers them to a firm's customers is known as the supply-chain. The value of supply-chain management becomes apparent when the complexity of the supply-chain is recognized. The performance of numerous suppliers deternines the inward flow of materials. The performance of the firm's marketing, production, and distribution processes determines the outward flow of products. Traditionally, organizations have divided the responsibility for managing the flow of materials and services among three deparments: purchasing, production, and distribution.

Distribution is the management of the flow of materials from manufacturers to customers and from warehouses to retailers, involving the storage and transportation of products. It may also be responsible for Itnished goods inventories and the selection of transportation service providers. Typically, firms are willing to undergo the rigors of developing integrated supply-chain progress through a series of phases. The starting point for most fims, external suppliers and customers are considered to be independent of the firm. Relations with this
entities are formal, and there is litle sharing of operating information and costs. Internally, purchasing, production, and distribution act independently, each optimiaing its own activities without considering other entitics. Traditionally, it is assumed that a parameter needs to be optimized through right operations management technique. However, there is no basis as to why a particular parameter is selected as the objective function. This research provides an idea that AHP which is a technique of MCDM (Multi Critcria Decision Making) tcehnique can be used to justify selection of the right parameter as the objective function of an optimization technique.

Afier determining where the demand for goods and services is greatest, management must select a location for the facility that will supply that demand. For warehousing and distribution operations, transporation costs and proximity to markets are extremely important. With a warehouse nearby, many fims can hold inventory closer to the customer, thus reducing delivery time, transportation cost and promoting sales.

### 4.2 Multi Criteria Decision Making

In many real world situations, there are many, often conflicting, objectives. For instance, if there are multiple potential suppliers requiting evaluation with conflicting criteria, such as quality of material, timely delivery, price, quickness of delivery, manatging sudden ordering, etc., then it requires a solution [65, 66]. Or, in selecting the right communication system, several conflicting criteria, such as speed of communication, cost, reliability of transaction, maintainability, ctc. becomes important, which requires a combination of qualitative and quantitative solution [67]. As another instance, a multi criteria solution is required when a selecting the right manufacturing system or material handling system out of many available ones [68]. In an advertising campaign, there might be a number of diflerent market segments to reach. In lire station problem, there might be two types of objectives: minimizing response time and minimizing service cost. The models discussed herc,
however, only allow one objective. How can they be adapted to handle multiple objectives? This requires Multi Critcria Decision making (MCDM) [69].

However, there arc a number of fundamental problems when there are multiple objectives. For instance, in case where there are a number of decision makers. cach with a preference ordering over a number of alternatives. The goal is to choose the "fair" alternative that aggeregates the preferences of the decision makers. This is an example of multiple criteria decision making (each decision makers represents one criteria), and it is required to balance those objectives in a fair way. The field of study that addresses these problems is called MCDM, and is filled with pessimistic results [65].

These issues of aggregating views about allematives are difficult cven with a single decision maker (or a group trying to reach consensus). Imagine trying to locate an "obnoxious facility", like a waste disposal plant. There are many factors that go into such a decision. These might include distance from highly populated arcas, transportation costs, land costs, geological stability, and so on. Is there any organized way that one might think about deternining the relative importance of these factors and then go about comparing alternative sitcs? One technique that is nsed is the Analytic Hiercrehy Process (AHP), which uses very simple calculations to try to put numerical values on factors and alternatives $[70,71]$.

Finally, a logical question follows as to how these models be used in more complicated situations, where the choice is not just a number of alternatives, but rather an entire decision set, say represented by a linear program. Obviously, a lincar programming approach to such situations will at least theoretically provide beter solutions. But it has been proved in many situations that MCDM, more specifically AIIP, can offset the benefits of more fine-tuncd optimality over possibility of getting a solution in a realistic time period [72].

### 4.3 Basic Concepts of Analytic Hierarchy Process (AHP)

Developed by Thomas Saaty, AHP provides a proven, effective ineans to deal with complex decision making and can assist with identifying and weighting selection criteria, analyzing the data collected for the criteria and expediting the decision-making process [70-72]. A large number of situations, with varieties of variables, have been analyzed using AHP method [73-74].

AHP helps capture both subjective and objective evaluation measures, providing a useful mechanism for checking the consistency of the evaluation measures and alkematives suggested by the leam thus reducing bias in decision making. Combined with meeting autumation, organizations can minimize common pitlalls of team decision making process, such as lack of focus planning, participation or ownership, which ultimalely are costly distractions that can prevent teams from inaking the right choice.

The first step is for the team to decompose the goal into its constituent parts, progressing from the general to the specilic. In its simplest form, this structure comprises a goal, criteria and alternative levels. Each set of alternatives would then be lurther divided into an appropriate level of detail, recognizing that the more critcria included, the less important each individual criterion may become.

Next, a relative weight is assigned to each onc. Each criterion has a local (immediate) and global priority. I'he sum of all the criteria beneath a given parent critcrion in cach ticr of the model must equal one. Its global priority shows its relative importance within the overall model

Finally, after the criteria are weighted and the information is collected, put the information into the model. Scoring is on a relative basis, not an absolute basis, comparing one choice to another. Relative scores for cach choice are computed within each leal of the hicrarchy. Scores are then synthesised through the model, yielding a composite score for cach choice at every tier, as well as an overall score.

## Theoretical Details of AHP

Analytic hierarchy is a framework for solving a problem. I he analytic hierarchy process is a systematic procedure for representing the elements of any problem. It organices the basic rationality by breaking down a problem into its smaller constituents and then calls for pairwise comparison judgents, to develop prioritics in cach level.

The analylic hicrarchy process provides a comprehensive framework to cope with intuitive, rational, and irrational factors in making judgments at the same time. It is a method of integrating perceptions and purposes into an overall synthesis. The analytic hietarchy process does not require that judgments be consistent or even transitive. The degree of consistency (or inconsistency) of the judgment is revealed at the end of the analytic hicrarchy process.

People making comparisons use their feelings and judgment. Both vary in intensity. To distinguish among different intensities, the scale of absolute numbers in the table is usefith.

Table 4.1 Measurement scalc

| Intensity of relative importance | Explanation |
| :--- | :--- |
| 1 (equal importance) | Two activities contribute cqually to the <br> obicetive |
| 3 (slight importance of one over another) | Experience and judgment sligbtly favor <br> one activity over another |
| 5 (essential or strong importance) | Experience and judgnent strongly favor <br> one activity over another |
| 7 (demonstrated importance) | An activity is strongly lavored and its <br> dominance is demonstrated in practice |
| 9 (absolute importance) | Ihc cvidence favoring one activity over <br> another is of the highest possible order <br> of affirmation |
| $2,4,6,8$ (internediate values between the <br> two adjacent judgments) | When compromise is needed |
| Reciprocals of above nonzero numbers (if an <br> activity has one of the above numbers <br> assigned to it when compared with second <br> activity, the second activity has the <br> reciprocal value when compared to the first) |  |

The analytic hicrarchy process can be decomposed into the following steps. Particular steps may be emphasized more in some situations than in others. Also as noted, interaction is genetally uscful for stimulation and for representing different points of view.

1. Define the problern and determine what knowledge is sought.
2. Structure the hicrarchy from the top (the objectives from a broad perspective) through the intermediate levels (criteria on which subsequent levels depend) to the lowest level (which usually is a list of the alternatives).
3. Construct a set of pair-wise comparison matrices for cach of the lower levels, one matrix for each element in the level immediately above. An element in the higher Level is said to be a governing element for those in the lower level since it contributes to it or affects it. In a complete simple hierarchy, every element in the lower level alfects every element in the upper level. The elements in the lower level are then compared to each other, based on their effect on the governing element above. This yiclds a square matrix of judgments. The pair-wise comparisons are done in terms of which clement dominates the other. These judgments are then expressed as integers according to the judgment values in the table. If element $A$ dominates element B , then the whole number integer is entered in row A , column B , and the reciprocal (fraction) is cntered in row B, column A .
4. There are $n(n-1) / 2$ judgments required to develop the set of matrices in step 3 , where $n$ is the number of elements in the lower level.
5. Having collected all the pair-wise comparison data and entered the reciprocals together with $n$ unit entries down the main diagonal, the eigenvalue problem $A w=$ $\lambda_{\text {mux }} w$ is solved and consistency is tested, using the departure of $\lambda_{\text {max }}$ from $n$ (see below).
6. Steps 3, 4, and 5 are performed for all levels and clusters in the hicrarchy.
7. Hierarchal composition is now used to weigh the eigenvectors by the weights of the criteria, and the sum is taken over all weighted cigenvector entries corresponding to those in the lower level of the hicrarchy.
8. The consistency ratio of the entire hicrarchy is found by multiplying each consistency index by the priority of the corresponding criterion and adding them together. The result is then divided by the same type of expression, using the random consistency index corresponding to the dimensions of each matrix weighted by the priorities as before. The consistency ratio should he about $10 \%$ or less to be acceptable. If not, the quality of the judgments shoutd be improved, perhaps by revising the manner in which questions are asked in making the pair-wise comparisons. If this should lail to improve consistency, it is likely that the problem should be more accurately structured; that is, similar elements should be grouped under more meaningful criteria. A return to step 2 would be required, allhough only the problematic parts of the hictarchy may need revision.

The main advanlage of this method is its ability to handle a complex problem to prepare a hicrarchy of choice and reasons of choices through decomposition and synthesis. It can compare different alternatives and atlibutes using a scale of relative importance.

The numerical results of atributes are presented to the decision maker to assign relative importance according to a predefined scale. Now a judgment matrix is prepared. It is an ( $n \times$ n) matrix. From the judgment matrix, nomalized weights are calculated as follows.

$$
\left[\begin{array}{cccccc}
1 & a_{12} & \cdots & a_{1 k} & \cdots & a_{1 n} \\
a_{21} & 1 & \cdots & a_{2 k} & \cdots & a_{2 n} \\
a_{k 1} & a_{k 2} & \cdots & 1 & \cdots & a_{k n} \\
a_{n 1} & a_{n 2} & \cdots & a_{n k} & \cdots & 1
\end{array}\right] \xrightarrow{\text { Germmetric mean }}\left[\begin{array}{c}
b_{1} \\
b_{2} \\
b_{k} \\
b_{n}
\end{array}\right] \xrightarrow{\text { Normalized weights }}\left[\begin{array}{l}
x_{1} \\
x_{2} \\
x_{k} \\
x_{n}
\end{array}\right]
$$

where, $i$ and $j$ are the altenatives or attributes to be compared. $a_{y g}$ is a value which represents comparison between alternatives / altributes $i$ and $j$.

The above judgment matrix may be consistent if $a_{y j}, a_{j k}=a_{i j}$ for all values of $i, j, k$.
In the above matrix, sum of all elements in a column is

$$
y_{k}=\sum_{j=1}^{j=n} a_{j}
$$

where $k=1,2, \ldots n$ and $j=1,2, \ldots n$.

Gcometric mean is calculated from the clements of rows as follows

$$
b_{k}=\left[\left(a_{k 1}\right),\left(a_{k 2}\right) \ldots\left(a_{k n}\right)\right]^{1 / n}
$$

where $k=1,2, \ldots n$.

Nomalized weights are calculated as follows

$$
X_{k}=\frac{b_{k}}{\sum_{k=1}^{k=n} b_{k}}
$$

Saty's measure of consistency is done in temas of consistency index (C.1)

$$
\text { C.I }=\frac{\lambda_{\text {max }}-n}{n-1},
$$

where $\lambda_{\text {tnax }}=y_{1} x_{1}+y_{2} x_{2}+\cdots+y_{k} x_{k}+\cdots+y_{n} x_{n}=\sum_{k=1}^{k=n} y_{k} x_{k}$

$$
=\text { largest Eigen value of matrix of order } n \text {. }
$$

Now, some randomly generated consistency index (R.I.) values are as follows:

| $n$ | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R.I. | 0 | 0 | 0.58 | 0.9 | 1.12 | 1.24 | 1.32 | 1.41 | 1.45 | 1.49 |

Acceptability of altemative or attribute is measured in terms of Consistency Ratio (C.R.).

$$
\mathrm{C}, \mathrm{R}=\frac{C I}{R . I}
$$

If C.R. $\leq 10 \%$, then the altemative or attribute is considerable; otherwise, the altemative or attribute is rejected. The over-all consistency may also be measured to justify the validity of selection.

## Use of AHP in this Research

It has been applied in complex material planning system. For instance, many organizations keep thousands of items in their warchouses, which at times may be in excess of $50 \%$ of all
the company's expenses. Each item typically possesses its own unique characteristics, since these are typically sourced from different suppliers. Under these circumstances, it may not be rational or economical to deal with each item via a gencric material control system (either push or pull system). A multi-criteria approach that utilizes the Analytic Hierarchy Process (AHP) has been reported in an occasion. The paper proposes a modificd AIIP, such that it is able to classify the materials and components for dilferent Material Planning and Control Systems (MPCS), i.e. Kamban, MRP, hybrid, and Re-Order Point (ROP) Systems. This modified AHP is better at rising to the challenge of diversity of material characteristics in deriving an optimal decision for MPCS system selection [75]. This research aims at utilizing this concept in evaluating a different situation of material planning, where the right parameter needs to be selected through AHP. Traditionally, it is assumed that a parameter needs to be optimized through right operations management technique. However, there is no basis as to why a particular parametcr is selected as the objective function. This rescarch provides an idea that AIIP can be used to justify selection of the right parameter as the objective function of an optimization technique.

### 4.4 Problem Description

Manulacturing firms rarely sell directly to the ultimate customer. Some buyers are manufacturing firms that buy products and serviecs and incorporate them into their own output. Other buycrs are wholesalers, retailers and distribution firms who buy the products and then distribute them further down the chain towards the ultimate customers.

What difference does it make whether the firms acts as the buyer from supplicrs or a suppliers to other buyers? Buyers talk about such things as schedules, lot sizes, costs, lead times, and just-in-time delivery. Firms often take this as a given when finding suppliers who comply with their demands. Schedules sent to the firm by their customers may not fit their schedules. The just-in-time deliveries that the firms demand from their vendors may not be compatible with, for example, their job-shop production.

The principles of MRP can also be applied to distribution inventories, or stocks of items held at retailers and distribution centers. Consider the distribution system of which the top level represents retail stores at various locations through the country. The middle levels are regional distribution centers that replenish retail store inventories on request. The bottom level consists of one or more plants that supply the distribution centers.

The distribution planning is an inventory control and scheduling technique that applies MRP principles to distribution inventories. An inventory record is maintained for each item at each location. Use of distribution plaming requires an integrated information systern. If the manufacturcrs operates its own distribution centers and retail stores, called fixed quantity model or self distribution, gathering demand information and relaying it back to the plants is casy. If the manufacturer does not own the distribution centers and retail stores then it is called fixed time period model or contacted distribution. In this research work three models are considered.

1) Fixed -quantity model or Self distribution model $\left(\mathrm{M}_{1}\right)$,
2) Fixed- lime period model or Contracted distribution model $\left(\mathrm{M}_{2}\right)$,
3) Partly self and parly contracted distribution or Mixed model $\left(\mathrm{M}_{3}\right)$.

The basic distinction is that fixed-order quantity models are "event triggered" and fixedtime period models are "time triggered." That is, a lined-order quantity model initiates an order when the event of reaching a specified reorder level occurs. This event may take place at any time, depending on the demand for the items considered, i.e. it is under hirm's control. In contrast, the fixed-lime period model is limited to placing orders at the end of a predetermined period; only the passage of time triggers the model. To use the fixed-order quantity model which places an order when the remaining inventory drops to a predetermined order point, the inventory remaining must be continually monitored. Thus, the fixed-order quantity model is a perpetual system, which requires that every time a withdrawal from inventory or an addition to inventory is made, records must be updated
to ensure that the reorder point has or has not been reached. In a fixed-time period model counting takes place only at the revicw period.

In this research work it has been assumed that there are four criteria that are being used to evaluate distribution model. Four criteria are management effort, cost, integration, reliability. Further, it has been assumed that there are three distribution models ( $\mathrm{M}_{1}, \mathrm{M}_{2}$. $\mathrm{M}_{3}$ ).

Management effort: The idea is to apply a total system approach to managing the flow of information, materials, and services from raw material suppliers through factorics and warehouses to the end customer. Recent trends such as outsourcing and mass customication are forcing companies to find flexible ways to meet customer demand. The focus is on optimizing those core activities to maximize the speed of response to changes in customer expectations.

For many years, lew companies regarded the operating processes of a firm as a source of competitive advantage. The goals of the lim relating to operations were cost reduction and improved labor utilization. Decisions were made on narrow, tactical grounds. This was the domain of the technically oriented engineering specialists. Little attention was paid to how the processes, which deliver the goods and services of the firm, fit with its strategy. To regain a competitive position, western managers realized that major change wás required. Operations had to become an integral part of the corporate strategy. This corporate strategy had to be responsive to the needs of the firm's customers. Companies learned how different eustomers had different priorities. The old idea that cost minimization was always the goal was shatlered. A new field called operations strategy emerged.

Operations strategy offers a new perspective about opcrations problems, as well as a new set of concepts and techniques. The new perspective relates to the context within which decisions are made. This context considers the needs ol customer together with the overall strategy of the firm. A company that is considered to be world class recognizes that its ability to compete in the market place depends on developing an operations strategy that is properiy aligned with its mission of serving the customer.

Cost: Within every industry, there is usually a segment of the market that buys strictly on the basis of low cost. To successfully compete in this niche, a firm must be the low-cost producer, but even doing this does not always guarantee profitability and success.

Products sold strictly on the basis of cost are typically commodity like in nature. In other words, customers cannot distinguish the products of one lirm from those of other, as a result, customers use cost as the primary determinant for making a purchase.

However, this segment of the market is frequently very large, and many companics are lured by the potential for significant profits, which they associate with the large unit volumes of product. As a consequence, competition in this segment is fierce and so is the failure rate. After all, there can only be one low cost producer, which usually establishes the selling price in the market.

Integration: Successful supply-chain management requires a high degrec of functional and organizational integration. Such integration does not happen ovemight. The firm initiates internal integration by creating a materials management deparment. Materials management is concenced with decisions about purchasing materials and services, inventories, production levels, staffing patterns, schedules, and distribution. The focus is on the integration of those aspects of the supply-chain directly under the firm's control to create an internal supplychain. Firms in this phase utilize a seamless information and materials control system from distribution to purchasing, integrating marketing, finance, accounting, and operations. The internal supply chain is extended to embrace suppliets and customers, thereby linking it to the external supply-chain, which is not under the direct control of the firm. The firm must change its focus from a product or service orientation to a customer orientation.

Reliability: Another dimension of quality related to product design is reliability, which refers to the probability that the product will he functional when used. Products offen consist of a number of components that all must be operative for the product to perform as intended. Suppose that a product has a number of subsy stems, each with its own reliability
measure. The reliablity of each subsystem contributes to the quality of the iotal system. Distribution reliability relates to the abjlity of the firm to supply the product to the customer on or before a promised delivery duc date.

### 4.5 Computational Results

There are four criteria that are being used to cvaluate the models are management effort, cost, reliability, and integration. Further, assume that models $M_{1}, M_{2}, M_{3}$ are being considered. The measurement scale and hierarchy for this application are shown. For analysis purpose, primary data and information have heen collected from several national and international logistics companies operating in Bangladesh.

The firm must now develop a set of pait-wise compatisons to define the importance of the criteria. If the firm believes that cost is cqually to moderately more important than reliability, a value of 2 expresses this judgnent. If reliabilty is moderately more important scrvice, a value of 3 is appropriate.

However, as previously mentioned, judgenents are not always perfectly consistent. Suppose that, for example, cost is judged moderately to strongly more important than management eftor, so a value of 4 is appropriate. Continaing with this process, the decision maker had decided that cost is moderately more imporlant than integration i.e. a value of 2 . These six judgments complete the pair-wise comparisons that are needed at this stage; this information is entered in a pair-wise comparison matrix shown in Exhibit. The other entrics in the matrix are along the diagonal and reciprocals of the six judgments as previously discussed.

## Measurement Scale

Pcople making comparisons use their feelings and judgment. Both vaty in intensity. To distinguish anong different intensitics, the scale of absolute numbers in Table 1.I is useful.

It is also called "Scale of relative imporance".

## Model Selection Hicrarchy



Figur 4.I Model Sclection Hierarchy used for Multi-altribute Evaluation.

On the basis of calculated results and above theoretical discussions, judgment matrices are prepared. The "scale of relative importance" is used for pait-wise comparison. On the basis of expert opinion, the following judgment matrices are prepared at each level of hictarchy.


Figure 4.2 Hierarchy used for Multi-altribute Evaluation

Pair-Wise comparison Matrix and Computations: Evaluation criteria

| Altributes | Elfor | Cost | Reliabilly | Integration |
| :---: | :---: | :---: | :---: | :---: |
| Effort | 1.00 | 0.25 | 0.50 | 0.33 |
| Cost | 400 | 100 | 3.00 | 2.00 |
| Reliability | 200 | 0.33 | 1.00 | 050 |
| Integration | 300 | 0.50 | 2.00 | 1.00 |
| $y_{1}$ | 1000 | 2.08 | 6.50 | 3.83 |


| Geometric <br> mean, $b$ | Normalized <br> weights, $x$ |
| :---: | :---: |
| 0.45180 | 0.09529506 |
| 221336 | 0.46684856 |
| 0.75984 | 0.16026656 |
| 1.31607 | 0.27758982 |
| 474107 |  |


| $\lambda_{\text {mala }}$ | 4.03138 |  |
| :--- | :--- | :--- |
| N | 4 |  |
| C.I. | 0.01046 |  |
| R.I. | 0.9 | For $n=4$ |
| C.R | $1.1622 \%$ |  |

Since C.R. $<10 \%$. So acceplable.

## Model Comparisons

With respect to Management Effort

| Alternatives | FTP <br> Model | FQ <br> Model | Mixed <br> Model |
| :---: | :---: | :---: | :---: |
| FTP Model | 1.00 | 4.00 | 3.00 |
| FQ Model | 0.25 | 100 | 050 |
| Mixed Model | 0.33 | 2.00 | 100 |
| $y_{1}$ | 1.58 | 7.00 | 4.50 |


| Geometric <br> mean, $b$ | Normalized <br> weights, $x$ |
| :---: | :---: |
| 228943 | 062501 |
| 0.50000 | 013650 |
| 0.87358 | 0.23849 |
| 3.66301 |  |


| $\quad \lambda_{\text {Iadax }}$ | 3.01829 |
| :--- | :--- |
| N | 3 |
| C.I. | 0.0091474 |
| R.L. | 0.58 |
| C.R | $\mathbf{1 5 7 7 1 3 \%}$ |

Since C.R. $<10 \%$, So acceptable.

With respeet to Cost

| Alternatives | FTP <br> Model | FQ <br> Model | Mlxed <br> Model |
| :---: | :---: | :---: | :---: |
| FTF Model | 100 | 0.25 | 0.50 |
| FQ Model | 4.00 | 1.00 | 200 |
| Mixed Model | 2.00 | 0.50 | 100 |
| $y_{1}$ | 700 | 175 | 3.50 |


| Geometric <br> mean, $b$ | Normalized <br> weights, $x$ |
| :---: | :---: |
| 0.50000 | 0.14286 |
| 2.00000 | 057143 |
| 1.00000 | 0.28571 |
| 3.50000 |  |


| $\lambda_{\max }$ | 3.00000 |
| :--- | :--- |
| N | 3 |
| C.I. | 0 |
| R.I. | 0.58 |
| C R | 0 |

Since C.R. $<10 \%$, So acceplable.

With respect to Reliability

| Alternatives | FTP <br> Model | Mixed <br> Model | Mixed <br> Model |
| :---: | :---: | :---: | :---: |
| FTP Model | 1.00 | 0.33 | 050 |
| FQ Model | 300 | 1.00 | 200 |
| Mixed Model | 200 | 0.50 | 1.00 |
| $y_{1}$ | 6.00 | 183 | 3.50 |


| Geometric <br> mean, b | Normalized <br> weights, x |
| :---: | :---: |
| 0.55032 | 0.16342 |
| 181712 | 0.53961 |
| 1.00000 | 0.29696 |
| 3.36744 |  |


| $\quad \lambda_{\text {max }}$ | 300920 |
| :--- | :--- |
| N | 3 |
| C.I. | 0.0046014 |
| RI. | 0.58 |
| C.R. | $0.79334 \%$ |

Since C.R. $<10 \%$, So acceptable.

With respect to Integration

| Alternatives | FTP <br> Model | FQ <br> Model | Mixed <br> Model |
| :---: | :---: | :---: | :---: |
| FTP Model | 1.00 | 033 | 0.50 |
| FQ Model | 3.00 | 100 | 2.00 |
| Mixed Model | 2.00 | 050 | 1.00 |
| $Y_{1}$ | 6.00 | 1.83 | 350 |


| Geometric <br> mean, $b$ | Normalized <br> weights, $x$ |
| :---: | :---: |
| 0.55032 | 016342 |
| 181712 | 0.53961 |
| 100000 | 029696 |
| 3.36744 |  |


| $\lambda_{\text {max }}$ | 3.00920 |
| :--- | :--- |
| N | 3 |
| C.I. | 00046014 |
| R: | 0.58 |
| C.R. | $079334 \%$ |

Since C . R $<10 \%$, So acceptable.

On the basis of the above matrices, an over-all evaluation is performed using the calculated weights of the alternatives and four criteria. The composite weights of the three alternatives are calculated. On the basis of these composite weights, the alternative models are ranked. These are given in the following table.

Overall Lvaluation: Comparison of model alternatives

| Alternatives | Attributes and their weights |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Effort <br> 0.09530 | Cost <br> 0.46685 | Rellabshty <br> 0.16027 | Integration <br> 027759 | Composite <br> weights | Overall <br> Ranking |
|  | 062501 | 0.14286 | 0.16342 | 0.16342 | 0.19781 | 3 |
| FQ Model <br> (M1) | 0.13650 | 0.57143 | 0.53961 | 0.53961 | 051605 | 1 |
| Mixed Model <br> (M3) | 0.23849 | 0.28571 | 0.29696 | 029696 | 0.28514 | 2 |

The data in the matrix can be used to gencrate a good estinate of the criteria weights. I he weights provide a measure of the relative importance of each criterion. The $\Lambda \mathrm{HP}$ allows individuals to use their own personal psychometric scale for making the requred pair-wise comparisons. Mcasuring the consistency of one's judgments allows a cross-check on how well that scale is being followed. As long as the scale is applied consistently by cach individual, the AHP can correctly process their judgments. Computations of the consistency ratio are somewhat more involved, but they are performed with a spreadshect package such as Microsodi Excel.

The three models must be compared pair-wise for each criterion. This process is virtually identical to the procedure that was used to develop the critcria comparison matrix. The only difference is that there is a model comparison matrix for each criterion. Therefore, the decision maker compares each pair of models with respect to the management effort criterion. This is repcated for the three other criteria.

The final step of the AHP analysis is summarized in overall evaluation table. This table shows how the overall formulation scores are computed. This procedure can be cxplained as a simple weighted average technique. For a given model, four weights are computed. one for each of the four evaluation critcria. These four weights are multiplied by the apptopriate criteria weights in meeting the goal of the hicrarchy and the results of the four multiplications are added together to compute the model score. Fach model score represents the estimated total benefits to be obtained from selecting this model. In this problem, according to the results obtained, the FQ model (M1) with a score of 0.51605 is ranked 1 i.c. judged to be best. Bused on the solution, model MI is selected. In this problem cost among all of the criteria is critical. So cost i.c. transportation cost should be minimized.

### 4.6 The Transportation Cost

The transportation problern, received this name because many of its applications involve determining how to optimally transport goods. Transportation costs play an important mole in location decisions. These can stem from the movement of either raw materials or finished goods. If a facility will be the sole source or destination of shipments, the company can include the transportation costs in a locational cost-volume analysis by incorporating the transporation cost per unit being shipped into the variable cost per unit.

When a problem involves shipment of goods from inultiple sending points to multiple receiving points, and a new location (sending or recciving point) is to be added to the system, the company should underake a separate analysis of transportation. In such instances the transportation model of linear programming is very helpful. It is a specialpurpose algorithm used to determine the minimum transportation cost.

### 4.6.1 Integrated Logistics: Needs and Variables

The conceptualization of integrated logistics can be delined as a 'unil', composed of various major functions of a supply chain systern. Logistics is viewed as the competency that links an enterprise with its customers and suppliers. Information from and about customers flows through the enterprise in the form of sales activity, forecasts, and orders |76|. The information is refined into specific manufacturing and purchasing plans. As products and materials are procured, a value-added inventory flow is initialed that ultimately results in ownership transfer of finished products to customers [77]. Thus, the process is viewed in tems of two interrelated eflors, inventory flow and information flow. Prior to diseussing each llow in greater detail, two observations are important. Firstly, an integrated operation is a must in hierarchical plaming system, or value-chain system, or smply a supply chain system. Sccondly, optimization in distribution network is necessary for not only cost mimimuation, but also other qualitative and quantitative variables $|78|$.

While such integration is prerequisite to success, it is not sulficient to guarantee that a firm will achicve its performance goals. Obviously, a related issue is how to achicve the goal and how to measure the performance. Possibly, operations rescarch, especially in the form of local search algorithm, is the only feasible solution, although it is true that global search algorithms may theorctically provide a better solution, however, at the expense of infeasibility and NP-lardness [79-80].

To be fully effective in today's compelitive environment, firms must expand their integrated behavior to incorporate customers and suppliers in the hieratchically integrated system. This extension, through external integration, is referred to as valuc-added supply chain management systern [81].

Second, the basic process is not restricted to for-profil business, nor is it unique to manufacturing lirms. The need to integrate requirements and operations occurs in all businesses as well as within public sector organizations. lor example, retailing or wholesaling firms typically link physical distribution and purchasing, since traditional manufacturing is not required. Neverheless, retailers and wholesalers must complete the Iogistics value-added process. The same is true for all public sector organizations that manufacture products or provide other services. In fact, that is the essence of hierarchical materials planning system.

### 4.6.2 Matcrials Flow in Hierarehical Planning System

The operational management of hicrarchical materials planning system has many components: materials itself, logistics to integrate materials flow, information flow and many others. This research is concentrated on physical integration issues, concerning materials and business logistics. It may be mentioned that business logistics is concemed with movement and storage of materials, finished products and associated service. Logistical operations start with the initial shipment of a material or component part from a supplier and are linalized when a manufactured or processed product is delivered to a
customer. Here, optimization would mean some objectives: materials flow al the shorest possible time and information passing from one stage of planning to the other, such that certain degree of intcgration is achieved. This rescarch aims both.
l-rom the initial purchase of a material or component, the logistical process adds value by moving inventory when and where needed. Providing all gocs well, a material gains value al each sicp of its transformation into linished inventory. In other words, an individual part has greater value afler it is incorporated into a machine. Likewise, the machinc has greater value once it is delivered to a buyer. This value addition should be maximum, if optimization is achieved from several dimensions, leading a multi-objective optimization, which is desired, but inost of the times not achicvable because of computational problems. This rescarch solves the problem of multi-criteria optimization using linear programming and multicriteria technique in two steps.

To support manufacturing, work-in-process inventory must be moved to support final assembly. The cost of each component and its movenent becomes part of the value-added process. The final or meaningful value that is added oceurs only with final ownership transler of products to customers when and where specilied [82]. For a large manufacturer, logistical opcrations may consist of thousands of movements, which ultimately culminate in the delivery of products to an industrial user, retailer, wholesaler, dealer, or other customer, which constitute the complex distribution network. For a large retailcr. logistical operations may commence with the procurement of products for resale and may terminate with consumer pickup or delivery. For a service organization, like a hospital, logistics start with procurement and end with full support of patient surgery and recovery. The significant point is that regardless of the size and type of enterprise, integrated logistics is essential for hicrarchical materials planning system and requires continuous management attention. For better understanding it is useful to divide logistical operations into three areas: physical distribution, manufacturing suppon, and procurement. These components constilute the center of the combined logistics operational units of an enterprise.

### 4.6.3 Physical Distribution

The area of physical distribution concems the last step of distribution network operations, which involves movement of a finished product to customers in shortest possible time and minimum possible cost. In physical distribution, the customer is the final destination of a markeling channel. The availability of the product is a vital part of each channel participant's marketing elfort. Even a manufacturer's agent, which typically does not own inventory, must depend on inventory availability to perform expected marketing responsibilities. Untess a proper assorment or products is efficiently delivered when and where needed, a great deal of the overall marketing effort can be jeopardized. It is through the physical distribution process that the time and space of customer service become an integral part of marketing. Thus physical distribution links a marketing channel with its customers. To support the wide varicty of marketing systems that exists in a highly commercialized nation, many dilletent physical distribution systems are utilized. Alt physical distribution systems have one common feature: they link manufacturers, wholesalers, and retailers into matketing channels that provide product availability as an integral aspect of the overall markeling process [83].

### 4.6.4 Operating Arrangements: Anticipatory versus Response-Based

The fundamental difference in anticipatory and response-based logistical arrangements is timing. Anticipatory arrangements are traditional and reflect the best practice developed durng a period prior to widespread availability of information technology. In contrast, response-based arrangements rellect strategies to exploit the potential of time-based logistics. Time-based logistics provide the basis for optimization.

This question again raises another derived question regarding Anticipatory-driven value chain against Response-driven value chain. Obviously, an anticipatery-driven value chain is desired at any manufacturer's network. However, this would require market driven forecast, originating from distribution network. If this is achicved. only then a true materials planning integration is achieved. However, this would require an integrated MRP (Matcrial

Requirements Planning) and Distribution Requirements Planning (DRP). Curnently, this integration is absent. As such, total Manufacturing Resource Planning (MRPI) is not yet realized. This research provides integration between MRP and DRP at the planning level. The following table shows the variables operating at different levels for such integration.

Table 4.2 Business variables for MRP-DRP integration.

| Anticipatory-driven hicrarchical inaterials planning chain | Response-driven hierarchical materials planning chain |
| :---: | :---: |
| Manufacturing level |  |
| Stochastic forecast | Deterministic forecast |
| M12-DRP planning | MRP-DRP planning |
| Anticipatory inventory including stochastic salety stock | Definitive inventory with optional salety stock |
| Multi-item dispatching with stochastic inventory at the downstrean | Multi-item dispatching with delinitive inventory at the downstream |
| Intermediate Distribution network pipeline |  |
| Stochastic forecast and inventory build-up as per : An integration with "Multi-itern dispatching from the upper manufacturing level". | Deterministic requirement-based inventory planning, as per MRP of MRPII system |
| Inventory speculation as per statistical distribution patten | Inventory postponement and flow through turn-over |
| Selection waves through fixed replenishment schedule | Selection waves bascd on requirements from MRPIl system. |
| Profit center philosophy | Service center philosophy |
| Sales Point / Relailer |  |
| Model stock (ROP, Safety stock) | Model stock (ROP) |
| Stochastic demand based replerishment | Scheduled replenishment |

Table 4.2 illustrates contrasting priorities and practices that managers can be expected to employ with logistics-related activities at each stage of the supply chain. Even a casual review of the detailed paradigms illustrates the stark differences between the two operating arrangements. especially during planning integration.

Anticipatory practices were developed during a lime period when business was primarily conducted on a transactional basis. Because information was not shared frecly and technology was not available to facilitate such sharing, firms tended to operate on the basis of long-term forecasts, which is highly stochastic in nature. It must be noted and remombered that the longer the (materials) planning period, the more stochastic the plan is. Thus, the operational goal becomes to build and push inventory with laigher degree of uncertainty to the next level in the channcl. Because of high cost and risk associated with anticipatory practices, the prevailing relationship between trading partsers was typically adversarial, Each pary to the transaction needed to look out and deal with uncertainty for its own sell-interest.

Response-based arrangements stress cooperation and information sharing. Because of channel-wide data concerning requirements, timely point-of-sale experience can be substituted for total reliance on forecasts. When all members in a marketing channel synchronize their operations, opportunities exist to reduce total supply chain inventory and eliminate duplicate practices that increase cost without gencrating customer value. Ilowever, this would require optimization and integration in the overall materials planning system. This research aims at that purpose.

The reality of today's best practice logistics is that it does not reflect the extrome of either an anticipatory or a response-based arrangement. Many well-established belicfs and practices tend to preserve conformance to anticipatory paradigms. Perhaps the greatest barrier to adopting response-based arrangements is the need for publicly held corporations to appropriately project sales volume to financial indices. Financial indices act as the base-ine cconomic accountability factor, which means that financial goals must be reflected in operating plans and forecasts. Such goais often encourage promotional strategics to "load the channel" in order to create timely sales volume. The financial burden to "deload" the channel in order to create a response-based environnent is never timely. 'Ihis deloading occurs, for example, every year in many retail stores right after celebration-based saleshikes (c.g. Christmas, Lid festivals, etc). Stores promote heavily to sell their remaining
stock before the end-of-the-ycar inventory is counted to help reduce the expense of taking inventory and to lower inventory cost. This overflow secnario is opposite to normally prevailing backlog situation in many stores downstream.

A second barricr to implemenling response-based operations is the fact that it is easicr to manage on an adversarial relation on power-dominated basis than to develop and leverage cooperative relationships. Cooperative relationship requires strong synchronized supply chain network. Most business managers simply do not have training or experience for instituting cooperative arangements designed to share both benefits and risks. While logistics managers report a high degrec of belief in the long-term potential for responsebased alliances, they report considerable frustration in how to get the job done.

For the foresecable future it appears that most firms will be simultancously involved in various combinations of anticipatory and response-based logistical arrangements. The trend toward increased involvement in response-based relationships with specific customers and suppliers appears to be well established and will continue to expand. This need for lirms to participate in a variety of different delivery arrangements has placed new performance demands on logistical strategy.

### 4.7 Transportation Economies

From the preceding discussion, it is clear that warchouses enter a logistical system only when a differential advantage in service or cost results from their inclusion between manufacturing and customers. From the viewpoint of transportation economies. cost advantage is accomplished by using the warehouse to achicve maximum consolidation of [reight [84]. The next discussion illustrates the cconomics of transportation consolidation that justify establishment of a warehousc, in comparison to direct shipment without intermediary warehouse. Then the chapter focuses on transporation cost minimization across a network of warehouses.

## Cost-Based Warehouse Justification

The basic economic principle justifying establishment of a warchouse is transporation consolidation. A manufacturer typically setls products over a broad geographical market area. If customer orders tend to be small, then the potential to consolidate may provide economic justification for establisbing a warchouse.

## Transportation Cost Minimization

It is a matter of question whether adding a warchouse in the distribution channel helps minimizing cost. As a general rule, warchouses would be added to the logistical system in situations, where -

$$
\sum \frac{P_{\bar{v}}+T_{\bar{v}}}{N_{\bar{x}}}+W_{\bar{x}}+L_{\bar{x}} \leq \sum P_{\bar{x}}+T_{\bar{x}},
$$

where
$P_{\overline{0}}=$ Processing cost of volume shipment
$T_{\bar{v}}=$ Transportation cost of volume shipment
$W_{\gamma}=$ Warehousing cost of average shipment
$L_{\bar{x}}=$ Local delivery of average shipment
$N_{\overline{3}}=$ Number of average shipments per volume shipment
$P_{\vec{X}}=$ Processing cost of average shipment
$T_{\bar{x}}=$ Direct freight cost of average shipment

The only limitation to this generalization is that sulficient shipment volume must be available to cover tbe lixed cost of each warchouse facility. As long as the combined cost of warchousing and local delivery is equal to or less than the combined cost of shipping direct to customers, the establishonent and operation of additional warchouse facilities would be economically justified.

The generalized relationship of transportation cost and consolidation location is illustrated in Figure 4.1. Total transportation cost will decrease as consolidation locations are added to
the logistical network. In actual operation, consolidation locations can be transportation break bulk or cross-dock facilitics. It is not necessary to stock inventory to achicve the lowest transporlation cost. The reduction in transport cost results from consolidated volume shipments to the break bulk location, coupled with shor-haul small shipments to final destination. The cost of shipping small orders direct from manulacturing to customers is at the extreme upper leff of the cost curve illustrated in Figure 4-1. Al the low point near the middle of the transportation cost curve, the number of facilities required to achieve maximum consolidation is indicated; and thus, the lowest transportation cost is identified.


Figure 4.3 Transportation cost as a function of warehouse locations.

If tacilities are expanded beyond the maximum consolidation point, total cost witl increase, because the inbound volume capable of being consolidated to each facility decreases. The increased frequency of smaller inbound shipments results in a higher rate per hundredweight shipped into the facility. In other words, the frequency of small inbound shipments inereases and total transportation cost begins to increase.

## Inventury Economies

Inventory level and velocity are directly related to the location structure of a logistical system. The framework for planning inventory deployment is the performanee cycle. Athough one element of the performance cycle is transportation, which provides spatial
closure, the key lactor in inventory economics is time. The forward deployment of inventory in a logistical system improves service response time. Such deployment also increases the overall system inventory requirements, resulting in greater costs and risk. In the following discussion, the impact of inventory on service response capability is initially presented, followed by a review of the impact of increasing the number of warehouses on total system inventory requirements.

## Service-Based Warehouse Justification

The use of warchouses can be a vital part of the logistics stralegy of a firm engaged in national distribution. To achicve essential economy of scale, firms are often required to sell over broad geographical areas. These manufacturing cconomics of scale often compel firms to locate plants where low production costs can be realized.

The dynamies of spatial competition enter an industry when products begin to gain customer acceptance in other than prime markets or ncar manulacturing locations. The enterprise may find it desirable to deploy inventory to suppor marketing. In highly competitive industries, the policy may be to locate a warehouse in a particular market area even if operation of the facility increases total cost. The availability of a local inventory offers the potential to provide high levels of customer service. For customers, this means faster replenishment and an overall reduction of inventory. Thus, the enterprise that commits to establishing a warchouse may be viewed as having a differential advantage.

The inventory required to support a warehouse consists of transit, base, and walety stock. This research considers the various inventory components, including MPS-type linished goods (base inventory), pipeline (transit) inventory, distribution inventory, cte. and describes how each relates to average inventory level.

Adding warchouses to a logistical system increases the number of performance cycles. The impact on transit inventory and safety stock can be significant. In contrast, the impact on base stock by adding inventory is not significant. The base stock level within a logistical
system is determined by manufacturing and transportation lot sizes, which do not change as a function of the number of warchouses [85]. The combination of maintenance and ordering cost, adjusted to take into consideration volume transportation rates and parchase discounts, determines the replenishment EOQ and the resultant base stock. In just-in- time procurement situations, base stock is determined by the discrete order quantity required to support the planned manufacturing run or assembly. In either situation, the base stock determination is independent of the number or warehouses included in the logistical system. Transit inventory is important to logistical system design because it requires capital commitnent. As more performance cycles are added to a logistical network, the expected result is that existing cycles will experience a reduction in transit inventory. This reduction oceurs because the total transit days in the system are reduced. It should be noted that the sccond warchouse does not create additional performance cycles on the physical distribution side of the logistics flow. However, on the inbound side, each product stocked in the new warchouse requires a replenishment source. Assuming a full product line at each warehouse, the number of performance cycles required to replenish the system will increase each time a new warehouse is added [86].

Despite the increased need for inventory replerishment, the average in-transit inventory for the total systen drops as new warchouses are added because of a reduction in days required to service customers. Thus, even if multiple plant-to-warehouse replenishment cycies were added to the logistical system. the average transit time reduces because of the reduction in total replenishment days.

In summary, the addition of facilities will generally have the net effect of reducing total intransit days and, thus, inventory level. This result will vary in accordance with the particulars of each situation. Each network of Iocations inust be carefully analyzed to determine the exact impact on average transit inventory. The key to understanding the impact of increasing warchouses on transit inventory is to remember that total transit days are reduced even though the number of required performance cycles increases. A qualification is that while an increase in the number of performance cycles typically reduces
transit days, it may also increase overall lead time unectainty. As the number of performance cycles is increased, the possibility of breakdowns leading to potential service failures also increases.. This potential impact is treated under salety stock.

From the viewpoint of safety stock, the expected result of adding warehouses will be an increase in average system inventory. The impact of sales and perfomance-cycle uncenainty on inventory must be evaluated using two independent frequency distributions. The purpose of Safety stock is to protect against unplanned stock-out during inventory replenishment. Thus, if safety stock is predicted to increase as a function of adding warehouses, then the overall system uncertainty must also be increasing.

The addition of warehouses to the logistical system impacts uncertainty in two ways. First, since perfonnance-cycle days are reduced, the variability in sales during replemshment and the variability in the cyele are both reduced. Therefore, reducing the length of the performance cycle relieves to some degree the need for salety slock to protect against variability.

Ite second impact of adding locations has a direct and significant effect on average inventory. Each new performance cycle added to the system creates the need lor additional safety stock. The introduction of an additional warehouse to service a specific markel arca reduces the applicable size of the demand database used to detennine salety stock requirements. In effect; the sis of the market area serviced by a given facility is reduced without a corresponding reduction in uncertainty [87]. For example, when the demand of several markets is aggregated to a single warehouse, the variability of demand is averaged across markets. This allows peaks in demand in one market to be offset by low demand in another. In essence. the use of probability allows the idle stock of one market to be used to meel salcty stock requirements of other markets.

The impact of adding warehouses on system safety stock is reaily vital in complete supply chain management. The imponant point to understand is that the increase in salety stock results from an inability to aggregate the uncertainty across a large markel area. As a consequence, separate safety slocks must accommodate all local demand variation.

## Inventory Cost Minimization

The overall inpact on average inventory of increasing the number of warchouses in a logistical system is of vital importance. A reduction in average transit inventory is obvious The assumption is that a linear relationship exists between average transit inventory and the number of warehouses in the network.

The actual inventory increases at a decreasing rate since the net increase for each facility is limited (the added safety stock required to accommodate uncertainty is related only to demand assigned to that warchouse less the reduction 'in safety stock required for less lead time uncertainty resulting from a shorter replenishment cycle). Thus, the incremental inventory required to maintain customer service performance diminishes for each new warchouse location added to the system. The average inventory represents the combined impact of safety stock and transit inventory. The signilicant obscryation is that the salety stock dominates the impact of transit inventory reduction. For the overall system, the average inventory is the safety stock plus half ol the order quantity plus transit inventory. Thus, given the same demand and customer service goals, total inventory increases at a decreasing rate as the number of warehouses used in a logistical system increases.

## Least Total Cost Design

As noted earlier, the identilication of the least-total-cost system dosign is the goal of logistical integration. The basic total cost for the overall logistical system is composed of minimum holding and ordering cost, as well as transit and safety stock. As a result, average inventory commitment increases with each additional warchouse. For the overall system, the lowest total cost network is a function of tocations. In fact, a trade-off relation exists among number of warehouses, amount of inventory and overall distribution cost.

The identification of the least-total-cost design of warehouses in the network may be illustrated by a trade-of between cost-generating activities. The minimal total-cost point for the system is not at the point of least cost for either transportation or inventory. This is the
hallmark of integrated logistical analysis. In actual practice, a great many problems must be overcome to cffectively examine total cost. l'oremost among them is that many absumptions must be made to operationalize the logistical system analysis. $A$ second concern is the fact that a two-dimensional analysis, although may provide a less trade-off, such system does not encompass the complexity of total cost integration. Each of the critical assumptions and associated implementational problems are matter of concern.

## Some Assumptions and Limitations

This tescarch assumes an average projected level of sales volume across a planning horizon. Transportation requirements are represented by one average-size shipment. In actual operations, neither of these simplifying assumptions would be valid. Jirst, the nature of logistical network design is not a shor-term planning problen. When lacility decisions are involved, the planning horizon extends across several years and must accommodate a range of different anmual sales projections. Second, actual shipment and order sizes will vary substantially around an average. In fact, the assumption that shipments must be serviced through a warehouse must be relaxed to accommodate high-volume customer-direct truckload or container distribution. A realistic approach to planning must incorporate a range of shipment sizes suppored by altemative logistical methods to salisly customer service requirements [89]. In actual operation, alternative modes of transportation are employed, as neccssary, to upgrade the speed of deli very

Significant cost trade-ofls exist between inventory and transportation. Inventory cost as a function of the number of warehouses is directly related to the desired level of inventory availability. If no safety stock is maintained in the system, the total inventory requirement is limited to base and transil stock. Under a no-safety-stock situation, the total least cost for the systen would be at or near the point of lowest transportation cost. Thus, assumptions made with respect to the desired inventory availability and fill rate are essential to trade-olf andysis and have a significant impact on the least-total-cost design solution.

The locational selection aspect of logistical network plànning is far more complex than simply deciding how many facilities to choose from a single array of locations. A linm engaged in nationwide logistics has wide latitude in choice of where to locate warehouses. In a large market, there may be as high as filty regions within which one or more distribution warchouses could be located. Assuming that the total allowable warchouses for a logistical system carnot exceed fifty and that locations are limited to a maximum of one in each region, there are $1.1259 \times 1015$ combinations of warchouses to be evaluated in the selection of a least-total-cost network.

To overcome some of the above noted simplifying assumptions. variations in shipment size and transportation alternatives need to be introduced. Extending the analysis to a more complete treatment of variables typically demands the use of computer planning inodels and lechniques. Application of lincar programming may provide an optimal point for a trade-off. Such refinement requires linkage of a full range of variables [90]. At least three critical ones to be considered are shipment size, transportation mode, and location altcrnatives. The constants are level of inventory availability, performance- cycle duration, and the specific warehouse locations being evaluated.

In constructing a more comprehensive analysis, shipment size can be grouped in tems of frequency of occurrence and transportation mode economically justificd handling each shipment size within the specified performance-cycle time constrants. For each shipment size. a tutal-cost relationship can be identificd. The result is a wo-dimensional analysis for each shipment size and appropriate transpontation mode. Next, the individual twodimensional protiles can be linked by joining the ponts of leasi cost to make a planning curve. In a technical sense, this is an envelope curve that joins the low total-cost points of individual shipment sise-transport mode relationships.

A compromise is required to select the final warehouse network. lnitially, the time duration of the perfomance cycle and inventory availability assumptions should be held constant. The service availability and performance-cycle duration serve as parameters to help isolate an initial least-cost approximation. At a later point in strategy formulation, these parameters
can bc relaxed and subjected to semsitivity analysis. The fit of the least-cost planning curve requires marginal cost analysis for cach shipment size transportation mode combination for the stipulated network.

### 4.8 Problem Description

The transportation problem involves linding the lowest-cost plan for distributing stocks of goods or supplies from multiple origins to multiple destinations that demand the goods. For instance, a firm might have some factories, all of which are capable of producing identical units of the same products, and some warehouses that stock of demand those products. 'lhe transportation model can be used to determine how to allocate the supplies avalable from the various factories to the warehouses that stock the demand of those goods, in such a way that total shipping cost is minimized (i.e. the optimal shipping plan).

The shipping (supply) points can be factorics, warchouses, departments, or any other place from which goods are sent. Destinations can be factories, warchouses, deparments, or any other points that receive goods. To describe the genetal model for the transporation problem, it is needed to use tems that are considerably less specific than those for the components of the prototype examples. In particular, the general transportation problem is concened with distributing any commodity from any group of supply centers, called sources, to any group of receiving centers, catled destinations, in such a way as to mintimize the total distribution cost. The model for a transportation problem makes the following assumption about supplies and demands.

1. Each source has a fixed supply of units, where this entire supply must be distributed to the destinations. Let $\mathrm{s}_{1}$ denote the number of units being supplied by source i , for $i=\mathrm{I}, 2$, .... m. Similarly, cach destination has a fixed demand for units, where this entire demand must be recerved from the source. Let $\mathrm{d}_{\mathrm{j}}$ denote the number of units being received by destination j , for $\mathrm{j}=1,2 \ldots \ldots, n$.
2. A transportation problem will have feasible solutions if and only if

$$
\sum_{i=1}^{m_{2}} s_{i}=\sum_{j=1}^{\mathrm{H}} d_{j} .
$$

3. The cost of distributing units from any particular source to any paricular destination is directly proportional to the number of units distributed. Therefore, this cost is just the unit cost of distribution times the mumber of units distributed. Let $\varepsilon_{\mathrm{y}}$ denote this unit cost for sourec I and destination j .

The only dala needed for a transporation problem model are the supplies, demands, and unit costs. 'lhese are the parameters of the model. All these parameters can be summarized conveniently in a single parameter table as shown below.

Table 4.3 Parameter table for the transportation problem

| Source | Cost per unil distribuled |  |  |  | Supply |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Destination |  |  |  |  |
|  | 1 | 2 | $\ldots$ | $n$ |  |
| 1 | $c_{11}$ | $c_{12}$ | ... | $c_{\text {m }}$ | $s$ |
| 2 | $c_{21}$ | $c_{22}$ | $\cdots$ | $c_{2 n}$ | $s_{2}$ |
| : |  | : |  | : | : |
| $M$ | $c_{m l}$ | $c_{m 1}$ | $\ldots$ | $c_{\text {ny/ }}$ | $s_{n t}$ |
| Demand | $d_{1}$ | $d_{2}$ |  | $d_{n}$ |  |

'l he problem lits the model for a transportation problem if it can be described completely in terms of a parameter table like table and it satisfies the assumptions mentioned above. The objective is to minimize the total cost of distributing the units. All the parameters of the model are included in this parameter table. Thercforc, formulating a problem as a transportation problem only requires filling out a parameter table in the format of table.

Let $Z$ be the total distribution cost and $\lambda_{1 j}(i=1,2, \cdots, j=1,2, \cdots, n)$ be the number of units to be distributed from source ito destination $j$, the linear programoning formulation of this problem is

Minimize

$$
Z=\sum_{j=1}^{m} \sum_{j=1}^{n} c_{i j} x_{i j},
$$

Subject to

$$
\begin{array}{ll}
\sum_{j=1}^{n} x_{i j}=s_{1} & \text { for } \mathrm{i}=1,2, \cdots, m, \\
\sum_{i=1}^{m} x_{i j}=d_{j} & \text { for } \mathrm{j}=1,2, \cdots, n, \text { and } \\
x_{i j} \geq 0, & \text { for all } \mathrm{i} \text { and } \mathrm{j} .
\end{array}
$$

### 4.9 Computational Results

The product of this research problem is a fixed chair of twelve models manufactured in a local renowned furniture company. The product is manufactured at three workcenters (Dhaka, Bogra, and Chiltagong) and then shipped by truck to nine distributing warchouses (Gazipur, Narayangang, Tangail, Rajshahi, Kustia, Khulna, Comilla, Cox-Bazar, Feni). Hecause the shipping costs are a major expense, management is initiating a study to reduce them ay much as possible. An estimate has been made of the output from tach workeenter, and each warchousc has been allocated a certain anount from the total supply of products. This information (in units of truckloads), along with the shipping cost per truckload for cach workenter-warchouse combination, is given in table. Thus, there are a total of 320 truckloads to be shipped. The problem is now to determine which plan for assigning these shipments to the various workenter-warehouse combinations would minimive the total shipping cost.

The problem is actually a linear programing problem of the transportation problem type. To tommulate the model, let $Z$ denote total shipping cost, and let $x_{i j}(i=1,2,3 ; j=1,2,3,4$,
$5,6,7,8,9$ ) be the number of truckloads to be shipped from workeenters $i$ to warehouse $j$. Thus the objective is to choose the values of these decision variables $\left(x_{y j}\right)$ so as to

$$
\begin{aligned}
\text { Minimize } \quad Z= & 1000 x_{14}+800 x_{12}+2000 x_{13}+5000 x_{14}+4000 x_{15}+7000 x_{16}+3000 x_{17}+ \\
& 8000 x_{18}+4000 x_{19}+4500 x_{21}+5500 x_{22}+3000 x_{27}+1000 x_{24}+3000 x_{25}+ \\
& 5000 x_{26}+6000 x_{27}+12000 x_{28}+6500 x_{29}+6000 x_{31}+5000 x_{32}+6500 x_{33} \\
& 10000 x_{34}+9000 x_{35}+12000 x_{36}+3000 x_{37}+1000 x_{38}+2000 x_{39}
\end{aligned}
$$

Subject to constraint

$$
\begin{aligned}
& x_{11}+x_{12}+x_{13}+x_{14}+x_{15}+x_{16}+x_{17}+x_{18}+x_{19}=120 \\
& x_{21}+x_{22}+x_{23}+x_{24}+x_{25}+x_{26}+x_{27}+x_{28}+x_{29}=125 \\
& x_{31}+x_{32}+x_{33}+x_{34}+x_{35}+x_{36}+x_{37}+x_{38}+x_{39}=75 \\
& x_{11}+x_{21}+x_{31}=20 \\
& x_{12}+x_{22}+x_{32}=40 \\
& x_{13}+x_{23}+x_{33}=20 \\
& x_{14}+x_{24}+x_{24}=55 \\
& x_{15}+x_{25}+x_{35}=50 \\
& x_{16}+x_{26}+x_{36}=45 \\
& x_{17}+x_{27}+x_{37}=20 \\
& x_{13}+x_{28}+x_{38}=50 \\
& x_{19}+x_{29}+x_{39}=20
\end{aligned}
$$

Table 4.4 Parameter table for the transporation problem

| Source | Destination |  |  |  |  |  |  |  |  | Supply |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Gazipur | Narayan gang | Tangail | Rajshahi | Kustia | Khulna | Comilla | $\begin{aligned} & \text { Cox- } \\ & \text { Bazar } \end{aligned}$ | Feni |  |
|  | Unit cost Per Truck load(TL) in Tk. |  |  |  |  |  |  |  |  |  |
| Dhaka | 1000 | 800 | 2000 | 5000 | 4000 | 7000 | 3000 | 8000 | 4000 | 120 |
| Bogra | 4500 | 5500 | 3000 | 1000 | 3000 | 5000 | 6000 | 12000 | 6500 | 125 |
| Chittagong | 6000 | 5000 | 6500 | 10000 | 9000 | 12000 | 3000 | 1000 | 2000 | 75 |
| Demand (TL) | 20 | 40 | 20 | 55 | 50 | 45 | 20 | 50 | 20 |  |

Table 4.5 Solution table for the transportation problem


Applications of the transporation problems tend to require a very large number of constraints and variables, so a straightforward computer application of the simplex method may require an exorbilant computational effor. Therefore, it is imporant to become sufficiently familiar with this special type of problems that one can recognize then when they arise and apply the proper computational procedure.

A major part of the study revolved around formulating and solving transponation problems for individual product categories. For each option regarding the plants to keep open, etc., solving the coresponding transporation problem for a product category shows what the
distribution cost would be for shipping the product calegory from those plants to the distribution centers and customer \%ones.

Any problem fits the model for a transporation problem if it can be described completely in tems of a parameter table like table 4.3 and it satisfies both the requirements assumption and the cost assumption. The objective is to minimice the total cost of distributing the units. All the parameters of the model are included in the parameter table 4.4.

To formulate and solve a transportation problem using Excel Solver, two separate tables need to be entered on a spreadsheet. The first one is the parameter table. All the parameters of the model are included in the parameter table 4.4. The second is the solution table 4.5, containing the quantities to distribute from cach source to cach destination. Spreadsheet software, such as Excel Solver, is a popular tool for analysing and solving linear programminy problems. The main feature of the linear programming noodel, including all its parameter, can be casily entered onto a spreadsheet. However, spreadshect software can do much more than just display data. In addition, the Excel Solser can quickly apply the simplex method to find an optimal solution for the model. For transpontation problems where every $s$, and $d_{\text {, }}$ have an integer value, all the basic variables (allocalions) in every basic feasible solution (including an optimal one) also have integer valucs. The solution procedure deals only with basic feasible solutions, so it automatically will obtain an integer solution for this case. The optimal total cost and distribution quantities have been shown in the solution table 4.5 .

### 4.10 Conclusions

Distribution is the management of the ftow of materials from manufacturers to customers and from warchouses to retailers, involving the storage and transportation of products. It may also be responsible for finished goods inventories and the selection of transportation service providers. This research provides an idea that AHP which is a technique of MCDM
(Multi Criteria Decision Aaking) technique can be used to justify selection of the right parameter as the objective function of an optimization technique

The AHP can also accommodate uncertain and subjective information, and allows the application of experience, insight, and intuition in a logical manner. This forces the decision maker to seriously consider and justify the relevance of the criteria. The AJP allows individuals to use their own personal psychometric scale for making the required pair-wise comparisons. In this research work, according to the resuths oblained, the FQ model (M1) with a score of 0.51605 is ranked 1 i.e. judged to be best. In this problem cost among all of the criteria is critical. So cost i.e. transportation cost should be minimized.

The transportation problem involves finding the lowest-cost plan for distrituling stocks of goods or supplies from multiple origins to multiple destinations that demand the goods. For instance, a firm has some factories, all of which are capable of producing identical units of the same products, and some warehouses that stock or demand those products. The transportation model can be used to determine how to allocate the supplies available from the various factorics to the warchouses that stock the demand of those goods, in such a way that total shipping cost is minimized (i.e. the optimal shipping plan). The problem is now to determine which plan for assigning these shipments to the various workcenter-warehouse combinations would minimize the total shipping cost. The problem is actually a linear programming problem of the transpontation problem type. Spreadshect soliware, such as Excel Solver. is a popular tool for analyzing and solving linear programming problems. The solution procedure deals only with basic feasible solutions, so it automatically obtains an integer solution for this case. The optimal total cost and distribution quantities have been shown in the solution table 4.5 .

## Chapter 5

## Conclusions and Recommendations

### 5.1 Summary of Findings and Conclusions

It is the age of coordinated inanufacturing and distribution. The manufacturing industries are now facing a time of intense international competition, which will only become more severe in the days to come. For manufacturing companies, the danger lies in lower costhigher quality producers taking an increasing share of both domestic and foreign markets. The opporunity lics in new technology that can enable a company to improve both productivity and quality, and obtain a competitive edge.

The new technology can be divided into two categories: (1) the automation of production activitics using computer-aided design and manufacturing, robotics, or flexible manufacturing systems and (2) computer-based production and inventory control. Computer-based production and inventory control embodies powerful tools for the use of new and better planning and control concepts and techniques

The research work focuses on production planning and distribution system of total supply chain. In this research work the production plaming and distribution system of a product (chair) of a furniture company have been optimized.

## Lot-Sizing

Internal matcrials planning or Production planning is an activity that considers the hest use of production resources in order to satisfy production goals (satisfying production requirements and anticipating sales opportunities) over a certain period named the planning horizon. Production planning typically encompasses three time ranges for decision making:
long-term, medium-term and short-term. In long-tern planning usually the focus is on anticipating aggregate needs. Medium-term planning often involves making decisions on material requirements planning and establishing production quantitios or lot sizing over the planning period, so as to optimize some performance criteria such as minimizing overall costs, while mecting demand requirements and satisfying existing capacity restrictions. In shor-term planning, decisions usually involve day-10-day scheduling of operations such as job sequeticing or control in a workshop.

Lot sizing is one of the nost imporant and also one of the most difficult problems in production planning. Lot sizing decisions give rise to the problem of identifying when and how much of a product to produce such that setup, production and holding costs are minimized. Making the right decisions in lot sizing will affect directly the system performance and its productivity, which are imporant for a manufacturing lims ability to compete in the market. Therefore, developing and improving solution procedures for lot sicing problems is very important. Due to their importance in industry and mathematical complexity, deterministic, dynamic demand lot-sizing problems are frequently studicd. This research work develops specialized formulations and solution procedures for each particular lot-sizing prohlem elass. This work synthesizes the research on this imporant problem class updating the survey to consider recent modeling and algorithmic advancenents. 'Fhis work complements the recent reviews on the multi-item single level capacitated lot-sizing problem 115 J to provide a complete pieture of state-ol-the-ar research in anyone conducting research in the deterministic dynamic demand capacitated lot-sizing field.

Considering the comparison study of Maes and Van Wassenhove [14] and other points as discussed in literature study the Dixon and Silver heuristic has been considered for firther improvenents in the present work. The heuristic was extended to include two very important parameters such as, (i) plant or machine set up time and (ii) maximum limit of production lot-size from a machine. From analysis and results, the present work has
demonstrated that feasible solutions could be obtaned with competitive computer usage. The consideration of set up time also led to increase in inventory holding cost. This inerease in cost could be attributed to increased inventory held for meeting demand of the later period. Available machine time, inventory holding cost were found to be highly sensitive to the change in setup time. However, setup cost was not found to be signilicantly influenced by the setup time.

Effect of the limitation on the lot-size is dependent on the extent of reduction of the lot-size. It is obvious that the snaller the allowable lot-size, the greater will be the number of setup which will ceventually lead to more splitted items. This in turn led to the increase number of reguired setups.

Costs due to implementation of this restriction on lot-size went up quite significantly. Further decrease in lot-size would obviously result in higher costs. But at the lower range of allowable lot-size, there has been a trend of slight increase in setup costs.

The applicability of these problems arises commonly in operations such as lorging and casting and in industries which consist of a single production process. or where all production process can be considered as a single operation, such as some medical or chemical industries.

## Production Scheduling

In short-term planning, decisions usually involve day-to-day scheduling of operations such as job sequencing or control in a workshop. Most real-world scheduling problems are naturally multi-criterion. There are several approaches that deal with the multi-objective problems. Traditionally, the most common way is to combine the multiple criterions into a single scalar valuc by using weighted aggregating functions according to the preferences set by the scheduler (or decision-makers) and then to find a compromise solution that rellects
these preferences However, in many real scenatios involving multi-criterion scheduling problems, it is preferable to present a set of promising solutions to the decision-makers so that the most adequate schedule can be chosen. This has increased the interest in investigating the application of Pareto-oplimization techniques to multi-criterion scheduling problems. A Parcto-optimal algorithm is developed in this paper for a scheduling problem on a single machine with periodic maintenance and non-premptive jobs. In literalure, most of the scheduling problems address only one objective function, while in the real world, such problems are always associated with more than one objective. In this work, both multiobjective functions and multi-maintenance periods are considered for the machine scheduling problem. A multi-critcrion non-preemptive scheduling that reduces the total cost of the problern is considered in this study. Three criterions are considered: reduction of flow time, maximum lardiness, and machine ide time in a periodically maintained single machine problem. The trade-off between minimum flow time, maximum tardiness and machine idle time is a complex problem. The objective of the model addressed in this work is to minimice the weighted function of the total job flow time, the maximum tardiness, and the machine idle time in a single machine problem with periodic maintenance and nonpreemplive jobs. An algorithm is developed to solve this mulliple criterion problem and to construct the pareto-set. In this study a new kind of approach that allows the use of weighted aggregation of the criterions is presented. All possible weight combinations for the criterions are computed. The search for the minimum total cost among all the Parctooptimal schedules with the assigned weights on criterions is oblained. Finally, a promising sequence is chosen that gives the minimum total cost for a particular sct of weights on the criterions. The parametric analysis of the trade-offs of all solutions with all possible weighted combination of the criterions is analyzed.

A nenghborhood scarch heuristic is also developed to provide the near-optimal solution for the problem. Results are provided to explore the best schedule among all the Pareto-optimal
sets and to compare the result of the modified Pareto-optimal algoritlim with the result of the neighborhood search heuristic. The perfomance of the modified Pareto-optimal algorithm has been evaluated by comparing its solution with the solutions derived by the neighbothood scarch heuristic. Results have shown that the modilied Pareto-optimal algorithm provides a betler solution than the neighborhood search heuristic, and this shows the efficiency of the modilied Pareto-optimal algorithen. Direct application of this study may be applied to the industrics where performance of machine maintenance is a routine work and worthwhile as well. Chemical processing equipments. boilers, fumaces, mechanical machineries ete. are the examples of such implications.

## Distribution Planning

Distribution is the management of the flow of materials from manufacturers to customers and from warchouses to rebilers, involving the storage and transportation of products. It may also be responsible for finished goods inventories and the selection of transportation service providers. After determining where the demand for goods and services is greatest, management must sclect a location for the facility that will supply that denand. For warchousing and distribution operations, transportation costs and proximity to markets are extremely important. With a warchouse nearby, many firms can hold inventory closer to the customer, thus reducing delivery time, transportation cost and promoting sales. The transporation problem, receved this name because many of its applications involve determining how to optimally transport goods. When a problem involves shipment of goods from mulliple sending points to multiple receiving points, and a new location (sending or receiving point) is to be added to the system, the company should undertake a separate analysis of transponation. In this work the transporation model of linear programming has been used. It is a special-purpose algorithm used to detemine the minimum transportation cost.

Applications of the transportation problems tend to require a very large number of constraints and variables, so a straightforward computer application of the simplex method requires an exorbitant computational elfort For each option regarding the plants solving the coresponding transportation problem for a product category shows what the distribution cost would be for shipping the product category from those plants to the distribution centers and customer zones. The optimal total cost and distribution quantities have been shown in the solution table of distribution chapter.

### 5.2 Recommendations

Suceessful supply-chan management requires a high degree of functional and organizational integration. The interconnected set of linkiges between suppliers of materials and services that spans the transformation of raw materials into products and services and delivers them to a firm's customers is known as the supply-chain. The value of supply-chain management becomes apparent when the complexity of the supply-chain is recognized. The performance of numerous suppliers determines the inward flow of materials. The performance of the firm's marketing, production, and distribution processes detembines the outward llow of products. Traditionally, organizations have divided the responsibility for managing the flow of materials and services among three departments: purchasing, production, and distribution. In this research work integration of internal production planning and distribution has been considered. Purchasing can be included as a luture work.

In case of aggregate planning and lot sizing though some practical and real-life situations have been incorporated in the Dixon-Silver model, there are plenty of scope of improvement of the model. Following recommendations can be made for further development:

1. The Dixon-Silver model was extended through inclusion of setup time and placing limitation on the maximum allowable lot-size. In the present work these two conditions were considered separately. Further work can be performed combining the two situations to develop a uniform model.
2. A restriction of the heuristic lies with number of production stages. Single production stage has been considered in the present work. Development of a heuristic for multiple production stages could be a significant contribution.
3. Setup costs and setup time have been considered independently. Realistically larger setup time would lead to increased setup costs. Linking of these two parameters in the heuristic would be clearly a more realistic approach.
4. Back-logging was not considered in this model. Heuristic with back-logging could be developed as further work
5. Other promising rescarch arcas are available. While genetic algorithons, tabu search and capacitated network llow models are successfully applied to solve other lot-size problems, their potential to solve CI.SP is unknown. Researeh examining sensitivity analysis of dynamic lot-sizing heuristics within the context of CLSP is also worhwhite. Finally, extending the CLSP problem representation to capture the impact of equipment downtime on capacity during item changeover and multiple product lamilies are important rescarch areas.

In case of scheduling, alfough some practical and real-life situations have been incorporated in the Parcto-Optimal algorithm and neighborhood search method, there are plenty of scope of improvernent in the model. Hollowing recommendations can be made for further development:

1. The performance of the modilied Pareto-optimal algorithm has been cvaluated by comparing its solution with the solutions derived by the neighborhood search heuristic.

The perfomance of the modified Parcto-optimal algorithon can be compared with other local search methods.
2. There are many sequencing rules that can be applied to the jobs through the machines in a job shop according to the freferences. Two of those basic sequencing rules, Shorlest Processing Time (SPT) and Earliest Due Date (EID) have been adopted in the modified Parcto-optimal algorithm. Additional priority rule, such as Critical Ratio can also be adopted in future.
3. In the modified Parcto-optimal algorithm single production stage has been considered Pareto-optimal algorithm can be developed for multiple production stages.

In case of distribution system beside the ifansportation method other linear programming methods can be applied for optimization.

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## Appendix A.

Table A. 1 Perfomance of schedules at different weights and maintenance alternatives.

| T | M | W1 | W2 | W/3 | SPT/EDD | EDPISPT | \$1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 4 | 0.1 | 0.1 | 08 | 47.775 | 33 5B3 | 45.675 | 45.675 | 46175 | 47775 |
|  |  | 01 | ¢ 2 | 07 | 54975 | 38283 | 50775 | 50775 | 51.775 | 54975 |
|  |  | 01 | 03 | 0.6 | 62.175 | 42983 | 55875 | 55.875 | 57.375 | 62175 |
|  |  | 0.1 | 0.4 | 05 | 69.375 | 47683 | 60.975 | 60.975 | 62.975 | 69375 |
|  |  | 01 | 05 | 04 | 76575 | 52.383 | 66075 | 66075 | 68.575 | 76575 |
|  |  | 01 | 06 | 03 | 83775 | 57.083 | 71175 | 71175 | 74.175 | 83.775 |
|  |  | 0.1 | 07 | 02 | 90975 | E1.783 | 76.275 | 76275 | 79.775 | 90975 |
|  |  | 0.1 | 08 | 01 | 9 B 175 | 66483 | 81.375 | 81375 | 85 375 | g8 175 |
|  |  | 02 | 0.1 | 07 | 52350 | 38.467 | 50.250 | 50.250 | 50.750 | 52350 |
|  |  | 02 | 02 | 0.6 | 59550 | 43.167 | 55350 | 55.350 | 56350 | 59550 |
|  |  | 02 | 03 | 0.5 | 65750 | 47.867 | 60450 | 60450 | 61950 | 66750 |
|  |  | 02 | 04 | 0.4 | 73.950 | 52.567 | 65550 | ¢5.550 | 67.550 | 73950 |
|  |  | 02 | 0.5 | 03 | 81.150 | 57267 | 70650 | 70650 | 73.150 | 61.150 |
|  |  | D 2 | 06 | 0.2 | 88.350 | 61967 | 75750 | 75.750 | 78.750 | 88350 |
|  |  | [ 2 | 0.7 | 01 | 95.550 | 66667 | 80850 | 80850 | 84350 | 95550 |
|  |  | 03 | 01 | 0.6 | 56925 | 43350 | 54825 | 54.825 | 55325 | 56.925 |
|  |  | 03 | 02 | 05 | 64125 | 4 B 050 | 59.925 | 59.925 | 60925 | 64125 |
|  |  | 03 | 0.3 | 04 | 71325 | 52750 | 65.025 | 65.025 | 66525 | 71325 |
|  |  | 03 | 0.4 | 03 | 78525 | 57450 | 70.125 | 70.125 | 72125 | 78525 |
|  |  | 03 | 05 | 02 | 85.725 | 62.150 | 75225 | 75.225 | 77725 | 85725 |
|  |  | ¢ 3 | 06 | 0.1 | 92.925 | 66.650 | 80325 | 80 325 | 83325 | 92925. |
|  |  | 04 | 01 | 05 | 61.500 | 48.233 | 59.400 | 59406 | 59900 | 61500 |
|  |  | 0.4 | 02 | 04 | 68.700 | 52.933 | 64.500 | 64506 | 65500 | 施.700 |
|  |  | G 4 | 03 | 03 | 75.900 | 57.63 .3 | 69.600 | 69600 | 71100 | 75900 |
|  |  | 04 | 04 | 02 | 83100 | 62333 | 74.700 | 74700 | 76700 | 83100 |
|  |  | 0.4 | 05 | 01 | 90300 | 67033 | 79.800 | 79.800 | 82.300 | 90300 |
|  |  | 05 | 01 | 04 | 66.075 | 53117 | 63.975 | 63975 | 64475 | 66075 |
|  |  | 05 | 02 | 0.3 | 73275 | 57.817 | 69075 | 69075 | 70075 | 73.275 |
|  |  | 05 | ¢ 3 | 0.2 | 80475 | 的 517 | 74175 | 74175 | 75675 | 80 475 |
|  |  | 05 | 04 | 0.1 | 87.675 | 67.217 | 79.275 | 79275 | 81275 | 87675 |
|  |  | 06 | 01 | 03 | 70650 | 58000 | 68.550 | 68.650 | 69050 | 70650 |
|  |  | 06 | 02 | 02 | 77.850 | 62.700 | 73650 | 73650 | 74650 | 77850 |
|  |  | 06 | 03 | 01 | 85050 | 67400 | 78750 | 78750 | 80250 | 85050 |
|  |  | 07 | 0.1 | 0.2 | 75225 | 62883 | 73125 | 73125 | 73625 | 75.225 |
|  |  | 0.7 | 0.2 | 01 | 82425 | 67583 | 78225 | 78225 | 79225 | 82.425 |
|  |  | D. 8 | 0.1 | 01 | 79800 | 67767 | 77700 | 77700 | 78200 | 79800 |
| SUM |  |  |  |  | 270900 | 2014.00 | 2457.00 | 245700 | 251700 | 2709.00 |


| T | M | Wh | W2 | W3 | SPTIEDD | EDDISPT | \$[1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 5 | 01 | 01 | 0.8 | 49.033 | 34.883 | 47133 | 47.133 | 47333 | 49.033 |
|  |  | 01 | 02 | 07 | 57033 | 40.483 | 53233 | 53233 | 53633 | 57033 |
|  |  | 01 | 0.3 | 06 | 65033 | 46.083 | 59.333 | 59.333 | 59.933 | 65033 |
|  |  | 01 | 04 | 0.5 | 73.033 | 51683 | 65433 | 65433 | 66233 | 73033 |
|  |  | 01 | 0.5 | 04 | 81.133 | 57283 | 71533 | 71.533 | 72.533 | 611.033 |
|  |  | 0.1 | 06 | 03 | 89.033 | 62883 | 77633 | 77.633 | 78.833 | 89.033 |
|  |  | 01 | 07 | 02 | 97033 | 68483 | B3 733 | 83733 | 85.133 | 97.033 |
|  |  | 0.1 | 08 | 01 | 605033 | 74083 | B9.833 | 89833 | 91.433 | 105.033 |
|  |  | 0.2 | 0.1 | 07 | 54.067 | 40167 | 52.167 | 52167 | 52367 | 54.067 |
|  |  | 02 | 0.2 | 06 | 62.067 | 45,767 | 58267 | 58267 | 58667 | 62.067 |
|  |  | 02 | 03 | 05 | 70067 | 51.367 | 64367 | 64367 | 64967 | 70.087 |
|  |  | 02 | 04 | D 4 | 78067 | 56967 | 70.467 | 70.467 | 71267 | 78067 |
|  |  | 0.2 | 05 | 03 | 86067 | 62567 | 76567 | 76567 | 77567 | 86.067 |
|  |  | 0.2 | 0.6 | 02 | 04067 | 68167 | 82667 | 82667 | 83 867 | 91.067 |
|  |  | 02 | 0.7 | 0.1 | 102.067 | 73767 | 88767 | 88767 | 90.167 | 102067 |
|  |  | 0.3 | 01 | 06 | 59.100 | 45450 | 57.200 | 57200 | 57.400 | 59100 |
|  |  | 03 | 0.2 | 0.5 | 67.100 | 51.050 | 63300 | 63300 | 63700 | 67100 |
|  |  | 0.3 | 0.3 | 0.4 | 75100 | 56650 | 69400 | 69.400 | 70000 | 75100 |
|  |  | 0.3 | 04 | 03 | 83100 | 62250 | 75500 | 75500 | 76300 | 83.100 |
|  |  | 03 | 05 | 02 | 91.100 | 67.850 | 81.600 | 81600 | 82600 | 91100 |
|  |  | 03 | ¢ 6 | 0.1 | 99100 | 73450 | 87700 | 87.700 | 88.900 | 99100 |
|  |  | 04 | 0.1 | 05 | 64133 | 50733 | 62.233 | 62233 | 62433 | 64133 |
|  |  | C 4 | 02 | 04 | 72133 | 56333 | 68.333 | 68333 | 69.733 | 72.133 |
|  |  | 04 | 03 | 03 | 80133 | 61.933 | 74433 | 74.433 | 75.033 | 80133 |
|  |  | 64 | D 4 | 02 | 88133 | 67533 | 80.533 | 80533 | 81333 | 88133 |
|  |  | 04 | 05 | 0.1 | 96133 | 73133 | 86 633 | 86 的3 | 87633 | 96.133 |
|  |  | 0.5 | 01 | 0.4 | 69167 | 56.177 | 67267 | 67267 | 67487 | 69167 |
|  |  | 0.5 | 02 | 03 | 77.167 | 61.617 | 73.367 | 73367 | 73767 | 77.167 |
|  |  | 05 | 03 | 02 | 85167 | 67.217 | 79.467 | 79.467 | 80067 | 85167 |
|  |  | 05 | 04 | 0.1 | 93.167 | 72817 | 85567 | 85567 | 86367 | 93167 |
|  |  | 06 | 0.1 | 03 | 74200 | 61300 | 72300 | 72300 | 72500 | 74200 |
|  |  | 06 | 02 | D 2 | B2 200 | 66900 | 78400 | 78400 | 78800 | 92.200 |
|  |  | 06 | 03 | 01 | 90200 | 72.500 | 84500 | 84500 | 85100 | 90200 |
|  |  | 0.7 | 01 | W2 | 79233 | 66.583 | 77333 | 77333 | 77.533 | 79.233 |
|  |  | 07 | 02 | 01 | 87.233 | 72.183 | 83.433 | E3 433 | 83833 | 87.233 |
|  |  | 08 | 0.1 | 01 | 94.267 | 71.867 | 82.367 | 82367 | 82567 | 84267 |
| SUM |  |  |  |  | 286000 | 2170.00 | 263200 | 263200 | 2656 ¢0 | 286000 |


| T | M | W1 | W2 | W3 | SPTJED | EDDISPT | S[1] | S 2 ] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 6 | 01 | 01 | 08 | 50292 | 36183 | 48592 | 48.592 | 48592 | 50252 |
|  |  | 01 | 02 | 07 | 59092 | 42683 | 55.692 | 55692 | 55692 | 59092 |
|  |  | 0.1 | 0.3 | 06 | 67.892 | 49.183 | 62.792 | 62792 | 62792 | 67.892 |
|  |  | 01 | 04 | 0.5 | 76692 | 55683 | 69892 | 69892 | 69892 | 76692 |
|  |  | 0.1 | 0.5 | 0.4 | 85492 | 62,183 | 76992 | 76992 | 76992 | 85492 |
|  |  | 01 | 06 | 03 | 94.292 | 68683 | 84092 | 84092 | 84.092 | 94.292 |
|  |  | 01 | 07 | 0.2 | 103092 | 75183 | 91192 | 91192 | 91192 | 103.092 |
|  |  | 0.1 | 0 B | 01 | 115.892 | 81683 | 98.292 | 98292 | 98292 | 111.892. |
|  |  | 02 | 0.1 | 0.7 | 55.783 | 41.867 | 54,08.3 | 54.083 | 54083 | 55.783 |
|  |  | 0.2 | 02 | 06 | 64583 | 42367 | 61183 | 61183 | 61.183 | 64583 |
|  |  | 02 | 03 | 05 | 73383 | 54.867 | 68283 | 68283 | 68283 | 73383 |
|  |  | 02 | 04 | 04 | 82183 | 61367 | 75.383 | 75.383 | 75.393 | 92.183 |
|  |  | 02 | 05 | 03 | 90983 | 67867 | 82483 | 82.483 | 82483 | 90983 |
|  |  | 0.2 | 06 | 0.2 | 99.783 | 74367 | 89583 | 89.583 | 89583 | 99783 |
|  |  | 02 | 07 | 01 | 108563 | 80867 | 96683 | 96683 | 96.683 | 108.583 |
|  |  | 03 | 01 | 06 | 61275 | 47550 | 59.575 | 59.575 | 59.575 | 61.275 |
|  |  | 03 | 02 | 0.5 | 70075 | 54050 | 66.676 | 66675 | 66675 | 70076 |
|  |  | 03 | 03 | 04 | 78.875 | 60550 | 73.775 | 73775 | 73.775 | 76875 |
|  |  | 03 | 04 | 03 | 37675 | 67.050 | 80875 | 80375 | 80875 | 87,676 |
|  |  | 03 | 0.5 | 02 | 96475 | 73550 | 87.975 | 87.975 | 87.975 | 96.476 |
|  |  | 03 | 06 | 01 | 105275 | 80.050 | 96075 | 95.075 | 95075 | 105.275 |
|  |  | 04 | 0.1 | 05 | 66.767 | 53233 | 65067 | 65067 | 65067 | 66.767 |
|  |  | 04 | 02 | 04 | 75567 | 59733 | 72167 | 72167 | 72167 | 75567 |
|  |  | 0.4 | 03 | ¢3 | 84 367 | 66233 | 79267 | 79267 | 79.267 | 84367 |
|  |  | 0.4 | 04 | ¢2 | 93167 | 72733 | 86367 | 86367 | 86367 | 93167 |
|  |  | 04 | 05 | 01 | 101.967 | 79233 | 93467 | 93467 | 93.467 | 101967 |
|  |  | 05 | 0.1 | 04 | 72,258 | 58.917 | 70.558 | 70558 | 70558 | 72.258 |
|  |  | 05 | 02 | 03 | 81058 | 65.417 | 77658 | 77688 | 77.658 | \$1.058 |
|  |  | 05 | 03 | 0.2 | 99.858 | 71,917 | 84.758 | 84,758 | 84.758 | 89.859 |
|  |  | 05 | 04 | 01 | 98658 | 78417 | 91858 | 91.858 | 91858 | 98658 |
|  |  | 05 | 0.1 | 03 | 77750 | 64600 | 76050 | 76050 | 76050 | 77750 |
|  |  | 05 | 02 | 02 | 86550 | 71100 | 83.150 | 83150 | 83150 | 86550 |
|  |  | 06 | 03 | 01 | 95350 | 77.600 | 90250 | 90.250 | 90.250 | 95.350 |
|  |  | 07 | 01 | 02 | 83.242 | 70.283 | 81.542 | 81.542 | 81.542 | 83242 |
|  |  | 07 | 02 | 0.1 | 92042 | 76783 | 88642 | 88.642 | 88.642 | 92.042 |
|  |  | 0 B | 01 | 0.1 | 88733 | 75967 | 87033 | 87033 | 87033 | 88.733 |
| SUM |  |  |  |  | 301100 | 2326.00 | 280700 | 2907.00 | 2807.00 | 301100 |


| T | H | W1 | W2 | W3 | SPTJEDD | EDDISPT | S[ ${ }^{\text {d }}$ ] | S[2] | S[3] | S 41 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 7 | 0.1 | 0.1 | 08 | 51550 | 37.493 | 50050 | 50450 | 50.050 | 51.550 |
|  |  | 01 | 02 | 07 | 61150 | 44883 | 58150 | 58150 | 58.150 | 61150 |
|  |  | 0.1 | 03 | 06 | 70750 | 52.283 | 66250 | 65250 | 66250 | 70750 |
|  |  | 0.1 | 04 | 0.5 | 80350 | 59683 | 74.350 | 74.350 | 74350 | 80.350 |
|  |  | 0.1 | 05 | 0.4 | 89950 | 67083 | 82450 | 82.450 | 82.450 | 89950 |
|  |  | 01 | 06 | 0.3 | 9 5 50 | 74 483 | 93550 | 90550 | 90550 | 99550 |
|  |  | 01 | 07 | 02 | 109.150 | 81883 | 98650 | 98650 | 98650 | 109.150 |
|  |  | 0.1 | 08 | 01 | 118.750 | 89283 | 106.750 | 106.750 | 106750 | 118.750 |
|  |  | 0.2 | 01 | 07 | 57.500 | 43567 | 56.000 | 56.060 | 56000 | 57.500 |
|  |  | 0.2 | 0.2 | 06 | 67.100 | 50967 | 64,100 | 64.140 | 64100 | 67.100 |
|  |  | 02 | 0.3 | 05 | 76700 | 58367 | 72.200 | 72200 | 72200 | 76.700 |
|  |  | 02 | 0.4 | 04 | B6 300 | 65.767 | 80.300 | 80.300 | 80300 | 86.300 |
|  |  | 02 | 05 | 0.3 | 55900 | 73 t67 | 88.400 | 88400 | 88450 | 95900 |
|  |  | 02 | 06 | 0.2 | 105500 | 8 867 | 96500 | 96500 | 96500 | 105500 |
|  |  | 02 | D 7 | 01 | 115100 | 87.967 | 104600 | 124 600 | 104600 | 115100 |
|  |  | 03 | 01 | 06 | 63450 | 49.650 | 61.950 | 61.950 | 61.950 | 63.450 |
|  |  | 03 | 02 | 65 | 73050 | 57050 | 70.050 | 70050 | 70.050 | 73050 |
|  |  | 03 | 03 | 0.4 | 82650 | 64450 | 78150 | 78.150 | 78.150 | 82650. |
|  |  | 03 | 04 | 0.3 | 92250 | 71850 | 86250 | 86.250 | 86.250 | 92250 |
|  |  | 0.3 | 05 | 02 | 101850 | 79250 | 94,350 | 94350 | 94.350 | 101850 |
|  |  | 0.3 | 06 | 0.1 | 111450 | 89.550 | 102450 | 102453 | 102.450 | 111.450 |
|  |  | 0.4 | 01 | 0.5 | 67.400 | 55.733 | 67900 | 67900 | 67.900 | 69400 |
|  |  | 04 | 02 | 04 | 79000 | 63133 | 76.000 | 76.00\% | 76000 | 79.600 |
|  |  | 04 | 03 | 03 | 88600 | 70.533 | 84.100 | 84100 | 84100 | 88600 |
|  |  | 04 | 04 | 02 | 98200 | 77.933 | 92200 | 92200 | 92200 | 98.200 |
|  |  | D 4 | 05 | 01 | 107.800 | 85333 | 100300 | 106300 | 100300 | 107.800 |
|  |  | D 5 | 01 | 04 | 75.350 | 61.817 | 73850 | 73850 | 73850 | 75.350 |
|  |  | D 5 | 02 | 03 | 84950 | 69.217 | 81.950 | 81950 | 81950 | 84950 |
|  |  | 05 | 03 | 02 | 94550 | 76617 | 90.050 | 90.050 | 90050 | 94550 |
|  |  | 0.5 | 0.4 | 0.1 | 104150 | 84017 | 98150 | 98150 | 98. 150 | 104.150 |
|  |  | 06 | G 1 | 03 | 81.300 | 67.900 | 79800 | 79800 | 79800 | 81.300 |
|  |  | 06 | 02 | 02 | 90900 | 75300 | 87.900 | 87900 | 87900 | 90900 |
|  |  | Q6 | 03 | 01 | 100500 | 82.700 | 96.000 | 96000 | 96000 | 100500 |
|  |  | 07 | 01 | 02 | 87.250 | 73983 | 85.750 | 85.750 | 85750 | 87.250 |
|  |  | 07 | 02 | 0.1 | 96850 | 81.383 | 93850 | 93850 | 93850 | 96.850 |
|  |  | 08 | 01 | 0.1 | 93200 | 80 067 | 91.700 | 91700 | 91700 | 93200 |
| SUM |  |  |  |  | 316200 | 2482.00 | 2982.06 | 298200 | 2982.00 | 316200 |


| T | M | W1 | W2 | W3 | SPTIEOO | EDDISPT | S[1] | S[2] | $5[3]$ | 5[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 8 | 01 | 01 | 0.8 | 52808 | 38783 | 51508 | 51.50 B | 51.508 | 52,808 |
|  |  | 01 | 02 | 0.7 | 63208 | 47083 | 60608 | 60.688 | 60608 | 63.208 |
|  |  | 01 | 03 | 06 | 73608 | 55.383 | 69708 | 69.708 | 69708 | 73608 |
|  |  | [1 | 0.4 | 05 | 84008 | 63693 | 78.809 | 78808 | 78808 | 84008 |
|  |  | 0.1 | 0.5 | 0.4 | 94408 | 71983 | 87908 | B7.906 | 87.908 | 94.408 |
|  |  | 01 | 06 | 03 | 104808 | 80.283 | 97.008 | 97.008 | 97.908 | 104808 |
|  |  | 01 | D 7 | 02 | 115208 | 88.583 | 106.108 | 106.108 | 106108 | 115208 |
|  |  | 0.1 | 08 | 01 | 125.608 | 96.883 | 115.208 | 115208 | 115.208 | 125608 |
|  |  | 02 | 01 | 0.7 | 59217 | 45.267 | \$7.917 | 57917 | 57.917 | 59217 |
|  |  | 0.2 | 0.2 | 06 | 的617 | 53567 | 67617 | 67017 | 67017 | 69617 |
|  |  | 02 | 03 | 05 | 80017 | 61867 | 76117 | 76117 | 76117 | 80017 |
|  |  | 02 | 04 | 04 | 90417 | 70.107 | B5.217 | 85217 | 85217 | 90.417 |
|  |  | 0.2 | 0.5 | 03 | 100817 | 78467 | 94317 | 94317 | 94317 | 100.817 |
|  |  | 02 | 06 | 02 | 111217 | 86767 | 103417 | 103417 | 103.417 | 111.217 |
|  |  | 0.2 | 0.7 | 0.1 | 121.617 | 95067 | 112517 | 112517 | 112517 | 121.617 |
|  |  | 03 | 01 | 06 | 65625 | 51.750 | 64.325 | 64325 | 64325 | 65625 |
|  |  | 03 | 02 | 0.5 | 76.025 | 60.650 | 73.425 | 73.425 | 73.425 | 76.025 |
|  |  | 0.3 | 03 | [ 4 | 86425 | 68.350 | 82.525 | 82.525 | 82.525 | 86.425 |
|  |  | 03 | 04 | D 3 | 96825 | 76 65 | 91.625 | 91625 | 91.625 | 96.82 .5 |
|  |  | 03 | 05 | 02 | 107.225 | 84.956 | 100.725 | 100725 | 100725 | 107.225 |
|  |  | 03 | 06 | D 1 | 117.625 | 93.250 | 109825 | 109825 | 109825 | 117.625 |
|  |  | 0.4 | 0.1 | 05 | 72033 | 58233 | 70733 | 70.733 | 70733 | 72033 |
|  |  | 0.4 | 0.2 | 0.4 | 82.433 | 66533 | 79833 | 79833 | 79833 | 82433 |
|  |  | 0.4 | 0.3 | 0.3 | 92833 | 74833 | 88933 | 88.933 | 88933 | 92833 |
|  |  | 0.4 | 04 | 0.2 | 103233 | 83133 | 98033 | 98.033 | 98633 | 103233 |
|  |  | 04 | 05 | 01 | 1.3633 | 91433 | 107133 | 107.133 | 107133 | 113633 |
|  |  | 05 | 01 | 04 | 78442 | 84.717 | 77.142 | 77.142 | 77142 | 78442 |
|  |  | 0.5 | 02 | 0.3 | 88842 | 73017 | 86.242 | 86242 | 86242 | $88 \mathrm{B42}$ |
|  |  | 05 | 0.3 | 62 | 99242 | 81317 | 95342 | 95342 | 95342 | 99242 |
|  |  | 05 | 0.4 | 01 | 109642 | 89617 | 104442 | 104.442 | 104.442 | 109.642 |
|  |  | 06 | 0.1 | 93 | 84850 | 71.200 | $83.5 \$ 0$ | 83550 | 83550 | 84850 |
|  |  | 0.6 | 02 | 02 | 95260 | 79500 | 92650 | 92656 | 92.650 | 95250 |
|  |  | 06 | 03 | 01 | 195650 | 87800 | 101750 | 101.750 | 101.750 | 105.650 |
|  |  | 07 | 0.1 | 6. 2 | 91258 | 77.683 | 89.958 | 89.958 | 89958 | 91258 |
|  |  | 07 | 02 | 01 | 101658 | 85983 | 99058 | 99.058 | 99058 | 101.658 |
|  |  | 0.8 | 0.1 | 01 | 97667 | 84167 | 96367 | 96367 | 96367 | $97.667^{\circ}$ |
| SUH |  |  |  |  | 331300 | 2638.00 | 3157.60 | 315700 | 3157.00 | 331300 |


| T | M | W1 | W2 | W3 | SPTJEDD | EDDISPT | S［1］ | \＄［2］ | \＄［3］ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 13 | 4 | 01 | 01 | 0.8 | 43700 | 41967 | 41808 | 41.808 | 420088 | 43708 |
|  |  | 01 | 02 | 07 | 50308 | 46667 | 46508 | 46.508 | 46908 | 50308 |
|  |  | 01 | 03 | 06 | 56908 | 51367 | 51.208 | 51208 | 51803 | 56908 |
|  |  | 01 | 04 | 05 | 63508 | 56067 | 55.908 | 55908 | 56708 | 53508 |
|  |  | 0.1 | D． 5 | 04 | 70108 | 60767 | 60608 | 60608 | 61.608 | 70.108 |
|  |  | 01 | 06 | 03 | 76708 | 65 467 | 65.306 | 65308 | 6650B | 76708 |
|  |  | 01 | 07 | 02 | 83．35B | 70．167 | 70.008 | 70008 | 71.408 | 83.308 |
|  |  | 01 | D8 | 01 | 89908 | 74867 | 74708 | 74.708 | 76.398 | 89．96B |
|  |  | 02 | 01 | 0.7 | 47.817 | 46.233 | 45917 | 45917 | 46.117 | 47.817 |
|  |  | 02 | $\bigcirc 2$ | 06 | 54417 | 50.933 | 50617 | 50617 | 51.017 | 54.417 |
|  |  | 02 | 03 | 05 | 61.017 | 55633 | 55317 | 55317 | 55917 | 61.017 |
|  |  | 02 | 0.4 | 0.4 | 67.617 | 60333 | 60.017 | 60017 | 60817 | 67617 |
|  |  | 0.2 | 05 | 03 | 74217 | 65.033 | 64717 | 64.717 | 65717 | 74，213 |
|  |  | 02 | 06 | 02 | 80817 | 69733 | 69417 | 69417 | 70.617 | 80817 |
|  |  | 02 | 07 | 01 | 87.417 | 74433 | 74.117 | 74.117 | 75517 | 87497 |
|  |  | 03 | 0.1 | 0.6 | 51.925 | 50500 | 50.025 | 50025 | 50225 | 51925 |
|  |  | 0.3 | 0.2 | 05 | 58.525 | 55200 | 54.725 | 54725 | 55125 | 58525 |
|  |  | 0.3 | 0.3 | $10^{4}$ | 65.125 | 59900 | 59425 | 59425 | 60025 | 65125 |
|  |  | 0.3 | 0.4 | D 3 | 71725 | 64．600 | 64.125 | 64125 | 64925 | 71.725 |
|  |  | 0.3 | 0.5 | ［2 | 7 B 325 | 59.300 | 68.825 | 6B825 | 69825 | 78.325 |
|  |  | 0.3 | 0.6 | 01 | 84925 | 74000 | 73.525 | 73525 | 74725 | 84.925 |
|  |  | 04 | 0.1 | 0.5 | 56033 | 54767 | 54.133 | 54133 | 54333 | 56.033 |
|  |  | 04 | 02 | 04 | 62.633 | 59467 | 58833 | 58833 | 59.233 | 62 633 |
|  |  | 04 | 03 | 03 | 69233 | 64.167 | 63.533 | 63.533 | 64133 | 69.233 |
|  |  | 04 | 0.4 | 0.2 | 75833 | 68867 | 68233 | 68．233 | 69033 | 75833 |
|  |  | 04 | 0.5 | 0.1 | 82433 | 73567 | 72933 | 72.933 | 73933 | 82433 |
|  |  | 0.5 | 0.1 | 04 | 60142 | 59033 | 58．242 | 58242 | 58.442 | 60142 |
|  |  | 0.5 | 02 | 03 | 66742 | 63733 | 62942 | 62942 | 63342 | 66.742 |
|  |  | 05 | 03 | 62 | 73.342 | 68 433 | 67642 | 67642 | 68242 | 73．342 |
|  |  | 0.5 | 0.4 | 01 | 79942 | 73133 | 72.342 | 72342 | 73142 | 79942 |
|  |  | 06 | 01 | 03 | 64250 | 63300 | 623.50 | 62350 | 62550 | 64250 |
|  |  | 06 | 02 | 02 | 70850 | 68000 | 67050 | 67050 | 67.450 | 70.850 |
|  |  | 06 | 03 | 0.1 | 77.450 | 72.700 | 71.750 | 71750 | 72.350 | 77450 |
|  |  | 0.7 | 01 | 0.2 | 68.359 | 67.567 | 66458 | 66458 | 66.658 | 68358 |
|  |  | 0.7 | 02 | 61 | 74958 | 72.267 | 71158 | 71158 | 71558 | 74．958 |
|  |  | 08 | 01 | 4.1 | 72467 | 71.833 | 70567 | 70.567 | 70767 | 72.467. |
| SUM |  |  |  |  | 247300 | 226400 | 22450 | 224500 | 226900 | 2473.00 |


| T | W | W1 | W2 | 4.3 | SPTJEDV | EDD／SPT | S［1］ | 5［2］ | S［3］ | 5［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 13 | 5 | 01 | 01 | 0 B | 44.792 | 43266 | 43.592 | 43092 | 43.092 | 44752 |
|  |  | 0.1 | 02 | 0.7 | 52.092 | 48858 | 48692 | 48692 | 48692 | 52452 |
|  |  | 01 | 63 | 06 | 59.392 | 54458 | 54292 | 54292 | 54.292 | 59392 |
|  |  | 01 | 64 | 05 | 66.692 | 60056 | 59892 | 59892 | 59.892 | 66692 |
|  |  | 01 | 65 | 04 | 73.992 | 65658 | 65452 | 65492 | 65.492 | 73992 |
|  |  | 0.1 | 06 | 03 | 81292 | 71.258 | 71，092 | 71092 | 71092 | 81.292 |
|  |  | 01 | 07 | 02 | 88592 | 76.858 | 76692 | 76692 | 76692 | 88.592 |
|  |  | 0.1 | 0.8 | $\square .1$ | 95 892 | 82458 | 82292 | 82292 | 82.292 | 95892 |
|  |  | 02 | 01 | 07 | 49.283 | 47.917 | 47.583 | 47583 | 47583 | 49283 |
|  |  | 0.2 | 0.2 | 06 | 56583 | 53517 | 53183 | 53183 | 53.193 | 56.583 |
|  |  | 0.2 | 03 | 0.5 | 63883 | 59117 | 58.783 | 58783 | 58783 | 63.883 |
|  |  | 02 | 04 | 04 | 71.183 | 64717 | 64.383 | 64.383 | 64383 | 71.183 |
|  |  | 0.2 | 0.5 | 0.3 | 78483 | 70.317 | 69.983 | 69.983 | 69983 | 78．483 |
|  |  | 02 | 0.6 | 02 | 25.783 | 75.917 | 75．583 | 75.583 | 75.583 | 85.783 |
|  |  | 42 | 07 | 0.1 | 93083 | 61.517 | 81.183 | 81183 | 81183 | 93083 |
|  |  | 0.3 | 0.1 | 06 | 53.775 | 52.575 | 52.075 | 52.075 | 52075 | 53.775 |
|  |  | 0.3 | 0.2 | 05 | 68.075 | 58.175 | 57.675 | 57.675 | 57.675 | 61075 |
|  |  | 0.3 | 0.3 | 04 | 68.375 | 63.775 | 63275 | 63 275 | 63 275 | 6 B 375 |
|  |  | 0.3 | 04 | 03 | 75675 | 69.375 | 68875 | 68 675 | 68．875 | 75675 |
|  |  | 03 | 0.5 | 12 | B2．975 | 74.975 | 74475 | 74.475 | 74475 | 82975 |
|  |  | 03 | 06 | 01 | 90275 | 81575 | 80075 | 80675 | 80.075 | 90.275 |
|  |  | 0.4 | 0.1 | 0.5 | 58.267 | 57.233 | 56567 | $55^{5} 57$ | 56.567 | 58267 |
|  |  | 0.4 | 02 | 04 | 65.567 | 62，933 | 62.167 | 62.167 | 62167 | 65.567 |
|  |  | 0.4 | 0.3 | 03 | 72.867 | 68.433 | 67767 | 67.757 | 白 767 | 72867 |
|  |  | 0.4 | 04 | 02 | 80.167 | 74.033 | 73367 | 73.367 | 73367 | 80167 |
|  |  | 04 | 05 | 0.1 | 87．467 | 79.633 | 78967 | 78967 | 78.967 | 97．467 |
|  |  | 0.5 | 0.1 | 04 | 62.758 | 61892 | 61058 | 61.058 | 它1．05宫 | 62758 |
|  |  | 05 | 02 | 03 | 70．058 | 67492 | 68．658 | 66658 | 66658 | 76．058 |
|  |  | 0.5 | 03 | 02 | 77.358 | 73092 | 72.258 | 72.258 | 72258 | 77358 |
|  |  | 0.5 | 01 | 0.1 | B4．658 | 7B692 | 77.858 | 77.858 | 77858 | 84658 |
|  |  | 0.6 | 01 | 03 | 67.250 | 66550 | 65550 | 65550 | 65.550 | 67250 |
|  |  | 0.6 | 0.2 | 02 | 74.550 | 72.150 | 71150 | 71.150 | 71.150 | 74550 |
|  |  | 0.6 | 0.3 | 0.1 | 81.850 | 77.756 | 76750 | 76350 | 76.750 | 81850 |
|  |  | 0.7 | 0.1 | 02 | 71.742 | 71.24 B | 70042 | 70.42 | 70.042 | 71742 |
|  |  | 0.7 | 0.2 | 0.1 | 79642 | 7689 B | 75642 | 75642 | 75.642 | 79042 |
|  |  | 08 | 0.1 | 01 | 76233 | 75867 | 74533 | 74533 | 74．533 | 76.233 |
| SUM |  |  |  |  | 2603．00 | 241900 | 2399.6 | 239900 | 235900 | 260300 |


| T | M | WY | W2 | W3 | SPTIEDD | EDDISPT | \$(1) | \$[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 13 | 6 | 01 | 0.1 | 08 | 45875 | 44550 | 44375 | 44375 | 44.375 | 45.875 |
|  |  | 01 | 02 | 07 | 53875 | 51050 | 50875 | 50875 | 50.875 | 53875 |
|  |  | 0.1 | 03 | 0.6 | 61875 | 57550 | 57375 | 57.375 | 57375 | 6.1875 |
|  |  | 0.1 | 0.4 | 0.5 | 69.675 | 64050 | 63875 | 63.875 | 63875 | 69.875 |
|  |  | 0.1 | 05 | 0.4 | 77.875 | 70550 | 75375 | 70.375 | 70375 | 77.875 |
|  |  | 0.1 | 06 | 03 | 85.875 | 77.050 | 76875 | 76875 | 76875 | 85875 |
|  |  | 0.1 | 07 | 02 | 93875 | 83.550 | 83.375 | 83375 | 83.375 | 93875. |
|  |  | 01 | 08 | 01 | 101875 | 90050 | 89.875 | 89.675 | 89875 | 109875 |
|  |  | 0.2 | 0.1 | 0.7 | 50750 | 49600 | 49250 | 49250 | 49250 | 50.750 |
|  |  | 02 | 0.2 | 0.6 | 58.750 | 56100 | 55750 | 55750 | 55750 | 58.750 |
|  |  | 02 | 03 | 0.5 | 66.750 | 62.600 | 62250 | 62250 | 62250 | 66.750 |
|  |  | 02 | 04 | 0.4 | 74.750 | 69100 | 68750 | 68.750 | 68.750 | 74.750 |
|  |  | 02 | 05 | 03 | 82.750 | 75600 | 75.250 | 75250 | 75250 | 82.750 |
|  |  | 02 | 06 | 02 | 90750 | 82.100 | 81.750 | 81750 | 81750 | 90750 |
|  |  | 02 | 07 | 0.1 | 98750 | 88.600 | 88.250 | 88250 | 88250 | 98750 |
|  |  | 03 | 01 | 0.6 | 55625 | 54.650 | 54.125 | 54125 | 54125 | 55625 |
|  |  | 03 | 02 | 05 | 63625 | 61.150 | 60.625 | 60625 | 60625 | 63625 |
|  |  | 0.3 | 03 | 0.4 | 71.625 | 67650 | 67.125 | 67.125 | 67125 | 71625 |
|  |  | 03 | 04 | 03 | 79.625 | 74.150 | 73625 | 73625 | 73.625 | 79.625 |
|  |  | 03 | 05 | 02 | 87.625 | 80550 | 80.125 | 80125 | 80125 | 87625 |
|  |  | 03 | 06 | 0.1 | 95.625 | 87.150 | 86.625 | 86.625 | 86625 | 95.625 |
|  |  | 04 | 01 | 05 | 50500 | 59.700 | 59.000 | 59000 | 59000 | 60500 |
|  |  | 0.4 | 02 | 04 | 68.500 | 66.200 | 65.500 | 65500 | 65500 | 68500 |
|  |  | 0.4 | 03 | 0.3 | 76500 | 72700 | 72000 | 72000 | 72.000 | 76500 |
|  |  | 04 | 0.4 | 02 | 84500 | 79200 | 78500 | 78500 | 78.500 | 84500 |
|  |  | 04 | 0.5 | 0.1 | 92.500 | 85.700 | 85.000 | 85000 | 85.000 | 92500 |
|  |  | 05 | 01 | 04 | 65375 | 84750 | 63875 | 63875 | 63975 | 65.375 |
|  |  | 05 | 02 | 03 | 73375 | 71.250 | 70.375 | 70.375 | 70375 | 73375 |
|  |  | 05 | 03 | 02 | 81375 | 77.750 | 76.875 | 76.875 | 76.875 | 81.375 |
|  |  | 05 | 0.4 | 0.1 | 89.375 | 84.250 | 83.375 | 83.375 | 83375 | 89375 |
|  |  | 0.6 | 0.1 | 0.3 | 70250 | 698800 | 68750 | 68.750 | 68.750 | 70250 |
|  |  | 0.6 | 0.2 | 02 | 78250 | 76300 | 75250 | 75250 | 75250 | 78250 |
|  |  | 06 | 03 | 01 | 86250 | 82800 | 81.750 | 81750 | 81750 | B6.250 |
|  |  | 4 | 01 | 02 | 75125 | 74850 | 73625 | 73.625 | 73.625 | 75.125 |
|  |  | 0.7 | 02 | 0.1 | 83125 | Bt. 350 | 80.125 | 80.125 | 80.125 | 83.125 |
|  |  | 0 B | 01 | 01 | 80000 | 79900 | 78500 | 78.500 | 78.500 | 80000 |
|  |  | SUM |  |  | 273300 | 257403 | 2553.00 | 255300. | 2553.00 | 273300 |


| T | M | W1 | W2 | W3 | SPTIEDD | EDDISPT | S[1] | S[2] | \$[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 13 | 7 | 0.1 | 0.1 | 08 | 46.958 | 45842 | 45658 | 45658 | 45658 | 46958 |
|  |  | 01 | 02 | 07 | 55658 | 53.242 | 53.058 | 53058 | 53.058 | 55.658 |
|  |  | 01 | 03 | 06 | 64358 | 60642 | 60458 | 60458 | 60458 | 64358 |
|  |  | 0.1 | D 4 | 05 | 73058 | 688042 | 67858 | 67858 | 67.958 | 73058 |
|  |  | 0.1 | 05 | 04 | 81758 | 75442 | 75258 | 75258 | 75.25B | 81.758 |
|  |  | 09 | 0.6 | 0.3 | 90.458 | 92.842 | 82653 | 82658 | 82658 | 90458 |
|  |  | 01 | 07 | 02 | 99158 | 90242 | 90058 | 90058 | 90 058 | 99158 |
|  |  | 01 | 0.8 | 01 | 107.858 | 97.642 | 97.458 | 97,459 | 97458 | 107.858 |
|  |  | 02 | 01 | 07 | 52217 | 51.283 | 50917 | 50.917 | 50917 | 52.217 |
|  |  | 02 | 02 | 0 古 | ¢0917 | 58683 | 58317 | 58317 | 58317 | 60.917 |
|  |  | 02 | 03 | 05 | 69617 | 66.083 | 65.717 | 65717 | 65.717 | 69617 |
|  |  | 0.2 | 0.4 | 0.4 | 78.317 | 73483 | 73117 | 73.117 | 73117 | 78317 |
|  |  | 02 | 05 | 03 | 87.017 | 80883 | 80.517 | 80517 | 80517 | 87017 |
|  |  | 02 | 06 | 02 | 95.717 | 88.283 | 87.917 | 87517 | 87917 | 95717 |
|  |  | 02 | 0.7 | 01 | 104417 | 95683 | 95317 | 95317 | 95317 | 104417 |
|  |  | 03 | 0.1 | ¢6 | 57475 | 56725 | 56175 | 56175 | 56175 | 57475 |
|  |  | 03 | 02 | 0.5 | 66175 | 64125 | 63575 | 63.575 | 63575 | 66.175 |
|  |  | 03 | 03 | 04 | 74.875 | 71525 | 70975 | 70975 | 70975 | 74.875 |
|  |  | 03 | 04 | 03 | 83.575 | 78.925 | 78.375 | 78.375 | 78375 | 83.575 |
|  |  | 0.3 | 05 | 02 | 92275 | 86325 | 85775 | 85.775 | 85775 | 92275 |
|  |  | 03 | 06 | 01 | 100975 | 93725 | 93175 | 93.175 | 93175 | 100975 |
|  |  | 04 | 0.1 | 0.5 | 62.733 | 62.167 | 61.433 | 61.433 | 51.433 | 62.733 |
|  |  | 0.4 | D2 | 0.4 | 71433 | 69567 | 68833 | 68.833 | 68833 | 71433 |
|  |  | 0.4 | 03 | 03 | 80133 | 76967 | 76.233 | 76233 | 76233 | 80133 |
|  |  | 04 | 04 | 0.2 | 88.833 | 84367 | 83.633 | 83633 | 83633 | 89.833 |
|  |  | 04 | 0.5 | 0.1 | 97.533 | 91,767 | 91.033 | 91,033 | 91.033 | 97633 |
|  |  | 05 | 01 | 04 | 67992 | 67608 | 66692 | 66692 | 66.692 | 67992 |
|  |  | 05 | 02 | 03 | 76692 | 75008 | 74.092 | 74092 | 74.092 | 76692 |
|  |  | 0.5 | 03 | 02 | 85392 | 82408 | 81.492 | 81.492 | 81.492 | 85.392 |
|  |  | 0.5 | 04 | 01 | 94092 | 89808 | 88.892 | 88 892 | 88.892 | 94092 |
|  |  | 0.6 | 01 | 03 | 73250 | 73050 | 71.950 | 71.950 | 71.950 | 73.250 |
|  |  | 0.6 | 02 | 02 | 81950 | 80450 | 79350 | 79350 | 79.350 | 81950 |
|  |  | 0.6 | 03 | 0.1 | 90650 | 87850 | 86.750 | B6.750 | 86750 | 90650 |
|  |  | 0.7 | 01 | 02 | 78508 | 78492 | 77208 | 77208 | 77.208 | 78508 |
|  |  | 07 | 02 | 01 | 87208 | 85892 | 84608 | 84608 | 84608 | 87208 |
|  |  | 08 | 0.1 | 0.1 | 83767 | 83.933 | 82,467 | 82467 | 82.467 | 83767 |
| SUM |  |  |  |  | 286300 | 272900 | 2707.00 | 2707.00 | 2707.00 | 286300 |


| T | M | W1 | W2 | W3 | SPTJEDD | EDDFSPT | S[1] | \$ [2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 13 | 8 | 01 | 01 | 0.8 | 48042 | 47.133 | 46.942 | 46.942 | 46942 | 48, 042 |
|  |  | 0.1 | 02 | 07 | 57.442 | 55.433 | 55242 | 55242 | 55.242 | 57.442 |
|  |  | 01 | 03 | 06 | 66842 | 63733 | 63542 | 63542 | 63542 | 66.842 |
|  |  | 0.1 | 04 | 05 | 76242 | 72033 | 71842 | 71.842 | 71 B42 | 76242 |
|  |  | 01 | 0.5 | 0.4 | 85.642 | 80.333 | 80.142 | 80.142 | 80.142 | 85642 |
|  |  | 01 | 0.6 | 03 | 95042 | 88 ¢ $8^{8}$ | 88.442 | 88442 | 88.442 | 95.042 |
|  |  | 0.1 | 07 | ¢ 62 | 104442 | 96933 | 96742 | 96742 | 96742 | 104.442 |
|  |  | 01 | 08 | 01 | 113842 | 105233 | 105042 | 105042 | 105042 | 113.842 |
|  |  | 0.2 | 0.1 | 0.7 | 53.683 | 52.967 | 52.583 | 52.593 | 52.583 | 53683 |
|  |  | 02 | 02 | 06 | 63083 | 61267 | 60883 | 60883 | 60883 | 63083 |
|  |  | 02 | 03 | 05 | 72483 | 69567 | 69.183 | 69.183 | 69.183 | 72483 |
|  |  | 02 | 04 | 0.4 | 81.883 | 77.867 | 77.483 | 77483 | 77483 | 84.883 |
|  |  | 62 | 05 | 0.3 | 91.283 | 86167 | B5783 | 85783 | 85.783 | 91.283 |
|  |  | 02 | 06 | 02 | 100683 | 94487 | 94083 | 94.083 | 94.083 | 100.693 |
|  |  | 0.2 | 07 | 01 | 110083 | 102.767 | 102.383 | 102.383 | 102.383 | 110083 |
|  |  | 03 | 01 | 06 | 59325 | 58800 | 58225 | 58225 | 58.225 | 59.325 |
|  |  | ${ }_{6} 3$ | 02 | 05 | 68725 | 67100 | 65525 | 66525 | 驼 525 | 68725 |
|  |  | 03 | 03 | 04 | 7B125 | 75400 | 74825 | 74.825 | 74825 | 78125 |
|  |  | 03 | 04 | [ 3 | 87525 | 83700 | 83125 | B3 125 | 83125 | 87525 |
|  |  | 0.3 | 0.5 | 0.2 | 96925 | 92.000 | 91.425 | 91.425 | 91425 | 96925 |
|  |  | 0.3 | 06 | 0.1 | 106.325 | 100.300 | 99.725 | 99.725 | 99.725 | 106.325 |
|  |  | 04 | 01 | 65 | 64967 | 64633 | $63 \mathrm{B67}$ | 63867 | 63.867 | 64967 |
|  |  | 0.4 | [2 | 04 | 74367 | 72933 | 72167 | 72167 | 72167 | 74367 |
|  |  | 0.4 | 03 | 03 | 83767 | 81233 | 80467 | 80467 | 80 467 | 83.767 |
|  |  | 0.4 | 04 | 02 | 93167 | 89533 | 88767 | 88767 | 88767 | 93.167 |
|  |  | 04 | 05 | 01 | 102567 | 97833 | 97067 | 97067 | 97067 | 102.567 |
|  |  | 05 | 0.1 | 0.4 | 70.508 | 70.467 | E9508 | 69.509 | 59.509 | $70.60{ }^{\circ}$ |
|  |  | 05 | 02 | 03 | 30008 | 78.767 | 77.808 | 77803 | 77808 | 80008 |
|  |  | 05 | 03 | 02 | 89408 | 87.067 | B6108 | 86.108 | 86108 | 89.408 |
|  |  | 0.5 | 04 | 01 | 98808 | 95367 | 94.408 | 94.408 | 94,40白 | 98.808 |
|  |  | 06 | 01 | 03 | 76250 | 76300 | 75150 | 75150 | 75150 | 76.250 |
|  |  | 06 | 0.2 | 02 | B5 650 | 84600 | 83450 | 83.450 | 83450 | 85650 |
|  |  | 06 | 0.3 | 01 | 95050 | 92900 | 91750 | 91.750 | 91750 | 95050 |
|  |  | 0.7 | 01 | 0.2 | 81.892 | 82.133 | 80.792 | 80792 | 80.792 | 81.892 |
|  |  | 07 | 02 | 01 | 91292 | 90433 | 89092 | 89092 | 89092 | 91292 |
|  |  | 0.8 | [1 | 0.1 | 87533 | 87967 | 86433 | 86433 | 86.433 | 87533 |
| SUM |  |  |  |  | 299300 | 288400 | 2861.00 | 2861.00 | 286100 | 299300 |


| T | H | Wit | WY2 | W3 | SPTJEDD | EDDISPT | \$[1] | S[2] | \$[3] | 5[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14 | 4 | 01 | 01 | 08 | 38900 | 50458 | 50292 | 36300 | 36300 | 32000 |
|  |  | 01 | 02 | 0.7 | 44000 | 55158 | 54.992 | 40600 | 40600 | 44.000 |
|  |  | 0.1 | 0.3 | 0.6 | 50 OPO | 59858 | 59692 | 44900 | 44900 | 50000 |
|  |  | 0.1 | 04 | 05 | 56000 | 64.558 | 64392 | 49.200 | 49.200 | 55000 |
|  |  | 01 | 05 | 04 | 62.000 | 69.258 | 69092 | 53500 | 53500 | 62000 |
|  |  | 01 | 0.6 | 03 | 68000 | 73958 | 73792 | 57.8 CO | 57800 | 68000 |
|  |  | 01 | 0.7 | 02 | 74000 | 78558 | 78492 | 62.100 | 62100 | 74000 |
|  |  | 01 | 08 | 01 | 80000 | 83358 | 83192 | 66.480 | 66400 | 80.000 |
|  |  | 02 | 0.1 | 07 | 42000 | 54297 | 53883 | 40.300 | 40300 | 42000 |
|  |  | 02 | 02 | 0\% | 48000 | 54. 917 | 54, 583 | 44600 | 44.680 | 48000 |
|  |  | 02 | 03 | ¢ 5 | 54000 | 63.617 | 63283 | 48900 | 48.900 | 54000 |
|  |  | 02 | 04 | 0.4 | 60.000 | 68317 | 67983 | 53200 | 53200 | 60000 |
|  |  | Q2 | 65 | 03 | 66800 | 73.177 | 72683 | 57500 | $5750 \times 3$ | 66000 |
|  |  | 02 | 66 | 02 | 72000 | 77717 | 77 3B3 | 61800 | 61800 | 72.000 |
|  |  | 02 | 07 | 0.1 | 78000 | 82417 | 820.63 | 66100 | 66100 | 78090 |
|  |  | 03 | 01 | 0.6 | 46000 | 57.975 | 57.475 | 44300 | 44300 | 46.000 |
|  |  | 03 | ¢2 | 0.5 | 52.000 | 62675 | 62.175 | 48600 | 48600 | 52000 |
|  |  | 03 | 03 | 04 | 58.000 | $67 \$ 75$ | 68975 | 52,900 | 52.900 | 58.000 |
|  |  | 03 | 04 | 03 | 64000 | 72075 | 71575 | 57.200 | 57200 | 64.000 |
|  |  | 03 | 0.5 | 0.2 | 70.000 | 76.775 | 76.275 | 61.500 | 61500 | 70.000 |
|  |  | 0.3 | 06 | 01 | 76000 | 81475 | 80975 | 65800 | 65 900 | 76.000 |
|  |  | 04 | 01 | 65 | 50000 | 61733 | 61067 | 48.300 | 48300 | 50000 |
|  |  | 0.4 | 02 | 04 | 56000 | 68433 | 65.767 | 52.600 | 52.500 | 56.000 |
|  |  | 0.4 | D 3 | 63 | 62000 | 71133 | 70467 | 56900 | 56.900 | 62000 |
|  |  | 04 | 0.4 | 02 | 68.000 | 75833 | 75167 | 612004 | 61.200 | 68000 |
|  |  | 04 | 0.5 | 01 | 74.000 | 80533 | 79 B67 | 65500 | 65.500 | 74000 |
|  |  | 05 | 0.1 | 04 | 54000 | 65492 | 64658 | 52300 | 52.300 | 54000 |
|  |  | 05 | 02 | 03 | 60 D00 | 70192 | 69358 | 56.600 | 56600 | 60000 |
|  |  | 05 | 03 | 02 | 661300 | $74 \mathrm{EP2}$ | 74058 | 60900 | 60.900 | 66050 |
|  |  | 05 | 04 | 01 | 72,000 | 79592 | 78,758 | 65.200 | 65.200 | 72.000 |
|  |  | 06 | 01 | 03 | 58.800 | 69250 | 66250 | 56.300 | 58.300 | 58.000 |
|  |  | 06 | 02 | 02 | 64000 | 73950 | 72.960 | 60.600 | 80.600 | 64000 |
|  |  | 0.6 | 0.3 | 0.1 | 70.000 | 78.650 | 77.650 | 64.900 | \$4.900 | 70000 |
|  |  | 07 | 0.1 | 0.2 | 62.000 | 73.008 | 71.842 | 60300 | 50300 | 62.000 |
|  |  | 07 | 02 | 01 | 68.900 | 77708 | 76542 | 64600 | 64600 | 68000 |
|  |  | 08 | 01 | 01 | 66500 | 76767 | 75433 | 64300 | 64306 | 66.090 |
| SUM |  |  |  |  | 220800 | 252700 | 250700 | 2004.00 | 200400 | 220800 |


| T | M | W1 | W2 | W3 | SPTJEDD | EDDISPT | S［1］ | S．2］ | S［3］ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14 | 5 | 01 | 01 | 08 | 38.925 | 51.750 | 51.575 | 37.425 | 37425 | 38925 |
|  |  | 0.1 | 0.2 | 0.7 | 45525 | 57350 | 57175 | 42525 | 42525 | 45.525 |
|  |  | 0.1 | 03 | 06 | 52125 | 62950 | 62.775 | 47，625 | 47.625 | 52.125 |
|  |  | 0.1 | 04 | 0.5 | 58725 | 68.550 | 68375 | 52，725 | 52.725 | 58． 725 |
|  |  | 0.1 | D 5 | 0.4 | 65.325 | 74.150 | 73.975 | 57.825 | 57 B25 | 65325 |
|  |  | 01 | 06 | 03 | 71.925 | 79.750 | 79575 | 62.925 | 62925 | 71925 |
|  |  | 01 | 67 | 02 | 78525 | 85350 | 85.175 | 68025 | 68025 | 78525 |
|  |  | 01 | 08 | 01 | 85125 | 90950 | 90.775 | 73.125 | 73.125 | 85125 |
|  |  | ¢ 2 | 0.1 | 07 | 43250 | 55900 | 55550 | 41750 | 41.750 | 43.250 |
|  |  | 02 | 02 | 06 | 49850 | 61.500 | 61150 | 46850 | 46850 | 49850 |
|  |  | 02 | 03 | 05 | 56450 | 67100 | 66750 | 51.950 | 51950 | 56450 |
|  |  | ¢2 | 04 | 04 | 63050 | 72700 | 72.350 | 57050 | 57．050 | あ3050 |
|  |  | 02 | 05 | 03 | 69.650 | 78300 | 77.950 | 62150 | 62150 | 69.650 |
|  |  | 02 | 06 | 02 | 76250 | 83.900 | 83.550 | 67．250 | 67250 | 76250 |
|  |  | 02 | 07 | 01 | 82850 | 89500 | 89150 | 72350 | 72350 | 82856 |
|  |  | 03 | 01 | 06 | 47575 | 60.050 | 59.525 | 46.075 | 46075 | 47575 |
|  |  | 03 | 0.2 | 0.5 | 59.175 | 65 ¢50 | 65125 | 51.175 | 51175 | 54．175 |
|  |  | 03 | 0.3 | 0.4 | 60.775 | 71250 | 70725 | 56275 | 56275 | 60.775 |
|  |  | 0.3 | 0.4 | 0.3 | 67375 | 76850 | 76325 | 61.375 | 61.375 | 67375 |
|  |  | 03 | 05 | 02 | 73975 | 82.450 | 81.925 | 66475 | 66475 | 73975 |
|  |  | 03 | 0.6 | 0.1 | 80.575 | 88050 | 87525 | 71575 | 71．575 | 80.575 |
|  |  | 0.4 | 0.1 | 0.5 | 51.900 | 64200 | 63500 | 50400 | 50.400 | 51.900 |
|  |  | 04 | 02 | 04 | 58.500 | 69.800 | 69.190 | 55500 | 55.500 | 58500 |
|  |  | 04 | 03 | 03 | 65.100 | 75400 | 74.700 | 60600 | 60600 | 65.100 |
|  |  | 04 | 04 | 02 | 71.700 | 81.000 | 80300 | 65700 | 65700 | 71700 |
|  |  | 04 | 0.5 | 01 | 78300 | 86600 | 85900 | 70800 | 708.00 | 78300 |
|  |  | 65 | 0.1 | 04 | 56225 | 68.350 | 67475 | 54725 | 54725 | 56.225 |
|  |  | 05 | 02 | 03 | 62825 | 73.950 | 73075 | 59825 | 59.825 | 62825 |
|  |  | 0.5 | 03 | 02 | 69425 | 79550 | 78.675 | 64.925 | 64.925 | 69425 |
|  |  | 05 | 04 | 01 | 761325 | 85150 | 84275 | 70.025 | 70025 | 76025 |
|  |  | 06 | 01 | 03 | 60550 | 72500 | 71.450 | 59.050 | 59050 | 60.550 |
|  |  | 06 | 02 | 02 | 67.150 | 78.100 | 77.050 | 它4．150 | 64150 | 67.150 |
|  |  | 0.6 | 03 | 01 | 73.750 | 83.700 | 82.650 | 的 250 | 69250 | 73750 |
|  |  | 07 | 01 | 02 | 64875 | 76.650 | ¢5 425 | 63.375 | 63375 | 64.875 |
|  |  | 07 | 0.2 | 0.1 | 71.475 | 82250 | 81025 | 68475 | 68.475 | 71475 |
|  |  | 0.8 | 0.1 | 0.1 | 69200 | 80800 | 79400 | 67.700 | 67.700 | 69200 |
| SUM |  |  |  |  | 231900 | 268200 | 266100 | 2139.00 | 2139.00 | 231900 |


| T | H | W | W2 | W3 | SPTJEDD | EDDISPT | \＄［1］ | S［2］ | S［3］ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14 | 6 | 0.1 | 01 | 0.8 | 39850 | 53042 | 52， 0 ¢， 5 | 38.550 | 38550 | 39850 |
|  |  | 0.1 | 02 | 07 | 47050 | 59.542 | 59358 | 44．450 | 44450 | 47.050 |
|  |  | 0.1 | 0.3 | 0.6 | 54250 | 65042 | 65858 | 50360 | 50.350 | 54250 |
|  |  | 0.1 | 04 | B 5 | 61.450 | 72542 | 72.358 | 56250 | 56250 | 61450 |
|  |  | 01 | 0.5 | 0.4 | 68650 | 79042 | 78856 | 62.150 | 62150 | 68.650 |
|  |  | 0.1 | 06 | 03 | 75830 | 85542 | 85.358 | 68.950 | 68050 | 75850 |
|  |  | 01 | 07 | 02 | 83050 | 92 ［42 | 91.858 | 73950 | 73950 | 83050 |
|  |  | 01 | 08 | 01 | 90． 250 | 98542 | 58.358 | 79.850 | 79850 | 90250 |
|  |  | 0.2 | 01 | 07 | 44500 | 57.583 | 57217 | 43.200 | 43200 | 44500 |
|  |  | 0.2 | 02 | 06 | 51700 | 64.083 | 63717 | 49.100 | 49100 | 51.700 |
|  |  | 02 | 0.3 | 05 | 58900 | 70.583 | 70.217 | 55000 | 55000 | 58900 |
|  |  | 02 | 04 | 04 | 66.100 | 77.083 | 76717 | 60500 | 60900 | 66.100 |
|  |  | 02 | 65 | G． 3 | 73300 | 83.583 | 83217 | 66800 | 66800 | 73.300 |
|  |  | 0.2 | 06 | 02 | 80500 | 90.083 | 89717 | 72700 | 72.700 | 80.500 |
|  |  | 0.2 | 07 | 01 | 87700 | 96583 | 96217 | 78680 | 78.600 | 87．700 |
|  |  | 0.3 | 0.1 | 06 | 49150 | 62125 | 61.575 | 47.950 | 47850 | 49150 |
|  |  | 03 | 02 | 0.5 | \＄5 360 | 58625 | 68075 | 53750 | 53.750 | 56350 |
|  |  | 03 | 03 | 0.4 | 63560 | 75.125 | 74575 | 59650 | 59650 | 63550 |
|  |  | 0.3 | 04 | 03 | 70750 | 88.625 | 81075 | 55.550 | 65550 | 70.750 |
|  |  | 03 | 05 | 02 | 77.950 | 88.125 | 87575 | 71．450 | 71450 | 77.950 |
|  |  | 03 | 66 | 01 | 85150 | 94625 | 94075 | 77 350 | 77.350 | 85150 |
|  |  | 04 | Q 1 | b 5 | 53.800 | 66667 | 65933 | 52500 | 52500 | 53500 |
|  |  | 04 | 02 | 04 | 61.000 | 73167 | 72.433 | 58400 | 58.4130 | 61000 |
|  |  | 0.4 | 03 | 03 | 68200 | 79667 | 78.933 | 64.300 | 64.300 | 68200 |
|  |  | 0.4 | 0.4 | 02 | 75400 | 86167 | 85433 | 70200 | 70200 | 75400 |
|  |  | 0.4 | 05 | 01 | 82600 | 92667 | 91.933 | 76100 | 76100 | 82600 |
|  |  | 05 | 01 | 04 | 58450 | 71208 | 70292 | 57.150 | 57150 | 58450 |
|  |  | 05 | 02 | 03 | 65650 | 77.708 | 76792 | 63050 | 63 D50 | 65.650 |
|  |  | 05 | 03 | 02 | 72850 | 84.208 | 93.292 | 68950 | 68.950 | 72850 |
|  |  | 0.5 | 04 | 01 | 8 ED 050 | 90.708 | 89792 | 74.850 | 74.850 | 80050 |
|  |  | 06 | 0.1 | 0.3 | 63100 | 75750 | 7465 | 61.800 | 61800 | 63100 |
|  |  | 0.6 | 02 | 02 | 70300 | 82250 | 81150 | 67，700 | 67.700 | 70300 |
|  |  | 06 | 03 | 0.1 | 77.500 | 88.750 | 87650 | 73600 | 73．60 | 77.500 |
|  |  | 07 | 01 | 02 | 67.750 | 80292 | 73008 | 56450 | 66450 | 67.750 |
|  |  | 07 | 02 | 01 | 74950 | 86.792 | 85508 | 72.350 | 72.350 | 74950 |
|  |  | 08 | 01 | 0.1 | 72.400 | 84833 | 83367 | 71.100 | 71.100 | 72400 |
| SUM |  |  |  |  | 243000 | 283700 | 281500 | 2274．00 | 2274.00 | 2430.00 |


| T | M | W11 | W2 | W3 | SPTIEDD | EDDISPT | S[1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14 | 7 | 01 | 01 | 09 | 40.775 | 54333 | 54.142 | 39675 | 39675 | AD 775 |
|  |  | D 1 | 0.2 | 07 | 48.575 | 61.733 | 61.542 | 46375 | 46375 | 48575 |
|  |  | 0.1 | 0.2 | 0.6 | 56 375 | 69.133 | 68942 | 53075 | 53075 | 56.375 |
|  |  | 01 | 04 | 0.5 | 64175 | 76.533 | 76342 | 59775 | 59.775 | 64.175 |
|  |  | 01 | 05 | 04 | 71975 | 83.933 | 83742 | 66475 | 66475 | 71.975 |
|  |  | 0.1 | 06 | 03 | 79775 | 91.333 | 91.142 | 73175 | 73.175 | 79.775 |
|  |  | 01 | 07 | 02 | 87.575 | 98733 | 98542 | 79.875 | 79875 | 87575 |
|  |  | 01 | 0.8 | 01 | 95.375 | 106133 | 105942 | 86575 | 86.575 | 95375 |
|  |  | 02 | 0.1 | 07 | 45.750 | 59267 | 58 B83 | 44650 | 44650 | 45750 |
|  |  | 02 | 02 | 06 | 53 550 | 66.667 | 66283 | 51350 | 51.350 | 53.550 |
|  |  | 02 | 03 | 05 | 61.350 | 74.067 | 73683 | 58050 | 56050 | 61.350 |
|  |  | 02 | 04 | 0.4 | 69150 | 81.467 | 81083 | 64750 | 64750 | 69.150 |
|  |  | G2 | 0.5 | 03 | 76950 | 88.867 | 88483 | 71.450 | 71450 | 76.950 |
|  |  | 02 | 06 | 02 | 84750 | 96267 | 95883 | 78150 | 78150 | 84750 |
|  |  | 0.2 | 07 | 0.1 | 92551 | 103667 | 103.283 | B4 850 | 84850 | 92550 |
|  |  | 0.3 | 01 | 0.6 | 50.725 | 64200 | 63.625 | 49625 | 49625 | 50725 |
|  |  | 0.3 | 02 | 05 | 58.525 | 71.600 | 71025 | 56325 | 56325 | 58525 |
|  |  | 0.3 | 03 | 04 | 66.325 | 79000 | 78425 | 63025 | 63025 | 6 6 325 |
|  |  | 0.3 | 04 | 03 | 74.125 | 86.400 | 85825 | 69725 | 69725 | 74.125 |
|  |  | 0.3 | 05 | 02 | 81.925 | 93.800 | 93225 | 76425 | 76425 | 81.925 |
|  |  | 0.3 | 06 | 0.1 | 89.725 | 104.200 | 100625 | 83125 | 83125 | 89725 |
|  |  | 04 | 0.1 | 05 | 55.700 | 69133 | 68367 | 54.600 | 54600 | 55700 |
|  |  | 04 | 0.2 | 04 | 63.500 | 76533 | 75767 | 61.300 | 61300 | 63500 |
|  |  | 0.4 | 03 | 03 | 71300 | 83933 | 83167 | 68000 | 68000 | 71300 |
|  |  | 0.4 | 04 | 0.2 | 79100 | 91.333 | 90567 | 74700 | 74,700 | 79100 |
|  |  | 04 | 05 | 0.1 | 86500 | 98933 | 97.967 | 81400 | 81.400 | 86.900 |
|  |  | 05 | 0.1 | 0.4 | 60.675 | 74067 | 73.108 | 59575 | 59575 | 60.675 |
|  |  | 0.5 | 02 | 0.3 | 68.475 | 81467 | 80.508 | 65275 | 66275 | 68.475 |
|  |  | 0.5 | 0.3 | 0.2 | 76275 | 88.867 | 87.908 | 72.975 | 72975 | 76.275 |
|  |  | 0.5 | 0.4 | 01 | 84075 | 96.267 | 95309 | 79.675 | 79675 | 84.075 |
|  |  | 06 | 0.1 | $\bigcirc 3$ | 65.650 | 79000 | 77850 | 64.550 | 64550 | 65650 |
|  |  | 06 | 12 | 02 | 73450 | 86400 | 85250 | 71.250 | 71250 | 73450 |
|  |  | 06 | D 3 | 01 | B1 250 | 938001 | 92.650 | 77950 | 77950 | 81.250 |
|  |  | 0.7 | D 1 | 02 | 70.625 | 83.933 | B2.592 | 69525 | 69.525 | 70625 |
|  |  | 07 | 02 | 0.1 | 76425 | 91.333 | 8.992 | 76225 | 76225 | 78.425 |
|  |  | 0.8 | 01 | 01 | 7560 | 88867 | B7.333 | 74500 | 74.500 | 75600 |
| SUM |  |  |  |  | 2541.00 | 259200 | 2969 | 240900 | 240900 | 2541.03 |



| 7 | M | W1 | W2 | WY3 | §FTIEDD | EDDISPT | S［1］ | S［2］ | \＄［3］ | S14］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | 4 | 01 | 0.1 | 0，8 | 45325 | 29350 | 29350 | 43825 | 43825 | 45325 |
|  |  | 0.1 | 02 | 07 | 51125 | 33250 | 33250 | 48.125 | 48125 | 51125 |
|  |  | 01 | 03 | 0.6 | 56.925 | 37150 | 37.150 | 52.425 | 52425 | 58.925 |
|  |  | 0.1 | 04 | 05 | 62725 | 41．050 | 41050 | 56.725 | 56725 | 62725 |
|  |  | 0.1 | 0.5 | 04 | 68525 | 44．950 | 44950 | 61025 | 61.025 | 6 E 525 |
|  |  | 01 | 0.6 | 03 | 74325 | 48.850 | 48850 | 65.325 | 65．325 | 74325 |
|  |  | 0.1 | 0.7 | 02 | 84125 | 52.750 | 52．750 | 69625 | 69.625 | 80125 |
|  |  | 01 | 0.6 | 0.1 | 85925 | 56.650 | 56.650 | 73.925 | 73925 | 85.925 |
|  |  | 02 | 01 | 07 | 48.850 | 33800 | 33800 | 47350 | 47350 | 48850 |
|  |  | 0.2 | 02 | 06 | 54，650 | 37.700 | 37700 | 51.650 | 51.650 | 54650 |
|  |  | 0.2 | 0.3 | 05 | 60450 | 41600 | 41．600 | 55950 | 55950 | 60.450 |
|  |  | 02 | 0.4 | 0.4 | 66250 | 45500 | 45.500 | 60250 | 60.250 | 66.250 |
|  |  | 02 | 0.5 | 0.3 | 72050 | 49400 | 49.400 | 64550 | 64.550 | 72.050 |
|  |  | 02 | 06 | 0.2 | 77.850 | 53300 | 53300 | 68.850 | 68.850 | 77 B50 |
|  |  | 02 | 07 | 0.1 | 83650 | 57200 | 57.200 | 73.150 | 73．15D | 83650 |
|  |  | 0.3 | 0.1 | 06 | 52375 | 38250 | 38.250 | 50875 | 50875 | 52.375 |
|  |  | 03 | 02 | 05 | 58175 | 42.150 | 42150 | 55175 | 55175 | \＄8．175 |
|  |  | 03 | 03 | 0.4 | ¢ 6.975 | 46050 | 46050 | 59.475 | 59.475 | 63975 |
|  |  | 0.3 | 04 | 03 | 69775 | 49.950 | 49.950 | 63775 | 63775 | 69，775 |
|  |  | 03 | 05 | 02 | 75575 | 53850 | 53850 | 68.075 | 68.075 | 75.575 |
|  |  | 03 | 0.6 | 0.1 | B1．375 | 57.750 | 57.750 | 72.375 | 72375 | 81.375 |
|  |  | 04 | 01 | 0.5 | 55.900 | 42700 | 42.700 | 54．400 | 54400 | 55.900 |
|  |  | 0.4 | 0.2 | 04 | 51，700 | 46600 | 46500 | 59.700 | 58700 | 65.700 |
|  |  | 04 | 0.3 | 03 | 67.500 | 50500 | 50500 | 63.000 | 63000 | 67.500 |
|  |  | 04 | 0.4 | 02 | 73300 | 54.400 | 54400 | 67300 | 67.300 | 73700 |
|  |  | 0.4 | 0.5 | 0.1 | 79100 | 58300 | 58.300 | 71.600 | 71600 | 79100 |
|  |  | 0.5 | 0.1 | 04 | 59425 | 47.150 | 47.150 | 57.925 | 57925 | 59425 |
|  |  | 05 | 02 | 0.3 | 65225 | 51.050 | 51.050 | 62225 | 62.225 | 65225 |
|  |  | 05 | D 3 | 0.2 | 71．025 | 54.950 | 54.950 | 66525 | 66525 | 71.025 |
|  |  | 05 | D 4 | 0.1 | 76825 | 58850 | 58.850 | 70825 | 70825 | 76.825 |
|  |  | 06 | 01 | 03 | 62.950 | 51.600 | 51.600 | 61450 | 61450 | 62.950 |
|  |  | 06 | ¢ 2 | 02 | 68750 | 55.500 | 55.500 | 65750 | 65.750 | 68，750 |
|  |  | 06 | 0.3 | 01 | 74550 | 59400 | 59400 | 70050 | 70050 | 74.550 |
|  |  | 07 | 01 | 02 | 66475 | 560.50 | 560.50 | 64975 | 64975 | 65475 |
|  |  | 07 | 02 | 01 | 72275 | 59.950 | 59.950 | 69275 | 69.275 | 72.275 |
|  |  | 18 | 01 | 0.1 | 70000 | 60.500 | 60500 | 施．500 | 68500 | 70.000 |
| S゙もH |  |  |  |  | 2415.00 | 175800 | 1758.00 | 223500 | 223500 | 24150 |


| T | ＂M | W1 | W2 | W3 | SPTFEDD | EDDISPT | S［1］ | S［2］ | S31 | \＄ 41 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | 5 | 0.1 | 0.1 | 08 | 46250 | 30342 | 30.342 | 44950 | 44.950 | 46250 |
|  |  | － 1 | ${ }^{6} 2$ | 07 | 52650 | 34.942 | 34942 | 50.950 | 50.050 | 52650 |
|  |  | 0.1 | 03 | 06 | 59050 | 39542 | 39.542 | 55150 | 55150 | 59050 |
|  |  | 6． 1 | 0.4 | 0.5 | 65.450 | 44142 | 44142 | 60250 | 60.250 | 65450 |
|  |  | 01 | 05 | 04 | 71850 | 48.742 | 18742 | 65350 | 65350 | 71.850 |
|  |  | 0.1 | 06 | 03 | 78250 | 53342 | 53342 | 70450 | 70450 | 78250 |
|  |  | 0.1 | 07 | 02 | 84650 | 57942 | 57.942 | 75.550 | 75550 | 84650 |
|  |  | 0.1 | 08 | 01 | 91050 | 62.542 | 62542 | 80650 | 80650 | 91.050 |
|  |  | 0.2 | 0.1 | 07 | 50100 | 35083 | 35083 | 48800 | 48．800 | 50100 |
|  |  | 02 | 02 | 06 | 56500 | 39.583 | 39.683 | 53.900 | 53900 | 56500 |
|  |  | 02 | 0.3 | 0.5 | 62，900 | 44283 | 44283 | 59000 | 59．000 | 62900 |
|  |  | 02 | 04 | 04 | 69300 | 48.883 | 48．8官3 | 64.100 | 64.100 | 69300 |
|  |  | 02 | 05 | 03 | 75.700 | 53483 | 53.483 | 69200 | 69.200 | 75.700 |
|  |  | 02 | 05 | 0.2 | 82.100 | 58083 | 58.083 | 74.300 | 74．300 | 82100 |
|  |  | 02 | 07 | 01 | 88500 | 62683 | 62．引83 | 79400 | 79400 | 88500 |
|  |  | 03 | 01 | 06 | 53950 | 39 B 25 | 39.825 | 52，650 | 52.650 | 53950 |
|  |  | 03 | 0.2 | 05 | 60350 | 44425 | 44425 | 57．750 | 57.750 | 60350 |
|  |  | 0.3 | 03 | 04 | 66750 | 49.225 | 49025 | 62.850 | 62.850 | 66750 |
|  |  | 03 | 04 | 03 | 73150 | 53625 | 53625 | 67950 | 67.950 | 73.150 |
|  |  | 03 | 05 | 02 | 79.550 | \＄8225 | 58225 | 73050 | 73050 | 79.550 |
|  |  | 03 | 06 | 0.1 | 85.950 | $62 \mathrm{B25}$ | 62825 | 7 B 150 | 78.150 | 85.950 |
|  |  | 04 | 01 | 05 | 57.800 | 44567 | 44567 | 56500 | 56.500 | 57.800 |
|  |  | 04 | 02 | 0.4 | 64，200 | 49167 | 49167 | 61600 | 61.500 | 64200 |
|  |  | 04 | 03 | 03 | 70600 | 53767 | 53.767 | 66700 | 66.700 | 70600 |
|  |  | 04 | 04 | 02 | 77000 | 58.367 | \＄9367 | 71800 | 71800 | 77000 |
|  |  | 04 | 05 | 01 | 83400 | 62967 | 62967 | 76900 | 76.900 | 9．3400 |
|  |  | 05 | 01 | 04 | 61650 | 49.308 | 49．308 | 60350 | 60.350 | 61650 |
|  |  | 05 | 02 | 03 | 58.050 | 53．808 | 53908 | 65450 | 65.450 | 68.050 |
|  |  | 05 | 03 | 0.2 | 74．460 | 58508 | 58508 | 70550 | 70550 | 74450 |
|  |  | 05 | 04 | 01 | 80850 | 6\％．108 | 63106 | 75650 | 75650 | 80.850 |
|  |  | 06 | 01 | 03 | 65500 | 54050 | 54 D50 | 64200 | 64200 | 85．500 |
|  |  | 06 | 02 | 02 | 71900 | 58650 | 58．650 | 69.300 | 69300 | 71500 |
|  |  | 06 | 03 | 01 | 78300 | 63250 | 63.250 | 74，400 | 74.400 | 78300 |
|  |  | 07 | 01 | 02 | 69350 | 58792 | 59.792 | 68050 | 68050 | 69350 |
|  |  | 07 | 0.2 | 0.1 | 75.750 | 63392 | 63392 | 73.150 | 73.150 | 75.750 |
|  |  | 08 | 01 | 01 | 73.200 | 63533 | 63533 | 71900 | 71.900 | 73200 |
| SUW |  |  |  |  | 252600 | 1877.00 | 1877.00 | 237000 | 237000 | 252600 |


| T | M | W1 | W2 | W3 | SP＇TED | EDDISPT | S［1］ | S［2］ | S［3］ | \＄［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | 6 | 0.1 | 01 | 68 | 47175 | 31.333 | 37333 | 46075 | 46075 | 47175 |
|  |  | 01 | 0.2 | 07 | 54175 | 36.633 | 36633 | 51975 | 51.975 | 54175 |
|  |  | 0.1 | 03 | 06 | 61175 | 41.933 | 41933 | 57875 | 57.975 | 61175 |
|  |  | 01 | 04 | 05 | 68.175 | 47233 | 47233 | 63.775 | 63775 | 68175 |
|  |  | 01 | 05 | 04 | 75175 | 52533 | 52.533 | 69675 | 69.675 | 75175 |
|  |  | 01 | 06 | 03 | 82.175 | 57833 | 57．833 | 75575 | 75575 | 82175 |
|  |  | 0.1 | 07 | 02 | 89175 | 63.133 | 63133 | 81475 | B1．475 | 89.175 |
|  |  | 01 | 08 | 01 | 96175 | 68.433 | 68433 | 87375 | 87.375 | 96175 |
|  |  | 02 | 01 | 07 | 51350 | 36367 | 36367 | 56 250 | 50250 | \＄1，350 |
|  |  | 02 | 02 | 06 | 59350 | 41667 | 41667 | 56．150 | 56.150 | 58350 |
|  |  | 02 | 03 | 05 | 65350 | 46967 | 46967 | 62.050 | 62050 | 65350 |
|  |  | 02 | 04 | 0.4 | 72350 | 52.267 | 52267 | 67950 | 67.950 | 72350 |
|  |  | 02 | 05 | 0.3 | $7{ }^{7} 350$ | 57567 | 57.567 | 73850 | 73850 | 79350 |
|  |  | 02 | 06 | 0.2 | 86350 | 62867 | 的 667 | 79.750 | 79750 | 86350 |
|  |  | 0.2 | 07 | 01 | 93350 | 68.167 | 68167 | 85650 | 85.650 | 93350 |
|  |  | 0.3 | 0.1 | 0.6 | 55525 | 41.400 | 41.460 | 54425 | 54425 | 55.525 |
|  |  | 0.3 | 0.2 | 0.5 | 62525 | 46700 | 46700 | 60325 | 6 B 325 | 62525 |
|  |  | 0.3 | 03 | 0.4 | 69525 | 52000 | 52.000 | 66225 | 66225 | 69525 |
|  |  | 0.3 | 0.4 | 03 | 75525 | 67．300 | 57.300 | 72125 | 72125 | 76525 |
|  |  | 0.3 | 05 | 02 | 83525 | 62600 | 62.600 | 781225 | 78025 | 83 525 |
|  |  | 03 | 0.6 | 0.1 | 90525 | 67.900 | 67.900 | 83.925 | 93．925 | 90.525 |
|  |  | 04 | 01 | 05 | 59706 | 46433 | 46，4．33 | 56.600 | 58600 | $5970 \square$ |
|  |  | W 4 | 02 | 0.4 | 86．700 | 51.733 | 51733 | 64．590 | 64500 | 66700 |
|  |  | 0.4 | 0.3 | 03 | 73700 | 57033 | 57033 | 70400 | 70400 | 73700 |
|  |  | 04 | 04 | 02 | 80700 | 62333 | 62.333 | 76300 | 76300 | 80700 |
|  |  | 04 | 05 | 61 | 87700 | 67.633 | 67.633 | 82200 | 32200 | 87700 |
|  |  | 65 | 91 | 04 | 83．875 | 51.467 | \＄1467 | 62775 | 62775 | 63875 |
|  |  | 05 | 02 | 03 | 70.875 | 56.767 | 56.767 | 68675 | 66675 | 70.875 |
|  |  | 05 | 03 | 62 | 77875 | 62067 | 62．067 | 74575 | 74575 | 77875 |
|  |  | 0.5 | 04 | 0.1 | 84875 | 67367 | 67367 | 80.475 | 80.475 | 84.875 |
|  |  | 06 | 0.1 | 0.3 | 68.050 | 56500 | 56500 | 66.950 | 66950 | 68.050 |
|  |  | 06 | 02 | 02 | 75050 | 61.800 | 61.800 | 72.650 | 72850 | 75 D50 |
|  |  | 06 | 03 | 01 | 82050 | 67.100 | 67.100 | 78750 | 78750 | 82050 |
|  |  | 07 | 0.1 | 02 | 72225 | 61533 | 的．533 | 71.125 | 71.125 | 72225 |
|  |  | 0.7 | 0.2 | 01 | 79225 | 66833 | E6833 | 77.025 | 77.025 | 79225 |
|  |  | 08 | 01 | 0.1 | 76400 | 的 567 | 66557 | 75300 | 75300 | 76400 |
| SUM |  |  |  |  | 2637.00 | 199600 | 1996，00 | 250500 | 250500 | 2637．00 |


| T | M | W1 | W2 | W3 | SPTIEDD | EDDISPT | S［1］ | $5[2]$ | S［3］ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | 7 | 01 | 01 | ¢ 8 | 48100 | 32325 | 32325 | 47.200 | 47．200 | 48100 |
|  |  | 01 | 02 | 07 | 55700 | 38325 | 38.325 | 53900 | 53900 | 56．700 |
|  |  | 01 | 03 | 06 | 53300 | 44.325 | 44.325 | 60600 | 60600 | 633005 |
|  |  | 01 | 04 | 05 | 70900 | 50.325 | 50.325 | 67.300 | 67.300 | 70900 |
|  |  | 0.1 | 05 | 04 | 78.500 | 56325 | 56325 | 74.000 | 74.000 | 78.500 |
|  |  | 01 | 06 | 03 | 86100 | 62325 | 82．325 | 80700 | 80700 | 86100 |
|  |  | 0.1 | 07 | 02 | 93700 | 68.325 | 68.325 | 87.400 | 37400 | 93700 |
|  |  | 01 | 08 | 01 | 101300 | 74325 | 74325 | 94.100 | 94.100 | 101300 |
|  |  | 02 | 01 | 07 | 52800 | 37650 | 37650 | 51.700 | 51.700 | 52.600 |
|  |  | 02 | 02 | 06 | 60200 | 43650 | 43650 | 58400 | 58400 | 60.200 |
|  |  | 02 | 03 | 05 | 67800 | 49650 | 49650 | 65108 | 65100 | 67．800 |
|  |  | 02 | 0.4 | 04 | 75400 | 55650 | 55.650 | 71.800 | 71.800 | 75.400 |
|  |  | 0.2 | 05 | 03 | 83000 | 61.650 | 81，650 | 78500 | 78.500 | 23 000 |
|  |  | 02 | 06 | 02 | 90600 | 67650 | 67650 | 85204 | 85.200 | 90600 |
|  |  | 0.2 | 0.7 | 01 | 98200 | 73.650 | 73.650 | 91．900 | 91.900 | 98200 |
|  |  | 03 | 01 | 06 | 57．100 | 42975 | 42975 | 56200 | 56200 | 57.100 |
|  |  | 0.3 | 02 | 0.5 | 64.700 | 48975 | 48975 | 62900 | 62900 | 64700 |
|  |  | 03 | 03 | 04 | 72300 | 54．975 | 54.975 | 69600 | 69600 | 72.300 |
|  |  | 03 | 04 | 0.3 | 79.900 | 00.975 | 60975 | 76300 | 76300 | 79.900 |
|  |  | 0.3 | D． 5 | 02 | 87.500 | 66.975 | 66.975 | 83000 | 83000 | 87．540 |
|  |  | 0.3 | 06 | 0.1 | 95100 | 72.975 | 72.975 | 89700 | 89700 | $95.10{ }^{10}$ |
|  |  | 04 | 01 | 05 | 61.600 | 48.300 | 48300 | 60700 | 66700 | 61．600 |
|  |  | 04 | 02 | 04 | 69200 | 54.300 | 54.300 | 67.400 | 67400 | 69208 |
|  |  | 04 | 03 | 03 | 76800 | 60.300 | 60300 | 74100 | 74100 | 7680 |
|  |  | 04 | 04 | 02 | 84400 | 65.300 | 66300 | 80.800 | 80800 | 84.40 F |
|  |  | D4 | 05 | 01 | 92．000 | 72.300 | 72.300 | 87.500 | 87.500 | 92000 |
|  |  | 05 | 01 | 04 | 65100 | 53625 | 53625 | 65200 | 65200 | 66105 |
|  |  | 05 | 0.2 | 03 | 73700 | 59625 | 59625 | 71.900 | 71900 | 73.700 |
|  |  | 05 | 03 | 02 | 81.300 | 65625 | 65625 | 78．600 | 78600 | 81.300 |
|  |  | 05 | 04 | 01 | 88.905 | 71625 | 71.625 | 85300 | 85300 | 88960 |
|  |  | 06 | 01 | 03 | 70.600 | 58.950 | 58950 | 69700 | 69.700 | 7 D 600 |
|  |  | 0.6 | 02 | 0.2 | 78200 | 64.950 | 64.950 | 76400 | 76400 | 78.200 |
|  |  | 06 | 03 | 0.1 | 85.800 | 70.950 | 70.950 | 83100 | 83100 | 85800 |
|  |  | 07 | 0.1 | 0.2 | 75100 | 64275 | 64275 | 74.200 | 74200 | 75.100 |
|  |  | 07 | 02 | 01 | 82.700 | 70275 | 70275 | 80900 | 80900 | 82700 |
|  |  | 08 | 01 | 01 | 79600 | 69600 | 69600 | 78700 | 78.700 | 79600 |
| SUM |  |  |  |  | 274800 | 211500 | 2115.00 | 264000 | 264000 | 2748.00 |


| F | M | W1 | W/2 | W/3 | SPTJEDD | EDD/SPT | S[1] | S[2] | 5[3] | $5[4]$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | 8 | 01 | 0.1 | 08 | 49025 | 33317 | 33317 | 48325 | 48325 | 49.025 |
|  |  | 0.1 | 02 | 0.7 | 57.225 | 40.017 | 40017 | 55825 | $55 \mathrm{B25}$ | 57.226 |
|  |  | 0.1 | 03 | 06 | 65.425 | 45717 | 46.717 | 63325 | 63.325 | 65425 |
|  |  | 0.1 | 04 | 0.5 | 73.625 | 53.417 | 53.417 | 70.825 | 76825 | 73625 |
|  |  | 0.1 | 05 | D. 4 | 81.825 | 60.117 | 60.117 | 78325 | 78.325 | 81.825 |
|  |  | 0.1 | 06 | 03 | 90025 | 66.817 | 66817 | 85825 | 85825 | 90.025 |
|  |  | 0.1 | 07 | 02 | 98225 | 73.517 | 73.517 | 93325 | 93325 | 98225 |
|  |  | 01 | (1) 8 | 01 | 104 425 | 80.217 | B0 217 | 100825 | 100825 | 106425 |
|  |  | 02 | 01 | 07 | 53850 | 38.933 | 38933 | 53150 | 53150 | 53850 |
|  |  | 02 | D 2 | 06 | 62050 | 45633 | 45633 | 60650 | 60650 | 62050 |
|  |  | 02 | 03 | [5 | 70250 | 52.333 | 52.333 | 68150 | 68, 150 | 70250 |
|  |  | 02 | 04 | 04 | 78450 | 59033 | 59033 | 75650 | 75.650 | 78450 |
|  |  | 02 | 05 | 03 | B6 650 | 65733 | 65733 | 83150 | 83.160 | 86650 |
|  |  | 02 | D 6 | 02 | 94.850 | 72.433 | 72.433 | 90650 | 90650 | 94850 |
|  |  | 02 | 07 | D1 | 103050 | 79133 | 79.133 | 98150 | 98150 | 103050 |
|  |  | 03 | 01 | 06 | 58675 | 44.550 | 44550 | 57.975 | 57.975 | 58675 |
|  |  | 03 | 02 | 05 | 66875 | 51.250 | 51250 | 65475 | 65.475 | 66.875 |
|  |  | 03 | 03 | 04 | 75075 | $57.95\}$ | 57950 | 72975 | 72975 | 75075 |
|  |  | 03 | 04 | 03 | 83275 | 64650 | 64.650 | 80475 | 80475 | 83275 |
|  |  | 03 | 05 | 02 | 91475 | 71.350 | 71.353 | 87.975 | 87.975 | 91.475 |
|  |  | 03 | 06 | 01 | 99675 | 78050 | 78050 | 95475 | 95475 | 99675 |
|  |  | W 4 | 01 | 05 | 63504 | 50167 | 50.167 | 62800 | 62 BOO | 63.500 |
|  |  | $\bigcirc 4$ | 02 | 04 | 71700 | 56867 | 56867 | 70300 | 70300 | 71.700 |
|  |  | $\bigcirc 4$ | 0.3 | 03 | 79906 | 53567 | 63567 | 77.800 | 77800 | 79900 |
|  |  | Q 4 | 04 | 0.2 | 88100 | 7 D 267 | 70267 | 85300 | 85300 | 88100 |
|  |  | W 4 | 65 | 01 | 96300 | 76967 | 76967 | 92.900 | 92 BOO | 96300 |
|  |  | 05 | 01 | 04 | 68325 | 55783 | 55783 | 67.625 | 67625 | 68325 |
|  |  | 05 | 02 | [13 | 76525 | 62.483 | 62483 | 75125 | 75.125 | 76525 |
|  |  | 05 | 0.3 | 02 | 84725 | 69193 | 69183 | 82.625 | 82.625 | 84725 |
|  |  | 65 | 04 | 0.1 | 92925 | 75883 | 75883 | 90125 | 90125 | 92.925 |
|  |  | 66 | 01 | 0.3 | 73150 | 61.406 | 51.400 | 72.450 | 72450 | 73150 |
|  |  | 06 | 0.2 | 02 | 81.350 | 68100 | 68100 | 79950 | 79.950 | 81.350 |
|  |  | 06 | 03 | 01 | 89550 | 74.800 | 74.800 | 87.450 | 87450 | 89550 |
|  |  | 07 | 0.1 | 02 | 77.975 | 67.017 | 67.017 | 77.275 | 77275 | 77.975 |
|  |  | 0.7 | 02 | 01 | 86 175 | 73.717 | 73717 | 84775 | 84.775 | 86.175 |
|  |  | 08 | 61. | 01 | B2800 | 72,633 | 72633 | 82100 | 82.100 | 82800 |
| SUM |  |  |  |  | 285900 | 223400 | 2234,00 | 277500 | 277500 | 2859.00 |


| T | M | W1 | W2 | W3 | SPTíEDD | EDDISPT | S[1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16 | 4 | 01 | 01 | 08 | 36.609 | 35942 | 35642 | 35308 | 35308 | 3660 B |
|  |  | 01 | 02 | 07 | 41.808 | 39,842 | 39542 | 39208 | 39208 | 4180 B |
|  |  | 0.1 | 0.3 | 06 | 47008 | 43.742 | 43442 | 43.108 | 43108 | 4700 B |
|  |  | 01 | 04 | 0.5 | 52208 | 47642 | 47.342 | 47.008 | 47.00.8 | 52208 |
|  |  | 01 | 05 | 0.4 | 57408 | 51542 | 51.242 | 50.908 | 50.908 | 57.408 |
|  |  | 01 | 06 | 0.3 | 62608 | 55442 | 55142 | 54.808 | 54808 | 62.608 |
|  |  | 0.1 | 07 | 02 | 67808 | 59.342 | 59.042 | 58.708 | 58.708 | 67808 |
|  |  | 01 | 0 B | 01 | 73.009 | 63242 | 62.942 | 62608 | 62.608 | 73008 |
|  |  | 02 | 01 | 0.7 | 40017 | 39983 | 39383 | 38717 | 38717 | 40017 |
|  |  | 02 | 02 | 06 | 45217 | 43883 | 43283 | 42617 | 42617 | 45217 |
|  |  | 02 | 03 | 0.5 | 50417 | 47.783 | 47.183 | 46517 | 66517 | 56417 |
|  |  | 02 | 04 | 04 | 55617 | 51.683 | 51.093 | 50417 | 50417 | 55617 |
|  |  | 02 | 05 | 03 | 60.817 | 55.583 | 54.983 | 54317 | 54.317 | 60817 |
|  |  | 02 | 06 | 02 | 66017 | 59.483 | 58883 | 58.217 | 58217 | 66.017 |
|  |  | 02 | 0.7 | 01 | 71217 | 63383 | 62.783 | 62.117 | 62117 | 71217 |
|  |  | 03 | 0.1 | 06 | 43425 | 44.025 | 43125 | 42.125 | 42125 | 43425 |
|  |  | 03 | 02 | 05 | 48625 | 47.925 | 47.025 | 46025 | 46.025 | 48625 |
|  |  | 03 | 03 | 04 | $53 \mathrm{B25}$ | 51825 | 50925 | 49.925 | 49925 | 53825 |
|  |  | 03 | 04 | 0.3 | 59.225 | 55.725 | 54825 | 53.825 | 53.825 | 59 D25 |
|  |  | 03 | 0.5 | 0.2 | 64225 | 59625 | 5B 725 | 57.725 | 57725 | 64225 |
|  |  | 03 | 06 | 0.1 | 69.425 | 63.525 | 62625 | 61.625 | 61.625 | 69425 |
|  |  | 04 | 01 | 0.5 | 46.833 | 48067 | 46867 | 45533 | 45.533 | 46833 |
|  |  | 04 | 02 | 04 | 52033 | 51967 | 50767 | 49.433 | 49433 | 52 D 33 |
|  |  | 04 | 03 | 03 | 57233 | 55867 | 54.667 | 53.333 | 53333 | 57233 |
|  |  | 04 | 04 | 02 | 62433 | 59767 | 58.567 | 57233 | 57233 | 62433 |
|  |  | 04 | 05 | 01 | 67.633 | 63667 | 62467 | 61133 | 61.133 | 67633 |
|  |  | 05 | 01 | 0.4 | 50242 | 52108 | 50608 | 49.942 | 48942 | 50242 |
|  |  | 05 | 02 | 03 | 55442 | 56008 | 54.508 | 52842 | 52842 | 55442 |
|  |  | 05 | 03 | 02 | 60642 | 59908 | 58.408 | 56742 | 56742 | 60642 |
|  |  | 05 | 04 | 01 | 65842 | 63808 | 52.304 | 60642 | 60642 | 65842 |
|  |  | 06 | 01 | 03 | 53650 | 56150 | 54.350 | 52.350 | 52350 | 53650 |
|  |  | 06 | 02 | 02 | 58.850 | 80050 | 58250 | 56250 | 56250 | 59.850 |
|  |  | 06 | 03 | 01 | 64050 | 63950 | 62.150 | 60150 | 60150 | 64050 |
|  |  | 07 | 01 | 0.2 | 57058 | 6 C 192 | 58092 | 55.758 | 55758 | 57058 |
|  |  | 0.7 | 02 | 0.1 | 62258 | 64092 | 61992 | 59.658 | 59658 | 62258 |
|  |  | 08 | 01 | 0.1 | 60467 | 64233 | 61833 | 59167 | 59.167 | 60467 |
|  |  | SUN |  |  | 2041.00 | 1961.0 | 192500 | 1885.00 | 188500 | 2041.00 |


| T | M | W1 | W2 | W3 | SPT／EDD | EDDISPT | S［1］ | S［2］ | S［3］ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16 | 5 | 0.1 | 01 | 0.8 | 37.367 | $3{ }^{6} 933$ | 36617 | 36267 | 36267 | 37.367 |
|  |  | 01 | 02 | 07 | 43067 | 41533 | 41217 | 40.867 | 40．867 | 43067 |
|  |  | 01 | 03 | 06 | 48767 | 46133 | 45817 | 45467 | 45．467 | 48.767 |
|  |  | 01 | 04 | 05 | 54467 | 50733 | 50.417 | 50.067 | 50.067 | 54，467 |
|  |  | 01 | 05 | 04 | 60167 | 55333 | 55.017 | 54667 | 54667 | 60167 |
|  |  | 0.1 | 0.6 | 0.3 | 85.867 | 59．93．3 | 59.617 | 59267 | 59267 | 65 267 |
|  |  | 0.1 | 07 | 02 | 71567 | 64533 | 64217 | 63867 | 63867 | 71567 |
|  |  | 01 | 0 B | 01 | 77267 | 69133 | 68817 | 5B467 | 68467 | 77.267 |
|  |  | 02 | 01 | 07 | 41033 | 41.267 | 40．633 | 39933 | 39 勺33 | 41.033 |
|  |  | 0.2 | 0.2 | 0.6 | 46.733 | 45867 | 45233 | 44533 | 44.533 | 46733 |
|  |  | 0.2 | 0.3 | 0.5 | 52.433 | 50467 | 49833 | 49133 | 49133 | 52433 |
|  |  | 02 | 04 | 04 | 59.133 | 55.067 | 54．433 | 53.733 | 53733 | 58133 |
|  |  | 0.2 | 05 | 0.3 | 63.833 | 59667 | 59033 | 58333 | 58333 | 63.833 |
|  |  | 02 | 0.6 | 0.2 | 䄪 533 | 64.267 | 63633 | 62.933 | 62.933 | 69.533 |
|  |  | 02 | 0.7 | 0.1 | 75233 | 68.867 | 68.233 | 67533 | 67533 | 75.233 |
|  |  | 0.3 | 0.1 | 06 | 44，700 | 45600 | 44.650 | 43600 | 43600 | 44.700 |
|  |  | 03 | 02 | 0.5 | 50400 | 50.200 | 49250 | 48200 | 48.200 | 50400 |
|  |  | 0.3 | 03 | 04 | 5 5 .100 | 54.800 | 53.850 | 52.600 | 52.800 | 56.100 |
|  |  | 03 | 0.4 | 03 | 61.800 | 59.400 | 58.450 | 57.400 | 57.400 | 61.800 |
|  |  | ¢ 3 | 05 | 02 | 67500 | 64000 | 63050 | 62000 | 62.000 | 67.500 |
|  |  | 0.3 | 0.6 | 0.1 | 73.200 | ¢8．60¢ | 67．650 | 66.600 | 66．600 | 73.200 |
|  |  | 04 | 0.1 | 05 | 48367 | 49933 | 48667 | 47267 | 47.267 | 48367 |
|  |  | 04 | 02 | 04 | 54067 | 54533 | 53267 | 51867 | 51.867 | 54067 |
|  |  | 0.4 | 03 | 0.3 | 59.767 | 59.133 | 57.867 | 56.467 | 55467 | 59．767 |
|  |  | 04 | 04 | 02 | 65467 | 63733 | 62467 | 61067 | 61.067 | 65467 |
|  |  | 04 | 05 | 01 | 71167 | 68333 | 67067 | 65667 | 65667 | 79167 |
|  |  | 05 | 0.1 | 04 | 52033 | 54.267 | 52683 | 50.933 | 50933 | 52.033 |
|  |  | 05 | 02 | 03 | 57733 | 58867 | 57．283 | 55533 | 55533 | 57.733 |
|  |  | 0.5 | 0.3 | 0.2 | 63433 | 53487 | 51.883 | 60133 | 60133 | 砛433 |
|  |  | 05 | 04 | 01 | 69.133 | 68.067 | 66.483 | 64733 | 64733 | 69133 |
|  |  | 06 | 01 | 03 | 55.700 | 58.600 | 56.700 | 54600 | 54600 | 55700 |
|  |  | 06 | 02 | 02 | 61.400 | 63200 | 61.300 | 59.200 | 59.200 | 61.400 |
|  |  | 06 | 03 | 01 | 67.100 | 67800 | 65900 | 63800 | 63800 | 57.100 |
|  |  | 07 | 01 | D 2 | 59.367 | 62933 | 6 E 717 | 58267 | 58267 | 59367 |
|  |  | 0.7 | 0.2 | 0.1 | 65.067 | 67.533 | 65.317 | 62967 | 62.867 | 65.067 |
|  |  | 0.8 | 0.1 | 0.1 | 63.033 | 67267 | 64.733 | 61.933 | 61.933 | 63033 |
| SUM |  |  |  |  | 213200 | 2080 00 | 204200 | 2400.00 | 200000 | 213200 |


| T | M | W1 | W2 | W3 | SPTJEDD | EDOISPT | S［1］ | S［2］ | S［3］ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16 | 6 | 0.1 | 0.1 | 08 | 38.125 | 37.925 | 37592 | 37225 | 37225 | 38.125 |
|  |  | 0.1 | 02 | 0.7 | 44.325 | 43.225 | 42.892 | 42．525 | 42，525 | 44325 |
|  |  | 01 | 03 | 06 | 50525 | 48525 | 48192 | 47825 | 17825 | 50.525 |
|  |  | 01 | 0.4 | 05 | 56725 | 53825 | 53.492 | 53125 | 53125 | 56725 |
|  |  | 0.1 | 0.5 | 0.4 | 62925 | 59.125 | 58.792 | 58425 | 58.425 | 62.925 |
|  |  | 0.1 | 06 | 0.3 | 69.125 | 64.425 | 64.092 | 63725 | 63725 | 69125 |
|  |  | 01 | 07 | 02 | 75.325 | 69.725 | 69392 | 69625 | 69 D25 | 75325 |
|  |  | D 1 | 08 | D 1 | 81.525 | 75025 | 74692 | 74.325 | 74325 | 81525 |
|  |  | ß 2 | 01 | 07 | 42050 | 42550 | 41883 | 41.150 | 41.150 | 42.050 |
|  |  | 02 | 02 | 06 | 48250 | 47， 650 | 47，183 | 46.450 | 46.450 | 48.250 |
|  |  | 62 | 03 | 45 | 54450 | 53150 | 52483 | 51.750 | 51，750 | 54，450 |
|  |  | 02 | 04 | 04 | 66.650 | 58.450 | 57783 | 57050 | 57.050 | 60650 |
|  |  | 02 | 05 | 03 | 66 B50 | 63750 | 63083 | 62350 | 62.350 | 66 B50 |
|  |  | 0.2 | 0.6 | 02 | 73.050 | 69.050 | 68383 | 67650 | 67.650 | 73050 |
|  |  | 02 | 07 | 01 | 79，250 | 74.350 | 73.683 | 72，950 | 72．950 | 79250 |
|  |  | 0.3 | 0.1 | 0.6 | 45975 | 47175 | 46175 | 45075 | 45075 | 45975 |
|  |  | 03 | 02 | 05 | 52175 | 52475 | 51475 | 50.375 | 50375 | 52.175 |
|  |  | 03 | 03 | 04 | 56.375 | 57.775 | 56775 | 55.675 | 55.675 | 58375 |
|  |  | 03 | D 4 | 03 | 64.575 | 63.075 | 62.075 | 60975 | 60975 | 64.575 |
|  |  | 03 | 05 | 02 | 70775 | 68.375 | 67375 | 66275 | 66275 | 70775 |
|  |  | 0.3 | 0.6 | 0.1 | 76975 | 73675 | 72.675 | 71.575 | 71.575 | 76975 |
|  |  | 0.4 | 0.1 | 0.5 | 49500 | 51.800 | 50467 | 49000 | 49000 | 49.900 |
|  |  | 04 | 02 | 04 | 56100 | 57100 | 55767 | 54.390 | 54300 | 56100 |
|  |  | 04 | 03 | 03 | 62300 | 62400 | 61067 | 59.600 | 59600 | 62300 |
|  |  | 04 | O4 | 02 | 68，500 | 67700 | 66.367 | 64.900 | 64．900 | 68500 |
|  |  | 04 | 05 | 0.1 | 74，700 | 73.000 | 71.667 | 70200 | 70200 | 74．700 |
|  |  | 05 | 0.1 | 0． 4 | 53825 | 56425 | 54758 | 52925 | 52.925 | 53825 |
|  |  | 05 | 02 | 03 | 69025 | 61725 | 60.058 | 58225 | 58.225 | 60025 |
|  |  | 05 | 03 | 02 | 66．225 | 67025 | 65.358 | 63.525 | 63525 | $6{ }_{6} 225$ |
|  |  | 05 | 04 | 01 | 72425 | 72325 | 70658 | 68825 | 68825 | 72.425 |
|  |  | 06 | 0.1 | 0.3 | 57.750 | 61．050 | 59.050 | 56850 | 56.850 | 57.750 |
|  |  | 0.6 | 0.2 | 02 | 63950 | 66350 | 64.350 | 62150 | 62150 | 63950 |
|  |  | 06 | 03 | 01 | 70150 | 71.650 | 69650 | 67450 | 67450 | 70.150 |
|  |  | 0.7 | 0.1 | 0.2 | 51.675 | 65 675 | 63342 | 60775 | 60.775 | 61675 |
|  |  | 0.7 | 0.2 | 0.1 | 67.875 | 70.975 | 68642 | 65.075 | 66.075 | 67.875 |
|  |  | 08 | 0.1 | 0.1 | 65.640 | 70.300 | 67633 | 64700 | 64，700 | 65600 |
| SUM |  |  |  |  | 222300 | 21990 | 215900 | 2115．00 | 211500 | 2223 O6 |


| T | M | WH1 | W2 | W3 | SPTJEDD | EDD／SPT | S［1］ | S［2］ | S［3］ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16 | 7 | 01 | 01 | 0.8 | 38883 | 38.917 | 38567 | 38.183 | 39.183 | 38883 |
|  |  | 01 | 02 | 07 | 45583 | 44917 | 44567 | 44.183 | 44.183 | 45583 |
|  |  | 0.1 | 0.3 | 0 O | 52.283 | 50917 | 50567 | 50.183 | 50183 | 52283 |
|  |  | 01 | 04 | 05 | 58983 | 56.917 | 56.567 | 56.183 | 56183 | 58.983 |
|  |  | 01 | 05 | 0.4 | 65．1393 | 62917 | 62567 | 62.183 | Б2．183 | 65683 |
|  |  | 01 | 0.6 | 0.3 | 72383 | 68917 | 68567 | 68183 | 63183 | 72383 |
|  |  | 0.1 | 0.7 | 02 | 79083 | 74917 | 74．567 | 74183 | 74183 | 79083 |
|  |  | 0.1 | 0.8 | 0.1 | 85.783 | 86917 | 80567 | 80.183 | 80183 | 85783 |
|  |  | 02 | 01 | 0.7 | 43.067 | 43833 | 43133 | 42367 | 42.367 | 43067 |
|  |  | 02 | 02 | 06 | 49.767 | 49.833 | 49133 | 48367 | 48.367 | 49.767 |
|  |  | 0.2 | 03 | 05 | 56467 | 55 B33 | 55.133 | 54.367 | 54.367 | 56467 |
|  |  | 02 | 04 | 0.4 | 6.3167 | 61833 | 61133 | 60367 | 60367 | 63.167 |
|  |  | 02 | 05 | 03 | 69.667 | 67.833 | 67.133 | 66367 | 66367 | 69.867 |
|  |  | 02 | 06 | 0.2 | 76567 | 73.833 | 73.133 | 72367 | 72367 | 76.567 |
|  |  | 0.2 | 07 | 01 | 83267 | 79.933 | 79.133 | 78367 | 78367 | B3．267 |
|  |  | 0.3 | 0.1 | 06 | 47.250 | 48.750 | 47，700 | 46550 | 46550 | 47.250 |
|  |  | 0.3 | 02 | 05 | 53.950 | 54，750 | 53.700 | 52550 | 52550 | 53.950 |
|  |  | 0.3 | 0.3 | 04 | 60650 | 60.750 | 59.700 | 58550 | 58550 | 60650 |
|  |  | 0.3 | 0.4 | 0.3 | 67.350 | 66750 | 65.700 | \＄64．550 | 64，550 | 67350 |
|  |  | 0.3 | 0.5 | 0.2 | 74.050 | 72.750 | 71.700 | 70550 | 70.550 | 74050 |
|  |  | 0.3 | 06 | 0.1 | 80.750 | 78.750 | 77.700 | 76550 | 76550 | 80750 |
|  |  | 04 | 01 | 0.5 | 51.433 | 53667 | 52267 | 50.733 | 50733 | 51.433 |
|  |  | 04 | 0.2 | 0.4 | 58133 | 59667 | 58267 | 56733 | 56733 | 58133 |
|  |  | 0.4 | 0.3 | 0.3 | 64833 | 65667 | 64267 | 62733 | E2733 | 64，833 |
|  |  | 0.4 | 0.4 | 0.2 | 71533 | 71667 | 76267 | 68733 | 68733 | 71.53 .3 |
|  |  | 0.4 | 0.5 | 0.1 | 78.233 | 77．667 | 76267 | 74.733 | 74733 | 78.233 |
|  |  | 05 | 0.1 | 0.4 | 55.617 | 58.583 | 56833 | 54917 | 54917 | 55617 |
|  |  | 05 | 02 | 03 | 62.317 | 64.583 | 62.833 | 60.917 | 60.917 | 62317 |
|  |  | 05 | 03 | 02 | 89017 | 70.583 | 68.833 | 66.917 | 66917 | 69017 |
|  |  | 05 | 04 | 01 | 75717 | 76.583 | 74.833 | 72.917 | 72.917 | 75717 |
|  |  | 06 | 01 | 03 | 59 BDO | 63500 | 61400 | 59.100 | 59.100 | 59800 |
|  |  | 06 | 02 | 02 | 66500 | 69500 | 67400 | 65.100 | 65100 | 66500 |
|  |  | 06 | 03 | 01 | 73200 | 75.500 | 73.400 | 71.100 | 71.100 | 73200 |
|  |  | 07 | 01 | 02 | 的 983 | 官客，417 | 65967 | 63283 | 63283 | 63983 |
|  |  | 07 | 02 | 01 | 70683 | 74417 | 71.967 | 69283 | 69283 | 70.683 |
|  |  | 08 | 0.1 | 0.1 | 68167 | 73.333 | 70.533 | 67.457 | 67，4．77 | 68167 |
|  |  | SUM |  |  | 2314．00 | 231800 | 227600 | 2230．00 | 223000 | 231400 |


| T | m | W1 | W2 | W3 | SPTIEDD | EDDISPT | S［1］ | S［2］ | $5[3]$ | 5［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16 | d | 01 | 01 | 08 | 39642 | 39.908 | 39542 | 39142 | 39142 | 39642 |
|  |  | 0.1 | 0.2 | 0.7 | 46682 | 46608 | 46242 | 45842 | 45842 | 46842 |
|  |  | 01 | 03 | 0.6 | 54.042 | 53.309 | 52.942 | 52.542 | 52542 | 54042 |
|  |  | 01 | 04 | 05 | 61242 | 60808 | 59642 | 59.242 | 59242 | 61.242 |
|  |  | 0.1 | 05 | 04 | 68442 | 66708 | 66342 | 65.942 | 65942 | 68.442 |
|  |  | 01 | 06 | 03 | 75.642 | 73.409 | 73.042 | 72542 | 72.642 | 75642 |
|  |  | 0.1 | 0.7 | 02 | 82342 | 80.108 | 79742 | 79342 | 79.342 | $82 \mathrm{BA2}$ |
|  |  | 01 | 08 | 01 | 90042 | 86208 | 86442 | 86042 | 86042 | $90 \times 42$ |
|  |  | 0.2 | 0.1 | 0.7 | 44．083 | 45.117 | 44.383 | 43583 | 43593 | 44083 |
|  |  | 02 | 02 | 06 | 51283 | 51817 | 51083 | 50283 | 50283 | 51.283 |
|  |  | 0.2 | 0.3 | 05 | 58483 | 58517 | 57.783 | 56.983 | 56.983 | 58483 |
|  |  | 0.2 | 04 | 0.4 | \＄5．683 | ¢5 217 | 64483 | 63683 | 63683 | 65.683 |
|  |  | 02 | 0.5 | 0.3 | 72883 | 71917 | 71.183 | 70383 | 70383 | 72.883 |
|  |  | 0.2 | 0.6 | 0.2 | 80083 | 78617 | 77．8B3 | 77083 | 77083 | 80.083 |
|  |  | 02 | 0.7 | 0.1 | 87.283 | 85317 | 84.583 | 83.783 | 83.783 | 87.283 |
|  |  | 0.3 | 01 | 06 | 48525 | 50325 | 49225 | 48.025 | 48.025 | 48.525 |
|  |  | D3 | 02 | 05 | 55.725 | 57.025 | 55.925 | 54725 | 54.725 | 55.725 |
|  |  | 03 | 03 | 04 | 62.925 | 63.725 | 62625 | 61425 | 61425 | 62925 |
|  |  | 03 | 04 | D 3 | 70.125 | 70.425 | 69.325 | 68125 | 68.125 | 7 D 125 |
|  |  | 0.3 | 0.5 | 0.2 | 77.325 | 77.125 | 76025 | 74825 | 74825 | 77325 |
|  |  | 0.3 | 0.6 | 0.1 | 84525 | 83825 | 82725 | 81525 | 81525 | 84525 |
|  |  | 0.4 | 0.1 | 0.5 | 52967 | 55533 | 54067 | 52467 | 52467 | 52967 |
|  |  | 0.4 | 0.2 | 04 | 60.167 | 62233 | 60767 | 59.167 | 59167 | 68167 |
|  |  | 04 | 03 | 03 | 67367 | 68 933 | 67467 | 65867 | 65.867 | 67．367 |
|  |  | 04 | 04 | 02 | 74567 | 75633 | 74．167 | 72.567 | 72.567 | 74667 |
|  |  | 04 | 05 | 0.1 | 81.767 | 82.33 | 80867 | 79.267 | 79267 | 81767 |
|  |  | 05 | 0.1 | 94 | 57408 | 60742 | 58.908 | 56908 | 56.908 | 57．409 |
|  |  | 05 | 02 | 0.3 | 64，609 | 57.442 | 65609 | 63608 | 63608 | 64，608 |
|  |  | 05 | 03 | 02 | 71808 | 74142 | 72308 | 70.308 | 70308 | 71808 |
|  |  | 05 | 04 | 01 | 79008 | 80842 | 79009 | 77.008 | 77.008 | 79.008 |
|  |  | 06 | 01 | 03 | 61850 | 65.950 | 63.750 | 61，350 | 61.350 | \＄1．850 |
|  |  | 06 | 02 | 02 | 69.050 | 72.650 | 70.450 | 68.050 | 68050 | 69050 |
|  |  | 06 | 03 | 01 | 76250 | 79.350 | 77.150 | 74．750 | 74．750 | 76250 |
|  |  | 07 | 01 | 02 | 66292 | 71158 | 68.592 | 65.732 | 65.792 | 66.292 |
|  |  | 0.7 | 02 | 01 | 73492 | 77858 | 75292 | 72.492 | 72482 | 73492 |
|  |  | 0.8 | 0.1 | 0.1 | 70.733 | 76367 | 73433 | 70233 | 70233 | 70733 |
| SUM |  |  |  |  | 240500 | 2437.00 | 2393.00 | 2345.00 | 234500 | 2405．00 |


| $006 \mathrm{CL1}$ | 006612 | 00＇E191 | 008691 | 00 Eazz | 006521 | WกS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 49049 | 006－99 | E¢9 25 | 00¢ 的 | 000＇レL | 290＇ 29 | レ0 | 10 | 日 0 |  |  |
| 80815 | 92L99 | Z62 29 | 0GL 95 | Gく912 | 808 29 | 10 | 20 | $\angle 0$ |  |  |
| 为諙 29 | 92179 | 26159 | 099＇09 | S10＇29 | 80日＇ZS | 20 | 10 | $\angle 0$ |  |  |
| 力SS＇89 | 09189 | 09699 | 002 89 | OSE ZL | 09989 | 10 | E0 | 90 |  |  |
| 0¢5¢¢ | 09\％＇¢9 | 098＇79 | 001＇ts | 0Gじく9 | OGG＇£9 | Z0 | 20 | 90 |  |  |
| OSS 时 | 啲的 | 092． $\mathrm{V}_{6}$ | 00009 | O¢1 E9 | QSS＇9\％ | $\varepsilon 0$ | 60 | 90 |  |  |
| Z6Z 69 | çs 69 | 809－99 | 05919 | GZ0＇EL | て6Z＇6S | 10 | ¢ 6 | 50 |  |  |
| C62 $\mathrm{p}_{5}$ | S26 +9 | $805{ }^{\circ} \mathrm{ZS}$ | O5S ES | Sてt－89 | こ6でじら | 乙0 | 80 | 50 |  |  |
| こ6こ6\％ | 92e＇09 | 8068 | OSt 6b | ¢Z8 ¢9 | て6で67 | \＆ 0 | 20 | 50 |  |  |
| て心Z＇ロ | 92l＇G9 | 90E bt | OGSGV | GZZ 69 | てもで切 | $\pm 0$ | 10 | 90 |  |  |
| E¢O O9 | 00602 | 192 99 | 00125 | 004 EL | EEOOG | 10 | 50 | $\nabla^{\circ} 0$ |  |  |
| ECO Sc | 008 99 | 291． ZS | 400＇ES | 00169 | EEO＇SG | 20 | $\dagger 0$ | 50 |  |  |
| EcO 05 | 00219 | ［90］ 8 | 00685 | 00559 | ¢c0 09 | 80 | 80 | $\pm 0$ |  |  |
| Ecd GV | 加ト＇29 | 196＇8b | 008 tb | 00669 | Eco ct | $\pm 0$ | 20 | 50 |  |  |
| ECOOb | 00525 | 49868 | 0020\％ | 00E SS | CEOOt | 50 | 10 | $\bigcirc 0$ |  |  |
| GL2＇09 | 它くでもく |  | OSc＇ss | GLE＇VI | SLL＇09 | L＇0 | 90 | E＇¢ |  |  |
| SLLSS | 51919 | SZB LS | 0St 79 | SL269 | GLL SS | 20 | 50 | EO |  |  |
| SLLOS | 910 c9 | ¢くたぐ | 6SE 8t | 92L 59 | 9LL OG | $\varepsilon 0$ | 10 | E0 |  |  |
| 9LL 9t | ¢Lt＇89 | ¢つ¢＇¢ | 0Sて＇0\％ | SLG＇09 | 922＇别 | 00 | E＇0 | $\varepsilon \cdot 0$ |  |  |
| SLEOt | GL8＇EG | GZ9＇6§ | OGl＇Ot | GL6＇GG | GLIOD | G＇0 | Z＇0 | $\varepsilon$ |  |  |
| 91L＇GE | GLZ 60 | GZt GE | 090＇98 | GLE＇LG | GLI＇GE | $9{ }^{\prime} 0$ | L＇0 | 80 |  |  |
| L＇s＇ts | 09962 | E8S＇G5 | 000＇95 | 090＇SL | L49＇19 | 10 | 10 | 2＇0 |  |  |
| LLG＇99 | 09069 | CEt＇LS | 006＇15 | OSt＇0L | L19＇99 | 20 | 90 | 2＇0 |  |  |
| LIS LS | OSt 79 | ERE $2 t$ | 008.5 | 0＇s＇99 | LIS LS | £＇0 | 90 | 20 |  |  |
| LIS 9t | 09865 | を日こ を\％ | DOL E $\%$ | OSC 19 | 2159 | $\dagger 0$ | ¢0 | 20 |  |  |
| LIS 16 | OSZ SS | と¢1－6E | 00968 | 35995 | く！9しゃ | 90 | E0 | 20 |  |  |
| LLS 9E | OS9 0 | E80 ¢ | 0095 C | O50 2S | く1宁9 | 90 | 2＇0 | 20 |  |  |
| 21玺しを | 09090 | を86＇0 | 00\％＇LE | $0 \cdot 6{ }^{\circ} \mathrm{L}$ | LLE＇LE | 10 | 10 | 20 |  |  |
| 852 29 | SZO St | てtz Ss | 05tsc | GELGL | ダでて9 | 10 | 80 | 10 |  |  |
| 的で29 |  | でじしら | OSE＇19 | Gそし＇12 |  | 20 | 20 | 10 |  |  |
| 8sでひs | S28 S9 | 2tolt | OSで 27 | gz5 99 | 9¢でてg | 50 | 90 | 10 |  |  |
| 8Gで2t | GZZ L9 | こち6で | 05じを | SC6I9 | 852 $\downarrow$ | 50 | 50 | 60 |  |  |
| 8らでで | 92995 | 26988 | 05円6E | SZE＇LS | 8Sて てt | 50 | $\checkmark 0$ | 10 |  |  |
| 85でLE | S20 75 | CtL pE | 096 $\downarrow$ ¢ | 92L 29 | 㚈て 5 | 90 | E0 | 10 |  |  |
| 89己 てE | Sてt 2 V | で9＇0s | OS8 OE | gで＇8\％ | ¢¢も゙で | 20 | 20 | 10 |  |  |
| 8Sでして | G78 25 | でF＇9\％ | OGL9Z | ¢ZS＇¢ | 89でして | 80 | 10 | 1.0 | $g$ | L1 |
| ［t］${ }^{\text {c }}$ | ［E］S | ［ $]$ S | ［l］S | LdSrang | －9케d | EM | 2 M | 1 M | W | 1 |


| 00 9891 | $00 \downarrow 802$ | 00\％ELS | 002651 | D0 0912 | 001889 | WกS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 298 bc | £¢9 29 | L9L S5 | 29295 | 29619 | C98 | ＋＇0 | 1.0 | $8 \cdot 0$ |  |  |
| ¢¢t ¢ $¢$ | 299 ¢9 | 8Stbs | BGS S5 | ECZ 89 |  | 10 | 20 | 10 |  |  |
| EE¢＇0s | 299＇69 | 95609 | 8G¢ 29 | EEctry | EEAOS | 20 | 10 | co |  |  |
| 00095 | 009＇rs |  | OSE＇bs | ODS 99 | 00095 | 10 | ¢0 | 90 |  |  |
| OOP＇LS | 00909 | $0 ¢ \mathrm{COg}$ | OGb＇LG | 009189 | 000 Is | 20 | 20 | 90 |  |  |
| 008＇90 | 004．99 | $0 ¢ 196$ | $0 G 62 \mathrm{~F}$ | 00209 | 008：96 | 80 | 10 | 90 |  |  |
| 296＇99 | cet ¢9 | z60 \＆s | 2bots | 19289 | 19599 | 10 | 50 | 50 |  |  |
| 196 | عES 15 | 2－56 6 | でStos | 296＊ | 496＇${ }^{\circ}$ | 20 | E0 | g＇0 |  |  |
| 29\％\％ | E¢9＇LS | てが9力 | 2 O 2 L | 10609 | 198\％ $2 ⿰$ | C0 | 20 | 50 |  |  |
| 192\％ | E¢L ¢G | 2DS てt |  | 19025 | L9L 2 L | －0 | 10 | 90 |  |  |
| とEL－29 | 29899 | Ece 29 | ¢¢5¢g | 880 69 | ¢81＇29 | $1 ' 0$ | g＇0 | ${ }^{+} \mathbf{0}$ |  |  |
| Eç\％ | L9t 79 | を¢9 \％ | ¢ ¢9 6t | Ect＇g9 | を¢c＇zs | て＇0 | $\bigcirc$ | ＋0 |  |  |
| EE6 2 t | 19585 | EE¢ 5 | をとし 9t | Eezirs | ¢ ¢ 6.2 |  | \＆＇0 | to |  |  |
| をโE \＆t | 29985 | と¢8け | E¢9 てt | £ ¢ $\angle 5$ | ¢ ¢ ¢ ¢ | $\checkmark$ | 20 | to |  |  |
| £ 21.85 | 29409 | ECE 㫙 | \＆EL 6E | EEt ES |  | G＇0 | L＇0 | to |  |  |
| 002 29 | O0E：29 | ¢Z9＇Ls | 922＇てg | OOE 69 | 00125 | 10 | 90 | ¢0 |  |  |
| 001 §S | 005 ¢9 | SZI 日b |  | 00\％＇59 | 001＇¢ | でO | 90 | 80 |  |  |
| 0098 | 00569 | geg to | czz cb | 00919 | 005 时 | c＇0 | $\pm 0$ | $\varepsilon 0$ |  |  |
| 006 Et | 00959 | 9でした | çitb | 00929 | 006 Et | $\checkmark 6$ | E0 | $\varepsilon 0$ |  |  |
| 00E 68 | 002\％ 19 | 9zg＇28 | szて＇e¢ | 002 EG | DOE 68 | 50 | 20 | $\varepsilon 0$ |  |  |
| 002 28 | 008 $2 ⿰$ | GZt「く | gziobe | 008＇66 | OOL $\angle 8 \mathrm{E}$ | 90 | 10 | $\varepsilon 0$ |  |  |
| 298 89 | cez 89 | 2L巨＇OS | LECLG | 29969 | L92 09 | 10 | 40 | z＇o |  |  |
| 499＇Es |  | いがっ | 21821 | 29959 | 49989 | 20 | 90 | z＇0 |  |  |
| 290＇6\％ | £ebog | 2168 | LLEtb | 192 19 | 190＇60 | $\varepsilon \cdot 0$ | G 0 | 20 |  |  |
| L90 7 b | EES 95 | 2V0\％ | 21800 | 298.19 |  | $\pm 0$ | $\pm 0$ | 20 |  |  |
| 19368 | عE9 て | 46698 | LLELE | 496¢S | 19868 | 50 | \％ 0 | 20 |  |  |
| 29\％ 98 | と $¢ 1.8$ | 2LDE | LLBEE | 1900 | L9Z9¢ | 90 | z＇0 | 20 |  |  |
| 29908 | E¢a＇by | 216.62 | くど0 | 2915 | 29908 | 20 | 10 | 20 |  |  |
| ¢ ¢ \％ 9 | 491．69 | 20Z DG | $80 \% 05$ | cee 6 | ces 89 | 1.0 | 80 | 10 |  |  |
| とยで的 | 492＇99 | 8029 | 80697 | EE6 59 | ¢¢で力の | 20 | 20 | 1.0 |  |  |
| ¢ ¢ 96 | 298＇19 | 802 Et | 80ヶ ¢ ¢ | ¢80＇29 | を¢9＇6 ${ }^{\text {b }}$ | E 0 | 90 | 10 |  |  |
| ¢EO ¢ $\downarrow$ | 190＇29 | 602＇6 | 80668 | Eとし 89 | ¢EO＇50 | $\nabla^{\prime} 0$ | 90 | 10 |  |  |
| \＆Eb 0 | 29685 | 90298 | 80\％＇98 | ¢¢で $\downarrow$ ¢ | £EtD | 50 | $\pm 0$ | 1.0 |  |  |
| ¢c8＇ce | 1996 | BOL 28 | $2062 \%$ | Ec\＆ 09 | Ecg c $\varepsilon$ | 9 D | E O | 10 |  |  |
| E¢EIE | 29\％＇st | 80268 | 80 tc 6 |  | をくて＇しદ | 10 | 20 | 10 |  |  |
| £¢9 9z | 198＇L6 | 80192 | 805 cz | £と¢ CH | عcs＇9z | a＇0 | 10 | 10 | $\dagger$ | 21 |
| ［t］s | ［15 | ［2］ 5 | ［1］S | IdSraug | －ablds | EM | 2 M | LM | H | 1 |


| 00＇6061 | 006208 | 098L8 | 00006 | 00＇LてS\％ | 00＇6061 | WITS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 296－19 | ES60L | 49929 | 29859 | 49012 | 296＇s9 | 1.0 | 10 | 80 |  |  |
| 8G9゙で | 261＇¢L | 656＇29 | ¢\＆G＇tg | 9¢S＇8L | Q¢¢＇Z9 | 10 | 20 | 40 |  |  |
| 89L 99 | て61＇49 | 6G9＇， 9 | をくて＇69 | 8SG2Z | 251．95 | z＇0 | 10 | $\angle 0$ |  |  |
| 099＇89 | OSb＇92 | 098.69 | $002 巾 9$ | OSO 08 | 0¢9 ¢ | 10 | E0 | 90 |  |  |
| 0S日＇L9 | 05ヶ69 | DSO 日S | 0076 6 | 050 pt | OSB L5 | ＜0 | 70 | 90 |  |  |
| OSO ZS | 05\％ 89 | 95t 65 | 加卜＇p | 09089 | 090＇ちs | E＇0 | 10 | 90 |  |  |
| Z $7 \pm 69$ | 80¢゙LL | Cv 29 | 498 \％ | てヤS 1日 | ごく | 10 | $\pm 0$ | 90 |  |  |
| 276日G | 802L | Zヤt＇8G | L99 69 | ZヤG GL | で685 | 20 | ¢0 | 50 |  |  |
| で1旳 | 80159 | てカレ ¢¢ | L9Z VG | で599 | でも゙をG | 80 | 20 | 50 |  |  |
| でら， | 60169 | Zレー＇tb | 19685 | 20ccs | こbc゙2b | $\dagger 0$ | 10 | G00 |  |  |
| EES G9 | 2966 2 | Eとし 79 | EEOS9 | EEOES | EEB＇ç | 60 | 50 | $\pm 0$ |  |  |
| EEO 09 | 196 Et | £E\％ 95 | EELGS | EEOLL | EEOOF | で0 | $\bigcirc 0$ | $t 0$ |  |  |
| EEZ 6 S | 29649 | EES ES | EEy゚゙g | CEO 14 | EEC ts | E0 | \％ | $\rightarrow 0$ |  |  |
| Eto av | 296．19 | £とで别 | を¢し＇6\％ | EEOGg | を¢\％ 8 p | $\bigcirc 0$ | 20 | $\bigcirc 0$ |  |  |
| Eヒロ゙で | 49695 | ES6 $\downarrow$ | E¢B Et | Cco fis | EE9 こt | 50 | 10 | $\bigcirc 0$ |  |  |
| 926＇99 | GZZ＇2G | GZG＇P | OOZ＇99 | ¢2G＇ti | 926＇99 | 1 ＇0 | 90 | E＇0 |  |  |
| Gくし19 | SZZ 92 | sZ2 69 | 00665 | 575 82 | SZ1． 19 | 20 | 50 | 50 |  |  |
| GZE SG | 9ZZ OL | 526 E5 | 009 \％ 9 | 975 2L | 乌で柠 | 50 | $\bigcirc 0$ | E0 |  |  |
| STS 6t | Sてでし9 | 5298 | 00E 6\％ | 97599 | 975 6t | $\bigcirc 0$ | \％ 0 | E0 |  |  |
| SZ」ど | 9くでgs | SてE Ep | 000 to | 929 0 |  | 50 | と0 | E0 |  |  |
| 526 28 | SZZ゙てS | S20 \％ | 002 88 | 979 狺 | 926 $2 \boldsymbol{1}$ | 90 | 10 | E0 |  |  |
| 21089 | を昞加 | 266 59 | 19859 | 21098 | ＜1689 | 10 | 10 | 20 |  |  |
| く1でて | C日t 21 | LL9 6G | 29009 | 21008 | L12 29 | Z0 | 90 | 己0 |  |  |
| 41799 | C日Vで | LLEVG | L91 vg | 410 V | く1t95 | E0 | 50 | Z0 |  |  |
| L19＇0 | CSp 99 | 1106\％ | 29\％6\％ | 21089 | 11905 | 市0 | ¢0 | Z D |  |  |
| 218 \％ | cgto 09 | LUEを | LS +7 | 21079 | L18 $\dagger$ | 50 | $\varepsilon 0$ | 70 |  |  |
| L1068 | E8V PG | th\％ | 19880 | L1099 | LID＇6̂ | 90 | 20 | z＇0 |  |  |
| くしてEE | 580＇8\％ | 〈レ＇を號 | L9G＇$¢$ | 210＇05 | LIZ＇E | 10 | 10 | z＇0 |  |  |
| 80169 | で2 98 | 80 s 9 | ECS S9 | 80526 | B0169 | 10 | 80 | 10 |  |  |
| 80 ¢9 | てもく吅 | 800 | をとこ＇09 | 80¢＇18 | 80 ¢ 89 | 二0 | 10 | 10 |  |  |
| 80515 | で 272 | 80479 | EEGVG | $80{ }^{\circ} \mathrm{F} 2$ | 80家 19 | \％ 0 | 90 | 10 |  |  |
| 00L＇LS | ごぢ89 | COV＇施 | ¢59＇6t | 80969 | $80 L^{\circ} 19$ | $\pm 0$ | 90 | 10 |  |  |
| B0E G\％ | でL＇Z9 | 80レ $\dagger t$ | ともぐヤ | 8¢5\％9 | 9065\％ | 50 | ＋0 | 50 |  |  |
| 96\％${ }^{\circ}$ | でく 9G | 80888 | EED＇6E | $805^{\circ} 5$ | 80じ0t | 90 | $\varepsilon 0$ | 10 |  |  |
| 90¢゙ヤ¢ | ZbL0G | 20G ¢ $¢$ | EELEE | 80515 | 80E＂te | 20 | 20 | 50 |  |  |
| g0G 82 | でったtb | $80 Z \mathrm{BZ}$ | ¢Et 8Z | 80s ct | 80582 | 80 | 100 | 10 | $t$ | L1 |
| tpls | ［E］S | 代姩 | ［i］ | ldsiogl | qugiddS | EM | ZM | LM | 1 N | 1 |


| 00 ¢¢81 | 00ゅİż | 00．8L1 | 006621 | 00 でゆって | 00＇reg3 | WกS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 492＇69 | 191－89 | 00109 | E¢¢ L9 | ¢ $20 \%$ ¢ | 49265 | 10 | 10 | 80 |  |  |
| cisl ${ }^{\text {ct }}$ | C6669 | GZ109 | 2ヶ9＇t9 | 41＇g 2 | £8109 | 10 | z0 | 10 |  |  |
| cg 2 ps | ¢ 89 tg | gzt 9s | 24G＇95 | 218＇69 | E8L＇vg | 20 | 10 | 10 |  |  |
| D01 19 | 008 12 | 05109 | 09\％ 19 | 00で92 | 001.19 | ＋＇0 | $\varepsilon \cdot 0$ | 90 |  |  |
| 00295 | 0099 | Ost $0^{\text {cs }}$ | 0stigs | D06＇0L | DOLSG | 20 | 20 | 90 |  |  |
| 00¢ 05 | 00 C 19 | 05t0s | $050 \mathrm{Z5}$ | 00959 | 00209 | $\varepsilon 0$ | 10 | 90 |  |  |
| $40 \mathrm{Z9}$ | くト9を | 9くt 09 | 6̧z＇19 | SBE＇LL | 210＇79 | 10 | ${ }^{\circ} \mathrm{O}$ | G＇0 |  |  |
| 2t9＇ss | 218＇89 | GLD Gg | 89595 | E86 WL | L1995 | 20 | $\varepsilon 0$ | 90 |  |  |
| ぐてし5 | Ll0 59 | GLLCO9 | 858 | E69 99 | くよでしg | 50 | z＇0 | G＇0 |  |  |
| A1895 | L1245 | 920 gt | 85120 | ¢6E＇L9 | 218 ¢ | $\checkmark 0$ | 10 | 90 |  |  |
| EE6Z9 |  | 00209 | 290＇19 | 29832 | EE689 | 10 | ¢0 | $\pm 0$ |  |  |
| £Ec゙29 | 紤＇0L | $00 ¢ \mathrm{Gq}$ | 29899 | 290\％ 2 | ¢eg＇2c | 20 | $\downarrow 0$ | to |  |  |
| ¢ELZS | Ec8 tg | 00805 | 1990＇19 | 292\％ 29 | とくしてら | 80 | $\varepsilon 0$ | ＋0 |  |  |
| cect 9 | E¢5 6G | 0015 | 19696 | 19629 | ¢EC＇St | \＄0 | 20 | \＄0 |  |  |
| EEE゙ip | Etて | 00ャ゙㖪 | 29Z Ct | 291．29 | EとE゙した | cio | 10 | 50 |  |  |
| 0¢8 ¢9 | DGZ 12 | szZ 09 | SIE 09 |  | OS8＇E9 | ＇0 | 90 | EO |  |  |
| OGV 8 C | GG6 LLI | çs cs | Sil 99 | OSL＇v 2 | OSb＇ss | でO | 90 | \＆＇0 |  |  |
| 090＇Es | 099＇99 | cza＇0s | git is | 09889 | OS¢ ES | CO | $\square 0$ | \＆＇0 |  |  |
| 0592 | O9E＇19 | 9Z1＇9b | GLL 9b | OGS Eg | 099 2 | $\bigcirc 0$ | E 0 | ¢0 |  |  |
| $098 \%$ | 080.95 | GZt しt | GLO Ct | 05z 85 | OSZ で | 90 | 60 | $\varepsilon{ }^{\prime} 0$ |  |  |
| ¢98＇98 | OSLOS | çice | SLE LE | 09625 | 098＇s | 90 | ＇0 | \＆＇0 |  |  |
| 292＇69 | 49062 | DSC 69 | ¢ 8909 | EcS 08 | 292．09 | $1{ }^{1} 0$ | 20 | $2 \cdot 0$ |  |  |
| LSC 69 | 29282 | OS＇Gs | £ $86 . \mathrm{GG}$ | EEL＇GL | 49869 | 20 | 90 | Z0 |  |  |
| 296＇s5 | 29089 | OS8 0 | ¢82 LS | ع¢6 69 | 496 ¢5 | 80 | 90 | 2＇0 |  |  |
| 2958 | L91－E9 | OSt 9 | Ets＇90 | ¢\％9＇v9 |  | t＇0 | $\pm 0$ | 20 |  |  |
|  | 1980 | OSがゆ | E88 16 | ¢¢E 65 | L91 EV | 90 | 80 | て＇0 |  |  |
| 191．2\％ | L9S 29 | 0519 C | E81LE | EEO 比 | c96\％ | 90 | 20 | zo |  |  |
| L98＇そ¢ | 292 5 | 050ze | ¢8゙っで |  | L9E＇2¢ | L＇0 | 10 | 20 |  |  |
| ع69＇¢9 | 88808 | SLZ 09 | 26t 69 | く69＇Lg | ¢69 99 | 10 | 80 | 10 |  |  |
| C8Z＇09 | ع8s＇ch | GLS Gg | 26499 | LtEg | E8Z 09 | 20 | 40 | 10 |  |  |
| CB8 6 － | 娒 02 | SL8＇09 | 26019 | LL0＇LI | c880ヶ¢ | E0 | 90 | 10 |  |  |
| 88t＇60 | ¢ 26 b |  | 268．9p | 21699 | c8t 66 | 50 | 5 | 10 |  |  |
| EBO＇b | E89＇65 | SLD＇ロ | 26917 | 14009 | を时加 | 90 | \＄0 | 10 |  |  |
| ¢8988 | 88E $\dagger 5$ | S $2 \angle 95$ | 26698 | 1いGg | E89 8E | 90 | ¢0 | 10 |  |  |
| ¢日乙 ¢ | c80 6t | SLO 2 を | て¢Z 2 Cc | LLB6 ${ }^{\text {\％}}$ | ¢ $¢ \mathrm{C}$ ¢ $\varepsilon$ | 10 | とO | 10 |  |  |
| EGB 12 | E8LEb | GLE $\angle Z$ | 26912 | LLG゙ゆt | E8E $\angle Z$ | 80 | 10 | 10 | 9 | 4 |
| ［ t$]$ ］ | ［ $\varepsilon$ ］S | ［2］ | ［1］ | 1dsiode | 003IIdS | EM | LM | LM | W | 1 |


| T | 9 | W9 | W2 | W3 | SPTJEDD | EDDISPT | S[1] | \$[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 17 | 8 | 0.1 | 0.1 | 08 | 29133 | 46500 | 29275 | 29042 | 45700 | 29 133 |
|  |  | 01 | 0.2 | 07 | 35333 | 53200 | 35.175 | 34.942 | 52400 | 35333 |
|  |  | 0.1 | 03 | 06 | 41533 | 59.900 | 41075 | 40842 | 59100 | 41.533 |
|  |  | 0.1 | 04 | 05 | 47733 | 66.600 | 46.975 | 46742 | 65800 | 47.733 |
|  |  | 0.1 | 05 | 04 | 53933 | 73.306 | 52.875 | 52.642 | 72500 | 53.933 |
|  |  | 01 | 06 | 03 | 60.133 | 80.000 | 58.775 | 58542 | 79200 | 60.133 |
|  |  | 01 | 0.7 | 02 | 耴. 333 | 86.706 | E4 675 | 64442 | 85900 | 6 6. 333 |
|  |  | 01 | 0.8 | 0.1 | 72.533 | 93.400 | 70.575 | 70342 | 92600 | 72.533 |
|  |  | 0.2 | 0.1 | 0.7 | 34067 | 51.300 | 34.650 | 34183 | 49700 | 34067 |
|  |  | 0.2 | 02 | 06 | 40267 | 58.0006 | 40550 | 40083 | 58.40' | 40, 267 |
|  |  | 02 | 03 | 0.5 | 46.467 | 64.700 | 46450 | 45983 | 63.100 | 46467 |
|  |  | 02 | 04 | 0.4 | 52.667 | 71.400 | 52.350 | 51883 | 59.800 | 52667 |
|  |  | 0.2 | 05 | 03 | 58.867 | 78.100 | 58250 | 57.783 | 76.500 | 58867 |
|  |  | 0.2 | 06 | 02 | 65067 | B4.806 | 64.150 | 63683 | 83200 | 65.067 |
|  |  | 02 | 07 | 01 | 71.267 | 91.500 | 70050 | 69.583 | 89900 | 71.267 |
|  |  | 0.3 | 01 | D6 | 39000 | 56.100 | 40025 | 39.325 | 53.700 | 39000 |
|  |  | 03 | 02 | 0.5 | 45200 | 62800 | 45.925 | 45.225 | 60400 | 45.200 |
|  |  | 03 | 03 | 04 | 51400 | 69500 | 51.825 | 51.125 | 67100 | 51.400 |
|  |  | 03 | 04 | 0.3 | 57600 | 76200 | 57725 | 57.025 | $73 \mathrm{B00}$ | 57.600 |
|  |  | 03 | 05 | 02 | 63800 | 82900 | 63 625 | 62.925 | 80500 | 63800 |
|  |  | 03 | 06 | B1 | 70000 | 89.600 | 69525 | 68.825 | 87.200 | 70000 |
|  |  | 04 | 01 | W5 | 43.933 | 60900 | 45400 | 44467 | \$7.700 | 43933 |
|  |  | 04 | $\bigcirc 2$ | 04 | 50.133 | 67600 | 51300 | 50367 | 64400 | 50133 |
|  |  | D 4 | 03 | 03 | 56333 | 74300 | 57.200 | 56267 | 71100 | 56333 |
|  |  | 04 | 04 | 0.2 | 62533 | 81000 | 63.100 | 62.167 | 77800 | 62.533 |
|  |  | 04 | 0.5 | 01 | 68733 | 87700 | 69.000 | 68.067 | 84500 | 68.733 |
|  |  | 05 | 01 | 0.4 | 48867 | 65700 | 50.775 | 49608 | 61700 | 48867 |
|  |  | 05 | 02 | 0.3 | 55067 | 72400 | 56 施5 | 56.508 | 68400 | 55067 |
|  |  | 05 | 03 | 02 | 61.267 | 79100 | 62575 | 61.408 | 75100 | 61267 |
|  |  | 05 | [) 4 | 01 | 67.467 | 85800 | 68.475 | 67.308 | 81.800 | 67467 |
|  |  | 06 | 0.1 | 03 | 53800 | 70.500 | 56150 | 54.750 | 65.700 | 53800 |
|  |  | 0.6 | 02 | 02 | 60000 | 77.200 | 62.550 | 60.650 | 72.400 | 60000 |
|  |  | 0.6 | 03 | 01 | 65200 | 83.900 | 67.950 | 66550 | 79100 | 66.200 |
|  |  | 0.7 | 0.1 | 02 | 58733 | 75300 | 61.525 | 59892 | 69700 | 58.733 |
|  |  | 0.7 | 02 | 0.1 | 64933 | 82000 | 67.425 | 65792 | 76400 | 64933 |
|  |  | 0.8 | 01 | 01 | 63667 | 80100 | 66.900 | 65033 | 73.700 | 63667 |
|  |  | SUM |  |  | 1984.00 | 264000 | 200100 | 1973.00 | 254400 | 1984,00 |


| $T$ | M | W! | W2 | W3 | SPTIED | EDDISPT | S(1) | S[2] | S[3] | $514]$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1{ }^{1}$ | 4 | 01 | 01 | 08 | 32058 | 31.175 | 31158 | 31175 | 31.158 | 32.058 |
|  |  | 01 | 02 | 07 | 36.458 | 34675 | 34658 | 34675 | 34658 | 36458 |
|  |  | 01 | 0.3 | 05 | 40.858 | 38175 | 38158 | 38175 | 38.158 | 40858 |
|  |  | 01 | 04 | 05 | 45258 | 41.675 | 41658 | 41675 | 41656 | 45.258 |
|  |  | 01 | 05 | 04 | 49658 | 45.175 | 45158 | 45175 | 45156 | 49.658 |
|  |  | 01 | 06 | 03 | 54058 | 48675 | 48.658 | 48675 | 48658 | 54058 |
|  |  | 01 | 0.7 | 02 | 58.458 | 52.175 | 52158 | 52175 | 52.158 | 58458 |
|  |  | 0.1 | 0.8 | 0.1 | 62858 | 55.575 | 55.658 | 55675 | 55658 | 62858 |
|  |  | 0.2 | 0.1 | 0.7 | 35717 | 34.850 | 34.817 | 34850 | 34817 | 35717 |
|  |  | 0.2 | 0.2 | 0.6 | 40.117 | 38.350 | 36317 | 38350 | 38317 | 40.117 |
|  |  | 02 | 0.3 | 05 | 44.517 | 41.850 | 41.817 | 41.850 | 41.817 | 44.517 |
|  |  | 02 | 04 | 0.4 | 48.917 | 45.350 | 45.317 | 45350 | 45317 | 48.917 |
|  |  | 02 | 05 | 03 | 53317 | 48950 | 48.817 | 488850 | 48.817 | 53.317 |
|  |  | 02 | 06 | 02 | 57.717 | 52.350 | 52.317 | 52,350 | 52317 | 57717 |
|  |  | 02 | 07 | 01 | 62.117 | 55.850 | 55817 | 55850 | 55817 | 62117 |
|  |  | 03 | 01 | 0.6 | 39.375 | 38.525 | 38.475 | 38525 | 38.475 | 39375 |
|  |  | 0.3 | 0.2 | 05 | 43775 | 42025 | 41.975 | 42.025 | 41975 | 43775 |
|  |  | 03 | 03 | 04 | 48175 | 45525 | 45475 | 45525 | 45475 | 48175 |
|  |  | 0.3 | 04 | 03 | 52575 | 49025 | 48.975 | 49025 | 48975 | 52575 |
|  |  | 03 | 05 | 02 | 56975 | 52.525 | 52475 | 52525 | 52475 | 56.975 |
|  |  | 03 | 06 | 01 | 61375 | 56.025 | 55975 | 56025 | 55975 | 81.375 |
|  |  | 04 | 01 | 05 | 43033 | 42200 | 42.133 | 42200 | 42133 | 43033 |
|  |  | 04 | 02 | 04 | 47433 | 45700 | 45633 | 45700 | 45633 | 47.433 |
|  |  | 0.4 | 03 | 03 | 51833 | 49200 | 49.133 | 49200 | 49133 | 51833 |
|  |  | 0.4 | 0.4 | 02 | 56233 | 52700 | 52.633 | 52.700 | 52633 | 56233 |
|  |  | 0.4 | 05 | 01 | 60633 | 56200 | 56.133 | 56200 | 56133 | 60633 |
|  |  | 0.5 | 0.1 | 04 | 46692 | 45875 | 45.792 | 45.875 | 45792 | 46692 |
|  |  | 0.5 | 02 | 03 | 51092 | 49375 | 49.292 | 49.375 | 49292 | 51092 |
|  |  | 0.5 | 03 | 02 | 55492 | 52.875 | 52792 | 52875 | 52792 | 55.492 |
|  |  | 0.5 | 04 | 01 | 59892 | 56375 | \$6.292 | 56375 | 56292 | 59.892 |
|  |  | 0.6 | 01 | 03 | 50.350 | 49550 | 49450 | 49550 | 49450 | 50.350 |
|  |  | 0.6 | 0.2 | 0.2 | 54750 | 53050 | 52950 | 53.050 | 52950 | 54750 |
|  |  | 0.6 | 0.3 | 01 | 59150 | 56550 | 56.450 | 56550 | 56.450 | 59150 |
|  |  | 07 | 01 | 02 | 54008 | 53.225 | \$3.108 | 53225 | 53.168 | 54.009 |
|  |  | 07 | 02 | 01 | 58.408 | 56725 | 56608 | 56725 | 56508 | 58408 |
|  |  | 08 | 01 | 01 | 57.667 | 56.900 | 56767 | 56900 | 56.767 | 57.667 |
|  |  | SLiM |  |  | 1831 D0 | 1725.00 | 172300 | 172500 | 172300 | 183100 |


| 001861 | 001261 | 00 £ 261 | 00126 | 00EZ61 | 90＇1861 | WHS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19029 | L9519 | 加ぐ1家 | $299^{\circ} \mathrm{L9}$ | W02L9 | 49029 | 10 | 10 | 80 |  |  |
| 851－89 | 89\％ 69 | 912＇Z9 | 8SI 79 | GLZ 79 | 官1＇89 | 10 | 20 | 10 |  |  |
| 8它＇15 | EGt LS | S $15^{\prime \prime} 4$ | 8gt 49 | GLE＇LS | 85629 | 20 | 10 | 10 |  |  |
| 0 cc 109 | 092 zg | OGB 29 | OSL 79 | 058 ＜9 | 0¢で时 | 10 | E 0 | 90 |  |  |
| OFO＇6S | 05085 | 05189 | が施＇日G | OS1 EG | 05065 | 20 | 2 ＇0 | 90 |  |  |
| OS9 ES | OSE ES | $0 \mathrm{O}+6$. | OSE ES | 05t c5 | －99＇EG | $\varepsilon 0$ | 10 | 90 |  |  |
| てVC59 | で「它 | Gで「と | てレC89 | 9で § | ZセE＇G9 | 10 | $\leqslant 0$ | c 0 |  |  |
| でレ＇09 | 2b98G | S2L 旳 | で59＇89 | 92L 89 | でレロ | \％0 | E0 | 50 |  |  |
| ごO゙切 | ごも6¢S | 520 ¢ | ご65S | 9COt ${ }^{\text {c }}$ | こち6 \＄9 | E0 | 20 | S0 |  |  |
| ござ而 | でで6゙ | 92E 67 | でで＇6b | SCE 6t | でん 所 | $\checkmark 0$ | 10 | 50 |  |  |
| とct 99 | EE6「9 | 000＇69 | E¢6 ¢9 | 000 \％ 6 | ¢cた＇99 | 10 | 50 | $\leqslant 0$ |  |  |
| £くて！g | EEZ 65 | 00\％＇65 | ¢¢乙 6G | OOE 65 | セeで！ 9 | 20 | 50 | －0 |  |  |
| ¢c099 | ¢EG゙ロs | 009 \＄5 | を枵けS | 009 ts | EEO 99 | EO | E＇0 | 0 |  |  |
| cc8＇09 | ¢¢867 | OD6 6\％ | をC8＇6\％ | 00667 | EEG OS | $\bigcirc$ | 20 | 10 |  |  |
| ¢ ¢9 ¢ | EEIGも | 002 5\％ | どと 5 | OOZ＇Gb | EE9 St | 50 | 10 | $\theta$ |  |  |
| S29 49 | 97S 69 | Gts b9 | 929 \％ |  | SCS 29 | $1 \cdot 0$ | 90 | E0 |  |  |
| 9て§＇そ9 | cza 69 | ci865 | 92869 | 920＇69 | STE 29 | ¢0 | 50 | $E 0$ |  |  |
| 9ZL＇LS | cZl 55 | 51159 | ¢で＇G9 | S1L cs | GZし 49 | ED | 90 | E0 |  |  |
| SC615 | ¢で09 | 91t0s | GLV OS | S1POS | ¢Z5＇Is | $\bigcirc 0$ | 80 | ¢0 |  |  |
| 92L゙9t | cRL St | 92LGy | 9zL 5\％ | GLL＇St | SZL9t | 50 | 30 | \＆ 0 |  |  |
| S2S し | gて0＇レ | GLO＇し\％ | sZolt | 9201\％ | GZGit | 90 | 10 | $\varepsilon$ |  |  |
| 119＇89 | 1い159 | OSt 99 | く1し「9 | 05159 | 21989 | －6 | 20 | 20 |  |  |
| しん\％c9 | 2t＊ 09 | OGt 09 | くんا 09 | 0¢＊D | 1689 | 20 | 90 | 20 |  |  |
| 41789 | LLEGG | OSLSS | 41259 | OGL＇GG | L1ट85 | E0 | 50 | と0 |  |  |
| 41059 | 1LO＇IS | 0SO LS | 410＇5 | 0GOLG | LLOES | 10 | 0 | 20 |  |  |
| 218 27 | 118゙9\％ | 95c 9r | 4189 | OSE St | 二1色L | 90 | ¢0 | 20 |  |  |
| 119 て | 1．9゙し | 059 しV | く191t | 0596 | く19で | $9{ }^{\prime} 0$ | 20 | 20 |  |  |
| 41ザ 5 ¢ | L169E | ¢G6 9E | L16＇9E | 09698 | こ1ヤLE | S＇0 | 10 | Z0 |  |  |
| 802＇69 | 80259 | çL 99 | 602＇c9 | 921 99 | 80269 | 10 | 80 | 10 |  |  |
| 80979 | 800.19 | 52019 | 800 19 | 920＇19 | 805 \％ | 亿0 | L＇0 | 10 |  |  |
| 60869 | $805^{\text {899 }}$ |  | $80 ¢$ | SZE 95 | 80 ES | E D | 90 | 10 |  |  |
| 801．59 | 80915 | 52919 | 209＇5 | GZ9 LS | 801．99 | 60 | 90 | 10 |  |  |
| \＄066t | 80697 | s26 9b | gos＇9\％ | 926＇9b | 8068 | 90 | 0 | 10 |  |  |
| 802 ct | 80ごで | GZZ Z | 80Z ל $\downarrow$ | 9でで | $8028 t$ | 90 | 50 | 10 |  |  |
| 80988 | 80815 | SZS $2 ¢$ | 80S 2 E | ¢ZG＇t¢ | 80588 | 10 | 60 | 10 |  |  |
| 90E E | \＄08 Z¢ | ço ce | 加宜で， | ¢ても＇てを | 80E \＆ | 80 | 10 | 10 | 9 | 目 |
| 11／5 | ［i］ | ［ $]$ ］ | ［l］S | 上dsjody | 미키d | EM | ZM | $1 / \mathrm{M}$ ． | W | 1 |


| 00＇906！ | 00 Z゙Z81 | が㲸く！ | 00＇z28L | 00 bc 89 | 00＇9061 | Wn\％ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 49865 | 491＇69 | O0E65 | 29169 | 00¢＇69 | 49865 | 10 | 10 | 80 |  |  |
| E8409 | ¢日E＇6G | OES 65 | 88c＇69 | DOG 69 | 88209 | 10 | Z0 | 10 |  |  |
| 886 9 9 | ¢9z＇cs | Weps 5 | を放＇与s | OOt ¢G | 886 55 | zo | 10 | 10 |  |  |
| 00219 | 00969 | 00265 | 00965 | 002＇65 | 00219 | 1.0 | c＇0 | 90 |  |  |
| 00695 | 0059 | 009 gc | 00955 | 009＇59 | 00695 | 20 | 20 | 90 |  |  |
| 0012\％ | 00619 | ORS 15 | 00t＇b | DOS 15 | 00178 | $\varepsilon 0$ | 10 | 90 |  |  |
| 119 29 | 218＇69 | 00669 | 210＇69 | 006＇69 | 41989 | 1.0 | $\checkmark 0$ | 90 |  |  |
| LIa 29 | LLCS9 | 008＇g | L1259 | 008.59 | 118.5 | z0 | $\varepsilon 0$ | g＇0 |  |  |
| L10Eg | 219゙9 | 002＇LS | 21915 | 002 15 | 40 EG | E0 | ＜ 0 | g＇0 |  |  |
| くで时 | 115 $2 ⿰$ | 009＇29 | L1G 27 | 00925 | 4で和 | ヤ0 | 10 | 90 |  |  |
| E\＆S Eg | ع6009 | 00108 | ¢ ¢ 09 | 001＇09 | E¢G E9 | 10 | 90 | to |  |  |
| E $£ 18 \mathrm{BS}$ | Ec6\％s | 00008 | E¢659 | 000＇99 | £ 218 | 20 | ＋0 | to |  |  |
| ¢¢6 ¢5 | ¢c6 2 s | 006 ls | ع¢в | 006＇LG | ع¢6 Є5 | 80 | $8 \cdot 0$ | $\triangleright 0$ |  |  |
| Eとト 施 | ¢¢ $¢ 2 \square$ | 00814 | E¢L＇Lb | 008 Lt | ع¢5＇b＇ | P0 | 20 | $\pm 0$ |  |  |
| を它氻 | とegrt | 00LEV | ¢¢9 ¢ $\downarrow$ | 002 \％ | £とE＇加 | 50 | 10 | $\checkmark 0$ |  |  |
| 0¢tpo | 09で09 | ODE 09 | OSZ 09 | 008.09 | OSt $\mathrm{P9}$ | 10 | 90 | 80 |  |  |
| 05965 | ost＇gs | 002 95 | 09199 | 00295 | 05965 | 20 | G0 | ¢0 |  |  |
| 058 | 09029 | 00175 | 090＇zs | OOL Z¢ | OS8 | $8 \cdot 0$ | $\bigcirc 0$ | E0 |  |  |
| 05005 | OS6 $2 t$ | 0008 | 096＇5b | 000 日b | 0 SO 05 | to | ¢0 | ¢0 |  |  |
| DSZ ¢f | 0988 | 0068 | 0¢8＇¢ | 006 E ¢ | 0cz 5\％ | 9 g | 70 | $\varepsilon \square$ |  |  |
|  | 09268 | 00868 | 05 268 | 00\％＇68 | OSt 0 | 90 | 10 | $\varepsilon 0$ |  |  |
| 29899 | 29509 | 00909 | 29t 09 | 009＇09 | L9E 59 | 10 | 10 | 20 |  |  |
| 299＇09 | 19699 | O0t 99 | L9899 | 00t 95 | 49909 | 20 | 90 | 20 |  |  |
| 2925 5 | 49239 | 00E 75 | 292＇29 | 00E ZS | 4SL＇S | $\varepsilon 0$ | 50 | 20 |  |  |
| $2960{ }^{6}$ | 491＇8t | ORE ${ }^{\text {a }}$ | 291＇8t | 002 Bt | 296＇0． | $\bigcirc 0$ | $\square 0$ | 20 |  |  |
| 29195 | 490 to | 001 切 | $290 \cdot 0$ | 001 $\dagger$ \％ | 4S1．9\％ | 90 | ¢ 0 | 20 |  |  |
| 29E to | 496＇68 | 9000 | L96．6E | 000 0t | L98＇LO | 90 | 20 | 20 |  |  |
| 29998 | 19958 | 00¢ 9 | 29858 | 00695 | 29998 | $\angle 0$ | ＇0 | 20 |  |  |
| \＆8z＇99 | ع9909 | 00609 | ¢89 09 | 00109 | 88299 | 10 | 80 | 10 |  |  |
| catiog | ع日5＇99 | 009＇9s | ¢89 9\％ | 009 9c | ¢8t 19 | $2{ }^{2}$ | 10 | 10 |  |  |
| E89 95 | cob $z ¢$ | OOS 25 | を明で | 005 ZS | ¢89＇9G | ¢ 0 | 90 | 1 ＇0 |  |  |
| 689 | c8c\％${ }^{\text {co }}$ | OOt 8 | をac＇er | 00t 87 | £8a＇Lc | $\checkmark 0$ | 90 | 1.0 |  |  |
| c80 27 | c8Z＇t | OOE 站 | caて＇to | 00e＇v\％ | £80 26 | 50 | To | 10 |  |  |
| c8Z で | 881＇07 | 002 0 \％ | cal $0 t$ | 00200 | cse zb | 90 | $\varepsilon^{\prime} 0$ | 10 |  |  |
| ¢8t $2 ¢$ | ¢ 80.9 E | 00198 | ¢80 9\％ | 001＇98 | と8t 18 | 10 | 20 | 10 |  |  |
| ¢ $89 \mathrm{Z} \mathrm{\varepsilon}$ | ¢65＇ | 000 z | ¢86 18 | 000＇z\％ | 889 2 E | 80 | 1.0 | 10 | 5 | 92 |
| ［t］s | ［8］5 | ［2］s | ［［］ | Lds／ag | GG3IIdS | EM | 2 M | L／M | N | 1 |


| T | M | W1 | W2 | W3 | SPTEEDD | EDDISPT | \$1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 18 | 7 | 0.1 | 0.1 | 0.8 | 33933 | 33.656 | 33633 | 33.650 | 33533 | 33933 |
|  |  | 0.1 | 02 | 0.7 | 39.533 | 38.950 | 38933 | 38.950 | 39.933 | 39533 |
|  |  | 0.1 | 0.3 | 06 | 45133 | 44250 | 44233 | 44250 | 44233 | 45.133 |
|  |  | 0.1 | 0.4 | 0.5 | 50.733 | 49550 | 49533 | 49550 | 49533 | 50.733 |
|  |  | 0.1 | 0.5 | 0.4 | 56.333 | 54.850 | 54633 | 54850 | \$4.833 | 56.333 |
|  |  | 0.1 | 06 | 0.3 | 61.933 | 60.150 | 60.133 | 60150 | 60.133 | 61933 |
|  |  | 0.1 | 0.7 | 0.2 | 67.533 | 65.450 | 65433 | 65450 | E5 433 | 67533 |
|  |  | 0.1 | 0.8 | 0.1 | 73.133 | 70750 | 70733 | 70750 | 70733 | 73.133 |
|  |  | 02 | 0.1 | 0.7 | 38.267 | 38000 | 37.967 | 38000 | 37.967 | 38267 |
|  |  | 02 | 02 | 06 | 43.867 | 433007 | 43267 | 43.300 | 43267 | 43867 |
|  |  | 02 | 03 | 0.5 | 49.467 | 48600 | 4 B 567 | 48600 | 48567 | 49.467 |
|  |  | 0.2 | 04 | 04 | 55.067 | 53900 | 53867 | 53900 | $53 \mathrm{B67}$ | 55.067 |
|  |  | 0.2 | 05 | 03 | 60.667 | 59200 | 59.167 | 59200 | 59167 | 60.667 |
|  |  | 02 | 0. | 02 | 66267 | 64.500 | 64467 | 54.500 | 64467 | 66.267 |
|  |  | 02 | 07 | 01 | 71.967 | 69800 | 69.767 | 69800 | 69.767 | 71867 |
|  |  | 03 | 0.1 | 0 | 42600 | 42.350 | 423001 | 42.350 | 42300 | 42600 |
|  |  | 0.3 | D2 | 05 | 48200 | 47.650 | 47600 | 47.650 | 47600 | 48.200 |
|  |  | 03 | 03 | 04 | 53800 | 52.950 | 52.900 | 52.950 | 52.900 | 53800 |
|  |  | 03 | 04 | 03 | 59400 | 58250 | 58200 | 58250 | 58200 | 59400 |
|  |  | 03 | 05 | 02 | 65000 | 63550 | 63500 | 63550 | 63500 | 65.000 |
|  |  | 0.3 | 06 | D1 | 70.500 | 6 B 850 | 58800 | 68850 | 68 BOO | 70600 |
|  |  | 04 | 01 | 05 | 46.933 | 46700 | 46633 | 46700 | 46633 | 46.933 |
|  |  | 04 | 02 | 04 | 52533 | 52.000 | 51933 | 52.000 | 51933 | 52533 |
|  |  | D 4 | 03 | 0.3 | 58133 | 57.300 | 57233 | 57.300 | 57.233 | 58133 |
|  |  | D 4 | 04 | 02 | 63733 | 62600 | 62.533 | 62 6¢0 | 62533 | 63.733 |
|  |  | OA | 05 | Q 1 | 69.333 | 67900 | 67833 | 67.940 | 67833 | 69.333 |
|  |  | 05 | $\bigcirc 1$ | © 4 | 51.267 | 51050 | 50967 | 51.050 | 50967 | 51.267 |
|  |  | 05 | $\bigcirc 2$ | ¢ 3 | 56867 | 56.350 | 56267 | 56.350 | 56267 | 58887 |
|  |  | 05 | 03 | 02 | 62.467 | 61650 | 61567 | 61.650 | 61567 | 62467 |
|  |  | 05 | W 4 | 01 | 68.067 | 66950 | 66867 | 66950 | 66867 | 88067 |
|  |  | 06 | 01 | 0.3 | 55600 | 55400 | 55300 60600 | 55.400 60.700 | 55300 60600 | 55.600 61.200 |
|  |  | 0.6 0.6 | 0.2 03 | 02 | 61200 66800 | 10.700 66.000 | 60600 65900 | 60.700 66000 | 60600 65.900 | 61.200 66.800 |
|  |  | 07 | 01 | 02 | 59933 | 59750 | 59633 | 59750 | 59633 | 59.933 |
|  |  | 07 | 02 | 0.1 | 65533 | 65050 | 64.933 | 65050 | 64933 | 65533 |
|  |  | 08 | 01 | 0.1 | 64267 | 64100 | 63.967 | 64100 | 63.967 | 64.267 |
| SUM |  |  |  |  | 205600 | 2022.00 | 2020.00 | 2022.00 | 2020.00 | 205600 |


| T | M | W1 | W2 | W3 | SPTJEDD | EDDISPT | S[1] | \$[2] | \$53] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 18 | 8 | 01 | 0.1 | 0.8 | 34558 | 34.475 | 34,458 | 34475 | 34458 | 34.558 |
|  |  | 01 | 0.2 | 0.7 | 40558 | 40375 | 40.358 | 40375 | 40.358 | 40.558 |
|  |  | 01 | 03 | 06 | 46.558 | 46275 | 46258 | 46275 | 46258 | 46558 |
|  |  | 0.1 | 04 | 05 | 52558 | 52.175 | 52158 | 52175 | 52158 | 52558 |
|  |  | 0.1 | 0.5 | 04 | 58558 | 58.075 | 58058 | 58075 | 58.058 | 58.556 |
|  |  | 01 | 06 | 03 | 64558 | 63.975 | 63956 | 63975 | 63.958 | 64 565 |
|  |  | 01 | 07 | 02 | 70558 | 69.875 | 69 85\% | 69875 | 69.85B | 70.558 |
|  |  | 01 | 08 | 01 | 76558 | 75775 | 75758 | 75.775 | 75.758 | 76558 |
|  |  | 02 | 0.1 | 07 | 39117 | 39050 | 39017 | 39050 | 39.017 | 39117 |
|  |  | 02 | 0.2 | 06 | 45117 | 44.950 | 44917 | 44950 | 44917 | 45117 |
|  |  | 02 | 03 | 05 | 51117 | 50.850 | 50817 | 50.850 | 50817 | 51117 |
|  |  | 02 | 04 | 04 | 57117 | 56750 | 56.717 | 56.750 | 56717 | 57117 |
|  |  | 02 | 05 | 03 | 63117 | 62650 | 52.617 | 62650 | 62617 | 63117 |
|  |  | 02 | 06 | 02 | 69117 | 68.550 | 68517 | 68.550 | 6 5 517 | 69.117 |
|  |  | 0.2 | 0.7 | 01 | 75117 | 74450 | 74.417 | 74,450 | 74417 | 75117 |
|  |  | 03 | 01 | 06 | 43675 | 43625 | 43575 | 43.625 | 43575 | 43.675 |
|  |  | 03 | 0.2 | 05 | 49675 | 49525 | 49475 | 49.525 | 19475 | 49675 |
|  |  | 03 | 03 | 0.4 | 55675 | 55425 | 55375 | 55.425 | 55.375 | 55.675 |
|  |  | 03 | 04 | 0.3 | 61.675 | 61325 | 61.275 | 61325 | 61.275 | 61.675 |
|  |  | 03 | 05 | 02 | 67.675 | 67225 | 67.175 | 67225 | 67.175 | 67.675 |
|  |  | 03 | 06 | 0.1 | 73675 | 73125 | 73075 | 73.125 | 73075 | 73675 |
|  |  | 04 | 01 | 05 | 48233 | 48200 | 48133 | 48.200 | 48133 | 48.233 |
|  |  | 04 | 02 | 04 | 54233 | 54.100 | 54.033 | 54100 | 54033 | 54.233 |
|  |  | 04 | 03 | 03 | 60.233 | 60000 | 59933 | 60000 | 59933 | 60233 |
|  |  | 04 | 04 | 02 | 66233 | 65900 | 65833 | 65.900 | 65833 | 66.233 |
|  |  | 04 | 05 | 01 | 72233 | 71.800 | 71.733 | 71800 | 71.733 | 72.233 |
|  |  | 05 | 01 | 04 | 52.792 | 52775 | 52692 | 52775 | 52.692 | 52.792 |
|  |  | 05 | 02 | 0.3 | 58792 | 58675 | 58592 | 58.675 | 58592 | 58.792 |
|  |  | 05 | 03 | 0.2 | 64792 | 64575 | 54492 | 64.575 | 64492 | 64.792 |
|  |  | 0.5 | 04 | 01 | 70792 | 70475 | 70392 | 70475 | 70.392 | 70792 |
|  |  | 06 | 01 | 0.3 | 57350 | 57350 | 57250 | 57.350 | 57.250 | 57350 |
|  |  | 0.6 | 0.2 | 02 | 63350 | 63250 | 63.150 | 63250 | 63150 | 63350 |
|  |  | 0.6 | 0.3 | 01 | 69350 | 69150 | 69.050 | 69.150 | 69050 | 69350 |
|  |  | 07 | 0.1 | 02 | 61908 | 61925 | 61.808 | 61,925 | 61808 | 61908 |
|  |  | 07 | 0.2 | 101 | 67.908 | 67825 | 67.708 | 67.825 | 67708 | 67908 |
|  |  | 08 | 01 | 01 | 66467 | 66.50 | 65.367 | 66500 | 66367 | 66.467 |
|  |  | SUM |  |  | 213100 | 212100 | 2719.00 | 2121.00 | 211906 | 213100 |


| T | W | W $\mathbf{W} 1$ | W2 | W3 | SPT/EDD | EDOWPT | S[1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19 | 4 | 01 | 01 | 08 | 37.483 | 36800 | 36783 | 36.800 | 36783 | 37483 |
|  |  | 01 | 02 | 0.7 | 41683 | 45300 | 40283 | 40300 | 40283 | 41683 |
|  |  | 01 | $\bigcirc 3$ | 06 | 45883 | 43.800 | 43783 | 43806 | 43.783 | 45.883 |
|  |  | 01 | 04 | 05 | 50093 | 47.300 | 47283 | 47300 | 47.283 | 50.083 |
|  |  | 01 | 05 | 04 | 54283 | 50.800 | 50.783 | 50800 | 50.783 | 54,283 |
|  |  | 01 | 06 | 03 | 58.483 | 54.300 | 54283 | 54300 | 54283 | 58.483 |
|  |  | 01 | 07 | 02 | 62. 693 | 57.800 | 57783 | 57800 | 57.783 | 62.683 |
|  |  | 01 | 68 | 01 | 68883 | 61.300 | 61,263 | 61300 | 61.283 | 66.883 |
|  |  | 02 | 01 | 0.7 | 40767 | 40.100 | 40.667 | 40106 | 40.067 | 40767 |
|  |  | 0.2 | 0.2 | 06 | 44967 | 43600 | 43.567 | 43.600 | 43.567 | 44967 |
|  |  | 02 | 03 | 0.5 | 49.167 | 47100 | 47067 | 47.100 | 47.067 | 49167 |
|  |  | 02 | 04 | 04 | 53.367 | 50.600 | 50567 | 50500 | 50567 | 53367 |
|  |  | 02 | 05 | 03 | 57567 | 54100 | 54.067 | 51100 | 54067 | 57.567 |
|  |  | 0.2 | 06 | 02 | 61767 | 57600 | 57.567 | 57.600 | 57567 | 61.767 |
|  |  | 02 | 07 | 01 | 65967 | 61100 | E1.067 | 61.100 | 61067 | 65.967 |
|  |  | 0.3 | 01 | 06 | 44050 | 43400 | 43350 | 43.400 | 43350 | 44050 |
|  |  | 03 | 02 | 05 | 48250 | 46900 | 4 E .850 | 46900 | 46850 | 4 B 250 |
|  |  | 03 | 03 | 04 | 52.450 | 50400 | 50.350 | 50400 | 50350 | 52.450 |
|  |  | ¢ 3 | 04 | 03 | 56650 | 53900 | 53.850 | 53.900 | 53.650 | 56650 |
|  |  | 03 | 0.5 | 0.2 | 60850 | 57.400 | 57.350 | 57400 | 57350 | 60850 |
|  |  | 03 | 06 | 01 | 65050 | 60.900 | 60.850 | 60950 | 60.850 | 65.050 |
|  |  | 04 | 01 | 0.5 | 47.3 .33 | 46700 | 46.633 | 46.700 | 46633 | 47.333 |
|  |  | D 4 | 02 | 04 | 51533 | 50.200 | 50.133 | 50.200 | 50133 | 51533 |
|  |  | D 4 | 03 | 03 | 55733 | 53.700 | 53.633 | 53.740 | 53633 | 55733 |
|  |  | 04 | 04 | 02 | 59933 | 57200 | 57.133 | 57.200 | 57.133 | 59933 |
|  |  | 0.4 | 05 | 01 | 64133 | 60700 | 60.633 | 60.700 | 60633 | 64133 |
|  |  | 0.5 | 0.1 | 04 | 50617 | 50.000 | 49917 | 50000 | 49917 | 50.647 |
|  |  | 0.5 | 0.2 | 0.3 | 54.817 | 53500 | 53417 | 53500 | 53.417 | 54.817 |
|  |  | 0.5 | 0.3 | 0.2 | 59017 | 57000 | 56.917 | 57000 | 56.917 | 59.017 |
|  |  | 0.5 | 0.4 | 01 | 63217 | 60500 | 60417 | 60500 | 60.417 | E63.217 |
|  |  | 0.6 | 01 | 03 | 53900 | 53300 | 53200 | 53300 | 53.200 | 53.900 |
|  |  | 06 | 02 | 02 | 58100 | 56800 | 56700 | 56800 | 56700 | 58100 |
|  |  | 06 | 03 | 01 | 62300 | 60300 | 60.200 | 60.300 | 60.200 | 62.300 |
|  |  | 07 | 01 | 02 | 57183 | 56600 | 56483 | 56.600 | 56.483 | 57.183 |
|  |  | 07 | 02 | 0.1 | 61.383 | 50.100 | 59.983 | 60100 | 59983 | 61.383 |
|  |  | 08 | 0.1 | 01 | 60467 | 59900 | 59.767 | 59900 | 59767 | 60.467 |
| SUM |  |  |  |  | 197800 | 189600 | 1894,00 | 189600 | 189400 | 197800 |


| T | M | W1 | W2 | W3 | SPTIEDO | EDDISPT | S[1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19 | 5 | D. 1 | 01 | 08 | 38.108 | 37625 | 37608 | $37.625^{\circ}$ | 37608 | 38.108 |
|  |  | 0.1 | 02 | 07 | 42.708 | 41725 | 41708 | 41.725 | 41708 | 42.708 |
|  |  | 0.1 | 0.3 | 0.6 | 47308 | 45825 | 45808 | 45.825 | 45808 | 47308 |
|  |  | 01 | 04 | 05 | 51.908 | 49.925 | 49.908 | 49925 | 49.908 | 51908 |
|  |  | 01 | 05 | 04 | 56508 | 54.025 | 54,008 | 54,025 | 54008 | 56508 |
|  |  | 01 | 06 | 0.3 | 61.109 | 58.125 | 58108 | 58125 | 58.108 | 61108 |
|  |  | 01 | 07 | 02 | 65708 | 62225 | 62208 | 62.225 | 62208 | 65.708 |
|  |  | 01 | ¢88 | 01 | 70308 | 66.325 | 66308 | 66325 | 66308 | 70308 |
|  |  | 02 | 01 | 07 | 41617 | 41150 | 41.117 | 41.150 | 41.117 | 41.817 |
|  |  | 02 | -2 | 0.6 | 46.217 | 45250 | 45217 | 45250 | 15217 | 46.217 |
|  |  | 02 | 03 | 0.5 | 50.817 | 49.350 | 49317 | 49.350 | 49317 | 50.817 |
|  |  | 02 | 0.4 | 04 | 55417 | 53450 | 53417 | 53450 | 53417 | 55.417 |
|  |  | 0.2 | 05 | 0.3 | 60017 | 57550 | 57.517 | 57550 | 57517 | 60.017 |
|  |  | 0.2 | 0.6 | 0.2 | 64617 | 61650 | 61.617 | 61650 | 51617 | 64617 |
|  |  | 0.2 | 0.7 | 0.1 | 69217 | 65750 | 65717 | 65750 | 65717 | 69217 |
|  |  | 0.3 | 0.1 | 0.6 | 45.125 | 44.675 | 44.625 | 44675 | 44625 | 45.125 |
|  |  | 03 | 02 | 05 | 49.725 | 48.775 | 48.725 | 48775 | 48725 | 49725 |
|  |  | $\bigcirc 3$ | 03 | 04 | 54.325 | 52.875 | 52825 | 52875 | $52 \mathrm{B25}$ | 54325 |
|  |  | 0.3 | 0.4 | 0.3 | 58.925 | 56975 | 56,925 | 56.975 | 56.925 | 58925 |
|  |  | 03 | 0.5 | 0.2 | 63.525 | 61.075 | 61.025 | 61.075 | 61.025 | 63.525 |
|  |  | 0.3 | 0.6 | 01 | 68125 | 65175 | 65125 | 65.175 | 65.125 | 68.125 |
|  |  | 0.4 | 0.1 | 0.5 | 48.633 | 48.200 | 48.133 | 48200 | 48133 | 48633 |
|  |  | 04 | 02 | 04 | 53233 | 52300 | 52233 | 52.300 | 52233 | 53233 |
|  |  | 04 | 03 | 03 | 57833 | 56400 | 56333 | 56400 | 56333 | 57.833 |
|  |  | 0.4 | 0.4 | 0.2 | 52.433 | 80.500 | 60.433 | 60500 | $6{ }_{6} 433$ | 62433 |
|  |  | 04 | 05 | 01 | 67033 | 64600 | 64533 | 64600 | 64.533 | 67.033 |
|  |  | 0.5 | 0.1 | 0.4 | . 52.142 | 51.725 | 51.642 | 51.725 | 51.642 | 52.142 |
|  |  | 05 | 02 | 03 | 56742 | 55325 | 55742 | 55825 | 55.742 | 56742 |
|  |  | 05 | 03 | 02 | 61342 | $59 \mathrm{S25}$ | 59842 | 59925 | 59.842 | 61342 |
|  |  | 05 | 04 | 0.1 | 65.942 | 64.025 | 63.942 | 64025 | 63942 | \$5 542 |
|  |  | 0.6 | 0.1 | 0.3 | 55.650 | 55.250 | 55.150 | 55.250 | 55150 | 55650 |
|  |  | 0.6 | 0.2 | 02 | 50250 | 59350 | 59250 | 59350 | 59250 | 60250 |
|  |  | 06 | 03 | 01 | 89.850 | 63450 | 63350 | 63450 | 63350 | 64.850 |
|  |  | 0.7 | 0.1 | 0.2 | 55.158 | 58775 | 58658 | 58.775 | 58658 | 59158 |
|  |  | 0.7 | 0.2 | 0.1 | 63.758 | 62.875 | 62758 | 62.875 | 62758 | 63758 |
|  |  | 08 | 01 | 01 | 62667 | 62.300 | 62.167 | 62.300 | 62.167 | 62,667 |
| SUM |  |  |  |  | 205300 | 1995.00 | 1993.00 | 199500 | 199300 | 205300 |


| T | 内 | W1 | W2 | W3 | \＄PTPEDD | EDDISPT | S］ 1 | S［2］ | S［3］ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19 | 6 | D 1 | 01 | 08 | 38.733 | 38450 | 38433 | 38450 | 38433 | 38.733 |
|  |  | Q1 | 02 | 07 | 43.733 | 43154 | 43133 | 43150 | 43133 | 43733 |
|  |  | 01 | 03 | 06 | 48733 | 47850 | 47833 | 47.850 | 47833 | 48．733 |
|  |  | 0.1 | 04 | 65 | 53733 | 52.550 | 52533 | 52.550 | 52.533 | 53733 |
|  |  | 01 | 0.5 | 0.4 | 5 5 733 | 57250 | 57.233 | 57.250 | 57233 | 58.733 |
|  |  | 01 | 0.6 | 0.3 | 63733 | 61950 | 61933 | 61.950 | 61933 | 63733 |
|  |  | 01 | 07 | 0.2 | 68733 | 66650 | 66633 | 66.650 | 66633 | 68.733 |
|  |  | 01 | 0 B | 01 | 73.733 | 71350 | 71333 | 71.350 | 71.333 | 73733 |
|  |  | 02 | 0.1 | 0.7 | 42467 | 42200 | 42.167 | 42，200 | 42.167 | 42467 |
|  |  | 0.2 | 02 | 0.6 | 47467 | 46．900 | 46867 | 46900 | 46887 | 47．467 |
|  |  | 02 | 03 | 0.5 | 52，4施 | 51600 | 51567 | 51600 | 51.567 | 52467 |
|  |  | 0.2 | 04 | 0.4 | 57467 | 56.300 | 56．267 | 56300 | 56267 | 57.467 |
|  |  | 0.2 | 05 | 03 | 62467 | 61．000 | 60.967 | 61000 | 60967 | 放．467 |
|  |  | 0.2 | 06 | 02 | 67467 | 65．70 | 65667 | 65700 | 65667 | 67．467 |
|  |  | 02 | 07 | 01 | 72467 | 70.400 | 70367 | 70400 | 70367 | 72167 |
|  |  | 0.3 | 01 | 06 | 46200 | 45.950 | 45900 | 45950 | 45.900 | 46200 |
|  |  | 0.3 | 02 | 05 | 51200 | 50.650 | 50.600 | 50650 | 50600 | 51.200 |
|  |  | 0.3 | 03 | 04 | 56200 | 55.350 | 55.300 | 55350 | 55300 | 56200 |
|  |  | Q 3 | 0.4 | 0.3 | 61200 | 60050 | E0000 | 60.050 | 60000 | 65.200 |
|  |  | 03 | 05 | 02 | 66.200 | 64750 | 64700 | 64750 | 64.700 | 66.200 |
|  |  | 03 | 06 | 01 | 71.200 | 69.450 | 69400 | 69450 | 69.400 | 71，200 |
|  |  | 04 | 01 | 05 | 49933 | 49.700 | 49633 | 49700 | 49533 | 49.933 |
|  |  | 04 | 02 | 0.4 | 54933 | 54.400 | 54.333 | 54.400 | 54333 | 54933 |
|  |  | 01 | 03 | 0.3 | 59.933 | 59.100 | 59033 | 59.100 | 59033 | 59933 |
|  |  | 0.4 | 04 | 0.2 | 64.933 | 63800 | 63.733 | 63800 | 63733 | 64933 |
|  |  | 0.4 | 05 | 01 | 69933 | 68500 | 68433 | 68500 | 68433 | 69.933 |
|  |  | 05 | 01 | 04 | 53.66 .7 | 53.450 | 53367 | 53.450 | 53317 | 53667 |
|  |  | 05 | 02 | 03 | 58667 | 58.150 | 58.067 | 58150 | 58.067 | 5 6 67 |
|  |  | 05 | 03 | 02 | 63667 | 62850 | 62767 | 62850 | 62.767 | 63667 |
|  |  | 0.5 | 04 | 01 | 68667 | 67.550 | 67467 | 57.550 | 67，467 | 68667 |
|  |  | 0.6 | 01 | 03 | 57.400 | 57200 | 57.100 | 57.200 | 57100 | 57400 |
|  |  | 0.6 | 02 | 02 | 62400 | 61900 | 61.800 | 61.900 | 61800 | 62400 |
|  |  | 0.6 | 03 | 01 | 67406 | 66600 | 66500 | 66.600 | 66500 | 67400 |
|  |  | 07 | 01 | 0.2 | 61.133 | 60.950 | 60833 | 60.950 | 60.833 | 61.133 |
|  |  | 07 | 02 | 01 | 66133 | 65.650 | 65.533 | 65650 | 65533 | 66133 |
|  |  | 0.8 | 0.1 | 0.1 | 64867 | 64700 | 64567 | 64700 | 64.567 | 64867 |
| SUM |  |  |  |  | 212800 | 209400 | 209200 | 209400 | 209200 | 212800 |


| T | M | W1 | $1+2$ | 7 N 3 | SPTJEDD | EDDISPT | S［1］ | S［2］ | \＄［3］ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19 | 7 | 0.1 | 0.1 | 0.8 | 39.358 | 39275 | 39258 | 39275 | 39258 | 3.358 |
|  |  | 0.1 | 0.2 | 0.7 | 44758 | 44575 | 44558 | 44575 | 44558 | 44，758 |
|  |  | 0.1 | 03 | 06 | 56158 | 49875 | 49.858 | 49.875 | 498.58 | 50158 |
|  |  | 01 | 04 | 05 | 55558 | 55175 | 55.158 | 55175 | 55158 | 55558 |
|  |  | 0.1 | 0.5 | 04 | 60.958 | 60475 | 60458 | 60475 | 60458 | 60．958 |
|  |  | 01 | 06 | 03 | 66358 | 65775 | 65.758 | 55.775 | 65758 | 66358 |
|  |  | 0.1 | 07 | 02 | 71．758 | 71075 | 71.058 | 71075 | 71058 | 71.758 |
|  |  | 0.1 | 08 | 0.1 | 77158 | 76375 | 76.358 | 76.375 | 76358 | 77．158 |
|  |  | 0.2 | 01 | 0.7 | 43.317 | 43250 | 43217 | 43250 | 43217 | 43.317 |
|  |  | 0.2 | 02 | 06 | 48.717 | 48550 | 48517 | 48550 | 48517 | 48717 |
|  |  | 02 | 0.3 | 05 | 54.117 | 53850 | 53.817 | 53 B50 | 53817 | 54.117 |
|  |  | 0.2 | 04 | 0.4 | 59.517 | 59150 | 59.117 | 59150 | 59117 | 59.517 |
|  |  | 02 | 0.5 | 0.3 | 64.917 | 64.450 | 64417 | 64．450 | 64417 | 64.917 |
|  |  | 0.2 | 06 | 0.2 | 70.317 | 69750 | 69.717 | 69750 | 69717 | 70317 |
|  |  | 0.2 | 07 | 0.1 | 75.717 | 75050 | 75017 | 75050 | 75017 | 75717 |
|  |  | 0.3 | 01 | 06 | 47275 | 47.225 | 47.175 | 47.225 | 47175 | 47275 |
|  |  | 03 | 0.2 | 0.5 | 52.675 | 52.525 | 52.475 | 52.525 | 52475 | 52675 |
|  |  | 03 | 03 | 04 | 58075 | 57825 | 57775 | 57.825 | 57775 | 58.075 |
|  |  | 03 | 0.4 | 03 | 63475 | 63125 | 63075 | 63125 | 63075 | 63.475 |
|  |  | 03 | 05 | 02 | 68875 | 68．425 | 68.375 | 68.425 | 68375 | 68875 |
|  |  | 0.3 | 0.6 | 0.1 | 74275 | 73725 | 73675 | 73.725 | 73675 | 74275 |
|  |  | 04 | 01 | 05 | 51233 | 51200 | 51133 | 51.200 | 51.133 | 51 233 |
|  |  | 04 | 02 | 04 | 56633 | 56.500 | 55.433 | 56500 | 56433 | 56.633 |
|  |  | 0.4 | 0.3 | 03 | 62033 | 61800 | 61733 | 61.800 | 61.733 | 62.033 |
|  |  | 04 | 04 | 02 | 67433 | 67100 | 67033 | 67.100 | 67．033 | 67433 |
|  |  | 04 | 65 | 01 | 72833 | 72.400 | 72.33 .3 | 72.400 | 72333 | 72833 |
|  |  | 05 | 01 | 04 | 55192 | 55175 | 55.092 | 56175 | 55992 | 55192 |
|  |  | 05 | 42 | 03 | 60592 | 60.475 | 60.392 | 60475 | 60392 | 60592 |
|  |  | 05 | 6． 3 | 02 | 65992 | 65.775 | 65.692 | 65.775 | 65692 | 65.992 |
|  |  | 05 | 04 | 01 | 71392 | 71075 | 70992 | 71075 | 70.392 | 71.392 |
|  |  | 06 | 01 | 03 | 59150 | 59150 | 59050 | 59150 | 59050 | 59.150 |
|  |  | 06 | 02 | 02 | 64550 | 64450 | 64.350 | 64．450 | 64.350 | 64550 |
|  |  | 06 | 03 | 01 | 69.950 | 69750 |  | 69750 | 69.650 | 69.950 |
|  |  | 07 | 61 | 02 | 63.108 | 63125 | 63.008 | 63125 | 63，008 | 63.108 |
|  |  | 0.7 | 02 | 01 | 68508 | 68.425 | 68308 | 68.425 | 68308 | 68508 |
|  |  | 08 | 0.1 | 0.1 | 67.067 | 67．100 | 66967 | 67.100 | 66967 | 67067 |
| SUM |  |  |  |  | 22.0300 | 219300 | 2191.00 | 219300 | 2191.00 | 2203.00 |


| T | M | W1 | W2 | W/3 | SPTIEDD | EDDISPT | S[1] | S[2] | S[3] | \$[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19 | B | 0.1 | 0.1 | 08 | 40 (1)3 | 40100 | 40083 | 40100 | 40.683 | 40083 |
|  |  | 01 | 02 | 0.7 | 45.983 | 46000 | 45.983 | 46.000 | 45.983 | 45983 |
|  |  | 01 | 03 | 0.6 | 51.883 | 51900 | 51.883 | 51.900 | 51883 | 51883 |
|  |  | 01 | 04 | 0.5 | 57.783 | 57.800 | 57783 | 57.800 | 577 73 | 57.783 |
|  |  | 0.1 | D 5 | 0.4 | 63683 | 63700 | 63.683 | 63.700 | 63.683 | 63.683 |
|  |  | 0.1 | D6 | D3 | 69583 | 69600 | 69593 | 69.600 | 69583 | 69.583 |
|  |  | 01 | 0.7 | 02 | 75483 | 75.500 | 75483 | 75.500 | 75483 | 75483 |
|  |  | 01 | 0.8 | 01 | 81383 | 81.400 | 81383 | 81.400 | 81383 | 81383 |
|  |  | 02 | 0.1 | 07 | 44267 | 44.300 | 44267 | 44.300 | 44267 | 44287 |
|  |  | 0.2 | 02 | 06 | 50167 | 50200 | 50167 | 50200 | 50167 | 50.167 |
|  |  | 02 | 03 | 05 | 56067 | 56100 | 58067 | 55100 | 56087 | 56.067 |
|  |  | 02 | 0.4 | 04 | 61967 | 62.00 | 61967 | 62.000 | \$1 867 | 61967 |
|  |  | 02 | 0.5 | 03 | 67.8安7 | 67900 | 67.867 | 67900 | 67867 | 67.867 |
|  |  | 02 | 06 | 0.2 | 73767 | 73800 | 73.767 | 73800 | 73,767 | 73767 |
|  |  | 62 | 0.7 | 01 | 79667 | 79.700 | 79667 | 79.700 | 79667 | 79667 |
|  |  | 63 | 0.1 | 06 | 48450 | 48.500 | 48.450 | 48500 | 48450 | 48.450 |
|  |  | 93 | 02 | 0.5 | 54350 | 54.400 | 54350 | 54400 | 54.350 | 54350 |
|  |  | 03 | 03 | 0.4 | 60250 | 60300 | 60.250 | 60300 | 60.250 | 60250 |
|  |  | 03 | 04 | 03 | 66.150 | 66200 | 66150 | 66200 | 66150 | 66.150 |
|  |  | 03 | 05 | 0.2 | 72050 | 72.100 | 72.050 | 72100 | 72.050 | 72050 |
|  |  | 03 | 06 | 01 | 77.950 | 78000 | 77.950 | 78000 | 77950 | 77.950 |
|  |  | 04 | 0.1 | 05 | 52 官33 | 52.700 | $52 \mathrm{B33}$ | 52.700 | 52633 | 52 b 33 |
|  |  | 04 | 02 | 0.4 | 58533 | 58.500 | 58.533 | 58600 | 58533 | 58533 |
|  |  | 04 | 03 | 0.3 | 64433 | 64500 | 64.433 | 64.500 | 64433 | 64.433 |
|  |  | 04 | 4.4 | 02 | 70.333 | 70400 | 70.333 | 70400 | 70.333 | 70.333 |
|  |  | 04 | 05 | 0.1 | 76233 | 76300 | 76.233 | 76300 | 76.233 | 76233 |
|  |  | 05 | 0.1 | 04 | 56817 | 56.900 | 56817 62717 | 56900 62800 | 56.817 62.717 | 66817 62717 |
|  |  | 0.5 | 02 63 | 03 02 | 62717 $\$ 8.617$ | 62800 68700 | 62717 68.617 | 62.800 68700 | 62,717 68617 | 62717 68.617 |
|  |  | 05 | 04 | 0.1 | 74517 | 74600 | 74.517 | 74.600 | 74.517 | 74517 |
|  |  | 96 | 0.1 | 0.3 | 61000 | 61.100 | 61000 | 61.100 | ¢1.000 | 61000 |
|  |  | 0.6 | 02 | 02 | 66900 | 67.000 | 66900 | 67.000 | 66900 | 66900 |
|  |  | 0.6 | 03 | 01 | 72800 | 72.900 | 72800 | 72.900 | 72800 | 72800 |
|  |  | 0.7 | 0.1 | 02 | 65183 | 65.300 | 65183 | 65300 | 65183 | 65183 |
|  |  | 0.7 | 0.2 | 41 | 71083 | 71.200 | 71083 | 71.200 | 71083 | 71083 |
|  |  | 08 | 0.1 | 0.1 | 69367 | 69500 | 69367 | 69500 | 69.367 | 69367 |
| SUM |  |  |  |  | 2290.00 | 2292.00 | 229000 | 2292 ch | 2290.00 | 22900 |


| $T$ | M | W1 | W2 | W3 | SPTIED | EDDISPT | S[1] | S[2] | 5[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | 4 | 01 | 01 | 08 | 42.908 | 23150 | 42408 | 42.425 | 42408 | 42.908 |
|  |  | 01 | 02 | 07 | 46.908 | 26250 | 45.908 | 45.925 | 45908 | 46.908 |
|  |  | 01 | 03 | 0.6 | 50908 | 29350 | 49.408 | 49.425 | 49408 | 50908 |
|  |  | 01 | 04 | 0.5 | 54908 | 32450 | 52.909 | 52.925 | 52.908 | 54908 |
|  |  | 0.1 | 05 | 04 | 58.908 | 35550 | 56.408 | 56425 | 55 403 | 58.908 |
|  |  | 01 | 06 | 0.3 | 62908 | 38650 | 59909 | 59925 | 59908 | 62.908 |
|  |  | 01 | 07 | 02 | 66.908 | 41750 | 63 408 | 63425 | 63 408 | 66.908 |
|  |  | 01 | 08 | 0.1 | 70.908 | $44 \mathrm{B50}$ | 66.908 | 66925 | 66908 | 70.909 |
|  |  | 02 | 01 | 07 | 45817 | 27200 | 45.317 | 45.350 | 45317 | 45817 |
|  |  | 02 | 02 | 06 | $49 \mathrm{B17}$ | 30300 | 48.817 | 48.850 | 48817 | 49.817 |
|  |  | 02 | 03 | 05 | $53 \mathrm{B17}$ | 33.400 | 52317 | 52.350 | 52.317 | 53.817 |
|  |  | 02 | 04 | 04 | $57 \mathrm{B17}$ | 36.500 | 55817 | 55.850 | 55817 | 57.817 |
|  |  | 0.2 | 05 | 03 | 61817 | 39600 | 59.317 | 59.350 | 59317 | 61.817 |
|  |  | 02 | 06 | 0.2 | 65817 | 42.700 | 62.817 | 62850 | 52817 | 65.817 |
|  |  | 0.2 | 07 | 0.1 | 69817 | 45 B00 | 66.317 | 66350 | 66.317 | 89.817 |
|  |  | 03 | 01 | 0.6 | 48725 | 31.250 | 49225 | 48275 | 48225 | 49.725 |
|  |  | 03 | 0.2 | 0.5 | 52725 | 34.350 | 51725 | 51775 | 51.725 | 52,725 |
|  |  | 0.3 | 0.3 | 04 | 56.725 | 37450 | 55225 | 55.275 | 55.225 | 56725 |
|  |  | 03 | 0.4 | 03 | 60725 | 40550 | 58725 | 58.775 | 58.725 | 60725 |
|  |  | 03 | 0.5 | 02 | 64725 | 43650 | 82.225 | 62275 | 62225 | 64725 |
|  |  | 03 | 06 | 01 | 68.725 | 46750 | 65725 | 65.775 | 65.725 | 68725 |
|  |  | 04 | 01 | 0.5 | 51633 | 35300 | 51133 | 51,200 | 51.133 | 51633 |
|  |  | 0.4 | 02 | 04 | 55633 | 39.400 | 54633 | 54700 | 54833 | \$5633 |
|  |  | 0.4 | 03 | 03 | 59633 | 41.500 | 58133 | 58200 | 58.133 | 59633 |
|  |  | 04 | 04 | 02 | 63633 | 44600 | 69633 | 61.700 | 61.633 | 63633 |
|  |  | 04 | 05 | 01 | 67.633 | 47700 | 65133 | 65.200 | 65.133 | 67633 |
|  |  | 05 | 01 | 04 | 54.542 | 39350 | 54042 | 54.125 | 54042 | 54542 |
|  |  | 05 | 02 | 03 | 58542 | 42450 | 57542 | 57625 | 57.542 | 58.542 |
|  |  | 05 | 03 | 02 | 62542 | 45.550 | 61542 | 61125 | 61.042 | 62542 |
|  |  | 05 | 04 | 01 | 66542 | 48650 | 64.542 | 64625 | 64.542 | 66.542 |
|  |  | 0.6 | 0.1 | 03 | 57450 | 43400 | 56950 | 57050 | 56.950 | 57.450 |
|  |  | 06 | 02 | 02 | 61.450 | 46500 | 60450 | 60550 | 60450 | 61.450 |
|  |  | 06 | 03 | 0.1 | 65.450 | 49680 | 63950 | 64050 | 63950 | 65.450 |
|  |  | 07 | 0.1 | 02 | 60.358 | 47450 | 59.858 | 59.975 | 59858 | 50.358 |
|  |  | 0.7 | 02 | 01 | 64.35 | 50.550 | 63358 | 63475 | 63358 | 64.358 |
|  |  | 03 | 01 | 01 | 63267 | 51.500 | 62767 | 62900 | 62.767 | 63267 |
|  |  | sum |  |  | 212500 | 1434.00 | 20550 | 206700 | 206500 | 2125.00 |


| T | H | W $\mathbf{W}$ | W2 | W3 | SPT/EDD | EDDISPT | \$[1] | S[2] | \$[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | D 1 | 01 | 0.8 | 43533 | 23833 | 43233 | 43250 | 43233 | 43533 |
|  |  | 01 | 02 | 0.7 | 47933 | 27.433 | 47.333 | 47350 | 47.333 | 47933 |
|  |  | 01 | 0.3 | 06 | 52333 | 31.033 | 51433 | 51450 | 51.433 | 52333 |
|  |  | 01 | 04 | 0.5 | 56733 | 34633 | 55.533 | 55550 | 55.533 | 56.733 |
|  |  | 01 | 05 | 0.4 | 61133 | 38233 | 59.633 | 59650 | 59.633 | 61133 |
|  |  | 01 | 0.6 | 0.3 | 65533 | 41 B33 | 63.733 | 63750 | 63.733 | 6.5633 |
|  |  | 0.1 | 0.7 | 02 | 69933 | 45.433 | 67833 | 67850 | 67.933 | 69933 |
|  |  | 01 | 0.6 | 0.1 | 74333 | 49033 | 71.933 | 71950 | 71.933 | 74333 |
|  |  | 02 | 0.1 | 0.7 | 46667 | 28067 | 46.367 | 46406 | 46.367 | 46.667 |
|  |  | 02 | 0.2 | 0.6 | 51067 | 31667 | 50.467 | 50500 | 50.467 | 51.067 |
|  |  | 02 | 03 | 0.5 | 55.467 | 35267 | 54.567 | 54600 | 54.567 | 55.467 |
|  |  | 02 | 04 | 04 | 59.867 | 38667 | 58667 | 58.700 | 58667 | 59867 |
|  |  | 02 | 05 | 03 | 64267 | 42,467 | 62767 | 62.800 | 62767 | B4 267 |
|  |  | 0.2 | 06 | 02 | 68667 | 46.067 | 66867 | 66900 | 66.867 | 68667 |
|  |  | 02 | 07 | 01 | 73067 | 49.667 | 70867 | 71000 | 70.967 | 73.067 |
|  |  | 0.3 | 01 | 06 | 49800 | 32.300 | 49500 | 49550 | 49.500 | 49.800 |
|  |  | 0.3 | 02 | 05 | 54200 | 35.900 | 53600 | 53650 | 53.600 | 54.20D |
|  |  | 03 | 03 | 04 | 58600 | 39.500 | 57.700 | 57750 | 57.700 | 58.600 |
|  |  | 03 | 04 | 03 | 63000 | 43100 | 61800 | 61.850 | 61800 | 63000 |
|  |  | 03 | 05 | 02 | 67.400 | 46700 | 65900 | 6.5 .950 | 65900 | 67.400 |
|  |  | 03 | 08 | 01 | 71800 | 50300 | 70000 | 70.050 | 70000 | 71.800 |
|  |  | 04 | 01 | - 5 | 52933 | 36533 | 52.633 | 52700 | 52633 | 52933 |
|  |  | 04 | 02 | 04 | 57333 | 40133 | 56733 | 56.800 | 56733 | 57.333 |
|  |  | 04 | 03 | 0.3 | 61733 | 43.733 | 60833 | 60900 | 60833 | 61.733 |
|  |  | 04 | 04 | 02 | 66133 | 47.333 | 64.933 | 65.000 | 64933 | 66.133 |
|  |  | 04 | 0.5 | 01 | 70.533 | 50933 | 69.033 | 69.100 | 69033 | 70.533 |
|  |  | 05 | 01 | 0.4 | 56067 | 40.767 | 55.767 | 55850 | 55.767 | 56.067 |
|  |  | 05 | 02 | 0.3 | 60467 | 44.367 | 59.867 | 59.950 | 59867 | 60467 |
|  |  | 05 | 03 | 02 | 64.867 | 47.967 | 63967 | 64.050 | 63967 | 64867 |
|  |  | 05 | 04 | 01 | 69.267 | 51.567 | 68067 | 68150 | 68067 | 69267 |
|  |  | 0.6 | 0.1 | 0.3 | 59200 | 45.060 | $58.96 \bigcirc$ | 59.000 | 58900 | 59200 |
|  |  | 0.6 | 0.2 | 02 | 63600 | 43.600 | $63.0 ¢ \bigcirc$ | 63.100 | 53.000 | 63.600 |
|  |  | 0.6 | 0.3 | 01 | 68000 | $52.20{ }^{\text {¢ }}$ | $67.10 \square$ | 67.200 | 67100 | 68000 |
|  |  | 07 | 01 | 02 | 62.333 | 49.233 | 62.033 | 62150 | 62033 | 62333 |
|  |  | 07 | 02 | 01 | 66.733 | 52833 | 66.133 | 66250 | 66133 | 68.733 |
|  |  | 0.8 | 01 | 01 | 65487 | 53467 | 65167 | 65300 | 65.167 | 65467 |
| SUM |  |  |  |  | 220000 | 1516.00 | 216400 | 2166.00 | 216400 | 2200.00 |


| 7 | M | WH1 | W2 | W3 | SPTIEDD | EDDISPT | S[1] | S[2] | \$ 31 | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | 6 | 0.1 | 01 | 08 | 44158 | 24517 | 44.058 | 44.075 | 44058 | 44.158 |
|  |  | 0.1 | 0.2 | 07 | 4B958 | 28617 | 48.758 | 48.775 | 48758 | 48958 |
|  |  | 01 | 03 | 0.6 | 53.758 | 32717 | 53458 | 53475 | 53458 | 53758 |
|  |  | 01 | 0.4 | 05 | 58558 | 36.817 | 58158 | 58175 | 58158 | 58.558 |
|  |  | 0.1 | 0.5 | 04 | 63358 | 40917 | 62.858 | 62975 | 62 B58 | 63358 |
|  |  | 01 | 06 | 0.3 | 68.158 | 45017 | 67558 | 67.575 | 67558 | 68158 |
|  |  | 01 | 07 | 0.2 | 72.958 | 49117 | 72258 | 72.275 | 72.258 | 72958 |
|  |  | 01 | 0.8 | 0.1 | 77759 | 53217 | 76958 | 75975 | 76958 | 77758 |
|  |  | 02 | 0.1 | 0.7 | 47517 | 28.933 | 47417 | 47450 | 47417 | 47.517 |
|  |  | 02 | 02 | 0.6 | 52.317 | 33 033 | 52117 | 52150 | 52.117 | 52.317 |
|  |  | 02 | 0.3 | 05 | 57117 | 37.133 | 58.817 | 56850 | 56.817 | 57117 |
|  |  | 0.2 | 0.4 | 0.4 | 61917 | 41233 | 61517 | 61.550 | 61.517 | 61917 |
|  |  | 02 | 05 | 03 | 66717 | 45333 | 68.217 | 66250 | 66.217 | 66717 |
|  |  | 02 | 06 | 02 | 71.517 | 49.433 | 70917 | 70950 | 70.917 | 71.517 |
|  |  | 0.2 | 0.7 | 0.1 | 76317 | 53533 | 75617 | 75.650 | 75617 | 76317 |
|  |  | 0.3 | 01 | 06 | 50875 | 33350 | 50.775 | 50825 | 50775 | 50.875 |
|  |  | 0.3 | 0.2 | 05 | 55675 | 37.450 | 55.475 | 56525 | 55475 | 55675 |
|  |  | 03 | 03 | 04 | 60.475 | 41.550 | 60175 | 60225 | 60175 | 施.475 |
|  |  | 03 | 04 | 03 | 65275 | 45650 | 64,875 | 64925 | 64875 | 65275 |
|  |  | 0.3 | 0.5 | 02 | 70.175 | 49750 | 69.575 | 69.625 | 69575 | 70.675 |
|  |  | 0.3 | 0.6 | 0.1 | 74875 | 53850 | 74275 | 74,325 | 74.275 | 74875 |
|  |  | 0.4 | 0.1 | 0.5 | 54,233 | 37767 | 54133 | 54200 | 54.133 | 54233 |
|  |  | 0.4 | 02 | 04 | 59.033 | 41.867 | 58.833 | 58.900 | 58833 | 59.033 |
|  |  | 04 | 03 | 0.3 | 63833 | 45 S 67 | 63533 | 63600 | 63.533 | 63833 |
|  |  | 04 | 04 | 0.2 | 68.633 | 50.197 | 68233 | 68300 | 68.233 | 68633 |
|  |  | 0.4 | 0.5 | 0.1 | 73433 | 54167 | 72933 | 73.000 | 72.933 | 73433 |
|  |  | 05 | 01 | 04 | 57592 | 42.183 | 57.492 | 57575 | 57492 | 57.592 |
|  |  | 05 | 02 | 03 | 62.392 | $4{ }^{4} 283$ | 62.192 | 62275 | 62192 | 62.392 |
|  |  | 05 | 0.3 | 02 | 67.192 | 50.383 | 66892 | 66975 | 66892 | 67.192 |
|  |  | 05 | 04 | ¢1 | 71.992 | 54.483 | 71592 | 71.675 | 71592 | 71.992 |
|  |  | 06 | 0.1 | 0.3 | 60.950 | 46 60以 | 60850 | 60.950 | 60.350 | 60950 |
|  |  | 06 | 02 | 0.2 | 65.750 | 50.700 | 65550 | 65650 | 65550 | 65750 |
|  |  | 06 | 0.3 | 0.1 | 70550 | 54.800 | 70250 | 70350 | 70250 | 70.550 |
|  |  | 0.7 | 0.1 | 0.2 | 64308 | 51.017 | 64208 | 64.325 | 64208 | 64.308 |
|  |  | 0.7 | 02 | 0.1 | 69.108 | 55.117 | 68.908 | 69.025 | 68.909 | 69.10 B |
|  |  | 08 | 01 | 01 | 67.667 | 55433 | 67567 | \$7.700 | 67567 | 67.667 |
| SUM |  |  |  |  | 227500 | 1598.00 | 226300 | 226500 | 2263.03 | 227500 |


| T | H | W 1 | W2 | W3 | SPTREDD | EDDISPT | S［1］ | S［2］ | S［3］ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | 7 | W1 | 01 | 08 | 44.893 | 25.200 | 44883 | 44900 | 44.883 | 44883 |
|  |  | 01 | 02 | 07 | 50．18．3 | 29800 | 50183 | 50200 | 50.163 | 50183 |
|  |  | 0.1 | 0.3 | 0.6 | 55483 | 34400 | 55.483 | $55 \$ 00$ | 55483 | 55483 |
|  |  | 0.1 | 04 | 05 | 60783 | 39000 | 的． 783 | 60800 | 60783 | 64783 |
|  |  | 01 | 05 | 04 | 66083 | 43600 | 66.083 | 66100 | 66.083 | 66.083 |
|  |  | 0.1 | 06 | 03 | 71.383 | 48200 | 71383 | 71400 | 71.383 | 71.383 |
|  |  | 0.1 | 0.7 | 0.2 | 76.683 | 52．800 | 76683 | 76700 | 76.683 | 76.683 |
|  |  | 01 | 0.8 | 0.1 | 81.983 | 57．400 | 81983 | 82000 | 81.983 | 81.983 |
|  |  | 02 | 01 | 0.7 | 48.467 | 29800 | 48467 | 48500 | 48487 | 48.467 |
|  |  | 02 | 02 | 06 | 53.767 | 34．400 | 53767 | 53800 | 53767 | 53.767 |
|  |  | 02 | 03 | 05 | 59067 | 39.000 | 59.067 | 59100 | 59067 | 59.057 |
|  |  | 02 | 04 | 04 | 64367 | 43.600 | 64367 | 64400 | 64367 | 64.357 |
|  |  | 02 | 05 | 0.3 | 69667 | 48200 | 69667 | 69．700 | 69667 | 69.667 |
|  |  | 0.2 | 06 | 02 | 74967 | 52.800 | 74967 | 75000 | 74，967 | 74.967 |
|  |  | 0.2 | 0.7 | 0.1 | 80267 | 57．400 | 80.267 | 80300 | 80267 | 80267 |
|  |  | 0.3 | 0.1 | 0.6 | 52.050 | 34.400 | 52.050 | 52100 | 52050 | 52.050 |
|  |  | 0.3 | 02 | 0.5 | 57.350 | 39000 | 57.350 | 57400 | 57350 | 57.350 |
|  |  | 0.3 | 03 | 04 | 62.650 | 43.600 | 62650 | 62700 | 62.650 | 62，650 |
|  |  | 03 | 04 | 03 | 67.950 | 48.200 | 67950 | 58000 | 67.950 | 67950 |
|  |  | 03 | 05 | 02 | 73250 | 52800 | 73.250 | 73300 | 73250 | 73250 |
|  |  | 03 | 06 | 01 | 78550 | 57400 | 78550 | 78600 | 78550 | 78.550 |
|  |  | 04 | 01 | 05 | 55633 | 39000 | 55633 | 55700 | 55.633 | 55.633 |
|  |  | 04 | 02 | 04 | 60933 | 43600 | 50.933 | 61.000 | 60933 | 60833 |
|  |  | W 4 | 03 | 03 | 66233 | 48.200 | 66.233 | 66300 | 66233 | 66233 |
|  |  | W 4 | 04 | 02 | 71533 | 52.800 | 71.533 | 71.600 | 71533 | 71533 |
|  |  | 04 | 05 | 01 | 76833 | 57.400 | 76.833 | 76900 | 76833 | 76833 |
|  |  | 05 | 01 | 04 | 59217 | 43.600 | 59.217 | 59.300 | 59217 | 59217 |
|  |  | 05 | 02 | 03 | 64517 | 48200 | 64517 | 64．600 | 64.517 | 64517 |
|  |  | 0.5 | 0.3 | 02 | 69817 | 52800 | 69817 | 69900 | 69.817 | 69.897 |
|  |  | 05 | 04 | 0.1 | 75.117 | 57.400 | 75117 | 75200 | 75.117 | 75117 |
|  |  | 06 | 01 | 03 | 62 B00 | 48.200 | 62.800 | 62.900 | 62.800 | 62 BDO |
|  |  | 06 | 02 | 02 | 68100 | 52 BDO | 68100 | $\$ 8.200$ | 68.100 | 68100 |
|  |  | 0.6 | 03 | 01 | 73400 | 57400 | 73400 | 73500 | 73400 | 73400 |
|  |  | 0.7 | 01 | 0.2 | 66.383 | 52 BOO | 66383 | 66500 | 65383 | 68.383 |
|  |  | 07 | 02 | 01 | 71683 | 57400 | 71683 | 71800 | 71.693 | $71683$ |
|  |  | 08 | 01 | 01 | 69967 | 57400 | 69967 | 70.100 | 69 967 | 69967 |
| SLMM |  |  |  |  | 2362.00 | 1580.00 | 2362 00 | 236400 | 236204 | 236200 |


| T | H | W1 | W／2 | W3 | SPTJEDD | EDDISPT | S［1］ | S［2］ | S［3］ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | 8 | 0.1 | 0.1 | 0.8 | 45.708 | 25.883 | 45.708 | 45.725 | 45.708 | 45708 |
|  |  | 01 | D 2 | 07 | 51.608 | 30.983 | 51.608 | 51.625 | 51.608 | 51608 |
|  |  | 01 | 03 | 0.6 | 57.508 | 36.083 | 57．508 | 57525 | 57.508 | 57.508 |
|  |  | 01 | 04 | 05 | 63408 | 41.183 | 63．408 | 63425 | 63408 | 63408 |
|  |  | D 1 | 05 | 04 | 69.308 | 46283 | 69.308 | 69.325 | 69308 | 69308 |
|  |  | 0.1 | 0.6 | 0.3 | 75208 | 51.383 | 75208 | 75225 | 75208 | 75.208 |
|  |  | 0.1 | 0.7 | 02 | 81108 | 56483 | 81 168 | 81.125 | 81.108 | 81.108 |
|  |  | 0.1 | 0.8 | 0.1 | 87008 | 61583 | 87008 | 87025 | 87008 | 87.008 |
|  |  | 02 | 01 | 0.7 | 49517 | 36667 | 49517 | 49550 | 49517 | 49.517 |
|  |  | 62 | 02 | 06 | 55417 | 35767 | 55417 | 55450 | 55.417 | 55.417 |
|  |  | 02 | 03 | 05 | 61.317 | 40.867 | 61.317 | \＄1．350 | 61317 | 61317 |
|  |  | 0,2 | 04 | 04 | 67217 | 45967 | 67217 | 67.250 | 67217 | 67.217 |
|  |  | 02 | 05 | 03 | 73117 | 51067 | 73.117 | 73150 | 73117 | 73117 |
|  |  | 02 | 06 | 02 | 79017 | 56167 | 79017 | 79050 | 79.017 | 79017 |
|  |  | 02 | 07 | 01 | 84.917 | 61.267 | 84.917 | 84950 | 8．917 | 84917 |
|  |  | 0.3 | 0.1 | 06 | 53.325 | 35450 | \＄3 325 | 53375 | 53325 | 53325 |
|  |  | 03 | 02 | 05 | 59225 | 40550 | 59225 | 59275 | 59225 | 59225 |
|  |  | 0.3 | 0.3 | 04 | 65125 | 45650 | 65125 | 65175 | 65.125 | 65.125 |
|  |  | 0.3 | 0.4 | 0.3 | 71025 | 50750 | 71.025 | 71.075 | 71．025 | 71.025 |
|  |  | 0.3 | 0.5 | 0.2 | 76925 | 55850 | 76.925 | 76.975 | 76.925 | 76.925 |
|  |  | 0.3 | 0.6 | 0.1 | 82825 | 50950 | B2825 | 82875 | 82.825 | 82.825 |
|  |  | 04 | 0.1 | 0.5 | 57133 | 40233 | 57.133 | 57200 | 57133 | 57.133 |
|  |  | 04 | 0.2 | 0.4 | 63633 | 45333 | 63.033 | 63100 | 63033 | 63.033 |
|  |  | 04 | 03 | 03 | 68.933 | 50433 | 68.933 | 69 DOO | 68.933 | 68.933 |
|  |  | 0.4 | 04 | 02 | 74833 | 55533 | 74833 | 74.900 | 74．833 | 74833 |
|  |  | 0.4 | 05 | 0.1 | 80.733 | 60.633 | 80.733 | 80.800 | 80.733 | 80733 |
|  |  | 0.5 | 0.1 | 0.4 | 50.942 | 45017 | 60.942 | 61.025 | 60.942 | 60942 |
|  |  | 05 | 02 | 0.3 | 站． 942 | 50.117 | 66842 | 66925 | 66842 | 65842 |
|  |  | 05 | 03 | 02 | 72.742 | 55217 | 72.742 | 72825 | 72742 | 72742 |
|  |  | 05 | 0.4 | 0.1 | 781842 | 6D 317 | 78642 | 78725 | 78642 | 78642 |
|  |  | 06 | 01 | 0.3 | 64.750 | 49.800 | 64750 | 64850 | 64.750 | 64.750 |
|  |  | 06 | 02 | 02 | 70850 | 54.900 | 70．650 | 70750 | 70650 | 70650 |
|  |  | 06 | 03 | 0.1 | 76.550 | 60000 | 76.550 | 76650 | 76.550 | 76550 |
|  |  | 0.7 | 0.1 | 02 | 施．558 | 54.583 | 68.558 | 68675 | 68558 | 68558 |
|  |  | 07 | 02 | 0.1 | 74458 | 59．683 | 74．458 | 74575 | 74458 | 74458 |
|  |  | 08 | 0.1 | 0.1 | 72367 | 59367 | 72367 | 72500 | 72367 | 72367 |
| SUM |  |  |  |  | 2461．00 | 1752．00 | 2451．00 | 2463.00 | $2461.00^{\circ}$ | 2461.00 |


| T | M | W1 | W/2 | W3 | SPTJEDD | EDDISPT | S[1] | S[2] | \$ ${ }^{\text {2] }}$ | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 4 | 0.1 | 0.1 | 号 | 29.025 | 27.833 | 29.592 | 27.817 | 28133 | 29.025 |
| 2 |  | 0.1 | 02 | 0.7 | 33.325 | 3 3 933 | 31892 | 30.917 | 31533 | 33325 |
|  |  | 01 | 0.3 | 06 | 37.625 | 34.033 | 35192 | 34.017 | 34933 | 37.625 |
|  |  | 0.1 | 0.4 | 0.5 | 41.925 | 37.133 | 38492 | 37.117 | 38333 | 41.925 |
|  |  | 0.1 | 0.5 | 0.4 | 46225 | 40.233 | 41792 | 40217 | 41.733 | 46225 |
|  |  | 0.1 | 06 | 0.3 | 50.525 | 43.333 | 45092 | 43.317 | 45133 | 50525 |
|  |  | 01 | 07 | 02 | 54825 | 46.433 | 48392 | 46417 | 48533 | 54825 |
|  |  | 0.1 | 08 | 01 | 59125 | 49533 | 51.692 | 49517 | 51.933 | 59.126 |
|  |  | 02 | 0.1 | 07 | 32.750 | 31567 | 32883 | 31.533 | 31867 | 32.750 |
|  |  | 02 | 02 | 06 | 37050 | 34667 | 36.183 | 34633 | 35267 | 37.050 |
|  |  | 0.2 | 03 | 0.5 | 41350 | 37.767 | 39483 | 37733 | 38.667 | 41.350 |
|  |  | 02 | 04 | 0.4 | 45650 | 40867 | 42783 | 41833 | 42.067 | 45650 |
|  |  | 0.2 | 05 | 03 | 49950 | 43967 | 46083 | 43933 | 45.467 | 49.950 |
|  |  | 02 | 06 | 0.2 | 54250 | 47.667 | 49.383 | 47033 | 48.867 | 54250 |
|  |  | 02 | 0.7 | 01 | 58550 | 50167 | 52.683 | 50133 | 52267 | 58.550 |
|  |  | 03 | 0.1 | 06 | 35.475 | 35300 | 37175 | 35.250 | 35600 | 36475 |
|  |  | 0.3 | 02 | 05 | 40.775 | 38400 | 40475 | 38.350 | 35000 | 40775 |
|  |  | 03 | 03 | 0.4 | 45075 | 41500 | 43.775 | 41450 | 42.400 | 45075 |
|  |  | 03 | 0.4 | 03 | 49.375 | 44600 | 47.075 | 44550 | 45.800 | 49.375 |
|  |  | 0.3 | 0.5 | 62 | 53.675 | 47700 | 50375 | 47.650 | 49.200 | 53675 |
|  |  | 0.3 | 06 | 0.1 | 57975 | 50.800 | 53675 | 50750 | 52.600 | 57975 |
|  |  | 0.4 | 01 | 05 | 40.200 | 39033 | 41467 | 38.967 | 39.333 | 40.200 |
|  |  | 04 | 0.2 | 04 | 44.500 | 42133 | 44.767 | 42067 | 42.733 | 44.500 |
|  |  | 04 | 03 | 0.3 | 48800 | 45.233 | 48067 | 45167 | 46133 | 48 BOO |
|  |  | 0.4 | 04 | 02 | 53.100 | 48333 | 51.367 | 48267 | 49.533 | 53.100 |
|  |  | 0.4 | 05 | 01 | 57.400 | 51433 | 54.667 | 51367 | 52.933 | 57.400 |
|  |  | 05 | 0.1 | 13 4 | 43925 | 42767 | 45.758 | 42683 | 43067 | 43.925 |
|  |  | 05 | 02 | 0.3 | 48225 | 45.867 | 49058 | 45.783 | 46467 | 48225 |
|  |  | D 5 | 03 | 02 | 52525 | 48967 | 52358 | 48.883 | 49867 | 52525 |
|  |  | 05 | 0.4 | 01 | 56825 | 52067 | 55658 | 51.983 | 53.267 | 56825 |
|  |  | 06 | D 1 | 03 | 47.6.50 | 46500 | 50.050 | 46.400 | 46800 | 47.650 |
|  |  | 06 | 02 | 0.2 | 51.950 | 49600 | 53350 | 49.500 | 50200 | 51.950 |
|  |  | 0.6 | 03 | 01 | 56250 | 52.700 | 56650 | 52600 | 53 mbO | 56250 |
|  |  | 07 | 01 | 02 | 51.375 | 50.233 | 54. 342 | 50117 | 50533 | 51.375 |
|  |  | 07 | 02 | 01 | 55.675 | 53.333 | 57.642 | 53.217 | 53933 | 55.676 |
|  |  | 08 | 01 | 01 | 5510 Cb | 53967 | 58633 | 53.833 | 54267 | 55.100 |
| SUM |  |  |  |  | 17190 | 157600 | 1667.00 | 157400 | 161200 | 171900 |


| T | M | W1 | W2 | W/3 | SPT/EDD | EDDISPT | S[1] | \$[2] | S[3I | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 5 | 0.1 | 01 | 08 | 29.508 | 28517 | 29200 | 28.500 | 28.617 | 29.508 |
|  |  | 0.9 | 02 | 07 | 34.108 | 32.117 | 32.900 | 32.100 | 32317 | 34.108 |
|  |  | 01 | 03 | 0.6 | 38708 | 35.717 | 36600 | 35700 | 36.017 | 38708 |
|  |  | 01 | 04 | 0.5 | 43308 | 39317 | 40300 | 39300 | 39.717 | 43.30 B |
|  |  | 01 | 0.5 | 0.4 | 47.908 | 42917 | 44.000 | 42900 | 43.417 | 47.908 |
|  |  | 01 | 0.6 | 03 | 52508 | 46517 | 47.700 | 46500 | 47117 | 52.508 |
|  |  | 01 | 07 | 02 | 57108 | 50117 | 51.400 | 50100 | 50817 | 57.108 |
|  |  | 01 | 0.8 | 01 | 61,708 | 53717 | 55100 | 53700 | 54517 | 61.708 |
|  |  | 02 | 01 | 07 | 33417 | 32433 | 33700 | 32,400 | 32533 | 33417 |
|  |  | 02 | 0.2 | 06 | 38.017 | 36033 | 37.400 | 36000 | 36233 | 38.017 |
|  |  | 02 | 03 | 05 | 42617 | 39.633 | 41100 | 39.600 | 39933 | 42.517 |
|  |  | 02 | 04 | 04 | 47.217 | 43233 | 448000 | 43200 | 43633 | 47.217 |
|  |  | 0.2 | 05 | 03 | 51.817 | 46833 | 48500 | 46800 | 47.333 | 51.817 |
|  |  | 02 | 06 | 02 | 56417 | 50433 | 52200 | 50400 | 51033 | 56.417 |
|  |  | 0.2 | 07 | 01 | 61.017 | 54 ¢33 | 55.900 | 54000 | 54.733 | 61.017 |
|  |  | 0.3 | 0.1 | 06 | 37.325 | 36350 | 38200 | 36300 | 36450 | 37.325 |
|  |  | 03 | 02 | 05 | 41.925 | 39950 | 41.900 | 39900 | 40.150 | 41925 |
|  |  | 03 | 0.3 | 04 | 46525 | 43550 | 45600 | 435004 | 43850 | 46525 |
|  |  | 03 | 04 | 03 | 51125 | 47.150 | 49300 | 47100 | 47.550 | 51125 |
|  |  | 0.3 | 06 | 02 | 55.725 | 50750 | 53.000 | 50700 | 51.250 | 55725 |
|  |  | 0.3 | 06 | 01 | 60.325 | 54350 | 56.700 | 54300 | 54.950 | 60325 |
|  |  | 04 | 01 | 0.5 | 41233 | 40.267 | 42700 | 40.200 | 40.367 | 41.233 |
|  |  | 04 | 0.2 | 04 | 45833 | 43867 | 46.400 | 438006 | 44.057 | 45833 |
|  |  | 04 | 0.3 | 03 | 50433 | 47.467 | 50100 | 47.400 | 47767 | 50.433 |
|  |  | 04 | 04 | 0.2 | 55033 | 51.067 | 53800 | 51.000 | 51467 | 55033 |
|  |  | 04 | 0.5 | 0.1 | 59633 | 54667 | 57.500 | 54.600 | 55.167 | 59633 |
|  |  | 05 | 01 | 04 | 45142 | 44183 | 47.200 | 44.100 | 44.283 | 45142 |
|  |  | 05 | 02 | D3 | 49742 | 47.783 | 50900 | 47.700 | 47983 | 49742 |
|  |  | 05 | 03 | 02 | 54342 | 51.383 | 54600 | 51300 | 51683 | 54342 |
|  |  | 05 | 04 | 0.1 | 58.942 | 54.983 | 58300 | 54.900 | 55383 | 58942 |
|  |  | 06 | D. 1 | 0.3 | 49050 | 48100 | 51700 | 48000 | 48200 | 49050 |
|  |  | 06 | 02 | 02 | 53.650 | 51.700 | 55400 | 51600 | 51900 | 53650 |
|  |  | 06 | 0.3 | 0.1 | 58250 | 55300 | 59.100 | 55200 | 55.600 | 58250 |
|  |  | 0.7 | 01 | 02 | 52.358 | 52.017 | 56200 | 51900 | 52.117 | 52.958 |
|  |  | 0.7 | 0.2 | 0.1 | 57.558 | 55617 | 59.900 | 55500 | 55.817 | 57.55 B |
|  |  | 09 | 0.1 | 0.1 | 56.867 | 55933 | 60700 | 55800 | 56033 | 56867 |
|  |  | SUM |  |  | 1777.00 | 1658 6D | 174000 | 1656.00 | 167000 | 177700 |


| T | 相 | W1 | W2 | W3 | SPTJEDD | EDDISPT | S［1］ | $5[2]$ | $5[3]$ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 6 | 01 | 0.1 | 08 | 29.992 | 29.200 | 29808 | 29183 | 29200 | 29992 |
|  |  | 01 | 02 | 07 | 34892 | 33.300 | 33.908 | 33.283 | 33300 | 34892 |
|  |  | 01 | 03 | 06 | 39792 | 37.400 | 38.098 | 37.383 | 37400 | 39792 |
|  |  | 01 | 0.4 | 0.5 | 44.692 | 41.506 | 42.108 | 41483 | 41500 | 44.692 |
|  |  | 01 | 05 | 0.4 | 49592 | 45606 | 46．20B | 45.583 | 45600 | 49.592 |
|  |  | 0.1 | 06 | 03 | 54492 | 49.700 | 50.308 | 49683 | 49.700 | 54.492 |
|  |  | 0.1 | 0.7 | 0.2 | 59392 | 53806 | 54，408 | 53783 | 53800 | 59.392 |
|  |  | 0.1 | 08 | 0.1 | 64.292 | 57.906 | 58508 | 57.883 | 57900 | 64.292 |
|  |  | 02 | 01 | 0.7 | 34.083 | 33306 | 34.517 | 33.267 | 33300 | 34.083 |
|  |  | 0.2 | 0.2 | 06 | 38983 | 37.400 | 38617 | 37367 | 37400 | 3 B 983 |
|  |  | 02 | 0.3 | 05 | 43883 | 41.500 | 42717 | 41467 | 41.500 | 43883 |
|  |  | 0.2 | 0.4 | 04 | 48783 | 45.600 | 46.817 | 45567 | 45600 | 4 B 783 |
|  |  | 02 | 05 | 03 | 53683 | 49700 | 50.917 | 49667 | 49700 | 53683 |
|  |  | 0.2 | 06 | §2 | 58583 | 53800 | 55017 | 53.767 | 53800 | 5B583 |
|  |  | 02 | 07 | 01 | 63493 | 57906 | 59117 | 57.867 | 57900 | 63.483 |
|  |  | $\bigcirc 3$ | 01 | 9．方 | 38175 | 37400 | 39.225 | 37.350 | 37400 | 38.175 |
|  |  | 03 | 02 | 0.5 | 43075 | 41500 | 43.325 | 41.450 | 41500 | 43.075 |
|  |  | 0.3 | 03 | 04 | 47975 | 45.600 | 47425 | 45550 | 45.600 | 47975 |
|  |  | 0.3 | 04 | 03 | 52875 | 49.700 | 51525 | 49.650 | 49700 | 52875 |
|  |  | 0.3 | 05 | § 2 | 57775 | 53.800 | 55625 | 53.750 | 53.600 | 57775 |
|  |  | 03 | 06 | 01 | 62675 | 57.900 | 59725 | 57.850 | 57.900 | 62675 |
|  |  | 0.4 | 0.1 | 05 | 42267 | 41.500 | 43933 | 41.433 | 41.500 | 42267 |
|  |  | 04 | 0.2 | 0.4 | 47167 | 45600 | 48.033 | 45.533 | 45600 | 47．167 |
|  |  | 04 | 03 | 03 | 52.067 | 49700 | 52133 | 49633 | 49700 | 52067 |
|  |  | 0.4 | 0.4 | 02 | 56967 | 53.800 | 56233 | 53.733 | 53800 | 56.967 |
|  |  | 0.4 | 0.5 | 01 | 61867 | 57900 | 60.333 | 57833 | 57900 | 61.867 |
|  |  | 05 | 0.1 | 0.4 | 46358 | 45600 | 48.642 | 45517 | 45600 | 46.358 |
|  |  | 05 | 0.2 | 0.3 | 51258 | 49700 | 52.742 | 49617 | 49700 | 51.258 |
|  |  | 0.5 | 0.3 | 62 | 56158 | 53 B00 | 56.842 | 53717 | 53800 | 56158 |
|  |  | 0.5 | 04 | 01 | 61058 | 57.900 | 60.942 | 57817 | 57.900 | 61058 |
|  |  | 06 | 6． 1 | 03 | 50.450 | 49.700 | 53350 | 49600 | 49700 | 50450 |
|  |  | 96 | 02 | 0.2 | 56350 | 53800 | 57．450 | 53.700 | 53.800 | 55350 |
|  |  | 06 | 0.3 | 0.1 | 60250 | 57900 | 61.550 | 57800 | 57900 | 60.250 |
|  |  | 0.7 | 0.1 | 02 | 54542 | 53800 | 58.058 | 53.683 | 53800 | 54.542 |
|  |  | 0.7 | 0.2 | 01 | 59442 | 57.900 | 62.158 | 57.783 | 57.900 | 59.442 |
|  |  | 08 | 0.1 | 0.1 | 58633 | 57.900 | 62.767 | 57.767 | 57900 | 58.633 |
| SUM |  |  |  |  | 183500 | 174000 | 181300 | 1738．00 | 174000 | 1835.00 |


| T | M | W1 | W2 | W／3 | SPTJEDD | EDDISPT | S［1］ | \＄［2］ | S［3］ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 7 | 0.1 | 01 | 08 | 30475 | 29883 | 30517 | 29867 | 29883 | 30475 |
|  |  | 0.1 | 02 | 07 | 35 ¢75 | 34，483 | 35117 | 34467 | 34.483 | 35675 |
|  |  | 0.1 | 0.3 | 06 | 40875 | 39.083 | 39717 | 39067 | 39083 | 40875 |
|  |  | 01 | 0.4 | 05 | 46.075 | 43683 | 44317 | 43667 | 43683 | 46.075 |
|  |  | 0.1 | 0.5 | 04 | 51275 | 48.283 | 48917 | 48267 | 48283 | 51275 |
|  |  | 01 | 06 | 03 | 56475 | 52.883 | 53517 | 52867 | 52.883 | 56475 |
|  |  | 01 | 07 | 02 | 61675 | 57.483 | 58117 | 57467 | 57.483 | 611．675 |
|  |  | 01 | 08 | 0.1 | 66875 | 62083 | 62717 | 62.067 | 62.083 | 68875 |
|  |  | 02 | 0.1 | 07 | 34750 | 34.167 | 35433 | 34133 | 34.167 | 34．750 |
|  |  | 02 | 02 | 06 | 39.950 | 38767 | 40.033 | 38733 | 38.767 | 39950 |
|  |  | 02 | 0.3 | 05 | 45150 | 43367 | 44.633 | 43333 | 43.367 | 45150 |
|  |  | 02 | 04 | 04 | 50350 | 47967 | 49.233 | 47933 | 47.967 | 50350 |
|  |  | 02 | 0.5 | 0.3 | 55550 | 52567 | 53.833 | 52533 | 52.567 | 55.550 |
|  |  | 0.2 | 0.6 | 0.2 | 60750 | 57.167 | 58.433 | 57133 | 57.167 | 60.750 |
|  |  | 02 | 07 | 0.1 | 65950 | 61.767 | ¢3 033 | 61.733 | 61767 | 65950 |
|  |  | 03 | 01 | 06 | 39.025 | 38450 | 40350 | 38.400 | 38.450 | 39.025 |
|  |  | 03 | 02 | 05 | 44.225 | 43050 | 44950 | 43000 | 43.050 | 44225 |
|  |  | 03 | 03 | 04 | 49.425 | 47650 | 49550 | 47600 | 47.650 | 49125 |
|  |  | 03 | D 4 | 0.3 | 54.625 | 52.250 | 54150 | 52200 | 52250 | 54.626 |
|  |  | 0.3 | 05 | 02 | 59825 | \＄6850 | 58.750 | 56800 | 56.850 | 59.825 |
|  |  | 03 | 06 | 0.1 | 65.025 | 61.450 | 63350 | 61．400 | 61450 | 65.025 |
|  |  | 04 | 01 | 05 | $43.30 円$ | 42.733 | 45267 | 42667 | 42733 | 43.300 |
|  |  | 0.4 | 02 | 04 | 48．500 | 47.333 | 49867 | 47.267 | 4 4 333 | 48.500 |
|  |  | 04 | 03 | 0.3 | 53.700 | 51.933 | 54.467 | 51867 | 51.933 | 53，700 |
|  |  | 04 | 04 | 02 | 58.900 | 56.533 | 59067 | 56467 | 56533 | 58.900 |
|  |  | 04 | 05 | 0.1 | 64.100 | 61.133 | 63.667 | 61.067 | 61.133 | 64.100 |
|  |  | 05 | 01 | 04 | 47.575 | 47.017 | 50.183 | 46933 | 47017 | 47.575 |
|  |  | 05 | 02 | 03 | 52.775 | 51.617 | 54.783 | 51533 | 51617 | 52.775 |
|  |  | 05 | 03 | 02 | 57.975 | 56217 | 59.383 | 56133 | 55.217 | 57.975 |
|  |  | 0.5 | 04 | 01 | 63175 | 60817 | 63.983 | 60.733 | 60817 | 63175 |
|  |  | 06 | 0.1 | 03 | 51850 | 51.360 | 55100 | 51.200 | 51.300 | 51.850 |
|  |  | 06 | 02 | 0.2 | 57.050 | 55900 | 59730 | 55800 | 55900 | 57050 |
|  |  | 06 | 03 | 0.1 | 62250 | 60500 | 64300 | 60400 | 60500 | 62.250 |
|  |  | 0.7 | 0.1 | 0.2 | 56.125 | 55583 | 60017 | 55.467 | 55.583 | 54125 |
|  |  | 07 | 02 | 0.1 | 61325 | 60183 | 64617 | 60067 | 60.183 | 61325 |
|  |  | 0.8 | 0.1 | 01 | 60400 | 59857 | 64933 | 59733 | 59867 | 60．400 |
| SUM |  |  |  |  | 1893 DD | 182200 | 189800 | 1820.00 | 1822．00 | 199300 |


| T | M | W1 | W2 | W3 | SPTIEDD | EDDISPT | S[1] | \$[2] | $5[3]$ | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 8 | 01 | 01 | 08 | 30958 | 30567 | 31225 | 30.550 | 30567 | 30.958 |
|  |  | 01 | 02 | 0.7 | 36458 | 35667 | 36325 | 35650 | 35.667 | 35458 |
|  |  | 0.1 | 0.3 | 0.6 | 41.958 | 40.767 | 41.425 | 40750 | 40767 | 41958 |
|  |  | 01 | 0.4 | 0.5 | 47.458 | 45867 | 45525 | 45850 | 45867 | 47.4.58 |
|  |  | 01 | 0.5 | 0.4 | 52959 | 50.967 | 51.625 | 50.950 | 50967 | 52.958 |
|  |  | 01 | 06 | 03 | 58458 | 56067 | 56.725 | 56.050 | 56067 | 58.458 |
|  |  | 01 | 07 | 0.2 | 63 958 | 61.167 | 61.825 | 61.150 | 61.167 | 63958 |
|  |  | 01 | 08 | 01 | 69.458 | 65.267 | 66925 | 66250 | 66267 | 69 458 |
|  |  | 0.2 | 01 | 07 | 35417 | 35033 | 16350 | 35000 | 35033 | 35.417 |
|  |  | 02 | 02 | 06 | 40.917 | 40133 | 41.450 | 40100 | 40133 | 40.917 |
|  |  | 02 | 03 | 05 | 46.417 | 45233 | 46550 | 45200 | 45.233 | 46417 |
|  |  | 02 | 04 | 04 | 51.917 | 50333 | 51650 | 50300 | 50333 | 51917 |
|  |  | 02 | 05 | 03 | 57.417 | 55433 | 56.750 | 55.400 | 55433 | 57.417 |
|  |  | 02 | D 6 | 02 | 62.917 | 60533 | 61850 | 60.500 | 60533 | 62.917 |
|  |  | 02 | D 7 | 01 | 68417 | 65633 | 66.950 | 65.600 | 65633 | 68.417 |
|  |  | 03 | 01 | D6 | 39875 | 39500 | 41475 | 39.450 | 39500 | 39.875 |
|  |  | 03 | 0.2 | 05 | 45.375 | 44.600 | 46575 | 44.550 | 44.600 | 45375 |
|  |  | 0.3 | 03 | 0.4 | 50.875 | 49700 | 51.675 | 49650 | 49700 | 50.875 |
|  |  | 03 | 04 | 03 | 56375 | 54800 | 56775 | \$4.750 | 54 BOO | 56.375 |
|  |  | 03 | 05 | 0.2 | 61.875 | 59900 | 61.875 | 59850 | 59.900 | 61875 |
|  |  | 0.3 | 06 | 01 | 67.375 | 65000 | 66975 | 64950 | 65.000 | 67375 |
|  |  | 0.4 | 01 | 05 | 44.333 | 43.967 | 46600 | 43900 | 43.967 | 44333 |
|  |  | 0.4 | 02 | 0.4 | 49833 | 49067 | 51.700 | 49.000 | 49.067 | 49.6837 |
|  |  | 04 | 03 | 03 | 55333 | 54.167 | 55800 | 54.100 | 54.167 | 55333 |
|  |  | 04 | 04 | 02 | 60833 | 59.267 | 61900 | 59.200 | 59.267 | 61833 |
|  |  | 0.4 | 05 | 0.1 | 65333 | 64367 | 67.000 | 64.300 | 64367 | 66.333 |
|  |  | 05 | D. 1 | 04 | 48792 | 4 B 433 | 51.725 | 48.350 | 48433 | 48.792 |
|  |  | 05 | 02 | 03 | 54292 | 53.533 | 56825 | 53450 | 53.533 | 54292 |
|  |  | 05 | 03 | 02 | 59.792 | 58633 | 61925 | 58.550 | 58633 | 59792 |
|  |  | 05 | 04 | 01 | 65292 | 63733 | 67.025 | 63650 | 63733 | 65292 |
|  |  | 06 | D 1 | 03 | 53250 | 52900 | 56850 | 52.800 | 52500 | 53250 |
|  |  | 06 | 02 | 02 | 58750 | 58000 | 61.950 | 67,900 | 58 DDO | 50750 |
|  |  | 06 | D 3 | 0.1 | 64250 | 63.109 | 67050 | 63.000 | 63100 | 64250 |
|  |  | 07 | 0.1 | 02 | 57.708 | 57367 | 61975 | 57.250 | 57.367 | 57708 |
|  |  | 07 | 02 | 0.1 | 63208 | 62467 | 67.075 | 62350 | 62467 | 63.208 |
|  |  | 08 | 01 | 01 | 62.167 | 61833 | 67100 | 61.700 | 61833 | 62167 |
|  |  | SUM |  |  | 1951.00 | 1974.09 | 198300 | 190200 | 1904 D0 | 195100 |


| T* | m | W1 | W2 | W3 | SPTİEDD | EDDISPT | S[1] | \$[2] | 5[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 22 | 4 | 01 | 01 | 0.8 | 33508 | 32517 | 32.517 | 32.500 | 32617 | 33.509 |
|  |  | 0.1 | 02 | 07 | 37608 | 35.617 | 35617 | 35600 | 35817 | 37.608 |
|  |  | 0.1 | 03 | 06 | 41708 | 38.717 | 38717 | 38.700 | 39017 | 41708 |
|  |  | 01 | 04 | 05 | 45.809 | 41817 | 41817 | 41.800 | 42217 | 45808 |
|  |  | 01 | 05 | 0.4 | 49.903 | 44917 | 44.917 | 44900 | 45417 | 49908 |
|  |  | 01 | 0.6 | 0.3 | 54008 | 48017 | 48.017 | 48000 | 48617 | 54.D09 |
|  |  | 01 | 07 | 0.2 | 58108 | 51117 | 51117 | 51,100 | 51.817 | 58108 |
|  |  | 0.1 | 0.8 | 01 | 62208 | 54217 | 54,217 | 54200 | 55017 | 62.208 |
|  |  | 0.2 | 01 | 07 | 36.917 | 35933 | 35933 | 35.900 | 35033 | 36917 |
|  |  | 0.2 | 02 | 06 | 41017 | 39.033 | 39033 | 39000 | 39233 | 41017 |
|  |  | 02 | 03 | 05 | 45.177 | 42.133 | 42133 | 42100 | 42.433 | 45117 |
|  |  | 0.2 | 04 | 04 | 49217 | 45.233 | 45233 | 45200 | 45.633 | 49217 |
|  |  | 0.2 | 0.5 | 03 | 53317 | 48333 | 48.333 | 48300 | 48833 | 53.317 |
|  |  | 0.2 | 0.6 | 02 | 57417 | 51.433 | 51.433 | 51400 | 52.033 | 57.417 |
|  |  | 0.2 | 0.7 | 01 | 61547 | 54533 | 54.533 | 54500 | 55.233 | 61.517 |
|  |  | 0.3 | 0.1 | 06 | 40325 | 39350 | 39.350 | 39300 | 39.450 | 40.325 |
|  |  | 03 | 02 | 05 | 44425 | 42.450 | 42450 | 42400 | 42.650 | 44425 |
|  |  | 03 | 0.3 | 0.4 | 48525 | 45550 | 45550 | 45.500 | 45.850 | 48525 |
|  |  | 0.3 | 0.4 | 0.3 | 52625 | 48.650 | 48.650 | 48600 | 49.050 | 52625 |
|  |  | 03 | 05 | 02 | 56725 | 51.750 | 51750 | 51700 | 52.250 | 56.725 |
|  |  | 03 | 06 | 0.1 | 50.825 | 54850 | 54 BSO | 54800 | 55.450 | 60825 |
|  |  | 04 | 0.1 | 0.5 | 43733 | 42767 | 42.767 | 42700 | 42.867 | 43733 |
|  |  | 0.4 | 02 | 04 | 47833 | 45.867 | 45867 | 45800 | 46067 | 47.833 |
|  |  | 0.4 | 03 | 03 | 51933 | 48.967 | 48967 | 48.900 | 49267 | 51933 |
|  |  | 0.4 | 04 | 02 | 56033 | 52.067 | 52067 | 52000 | 52.467 | \$6.033 |
|  |  | 04 | 05 | 01 | 60 133 | 55167 | 55167 | 55100 | 55667 | 60133 |
|  |  | 0.5 | 01 | 04 | 47142 | 46.183 | 46183 | 46100 | 45283 | 47142 |
|  |  | 05 | 02 | 03 | 51242 | 49.283 | 49283 | 49200 | 49463 | 51.242 |
|  |  | 05 | 03 | 02 | 55342 | 52.383 | 52383 | 52300 | 52.683 | 55.342 |
|  |  | 05 | 04 | 01 | 59442 | 55.483 | 55483 | 55400 | 55883 | 59.442 |
|  |  | 06 | 01 | 03 | 50.550 | 49600 | 49600 | 49.500 | 49700 | 50.550 |
|  |  | 06 | 02 | 02 | 54.650 | 52.700 | 52700 | 52800 | 52900 | 54650 |
|  |  | 0.6 | 0.3 | 01 | 56750 | 55.800 | 55800 | 55.700 | 56100 | 58.750 |
|  |  | 0.7 | 01 | 02 | 53958 | 53017 | 53017 | 52900 | 53117 | 53.958 |
|  |  | 07 | 02 | 01 | 581058 | 56117 | 56117 | 56000 | 56317 | 58058 |
|  |  | 08 | 01 | 01 | 57367 | 56433 | 56433 | 56300 | 56.533 | 57367 |
|  |  | SUM |  |  | 183700 | 171800 | 1718.00 | 1716.00 | 1730.00 | 183700 |


| T | M | W/1 | W2 | W3 | SPTIEDD | EDDISPT | S[1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 22 | 5 | 01 | 01 | 0.8 | 33992 | 33200 | 33.200 | 33183 | 33200 | 33992 |
|  |  | 0.1 | 02 | 0.7 | 38.392 | 3680 | 36.800 | 36.783 | 36800 | 36,392 |
|  |  | 01 | 03 | 0.6 | 42,792 | 40400 | 40400 | 40383 | 40400 | 42792 |
|  |  | 0.1 | 04 | 05 | 47.192 | 44.000 | 44000 | 43.983 | 44000 | 47192 |
|  |  | 01 | 05 | 0.4 | 51592 | 47600 | 47600 | 47583 | 47600 | 51592 |
|  |  | 01 | 06 | 0.3 | 55.992 | 51200 | 51.200 | \$1,183 | 51200 | 55.992 |
|  |  | 01 | 07 | 02 | 60392 | 54.860 | 54800 | 54.783 | 54800 | 60.392 |
|  |  | 0.1 | 08 | 01 | 64792 | 58.400 | 58400 | 58383 | 58.400 | 64792 |
|  |  | 02 | 01 | 07 | 37.583 | 36800 | 36800 | 36.767 | 36800 | 37.583 |
|  |  | 02 | 02 | 06 | 41.983 | 40400 | 40.400 | 40367 | 49400 | 41.983 |
|  |  | 0.2 | 0.3 | 05 | 46383 | 44.000 | 44000 | 43967 | 44000 | 46383 |
|  |  | 02 | 0.3 | 0.4 | 50783 | 47.600 | 47.600 | 47567 | 47.600 | 50783 |
|  |  | 0.2 | 0.5 | 0.3 | 55.183 | 51.200 | 51.200 | 51.167 | 51.200 | 55123 |
|  |  | 0.2 | 06 | 0.2 | 59.583 | 54.800 | 5-4800 | 54767 | \$4800 | 59583 |
|  |  | 0.2 | 0.7 | 0.1 | 63.983 | 58.400 | 58400 | 56.367 | 58400 | 63983 |
|  |  | 03 | 01 | 06 | 41.175 | 40400 | 40400 | 40.350 | 40400 | 41.175 |
|  |  | 03 | 02 | 05 | 45575 | 44000 | 44.000 | 43.950 | 44000 | 45.575 |
|  |  | 0.3 | 03 | 04 | 49.975 | 47.600 | 47.600 | 47.550 | 47600 | 49.975 |
|  |  | 03 | 0.4 | 03 | 54.375 | 51.200 | 51200 | 51.150 | 51200 | 54.375 |
|  |  | 03 | 05 | 02 | 58.775 | 54800 | 54.800 | 54.750 | 54800 | 58.775 |
|  |  | 03 | 0.6 | 01 | 63175 | 58400 | 58.400 | 58.350 | 58400 | 63.175 |
|  |  | D 4 | 61 | 05 | 44767 | 44000 | 44000 | 43933 | 44,000 | 44767 |
|  |  | 04 | 0.2 | 04 | 49167 | 47600 | 47.600 | 47.533 | 47600 | 49.167 |
|  |  | 04 | 03 | 0.3 | 53567 | 51200 | 51.200 | 51.133 | 51200 | 53567 |
|  |  | 04 | 04 | 02 | 57.967 | 54800 | 54800 | 54733 | 54.800 | 57967 |
|  |  | 04 | 95 | 01 | 62.367 | 58400 | 58.400 | 58333 | 58.400 | 62367 |
|  |  | 05 | 01 | 0.4 | 48358 | 47600 | 47600 | 47.517 | 47.600 | 48358 |
|  |  | 05 | 02 | 03 | 52758 | 51.200 | 51.200 | 51117 | 51.200 | 52758 |
|  |  | 05 | 03 | 0.2 | 57.158 | 54800 | 54800 | 54.717 | 54800 | 57158 |
|  |  | 0.5 | 0.4 | 01 | 61558 | 58400 | 59.40\% | 58317 | 58400 | 61558 |
|  |  | 06 | 01 | 03 | 51950 | 51.200 | 51.200 | 51100 | 51.200 | 51.950 |
|  |  | 06 | 02 | 02 | 56.350 | 54800 | 54800 | 54700 | 54.800 | 56350 |
|  |  | 06 | 03 | 01 | 60750 | 58400 | 58400 | 58306 | 58400 | 60750 |
|  |  | 07 | 01 | 42 | 55542 | 54,800 | 54800 | 54683 | 54.800 | 55.542 |
|  |  | 0.7 | 02 | 01 | 59942 | 58.400 | 58.400 | 58283 | 58.400 | 59942 |
|  |  | 08 | 01 | 0.1 | 59133 | 58400 | 58400 | 58.267 | 58400 | 59133 |
|  |  | SUM |  |  | 1895.00 | 180300 | 180000 | 1798.00 | 180000 | 189500 |


| T | M | W1 | W2 | W3 | SPTJEDD | EDDISPT | S[1] | S[2] | S[3] | \$[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 22 | 6 | 01 | 0.1 | 08 | 34475 | 33883 | 33883 | 33.867 | 33883 | 34.475 |
|  |  | 01 | 0.2 | 07 | 39175 | 37983 | 37.983 | 37967 | 37983 | 39.175 |
|  |  | 01 | 03 | 06 | 43875 | 42 ¢В3 | 42083 | 42.067 | 42083 | 43.875 |
|  |  | 0.1 | 04 | 05 | 48575 | 46183 | 46183 | 46.167 | 46183 | 48.575 |
|  |  | 0.1 | 0.5 | 0.4 | 53275 | 50283 | 50283 | 50267 | 50283 | 53275 |
|  |  | 0.1 | 06 | 0.3 | 57.975 | 54383 | 54.383 | 54367 | 54383 | 57.975 |
|  |  | 0.1 | 07 | 02 | 62.675 | 58483 | 58.483 | 58467 | 58483 | 62.675 |
|  |  | 01 | 08 | 01 | 67.375 | 62.583 | 62.583 |  | 62583 | 67375 |
|  |  | 02 | 01 | 07 | 38250 | 37.667 | 37.667 | 37633 | 37667 | 38.250 |
|  |  | 02 | 0.2 | 0.5 | 42.950 | 41.767 | 41.767 | 41733 | 41.767 | 42,950 |
|  |  | 02 | 03 | 05 | 47.650 | 45867 | 45867 | 45.833 | 45867 | 47650 |
|  |  | 0.2 | 0.4 | 04 | 52.350 | 49.967 | 49.967 | 49.933 | 49967 | 52350 |
|  |  | 02 | 0.5 | 0.3 | 57.050 | 54067 | 54067 | 54033 | 54.067 | 57.050 |
|  |  | 02 | 06 | 02 | 61750 | 58.167 | 58167 | 58.133 | 58167 | 61.750 |
|  |  | 02 | 07 | 01 | 66450 | 62267 | 62.267 | 62233 | 62267 | 66450 |
|  |  | 03 | 01 | 06 | 42025 | 41450 | 41.450 | 41.400 | 41450 | 42025 |
|  |  | 03 | 02 | 05 | 48725 | 45.550 | 46.550 | 45500 | 45550 | 46725 |
|  |  | 03 | 03 | 0.4 | 51.425 | 49650 | 49650 | 49600 | 49650 | 51.425 |
|  |  | 03 | 0.4 | 0.3 | 56.125 | 53750 | 53750 | 53700 | 53750 | 56.125 |
|  |  | 03 | 0.5 | 02 | 60325 | 57850 | 57.850 | 57.900 | 57850 | 60325 |
|  |  | 03 | 0.6 | 0.1 | 65.525 | 61950 | 61950 | 61.900 | 61950 | 65.525 |
|  |  | 04 | 0.1 | 05 | 45800 | 45233 | 45.233 | 45.167 | 45233 | 45800 |
|  |  | 04 | 0.2 | 0.4 | 50500 | 49333 | 49333 | 49267 | 49333 | 5050 |
|  |  | 0.4 | 03 | 03 | 55200 | 53433 | 53.433 | $53 \$ 67$ | 53433 | 55200 |
|  |  | 0.4 | 0.4 | 02 | 59900 | 57.533 | 57.533 | 57.467 | 57533 | 59900 |
|  |  | 04 | 45 | 01 | 64600 | 61.6 | 61633 | 61.567 | 61633 | 64500 |
|  |  | 05 | 61 | 04 | 49.575 | 49.017 | 49.017 | 48.933 | 49.617 | 49.575 |
|  |  | 65 | ¢ 2 | 03 | 54.275 | 53.117 | 53.117 | 53.033 | 53117 | 54275 |
|  |  | 05 | 03 | 02 | 58975 | 57.217 | 57.217 | 57.133 | 57,217 | 58975 |
|  |  | 05 | 0.4 | 0.1 | 63675 | 61397 | 61317 | 61.233 | 61.317 | 63675 |
|  |  | 0 O | 0.1 | 0.3 | 53.350 | 52.800 | 52800 | 52.700 | 52800 | 53350 |
|  |  | 06 | 02 | 02 | 58050 | 56900 | 56900 | 56.860 | 56900 | 58.050 |
|  |  | 06 | 03 | 01 | 62.750 | 61.000 | 61000 | 60.900 | 61000 | 62750 |
|  |  | 07 | 01 | 02 | 57125 | 56.583 | 56.583 | 56467 | 56583 | 57125 |
|  |  | 67 | 0.2 | 0.1 | 61.82 .5 | 60683 | 60683 | 60567 | 50683 | 61.825 |
|  |  | 08 B | 0.1 | 0.1 | 60.900 | 60367 | 60367 | 60233 | 60367 | 50.900 |
| SUM |  |  |  |  | 195300 | 1882.00 | 188200 | 1880.00 | 188200 | 195300 |


| ¢ | M | W1 | W2 | W3 | SPTKED | EDDISPT | S[1] | S[2] | S[3] | \$[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 22 | 7 | 01 | 01 | 08 | 34.958 | 34567 | 34,567 | 34550 | 34567 | 34.958 |
|  |  | 0.1 | 02 | 07 | 39.958 | 39167 | 39167 | 39150 | 39.167 | 39958 |
|  |  | 01 | 0.3 | 06 | 44958 | 43.767 | 43767 | 43750 | 43.767 | 44958 |
|  |  | 01 | 0.4 | 05 | 49958 | 49.367 | 48367 | 48350 | 48367 | 49958 |
|  |  | 0.1 | 0.5 | [6. 4 | 54958 | 52.967 | 52967 | 52.950 | 52.967 | 54958 |
|  |  | 0.1 | 06 | 03 | 59.958 | 57567 | 57567 | 57.550 | 57.567 | 59958 |
|  |  | 01 | 07 | 02 | 64,958 | 62167 | 62167 | 62, 150 | 62.167 | 64958 |
|  |  | 01 | 0 B | 01 | 69.958 | 66767 | 66767 | 66.750 | 66.767 | 59958 |
|  |  | 02 | 01 | 07 | 38.917 | 38533 | 38533 | 38.500 | 38533 | 38917 |
|  |  | 02 | 02 | 06 | 43917 | 43.133 | 43133 | 43100 | 43.133 | 43917 |
|  |  | 02 | 03 | 05 | 48917 | 47733 | 47.733 | 47,700 | 47733 | 48917 |
|  |  | 02 | 04 | 04 | 53917 | 52333 | 52333 | \$2.300 | 52333 | 53917 |
|  |  | 02 | 05 | 03 | 58917 | 56933 | 56933 | 56.900 | 56933 | 58.917 |
|  |  | 02 | 06 | 0.2 | 的 917 | 64.533 | 61.533 | 61500 | 61.533 | 63917 |
|  |  | 02 | 0.7 | 0.1 | 68917 | 66.133 | 66.133 | 驼100 | 66.133 | 68.917 |
|  |  | 0.3 | 0.1 | 06 | 42.975 | 42.50 ¢ | 42.500 | 42.450 | 42,500 | 42875 |
|  |  | 03 | 02 | 05 | 47.875 | $47.10 \square$ | 47.100 | 47.050 | 47100 | 47.875 |
|  |  | 03 | 03 | 0.4 | 52.875 | 51.700 | 51.700 | 51650 | 51700 | 52.875 |
|  |  | 03 | 0.4 | 0.3 | 57.875 | $55_{6.300}$ | 56.360 | 56250 | 56300 | 57.675 |
|  |  | 0.3 | 0.5 | 0.2 | 62.875 | 60.900 | 60.901 ] | 60850 | 60.900 | 62875 |
|  |  | 03 | 06 | 01 | 67.875 | 65.500 | 65506 | ¢5 450 | 6.5 .500 | 67875 |
|  |  | 0.4 | 01 | 05 | 46833 | 46467 | 45467 | 46400 | 46.467 | 46833 |
|  |  | 0.4 | 02 | 04 | 51.833 | 51067 | 51067 | 51.090 | 51067 | 51.833 |
|  |  | 04 | 03 | 03 | 568.33 | 55667 | 55667 | 55600 | 55067 | 56.83 .3 |
|  |  | 04 | 04 | © 2 | 61833 | ¢0.267 | 60267 | 60.200 | 60267 | 61833 |
|  |  | D 4 | 05 | 01 | 66833 | 64.867 | 64.867 | 64800 | 64.867 |  |
|  |  | 0.5 | 01 | 04 | 50792 | 50433 | 50.433 | 50350 | 50433 | 50792 |
|  |  | 0.5 | 0.2 | 03 | 55792 | 55033 | 55033 | 54.950 | 55033 | 55 792 |
|  |  | 0.5 | 0.3 | 02 | 60792 | 59633 | 59633 | 59.550 | 59633 | 60792 |
|  |  | 05 | 0.4 | 0.1 | 66.792 | 64233 | 64233 | 64150 | 64.233 | 65.792 |
|  |  | 06 | 01 | 0.3 | 54.750 | 54400 | 54400 | 54300 | 54400 | 54.750 |
|  |  | 06 | 0.2 | 0.2 | 59750 | 59000 | 59000 | 58.900 | 59000 | 59750 |
|  |  | 0.6 | 0.3 | 0.1 | 64750 | 63600 | 63600 | 63.500 | 63600 | 64750 |
|  |  | 07 | 01 | 02 | 58.708 | 58367 | 58.367 | 58250 | 58.367 | 58708 |
|  |  | 07 | 02 | 0.1 | 6.7 .708 | 62967 | 62567 | 62850 | 62.967 | 63,708 |
|  |  | 0.8 | 0.1 | 01 | 62667 | 62333 | 62333 | 62200 | 62.333 | 62667 |
| SUM |  |  |  |  | 201100 | 1964.00 | 1964.00 | 1982.00 | 1964.00 | 201100 |


| 1 | \% | W1 | W2 | W\% | SPTJEDD | EDDFSPT | S[1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 22 | 8 | 01 | 01 | 08 | 35.442 | 35250 | 35250 | 35233 | 35250 | 35.442 |
|  |  | 01 | 02 | 07 | 40742 | 40350 | 40.350 | 40333 | 40350 | 40.742 |
|  |  | 01 | 0.3 | 06 | 46.042 | 45450 | 45450 | 45433 | 45450 | 46042 |
|  |  | 01 | 0.4 | 05 | 51342 | 50550 | 50.550 | 50533 | 50550 | 51.342 |
|  |  | 0.1 | 05 | 0.4 | 56.642 | 55650 | 55.650 | 55633 | 55.650 | 56.642 |
|  |  | 0.1 | D6 | 0.3 | 61.942 | 60750 | 60.750 | 60733 | 60750 | 51942 |
|  |  | 0. 1 | 07 | 02 | 67.242 | 65850 | 65950 | Б5 833 | 65850 | 67242 |
|  |  | 01 | 18 | 01 | 72542 | 70950 | 70.950 | 70933 | 70.950 | 72542 |
|  |  | 02 | 01 | 07 | 35583 | 39400 | 39.400 | 39367 | 39.40' | 39593 |
|  |  | 02 | 02 | 06 | 44883 | 44500 | 44500 | 44.467 | 44500 | 44883 |
|  |  | 02 | 0.3 | 05 | 50183 | 49600 | 49600 | 49567 | 49.600 | 50183 |
|  |  | $\bigcirc 2$ | 04 | 04 | 55483 | 54,700 | 54700 | 54.667 | 54700 | 55483 |
|  |  | 02 | 0.5 | 03 | 60783 | 59800 | 59806 | 59.767 | 59.800 | 50.783 |
|  |  | $\bigcirc 2$ | 06 | 02 | 66083 | 64.900 | 64.900 | 64.867 | 64900 | 66.063 |
|  |  | 02 | 07 | 01 | 71.383 | 70.000 | 70000 | 69.967 | 70.050 | 71383 |
|  |  | 03 | 01 | 0.6 | 43.725 | 43550 | 43550 | 4350 [ | 43.550 | 43725 |
|  |  | 0.3 | 0.2 | 0.5 | 49.025 | 48650 | 48650 | 48600 | 48.650 | 49.025 |
|  |  | 03 | 03 | 0.4 | 54.325 | 53750 | 53750 | 53700 | 53.750 | 54325 |
|  |  | 03 | 04 | 0.3 | 59625 | 58.850 | 58.850 | 58.000 | 58850 | 59625 |
|  |  | 63 | 05 | 62 | 64925 | 63950 | 63950 | 63.900 | 63.950 | 64925 |
|  |  | 0.3 | 0.6 | 0.1 | 70225 | 69050 | 69550 | 69000 | 69050 | 70.225 |
|  |  | 0.4 | 01 | 0.5 | 47.867 | 47.700 | 47700 | 47633 | 47.700 | 47.887 |
|  |  | 0.4 | 02 | 0.4 | 53167 | 52 BOO | 52800 | 52733 | 52800 | 53167 |
|  |  | 04 | 03 | 03 | 58467 | 57900 | 57900 | 57.833 | 57.900 | 58467 |
|  |  | 04 | 04 | 62 | 63767 | 63000 | 63.000 | 62.933 | 63.000 | 63767 |
|  |  | 04 | 05 | 01 | 69.067 | 68.100 | 68100 | 68033 | 68.100 | 69.667 |
|  |  | 05 | 0.1 | 0.4 | 52,008 | 51850 | 51850 | 51767 | 51.850 | 52.008 |
|  |  | 05 | 02 | 03 | 57308 | 56 g 50 | 56950 | 56.867 | 55.950 | 57308 |
|  |  | 05 | 03 | 02 | 62.509 | 62.050 | 62.050 | 61.967 | 62 050 | 626 CB |
|  |  | 05 | 04 | 01 | 67.908 | 67150 | 67150 | 67067 | 67.150 | 67.908 |
|  |  | 0.6 | 01 | 03 | 56150 | 56000 | 56000 | 55900 | 56000 | 56150 |
|  |  | 06 | 02 | 02 | 61450 | 61100 | 61100 | 61.000 | 61100 | 61.450 |
|  |  | 06 | 03 | 01 | 66750 | 66.200 | 66200 | 66.100 | 66200 | 66.750 |
|  |  | 07 | 01 | 02 | 60292 | 60150 | 60.150 | 60.033 | 60.150 | 60292 |
|  |  | 07 | 0.2 | 0.1 | 65592 | 65.250 | 65250 | 65.133 | 65.250 | 65.592 |
|  |  | 08 | 01 | 01 | 64433 | 64300 | 64.300 | 64167 | 64300 | 64433 |
| SपW |  |  |  |  | 206904 | 2046.0.0 | 2046.09 | 2044.00 | 204500 | 206900 |


| 009091 | 00997 L | $00^{\circ} \mathrm{LOZL}$ | 009185 | 00＇2ヶ6ロ | 04 90S1 | WกS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 00009 | EC6 $1 \$$ | 49G＇ct | EEL 6G | 29809 | 00009 | 10 | 10 | 80 |  |  |
| 05015 | 26697 | 80190 | 19969 | と日19 | －90＇L9 | 10 | 20 | 20 |  |  |
| 0965 | 26E Et | 800＇st | 290＇99 | 895゙く9 | Q¢b gt | で0 | 50 | LO |  |  |
| 00179 | 05090 | 099 v\％ | 00209 | 08519 | OOL＇ZS | 10 | 80 | 90 |  |  |
| 009\％ | 0St で | 0¢S＇t | 00999 | 006\％ 29 | 0099\％ | 20 | 20 | 90 |  |  |
| 00601 | 0988 cc |  | 00085 | 005゙サら | 0060 O | 80 | 10 | 90 |  |  |
| 05185 | 8015 | 26l ct | EEL 09 | 11819 | OS1－をS | 10 | －0 | 50 |  |  |
| O5920 | $809 \downarrow$ | $2600 \%$ | ¢§ト2G | 1．285 | 955 $2 ⿰$ | 20 | 50 | $\mathrm{c}_{5} 0$ |  |  |
| OG6 LV | $3064 \Sigma$ | 266＇9¢ | EESES | 119\％9 | OG5゙引 | 80 | 20 | 90 |  |  |
| DSE GE | 80¢＇5¢ | 26日 £ | ES6 6t | 210＇LG | OSc－98 | 70 | 10 | 50 |  |  |
| 002 05 | 191．to | CEL した | 492゙19 | EELZG | 90 でャ9 | 10 | 90 | 70 |  |  |
| 009＇日y | 49500 | EE9 ${ }_{\text {c }}$ | 299＇19 | EES 8S | 0098 | 20 | $\dagger 0$ | $\dagger 0$ |  |  |
| 0001 e | 49698 | と禹ら「 | 29069 | EE6゙ロS | 00080 | ¢ 0 | 80 | $\dagger 0$ |  |  |
| DOt Le | LSE EE | を¢ってく | 29605 | EEE LG | 00\％＇28 | $\bigcirc 0$ | 20 | $t 0$ |  |  |
| 008 LE | 49262 | ECE 6 C | 4989 | ¢EL20 | 008 1E | 50 | 10 | $\nabla^{\prime} 0$ |  |  |
| OSZ 5s | 9てで施 | çZ Ot | 00819 | $05 \%$ | OSZ SG | 10 | 90 | $\varepsilon 0$ |  |  |
| $0996 t$ | 929 6E | 92tie | 002 85 | 058 85 | Of9 6\％ | 20 | 50 | $\varepsilon 6$ |  |  |
| OGO \％ | 52098 | 920 tc | 009159 | 052 95 | OFO＇VO | 80 | ¢ 6 | $\varepsilon \square$ |  |  |
| DGVEE | Sご てE |  | 000 LG | 05915 | O5t 㬉 | t＇0 | E0 | \＆ 0 |  |  |
| 0582 LE | ¢こも 82 | 928 22 | 006＇2t | 650 8\％ | 058 て | 90 | 20 | ¢ 0 |  |  |
| $09 Z \angle Z$ | sこて 5己 | 92L＇tz | 008 ct | ¢5が守 | OSZ＇2z | 90 | 10 | 80 |  |  |
| 00895 | c82 Ct | 4188E | ¢ccz 9 | 19479 | OOE 9S | 10 | $\leq 6$ | 20 |  |  |
| 00295 | 敋928 | $\angle 1 \angle \mathrm{GE}$ | ECL 85 | 191．69 | OOL OS | 20 | 90 | 20 |  |  |
| ODi＇Gb | ¢80 58 | $\angle 1928$ | EEL GG | 29S SS | 0019 | ¢＇0 | $\mathrm{G}^{\prime}$ | 20 |  |  |
| OOS 5E | ¢8t＇$\stackrel{\text { c }}{ }$ | くLG＇6Z | EES゙LS | 196\％${ }^{\circ}$ | OOS＇68 | $\dagger 0$ | $t 6$ | 20 |  |  |
| ODGEE | ¢89＇ど | くlv92 | EEG\％ $2 ⿰ ⿺ 乚 一 匕$ | 29887 | 00688 | 90 | と＇0 | z＇0 |  |  |
| 00882 | 敋で吃 | LLE EZ | EEC晈 | 192\％ | 00¢ 82 | 90 | 20 | 20 |  |  |
| 60L てZ |  | LICOZ | ESt 0 | 291\％ | 00t 27 | 10 | 10 | 20 |  |  |
| OSE＇29 | でじい | ¢SEtE | 49629 | ERO－59 | 95E 49 | 10 | 80 | 10 |  |  |
| OGL LS | でっLLE | ¢sも゙饾 | 19265 | CRt 69 | OSLIG | 20 | 10 | 10 |  |  |
| 05190 | ごい昒 | 8SL1E | 19999 | ¢68 99 | OSt「9t | $\varepsilon 0$ | 90 | 10 |  |  |
| 0scor | ZたS DE | 890＇82 | 19075 | EBZ Z9 | $0 ¢ 907$ | ¢0 | 50 | 10 |  |  |
| OS6＇6 | でロ 9 | 㓪6が | 49t8t | E日S＇8t | OSE゙ち | 90 | $t 0$ | 10 |  |  |
| 058 62 | ごぐとて | 89\％して | 198゙も | E80 9t | 95c－62 | 90 | $\varepsilon$ | 10 |  |  |
| OGLEZ | てもくらも | 39281 | 192゙した | E8r＇L | OGL CZ | 10 | 20 | 10 |  |  |
| 0S！日l | Cot9！ | 85951 | $\angle 992 E$ | E88＇2 | OS181． | 80 | 10 | 10 | $G$ | EZ |
| ［ $\%$ ］ | E］s | ［z］3 | ［1］ | 1dSraga | 003／1dS | EM | 2M | 1 M | H | 1 |


| 00857 | 00 かてZ1 | 00 でャレ | 00 Scab | （1）0981 | 00＇¢¢ち！ | WกS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 299 时 | 009＇9\％ | ¢Eか9\％ | EEC 29 | 00689 | 1958t | 10 | 10 | 80 |  |  |
| 8St60 | 009 St | LLE $\dagger t$ | 200＇2G | 00685 | 85＊的 | 10 | Z0 | 10 |  |  |
| EGI时 | 002 CH | ＋191t | でぐから | 00899 | 6GL゙切 | 200 | 10 | 20 |  |  |
| 0ç 05 | 009\％\％ | 009 Zt | 45929 | $000^{\circ} 8$ | OGEOS | 6 | ¢ 0 | 90 |  |  |
| 09056 | 002 16 | 006＇6E | 6S5゙『9 | 0089 | 950 St | で0 | 20 | 90 |  |  |
| 彨 2 的 | 009＇28 | 002 28 | $05 \% 19$ | 004 ZG | 95E6E | $\varepsilon 0$ | 10 | 90 |  |  |
| でて 15 | 009＇¢ | c日日 0\％ | 858 29 | 00609 | でで15 | 10 | ¢0 | 90 |  |  |
| てt6 Sb |  | col 8 C | －5L109 | 00899 | て66－9\％ | 20 | EO | 90 |  |  |
| で90\％ | 008 號 | 890 S8 | 85915 | 002\％9 | て690\％ | $\varepsilon 0$ | 20 | 90 |  |  |
| でだGE | 00\％¢ ¢ | E日C゙で | 8 gc 8 | 0096 | ぞFE9 | $\pm 0$ | 10 | 50 |  |  |
| EE！ CS | 009で | 19165 | 19069 | 00689 | ECF＇ZS | 10 | 90 | $\pm 0$ |  |  |
| Eeg 9\％ | 002＇68 | 19698 | 196 Fs | 00859 | ES89\％ | Z＇0 | \％0 | $\pm 0$ |  |  |
| E¢S 1\％ | 00858 | 4928E | 298 LS | 001＇29 | EEG＊ 7 | $\varepsilon 6$ | $\varepsilon$ | $\pm 0$ |  |  |
| E¢Z 9E | 00t c¢ | 49018 | 2928 | 909＇60 | EEZ 9E | ¢0 | 20 | $\pm 0$ |  |  |
| ¢¢6＇OE | 00062 | 49¢＇RZ | 299 5t | O0＇900 | ¢EG OE | 59 | 10 | $\pm 0$ |  |  |
| GZO EG | 009 ！$\downarrow$ | 0¢\％゙2 | St2 85 | O06 ${ }^{\text {g }}$ | GZO ES | 10 | 90 | $\varepsilon 0$ |  |  |
| 52L ${ }^{\text {d }}$ | 002＇88 | 052bc | GLI＇GG | 008 SS | 92tit | z＇0 | 50 | $\varepsilon 0$ |  |  |
| ぶっです。 | 00日 $\downarrow \mathrm{C}$ | OSO てE | St0 ZS | 004 29 | Gでで | $\varepsilon 0$ | $\forall 0$ | ¢＇0 |  |  |
| GZ1 28 | 00\％18 | 0GE6Z | 526 8b | 0096 | SZl＇2e | $\pm 0$ | E＇0 | \＆0 |  |  |
| ç8 LE | 000＇82 | 059.92 | ¢L8＇gb | 0059 | 9Z家 18 | 90 | 20 | $\varepsilon 0$ |  |  |
| çs 9\％ | 009＇も己 | 0c6＇cz | SLLで | 00t ¢\％ | ¢ZS＇9\％ | 90 | 10 | $\varepsilon 0$ |  |  |
| 1168 | 00900 | EEESE | E它昭 | 00685 | くもの＇®乌 | 10 | $\leq 0$ | 20 |  |  |
| 4198 | 00で2 | EEOEE | cose＇s | 00855 |  | 20 | 90 | 20 |  |  |
| LIEEV | 008 捾 | cecos | ESZてS | 00125 | く6E ¢\％ | 80 | 50 | 20 |  |  |
| 47088 | 00\％ 0 ¢ | ceg 2 | 8816 | 009＇60 | 210 日E | $\nabla^{\circ} 0$ | t0 | 20 |  |  |
| くんして¢ | 009 LZ | E¢ら゙って | 88097 | D0S＇90 | L！LZE | S＇0 | 80 | 20 |  |  |
| く！ 1 L | 009 CZ | とEでてZ | 〔86＇ZV | 00t tb | くもちくて | 90 | 20 | 20 |  |  |
| こい1 乙て | 00202 | EEc゙6l | C榢6E | OOE Ob | く11で | $\leq 0$ | 10 | 20 |  |  |
| 808 bs | 00968 | 1LOVC | で¢9＇9 | 00685 | 608＇Vs | 10 | 80 | 10 |  |  |
| 80967 | 00で96 | LLE゙1E | 269＇94 | $008 \mathrm{S5}$ | 80官60 | 20 | $\leq 0$ | 10 |  |  |
| BOZ to | 008＇乙¢ | 14988 |  | 002 ZS | 80で院 | 80 | 90 | 10 |  |  |
| B06 8c | 90v＇6z | L169 | て．¢¢＇6V | 009 6r | $806{ }^{\prime} 88$ | $t$ ¢ | 90 | 10 |  |  |
| B09 E¢ | 00092 | $\angle 1 乙$ ¢ $\chi$ | 2629y | 009 gr | $6098 E$ | 90 | \％ 0 | 10 |  |  |
| ¢0E＇8Z | 00922 |  | 261 E\％ | OD\％E\％ | BOE 8 C | 90 | 80 | 10 |  |  |
| 800 EZ | 00261 | 21815 | 260 0V | 00¢ 0 | 800 cz | 10 | 20 10 | 10 |  |  |
| 802LI | 008 ¢1 | く1！51． | －Z66＇9E | 002 28 | B0L21 | 80 | 10 | 10 | $p$ | $\varepsilon 乙$ |
| ［t］S | ［C］ | ［z］S | ［L］ 5 | 1．dS「吅当 | Gajulds | EM | 2 M | L／M | 1 | 1 |


| 7 | M | W1 | W/2 | W3 | SPTJEDD | EDDJSPT | S[1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 23 | 6 | 0.1 | 0.4 | 0.8 | 18592 | 38567 | 38.342 | 16200 | 16.483 | 18592 |
|  |  | 0.1 | 02 | 0.7 | 24492 | 42.667 | 42.442 | 19700 | 20283 | 24492 |
|  |  | 0.1 | 03 | 06 | 30392 | 46767 | 46542 | 23200 | 24083 | 30392 |
|  |  | 0.1 | 0.4 | 0.5 | 36.292 | 50867 | 50642 | 26700 | 27.883 | 36.292 |
|  |  | 0.1 | 0.5 | 0.4 | 42.192 | 54967 | 54.742 | 30200 | 31.683 | 42.192 |
|  |  | 01 | 0.6 | 0.3 | 48092 | 59067 | 58.842 | 33700 | 35.483 | 48.092 |
|  |  | 01 | 0.7 | 02 | 53,992 | 63167 | 62.942 | 37200 | 39.283 | 53.992 |
|  |  | 0.1 | 0.8 | 0.1 | 59892 | 67.267 | 67.042 | 40700 | 43.083 | 59892 |
|  |  | 02 | 0.1 | 0.7 | 23283 | 42033 | 41583 | 20900 | 21167 | 23.283 |
|  |  | 02 | 02 | 06 | 29.183 | 46133 | 45683 | 24,400 | 24967 | 29.183 |
|  |  | ¢ 2 | 03 | 0.5 | 35083 | 50.233 | 49783 | 27900 | 28.767 | 35083 |
|  |  | 02 | 04 | 04 | 40983 | 54333 | 53.883 | 31400 | 32567 | 40.983 |
|  |  | 02 | 0.5 | 03 | 46.883 | 58433 | 57983 | 34.900 | 36367 | 46883 |
|  |  | 02 | 06 | 02 | 52.783 | 62533 | 62083 | 38.400 | 40167 | 52783 |
|  |  | 0.2 | 07 | 01 | 58.683 | 68633 | 66183 | 41.900 | 43967 | 58683 |
|  |  | 03 | 01 | 06 | 27.975 | 45500 | 44.825 | 25600 | 25850 | 27975 |
|  |  | 03 | 0.2 | 0.5 | 33.875 | 49500 | 48.925 | 29100 | 29.650 | 33.875 |
|  |  | 03 | 0.3 | 04 | 39.775 | 53700 | 53025 | 32.600 | 33.450 | 39775 |
|  |  | 0.3 | 0.4 | 6 | 45.675 | 57800 | 57.125 | 36100 | 37.250 | 45.675 |
|  |  | 03 | 0.5 | 02 | 51575 | 61900 | 61.225 | 39600 | 41.050 | 51.675 |
|  |  | 03 | 0.6 | 01 | 57.475 | 66000 | 65325 | 43.100 | 44850 | 57.475 |
|  |  | 04 | $0 . t$ | 05 | 32.667 | 48967 | 48.067 | 30.300 | 30533 | 32.667 |
|  |  | 04 | 0.2 | 04 | 3B 567 | 53067 | 52.167 | 33.800 | 34.333 | 38.567 |
|  |  | 04 | 0.3 | 03 | 44467 | 57167 | 58267 | 37.350 | 38133 | 44,467 |
|  |  | 04 | 0.4 | 02 | 50367 | 61267 | 60.367 | 40800 | 41933 | 50.367 |
|  |  | 04 | 05 | 01 | 56267 | 65367 | 64467 | 44.300 35000 | 45733 35217 | 56267 37.358 |
|  |  | 05 | 01 | 04 | 37.358 43258 | 52.433 56.533 | 51308 55.408 | 35900 38500 | 39.017 | 43.258 |
|  |  | 0.5 05 | 02 | 0.3 | 43258 49158 | 66.531 60633 | 52.408 59.508 | 42.000 | 42817 | 49168 |
|  |  | 05 | 04 | 0.1 | 55058 | 64.733 | 63.608 | 45500 | 46.617 | 55058 |
|  |  | 06 | 01 | 0.3 | 42.050 | 55.960 | 54.550 | 39700 | 39900 | 42.050 |
|  |  | 0.6 | 02 | 02 | 47.950 | 60 OWO | 58650 | 43200 | 43700 | 47.950 |
|  |  | 06 | 03 | 01 | 53850 | 64100 | 62.750 | 46700 | 47.500 | 53850 |
|  |  | 07 | 01 | 0.2 | 46742 | 59.367 | 57792 | 44,400 | 44583 | 46742 |
|  |  | 0.7 | 02 | 01 | 52.642 | 63467 | 61892 | 47.900 | 48383 | 52642 |
|  |  | 08 | 01 | 01 | 51.433 | 62.833 | 61.033 | 49.100 | 49267 | 51433 |
| SUM |  |  |  |  | 155900 | 202400 | 199700 | 1272.00 | 130606 | 1659.00 |


| 7 | M | W91 | W2 | W3 | SPT/ED | EDDISPT | S[1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 23 | 7 | 0.1 | 01 | 08 | 19033 | 39250 | 39017 | 16742 | 16825 | 19.033 |
|  |  | 01 | 02 | 0.7 | 25233 | 43.850 | 43617 | 20.642 | 20.825 | 25233 |
|  |  | 0.1 | 03 | 0.6 | 31433 | 48.450 | 48217 | 24.542 | 24825 | 31433 |
|  |  | 01 | 04 | 0.5 | 37633 | 53.050 | $52 \mathrm{B17}$ | 28442 | 28.825 | 37633 |
|  |  | 01 | 0.5 | 04 | 43833 | 57.650 | 57417 | 32342 | 32.825 | $43 \mathrm{B33}$ |
|  |  | 0.1 | 06 | 0.3 | 50033 | 62.250 | 62017 | 36242 | 36825 | 50.033 |
|  |  | 0.1 | 07 | 02 | 56.233 | 66850 | 66.617 | 40.142 | 40.825 | 56233 |
|  |  | 01 | 08 | 0.1 | 62.433 | 71450 | 71217 | 44.042 | 44825 | 62.433 |
|  |  | 02 | 01 | 0.7 | 23367 | 42900 | 42433 | 21.583 | 21650 | 23.867 |
|  |  | 02 | 02 | 06 | 30067 | 47500 | 47033 | 25483 | 25650 | 30067 |
|  |  | 02 | 03 | 0.5 | 36267 | 52100 | 51633 | 29383 | 29650 | 36.267 |
|  |  | 02 | 04 | 04 | 42467 | 56700 | 56233 | 33283 | 33650 | 42467 |
|  |  | 0.2 | 05 | 03 | 48667 | 61300 | 60833 | 37183 | 37650 | 48.687 |
|  |  | 02 | 06 | 0.2 | 54867 | 65900 | 65433 | 41.083 | 41650 | 54867 |
|  |  | 02 | 07 | 01 | 61067 | 7 D 500 | 70033 | 44983 | 45650 | 61067 |
|  |  | 03 | 0.1 | 06 | 28700 | 46.550 | 45950 | 26425 | 26.475 | 28700 |
|  |  | 03 | 02 | 05 | 34900 | 51.150 | 50450 | 30325 | 30475 | 34900 |
|  |  | 0.3 | 03 | 64 | 41.100 | 55.750 | 5505 D | 34225 | 34,475 | 41100 |
|  |  | 03 | 54 | 03 | 47.300 | 60350 | 59.650 | 38125 | 38475 | 47.300 |
|  |  | 03 | 0.5 | 02 | 53.500 | 64.950 | 64.250 | 42025 | 42475 | 53500 |
|  |  | 0.3 | 0.6 | 0.9 | 59.700 | 69550 | 68950 | 45925 | 46.475 | 59.708 |
|  |  | 04 | 0.1 | 05 | 33533 | 50200 | 49267 | 31.267 | 31300 | 33.533 |
|  |  | 04 | 02 | 04 | 39733 | 54.800 | 53867 | 35.167 | 35300 | 39733 |
|  |  | 04 | 03 | 0.3 | 45933 | 59.400 | 58467 | 39.067 | 35300 | 46.933 |
|  |  | 0.4 | 04 | 02 | 52.133 | 64000 | 63.067 | 42967 | 43305 | 52133 |
|  |  | 0.4 | 05 | 01 | 58.333 | 68600 | 67.667 | 46867 | 47.300 | 58333 |
|  |  | 05 | 0.1 | 04 | 38367 | 53850 | 52683 | 36108 | 36125 | 38367 |
|  |  | 05 | 0.2 | 0.3 | 44567 | 58.450 | 57283 | 40008 | 40.125 | 44567 |
|  |  | 05 | 0.3 | 02 | 50767 | 63.050 | 61883 | 43.908 | 44.125 | 50.767 |
|  |  | 05 | 04 | 0.1 | 56967 | 67.650 | 66483 | 47.808 | 48125 | 56.967 |
|  |  | 06 | 01 | 03 | 43200 | 57500 | 55.100 | 40.950 | 40950 | 43200 |
|  |  | 06 | 02 | 02 | 49400 | 62.100 | 60700 | 44850 | 44960 | 49.400 |
|  |  | 0.6 | 03 | 0.1 | 55600 | $6 ¢ .700$ | 65.300 | 48750 | 48950 | 55600 |
|  |  | 07 | 01 | 02 | 48033 | 61.150 | 59517 | 45792 | 45775 | 48033 |
|  |  | 07 | 02 | 01 | 54233 | \$5 750 | 64117 | 49692 | 49775 | 54.233 |
|  |  | 08 | 01 | 01 | 52.867 | 64800 | 62.933 | 50663 | 50500 | 52867 |
|  |  | SUM |  |  | 161200 | 210600 | 207800 | 1337.00 | 134700 | 1612.00 |


| 00 bGGL | $00 \mathrm{ELE1}$ | 00 ģ゙， | $00^{\circ} 0991$ | （00） 989 | $000 \pm 551$ | WกS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 00t＇09 | ¢EE 8t | 496\％ | 29095 | 00849 | 00705 | 10 | 10 | 80 |  |  |
| 09tic | こ6E゙く | 80S90 | £どちら | 0 㿟99 | OSt゙LS | 10 | 20 | 10 |  |  |
| 092＇9t | 26ヶ゙リ | 008 5 | c¢t CS | 096＇EG | OSZ 96 | $2 ' 0$ | 10 | $\angle 0$ |  |  |
| 00529 | $0 ¢ 096$ | WSO 5\％ | 008＇物 | 001．gs | D09＇z＇ | $1 \cdot 0$ | $\varepsilon 0$ | 90 |  |  |
| 00c\％ $2 \downarrow$ | OGZ＇Ep | OSE てt | －08＇19 | 00L ES | OOE＇ $2 t$ | 20 | \％ | 9 S 0 |  |  |
| 001 Zt | 050 \％p | 09968 | 0088 | OOL＇09 | 00レ てt | E＇0 | 10 | 90 |  |  |
| OGG＇EG | 80S 50 | Z6S＇¢も | 29169 | QGZ Ģ | 05589 | －0 | $\pm 0$ | $5 \%$ |  |  |
| OSE Gy | 80 Ct | 2680 | 291＇LS |  | 0588 | 20 | £＇0 | 50 |  |  |
| OG1Et | gol Ec | 26185 | 4918\％ | OGZ 6b | 656゙を | E＇0 | 20 | 50 |  |  |
| OG6． 28 | 80658 | 26598 | 295 St | OSZ＇9t | O56 LE | $\bigcirc 0$ | 10 | 50 |  |  |
| 00969 | L9G $\dagger \downarrow$ | とぐでV | ESGES | 006＇析 | 00965 | 10 | 90 | $\pm 0$ |  |  |
| 00t 6\％ | 19¢！ | Etroc | E¢G 0¢ | OOt ls | OOt 6\％ | 20 | $\nabla^{\circ}$ | t0 |  |  |
| 002 $5 \%$ | 191．88 | EELGE | ESS $\downarrow$ | D0t 时 | 002＇bor | 80 | ¢ 0 | ヤO |  |  |
| 00068 | 496＇tc | EEO FE | Scs＇bo | 00t 5\％ | 00068 | 70 | 20 | $\checkmark 0$ |  |  |
| 008 Ec | 192゙も | ESE LE | ESG Lt | 00t CH | 009 EE | S0 | 10 | 70 |  |  |
| dS9＇99 | Gく9「も | 92900 | 00625 | OGS E\％ | $0 ¢ 9 \mathrm{GS}$ | 10 | 90 | 80 |  |  |
| OGVOS | Sで0t | GL6＇LE | 00667 | OSS＇QS | 0st DS | 乙 0 | 90 | E 0 |  |  |
| OGC St |  | GLZ GE | 0065 | OGG t $t$ | OSC 5\％ | §＇0 | $\square 0$ | E 0 |  |  |
| 0500 t | cto ri | StS 2 | 006 Et | OSS $\dagger$ | 0900 | 70 | E0 | E0 |  |  |
|  | G280E | 54862 | 00607 | OSS［t | 098＇饮 | 50 | 20 | ¢＇0 |  |  |
| 05962 | 9z家2己 | $c: 12 Z$ | 006 九它 | 0 GG 88 | 09982 | 90 | 10 | E0 |  |  |
| 00199 | ¢99 Cb | ごて6E | 49Z＇Z9 | $00 \pm 25$ | 002＇99 | 10 | 40 | \％0 |  |  |
| O05 19 | E日も 65 | LIG9E | 1926 | 002 6 F | OOG＇LG | 20 | 90 | 20 |  |  |
| 00E 9\％ | ERZ 9\％ | LIGEE | L9\％9t | 002＇9b | OOE 9t | E0 | 40 | 20 |  |  |
| 00し「け | E日0 ¢ | く11しを | 49て غt | 00 02 L | 001 Et | V＇0 | $t 0$ | 20 |  |  |
| 006 SE | E88 62 | 比时 | 19才 Dt | OOL $0 t$ | 0065 | G＇0 | E0 | 20 |  |  |
| 00L OE | ¢899\％ | LbLS | 192＇L¢ | 00128 | OOLO | 90 | 20 | 20 |  |  |
| 00 Sc 2 | ESt Ct | C10 EZ | 192tc | 002 0 ¢ | 005 ¢ | 10 | 10 80 | 20 10 |  |  |
| OGELG | でくじ | 89\％ 28 | EE9 19 | OS日＇IG | OSL29 | 10 20 | 80 20 | 10 10 |  |  |
| OSG7S | でG 98 | EGO＇G8 | E¢98\％ | OGQ＇8t | OS5 29 | 10 20 | 10 90 | 10 100 |  |  |
| OSE＇2t OGIZ | でぐgに | 895 89868 | を699t | OGEGt | OGE＇Lt | 80 00 | 90 90 | 100 100 |  |  |
| OG698 | くた6 日 | 89692 | EES 6 ce | O¢G6¢ | 05698 | 90 | $\bigcirc 0$ | 10 |  |  |
| OGL＇LE | でくらも | 8sて＇ゆて | EES9E | 09898 | 05cle | 90 | ¢0 | 10 |  |  |
| OGG9Z | でG て己 | 89G！Z | EESEE | OFE CE | OS5＇92 | 20 | 20 | 60 |  |  |
| 65¢ して | ZゆE＇GL | 858 81 | Ec90 | 95808 |  | 60 | 10 | 10 | $t$ | 吅 |
| ［6］ | ［E］S | ［7］s | ［1］S | Id500 | QaヨコdS | EAM | ZAM | LA | W | 1 |


| 0109991 | 00\％006 | 00 Z0ヶt | OO＇GGLZ | Cis8lz | 00＇G991． | Whis |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eco ${ }^{\text {c }}$ |  | EES $\dagger 9$ | 29C＇99 | $008{ }^{\text {b }}$ | 10 | 10 | 80 |  |  |
| ¢ 2899 | 49 Lc | を即しら | 20EC99 | E60\％9 | g ze cs | 10 | 20 | $\angle 0$ |  |  |
| SZE 6b | 490 Lb | E8t＇Lt | 2bで19 | ECEC\％ | ¢で「\％ | 20 | 10 | $\leq 0$ |  |  |
| osc： 29 | O02＇09 | 00805 | 058.49 | ORE＇69 | OSERS | 10 | \％ 0 | 90 |  |  |
| OGE OG | 00t90 | 0099 | OSLです | OセZ®¢ | 05809 | で0 | 20 | 90 |  |  |
| OSE゙け | DOL Zt | OOでで | 05929 | 00169 | 95EV | $\varepsilon 0$ | 10 | 90 |  |  |
| G4889 | E¢O OS | LH＇OS | 8SE 69 | 19902 | SL8 85 | 10 | $\bigcirc 0$ | 50 |  |  |
| SLEZG | £ $¢ 2 \mathrm{ct}$ | 2189\％ | 6GZ ゆ9 | 19099 | GLEZS | 20 | $\varepsilon 0$ | 90 |  |  |
| cas gb | とくt ！ | 2にずも | 日cl 69 | 49809 | ¢ 28 St | $\varepsilon 0$ | 20 | 50 |  |  |
| GLE＇68 | £ ¢ 18 | んしでくを | Bco bS | L929s | SLE 6E | $\pm 0$ | 10 | 50 |  |  |
| O0t＇09 | 2906 6 | ¢¢0 6t | 29802 | ¢68．L2 | D0t 09 | 10 | 50 | $\checkmark 0$ |  |  |
| 006 ES | 490 | ceb5t | ［54＇99 | EEL 99 | 006＇s | 20 | $\bigcirc 0$ | TO |  |  |
| 00t Lt | 49c＇0t | ECS Or | 499.09 | $8 ¢ 919$ | $00{ }^{\circ} 15$ | ¢0 | co | $\square^{\circ} 0$ |  |  |
| 008＇00 | 19\％98 | ¢Es 9 ¢ | 495 55 | cis es | 0060 | T＇0 | 20 | $\pm 0$ |  |  |
| 00t＇se | 291－28 | EEZZE | 29tos | Eet LS | 00t ret | 50 | 10 | ${ }^{\circ} \mathrm{O}$ |  |  |
| cz6 19 | 002 施 | OSts | ¢LEVL | 00181 | ¢でじ19 | 10 | 90 | $\varepsilon \cdot 0$ |  |  |
| ¢Zヤ59 | OOb bt | OSt | GLZ 29 | 000＇89 | ¢Zヤ SS | 20 | 90 | $\varepsilon 0$ |  |  |
| 52685 | 00 l | 05108 | cLl 29 | 0086 | ¢Z6 8 | \＆0 | ${ }^{\text {¢ }}$ | $\varepsilon 0$ |  |  |
| ç゙もで | 00898 | 05898 | 9L0 29 | 00815 | GZb Cb | $\checkmark 0$ | $\varepsilon \cdot 0$ | $\varepsilon 0$ |  |  |
| 92658 | $009^{\prime} 18$ | OSS LE | GL6 LG | 002＇t5 | GZE SE | 50 | 20 | ¢0 |  |  |
| 92668 | $00 z^{\circ} \mathrm{Lz}$ | gGz $\angle 己$ | 9L8＇9b | 00925 | 9\％か＇62 | 90 | L＇o | 80 |  |  |
| O¢ロ＇¢ | EEORt | 49080 | C88 EL | 298bt | 0 ¢tes | 10 | $\angle 0$ | 20 |  |  |
| 096＇99 | ¢ELEt | L92＇8y |  | 49869 | 0＇s＇99 | 20 | 90 | 20 |  |  |
| OSt 09 | Ectocis | 29t 68 | ¢89 E9 | L91＇09 | OSt 05 | $8 \cdot 0$ | G0 | 20 |  |  |
| OS6 ct | cet ce | 29198 | ¢89 89 | 290＇69 | 096 ¢t | $\checkmark$ | $\pm 0$ | 20 |  |  |
| OSt 28 | ¢E8 0 ¢ | 29808 | E8t EG | L96＇s | OSt 28 | $9{ }^{\prime} 0$ | E0 | Z0 |  |  |
| 056 OE | ¢E9 9 L | 29990 | ¢8E 8t | $4 \mathrm{SO}_{6} 6 \mathrm{p}$ | 05608 | $9{ }^{\prime} 0$ | Z0 | $\checkmark 0$ |  |  |
|  | ¢¢Zzz | L9Z 26 | cal et | 492 tp | 05t $\downarrow$ ¢ | 40 | 10 | 20 |  |  |
| SL6 $\quad \mathrm{tg}$ | $298 \%$ | 58c＇Lb | 26E 5L | EE9 GL | 926.19 | $1 \cdot 0$ | 80 | 10 |  |  |
| SLE 99 | 290 EP | ¢80＇ED | 26z＇04 | EES 02 | GLV＇GS | 20 | 20 | 10 |  |  |
| SL6＇19 | 292 日E | ¢82 BE | 281＇99 | ¢¢¢ 59 | G16 15 | 80 | 90 | 10 |  |  |
| SLV Gt | 29t $\dagger$ ¢ | $\varepsilon 8 \downarrow \downarrow \downarrow$ | 26009 | Ece 09 | GLv 5 | 50 | 50 | L＇0 |  |  |
| 9 26.88 | L32 Os | E81 $\mathrm{DE}^{\text {c }}$ | $26.6 \pm 9$ | cez 99 | SL6 8 E | $9{ }^{\text {c }}$ | $\checkmark 0$ | 10 |  |  |
| SLD 2 C | L989z | ¢88 cz | 26867 | cel 09 | SLP ZE | 90 | ع00 | 10 |  |  |
| 92692 | 299＇L2 | E85 L | 265 | ¢EO 9 | GL6 9Z | 20 | で0 | 1.0 |  |  |
| SLくら5 | L9Z Ll | と日で！ | 26965 | EC5 50 | GLb 6b | 80 | 10 | 10 | 8 | $\varepsilon$ |
| ［t］s | ［Els | ［2］ | ［1］ | IdS「OUE | OOGILdS | EM | ZM | LM | W | 1 |


| 000991 | 005681 | 0がc8Eし | 00 96L1 | 00 サと时 | 000991 | WกS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 192 ¢5 | 000＇19 | 8eO！G | ESG 69 | 00t19 | 192 ¢9 | 10 | 10 | 80 |  |  |
| ESG $\downarrow 5$ | SLl OS | て60 09 | 498＇6G | 00019 | EES V＇ | 10 | 20 | ＜ 0 |  |  |
| ECS时 | 919 9t | 76598 | ［99＇59 | 00225 | E¢8 87 | 20 | 10 | L6 |  |  |
| 00099 | 0¢E 6t | 0 GI 6 | D02 65 | 00909 | 00095 | 10 | 80 | 99 |  |  |
| OOZ DS | 旳LGV | 099＇sp | OOt GG | 00895 | 00265 | 20 | 20 | 90 |  |  |
| 00\％$\downarrow$ | OStで | $0 \%$＇ど | 009＇ts | 000 ec | 00ヶ $\downarrow$ | E0 | 1.0 | 90 |  |  |
| 49849 | ¢ぐ家 | 602＇6t | ceo 69 | 00209 | L9E LS | 10 | $\dagger 0$ | 90 |  |  |
| 29519 | ç6 tb | 80212 | ¢¢Z GG | 00t＇99 | 29G LS | 乙0 | E0 | 50 |  |  |
| 29C9\％ | らでした | 602＇to | E¢vig | 009 乙S | 29 25 | E0 | Z0 | G0 |  |  |
| 49658 | ¢ZL2E | 802 28 | EE9 $2 t$ | 0088 | 49668 | $\pm 0$ | 10 | 90 |  |  |
| ¢¢L SG | 00220 | c9Z $\angle t$ | 29839 | 00865 | Eとぐ家 | 10 | G＇0 | \％＇0 |  |  |
| EE6゙てG | 004 tr | 292 Et | 19099 | 000＇99 | EE6 ZS | Z0 | $\dagger 0$ | $\pm 0$ |  |  |
| をどろも | 009＇06 | 4920\％ | 292 bs | 00Z 25 | をとしくt | E0 | E＇0 | $\nabla^{\prime} 0$ |  |  |
| EEE゙けt | DOE 9E | $\angle 9 \angle 98$ | $49 \%$ t | 加比的 | EEE＇L | \％ 0 | z0 | $\downarrow 0$ |  |  |
| ECS ¢ | OOE＇EE | 192＇¢¢ | 1998t | $009 \% \%$ | E®S 58 | 90 | 10 | $\dagger 0$ |  |  |
| 001＇09 | G189\％ | çE 9b | 00185 | 00t 65 | 001 09 | 10 | 90 | $\mathrm{c}^{\prime} 0$ |  |  |
| 00¢ ts | GLZ Et | çe ct | 006 \＄5 | 009 55 | 加と＇ヶ它 | 20 | G＇0 | \＆＇0 |  |  |
| 0098 t | G296E |  | 0015 | 0081 | 009＇8\％ | E＇0 | $V^{\prime} 0$ | E＇0 |  |  |
| 00」で | GLO 98 | GZQ SE | 00 E ¢ | 000 日 | 002 己t | $\pm 0$ | ED | E0 |  |  |
| 00698 | GLP＇Z¢ | ૬Z\＆＇రీ | OOS Et | 002 bt | 00698 | G D | Z0 | E0 |  |  |
| COL 5 | 918゙とう |  | OOL＇6E | 006\％6\％ | OOL LE | 90 | 10 | E0 |  |  |
| 29619 | ¢S0 5\％ | ERE GV | ¢¢G＇gG | 00069 | L9\％ 19 | 10 | $\angle 0$ | 20 |  |  |
| 19959 | 0Gb で | C8S LV | EEL＇下G | OOZ＇SG | 29999 | 20 | 90 | 20 |  |  |
| 4908 | ¢G8＇8t | ces 88 | EE6 GS | 00t 15 | 29865 | E0 | 90 | 20 |  |  |
| 人的时 | Qçics | C88 DE | ECI 17 | W09 $2 巾$ | 190比 | $\geqslant 0$ | b＇0 | z＇0 |  |  |
| 29\％日6 | 059 L¢ | と日E 1E | EEE EV | 008 E\％ | 29\％98 | 90 | ¢0 | 20 |  |  |
| L9t C ¢ | ゆGQ＇日Z | とลษ＇LZ | EES 6E | 00007 | 19t てE | 90 | 20 | 20 |  |  |
| 299＇92 | 0Gtrz | 88E tて | EELGE | ODZ ${ }^{\text {O }}$ | 29992 | $\angle 0$ | 10 | 20 |  |  |
| ES8 29 | 5Z2 5\％ | でけが | 49E85 | 00989 | Ecs 29 | 10 | 80 | 10 |  |  |
| ESO 49 | 它ご＇t | でotot | 29s＇bs | $008{ }^{\circ}$ | EED 29 | 20 | $\angle 0$ | ${ }^{\prime}$ |  |  |
| EEZ LS | 52088 | でV 2 E | L920S | 000.15 | をモで！ | ع－0 | 90 | 1.0 |  |  |
| EEbらt | ¢゙も pe | ですぐ， | 19690 | $00 \% 27$ | ¢¢\％G\％ | $\square^{\circ} 0$ | G0 | $1 \cdot 0$ |  |  |
| ¢E968 | S28 ©e | でVOE | く91を | 00\％Et | E¢96¢ | 50 | 10 | 10 |  |  |
| CES E | 9ZZ LZ | で6 9Z | 49068 | 04 Cb 6 | E¢E EC | 90 | EO | 10 |  |  |
|  | ૬Z¢＇¢z | でャ ¢ | 19958 | 008 58 | EEO \＄2 | $\angle 0$ | 20 | 10 |  |  |
| EEZ てZ | ¢てO＇0\％ | です61 | L9LIE | 00028 | EEZ 己て | 80 | 10 | 1＇0 | 9 | $\square 乙$ |
| ［\＄］5 | ［C］S | ［2］${ }^{\text {c }}$ | ［l］ | 1dSiO03 | －0ヨ／1dS | EM | 3 M | WM | W | 1 |


| 00＇2091 | 00 D9¢5 | 0002 za | $00 \mathrm{BCL1}$ | 00 95 4 | 00.2091 | WกS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| عeq＇ts | 199＇6b | 005 63 | $0082{ }^{\text {c }}$ | 009＇6s | ع¢8 LS | 10 | 10 | 80 |  |  |
| ZtO Ec | EBL8t | OOE 6 | 00tes | GLG＇Gg | ZtOES | 10 | 20 | 20 |  |  |
| ですく | E8E\％ | ODZ＇Sb | 000 vg | SLS Sc | でG 2 | zo | 10 | 20 |  |  |
| OFS ${ }^{\text {b }}$ | $006 \%$ | 001 Lt | 000 L5 | OSE 85 | Ofers | 10 | 80 | 90 |  |  |
| 092＇6t | 00ctot | 000 比 | 009 Es | 0 ¢ $6^{\prime \prime}$ | OGL＇GV | 20 | 20 | 90 |  |  |
| OGZ Et | 001\％ | 0060 | OLZ 09 | DGG LS | DSZ EP | $\varepsilon 0$ | 10 | 90 |  |  |
| 85t 55 | 20\％ | O06 90 | 009＇9G | GZL 25 | 85t 95 | 10 | \％0 | 50 |  |  |
| BG6 6t | L198t | 008 CD | 002＇\＆ | Gzebs | BC6 6t | 20 | \＆ 0 | 50 |  |  |
| 8らも切 | LUCOt | 002\％68 | 009＇65 | 9Z6 OS | 㫙けも | $\varepsilon 0$ | zo | 90 |  |  |
| 8¢6．8¢ | L6 98 | 909 9e | 00t＇9r | gzc＇Lb | BG6 8E | $\dagger 0$ | 10 | 50 |  |  |
| 299＇99 | ¢¢ 9 p | 00t | POZ 95 | 00129 | 29999 | 10 | 50 | 50 |  |  |
| 291 15 | celzb | 009\％ 17 | 00825 | OOLCs | 191＊ | 20 | to | \％ 0 |  |  |
| 49995 | EEE 6E | 0058 c | 00t＇60 | OOCOG | 2995 | $\varepsilon 0$ | $\varepsilon 0$ | － 0 |  |  |
| 2910\％ | $\varepsilon ¢ 6 ¢ ¢$ | 00\％ 5 c | $000 \% 0$ | 006\％ 9 | 2960\％ | 50 | zo | \％ 0 |  |  |
| 499＇0t | ¢¢G Z | OOE 乙 | $009 \%$ | O0F ${ }^{\circ}$ | 199\％$\dagger$ ¢ | 50 | 5 | vo |  |  |
| 428．29 | OGZ ¢b | OOS \＆$\downarrow$ | 00899 | GLD 9G | G28－29 | 10 | 90 | $\varepsilon 0$ |  |  |
| GLE＇ZS | 058 | 00tot | 000＇89 | GLOEG | SLE 29 | 20 | 50 | E0 |  |  |
| St3 96 | DGt 8E | ¢0¢ 28 | 00068 | 91965 | 928 gr | 60 | $\checkmark 0$ | E0 |  |  |
| GLELV | OGO＇GE | OOC $\downarrow$ ¢ | 009 St | 9LZ $\mathrm{gb}^{\text {c }}$ | GLELt | $\checkmark 0$ | 80 | E0 |  |  |
| GLE ¢ ¢ | $0 ¢ 9$ LE | 00118 | 00でも | GLG Zt | SLB SE | 50 | 20 | ¢0 |  |  |
| GLE OE | OGZ 日Z | 00082 | 00888 | GLt 68 | SLE OE | 90 | 10 | E0 |  |  |
| E80 69 | L98 $\square^{\text {b }}$ | 00¢ で | 000 GG | OGB cs | ¢80 69 | 10 | $\angle 0$ | 20 |  |  |
| ¢ $¢ ¢$ | L960\％ | 002＇68 | 000 Zs | OSP 29 | ¢8G＇¢ | 20 | 90 | 20 |  |  |
| ¢ 8085 | 29518 | 001．98 | $0098 \downarrow$ | 05066 | c80 8\％ | $\varepsilon 0$ | 50 | Z0 |  |  |
| と日G Zt | 291 ver | 000 E ¢ | 002 ct | 0 Gg ¢t | E日g zt | $\checkmark 0$ | $\bigcirc 0$ | Z0 |  |  |
| 890\％ 28 | 2920E | 0068 C | 008＇も | OGC Z | E80 $2 \varepsilon$ | 9.0 | $\varepsilon 0$ | 60 |  |  |
| Eas 1E | L9E＇2z | 00898 | 00t 8 8 | 098＇6E | ¢ag LE | 90 | 20 | z＇0 |  |  |
| ¢90 92 | $1968 Z$ | 00L＇ 2 | 000 Sc | 05\％5 ¢ | E80＇92 | 10 | 10 | z0 |  |  |
| 26209 | ¢8t $\underbrace{\text { ct }}$ | 00115 | 000＇59 | çZ cs | 26809 | $1{ }^{1} 0$ | 80 | 10 |  |  |
| 26L $\dagger$ ¢ | c80 OV | OOO 日E | 00915 | 928＇19 | 26L t ¢ | 20 | 20 | 10 |  |  |
| 2626b | ¢89\％ | OOG＇6E | 0028 | 「ごす＊ | ZGZ 68 | ¢0 | 90 | 1＇0 |  |  |
| Z62 ¢ $\square^{\text {b }}$ | ¢日でを | 008＇LE | 008 \％ | ¢20＇5\％ | 26L ¢0 | ¢0 | 50 | 10 |  |  |
| 26\％ 88 | ¢88\％ 6 | 00， 8 \％ | 00t 1. | 929＇し＊ | 262 日e | 50 | $\checkmark 0$ | 10 |  |  |
| Z62 28 | ¢8\％ 92 | 0098 | 00088 | ¢zz＇的 | 262 2 E | 90 | 80 | 10 |  |  |
| ででさz | ¢ 80 ¢ 2 | $009 z z$ | 009＇ve | cz8 18 | 262．2\％ | 20 | 20 | 10 |  |  |
| 26L＇IZ | E8961 | 00t\％ |  | くでいしを | 26212 | 80 | 10 | 10 | ． | ¢2 |
| ［t］s | 錞 | Izs | ［l］s | Ldsiadg | 0931］dS | EM | ZM | LM | W | 1 |


| 009921 | O『＇ELSb | Q0 Slal | 00 Z861 | 00 Z961 | 00.9941 | 3NกS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| E¢1． 99 | 296゙¢ | 001 19 | 000 cg | 加O＇G9 | EE195 | 10 | 10 | 日 0 |  |  |
| 1F\％ 29 | 旳官を的 | St9 Es | OOE E9 | 090＇59 | 21日 59 | 10 | 20 | $\angle 0$ |  |  |
| UV＇！ | 8Gで67 | 5¢E＇6\％ | 00289 | 05\％${ }^{\text {¢ }}$ | L1も＇G | C0 | 10 | $\leq 0$ |  |  |
| 00969 | OSL゙¢G | OSZ ES | 009 ¢9 | 001．59 | D0S＇69 | 10 | E 0 | 90 |  |  |
| OOL ES | －4588 | 056 时 | 00065 | 009＇09 | OOL ES | 20 | 20 | 90 |  |  |
| $00<97$ | OS5゙詻 | OG9 to | 00\％$\downarrow 9$ | 006＇59 | 0029t | E＇0 | 10 | 90 |  |  |
|  | Cbtzs | らでです | 006 E9 | 0¢159 | ¢81＇L9 | 10 | $\pm 0$ | $G^{\prime} 0$ |  |  |
| ¢8L＇ゆG | こちザgt | ¢ZS＇80 | 00865 | OSS＇09 | E8L tr | 20 | E＇O | G 0 |  |  |
| Esc＇eb | でっ゙け | GてZ＇Vも | $001 \% 5$ |  | E8E 旳 | $\varepsilon 0$ | 20 | 90 |  |  |
| E86 bt | てbs 60 | GZ6 66 | 0010 | 09E＇LS | 886 | 10 | 10 | 50 |  |  |
| L98＇Z9 | EECZS | ODV＇ZG | $002 \% 9$ | 002 59 | 19829 | 10 | 90 | $\nabla^{\prime} 0$ |  |  |
| 49799 | CED 80 | 901 8p | D09 㛡 | 00909 | 49795 | $2 \cdot 0$ | 70 | ¢0 |  |  |
| 49009 | EEt゙をt | 008 8\％ | 000＇GG | 00095 | 49009 | ¢0 | E 0 | $\pm 0$ |  |  |
| 1998t | EET6E | OOS 6E | 00t 0G |  | 2998t | $\forall 0$ | $2 \cdot 0$ | t0 |  |  |
| L9Z 28 | 6¢ | 902 SE | 009＇50 | 0089 | 192 LS | $9^{\prime} 0$ | 10 | $\checkmark 0$ |  |  |
| OSS 79 | G76\％LG | 51615 | dos＇rg | 09259 | OSG 99 | 1.0 | 90 | ED |  |  |
| OSL \＄9 | g29＇」t | 52916 | 00669 | 09909 | 0SL 69 | 20 | 50 | ED |  |  |
| OGLIS | 9ZE ¢6 | G2AEF | 00¢ 99 | OSO 99 | 09215 | \＆＇0 | 0 | E0 |  |  |
| OSE Gt | G20 6E | SLO＇6S | 00205 | OSサ＇L9 | OGE Gt | 70 | E0 | E0 |  |  |
| 096＇86 | çtivi | ¢Ll． 0 S | OOL 9t | 0S安9\％ | OF6 88 | 50 | 20 | E＇O |  |  |
| OS5 乙 | ¢ですく | C1tos | OOG＇ı | OSC $2 t$ | 0¢S＇Z¢ | 90 | 10 | EO |  |  |
| EEZ99 | L19＇LG | OS5 15 | 008＇巾9 | 00E g9 | 比的 | 10 | 50 | Co |  |  |
| EE8 的 | 2Lこ $1 t$ | OSZ 16 | 007＇09 | 00109 | £と8＇的 | 20 | 90 | 70 |  |  |
| ECt ¢S | 2L6 Ct | 056 $\mathrm{Cb}^{\text {b }}$ | 009 GS | 00195 | ¢¢V＇¢9 | E0 | 50 | 20 |  |  |
| ECOLt | LL98E |  | 009 IS | 00519 | CEO＇tb | $\$ 0$ | 50 | 20 |  |  |
| CES Ot | 21808 | OSE PE | 00t 9t | 006＇9t | EE9 Ot | 90 90 | 60 | 20 20 |  |  |
| ¢¢て | 2100E | 05008 $0 ¢ 258$ | 00¢ 0 L | O0E Ct |  | 90 | 20 10 | 20 20 |  |  |
|  | 80b | ¢く，LG | 00159 | OS¢ ¢9 | 21649 | $1-0$ | 80 | 10 |  |  |
| 11919 | 8099 | GZ89t | 00509 | 092＇09 | LLS Ig | 20 | 10 | 10 |  |  |
| 2ll9g | 805 zr | 5て9 てV | 00655 | 09199 | LLI SS | E\％ | 90 | 10 |  |  |
| ムじ8t | 802 昭 | GZ2 8¢ | 008－19 | OSG＇IG | LLC ${ }^{\text {b }}$ | $\checkmark 0$ | 50 | 10 |  |  |
| ニLEで | b06ec | 966＇¢ | 00LC 9t | OS6＇9t | LLEて | 90 | $\downarrow 0$ | 10 |  |  |
| 21言9¢ | 80982 | 529＇6己 | 00レても | OGE゙で | 11698 | 90 | $\varepsilon 0$ | 10 |  |  |
| 1156Z | 8089 | SZE ¢も | 00G＇L | OSL゙2 | 2LG6Z | $\angle 0$ | 20 | 10 |  |  |
| 1LLCL | B00＇レて | GZOLZ |  | OG1．EE | レレレをて | 80 | 10 | 10 | 8 | $\downarrow 2$ |
| ［㿾5 | ［ $¢$ ］S | ［］ 5 | ［t］S | IdS／003 | －0ヨ1 1 dS | EM | ZM | LA | H | 1 |


| 00¢L2L | 00＇日もゆ | 00＇0gpt | 00 ＋996 | 00＇6691 | 00 Cl 21 | Wins |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0025 | と¢も 25 | 29 CG | 297＇19 | 0 OZ ¢9 | $002 \pm 9$ | 10 | 10 | 80 |  |  |
| SZ2 95 | 4．92＇LG | ع8日 6 | ¢¢¢ ${ }^{\text {cto }}$ | geosg | 9で99 | 10 | でO | 10 |  |  |
| 9ziog | 298 27 | ¢86 $4 t$ | \＆EL＇LG | 52889 | gzt 0s | 20 | 10 | 10 |  |  |
| Ogit 29 | 001 Ls | 00\％＇19 | 00619 | 09689 | 0G225 | 10 | $\varepsilon 0$ | 90 |  |  |
| oss 15 | 002 2 | 00 E | $002<9$ | OG9 85 | 05919 | 20 | 20 | 90 |  |  |
| gcs $\mathrm{ct}_{5}$ | 008＇¢ ${ }^{\text {d }}$ | 00t $\mathrm{Cb}^{\text {b }}$ | 000 \＆¢ | $0 ¢ \downarrow$－ | Osc sb | 80 | 10 | 90 |  |  |
| G LZ 65 | Ectoc | LLS OS | 490＇19 | ci929 | GLZ 65 | 10 | ＋0 | 90 |  |  |
| SLL ES | ¢cG $9 t$ | 2199\％ | 29 LS | SLt 89 | GLL ¢G | 20 | $\varepsilon$ | 90 |  |  |
| GLO 2 V | \＆c9＇z | くいです | 2908G |  | 920.20 | $\varepsilon 0$ | 20 | $9{ }^{\circ} \mathrm{O}$ |  |  |
| G26 0t | E $¢ 1.8 \varepsilon$ | LLE 8E | 1988 | 920 OS | g26 07 | $\checkmark 0$ | 10 | 50 |  |  |
| 00809 | 2916 6 | cee 6 t | EES 19 | 00929 | 00809 | 10 | G0 | $\dagger 0$ |  |  |
| 002＇ts | 4985 | をef＇g | EEE 19 | COE B9 | 00t＇rs | 20 | $\dagger 0$ | $\square 0$ |  |  |
| 009 旳 | 496＇tb | EEDてt | ¢EL＇¢G | OOL 6 S | 009＇86 | $\varepsilon 0$ | $\varepsilon 6$ | to |  |  |
| 005 Z | 49088 | ¢ELRE | CEG＇80 | 0066 | 009＇2b | $\checkmark 0$ | 20 | $\mathrm{t}^{\prime} 0$ |  |  |
| 00t 98 | LSく＇の | とEZ VC | EEL＇tr | 0025 | 00t＇si | 50 | 10 | $\nabla^{\prime} 0$ |  |  |
| sてを 79 | 001＇6t | 0¢ド6t | 009＇19 | ¢ZE 79 | ¢ 2 ＇z9 | 10 | 90 | $\varepsilon \cdot 0$ |  |  |
| 52895 | 002 Gb | osでg | 00t 29 | 521的 | 9ZZ 95 | 20 | 9.0 | $\varepsilon 0$ |  |  |
| çios | OOE It | CsE゙レ | OOZ ES | g\％beg | S2105 | $8 \cdot 0$ | ${ }^{\circ} \mathrm{O}$ | $\varepsilon 0$ |  |  |
| GzO \＄ | 00゙く过 | 0 Cb LE | 000＇6s | çL 68 | cza＇or | $\checkmark 0$ | $\varepsilon \%$ | $\varepsilon{ }^{\text {c }}$ |  |  |
| gz6 18 | oos Ec | OSce | 009＇06 | SZS ¢ | GZ6 2 E | 50 | z＇0 | \＆0 |  |  |
| cza 18 | 00962 | 05962 | 00900 | çELV | GZ8 LE | 90 | 1＇0 | $\varepsilon 6$ |  |  |
| OS8 89 | cet 8 t | L96的 | 4991.9 | 09129 | 0¢8 E9 | L＇o | 10 | 20 |  |  |
| OS 229 | ECGbt | L95 | L9t 25 | $06^{6} / 29$ | OS 215 | 20 | 90 | 20 |  |  |
| $0 ¢ 9$ ¢g | ¢c90t | L9900 | $\angle 9 Z E G$ | OSLes | OS9 L5 | $\varepsilon{ }^{6} 0$ | $\mathrm{G}^{\prime} 0$ | 20 |  |  |
| OGs ¢ | ¢ 1298 | L9498 | 4906 | 099＇60 | DSS 5 | bo | $\pm 0$ | 20 |  |  |
| OSt 68 | ¢¢6＇z¢ | 298 Z | L98 6 | $0 \delta^{\prime} 5$ | O¢t 68 | 9.0 | $\varepsilon^{\prime} 0$ | z0 |  |  |
| OGE E | ¢ ¢ 682 | 29688 | L9900 | OSL 16 | OSE＇6E | 90 | z＇0 | 30 |  |  |
| 092＇ 2 | EcD gz | 690 ç | tst＇98 | O9698 | Osz＇lz | 10 | 10 | $2{ }^{\prime}$ |  |  |
| SLE 99 | 1920 | 8822y | E¢L LS | 94619 | 5LE 99 | 10 | 80 | L＇0 |  |  |
| SIZ 65 | 498 ct | 888 ¢p | ¢EG 45 | 52L＇LS | ctz 65 | 20 | 10 | 10 |  |  |
| SLL ¢G | 29665 | 886 68 | ¢EE ES | SLG＇E | GLl ES | $8 \cdot 0$ | 90 | 10 |  |  |
| SLO 2 t | 290＇98 | C80 98 | Cel $6 \downarrow$ | 5LE 6\％ | G20 26 | $\pm 0$ | 96 | しわ |  |  |
| SL6 0 t | L9128 | ع81 28 | Ec6 $\dagger t$ | GLL＇so | 9260\％ | 90 | $\bigcirc 0$ | 10 |  |  |
| g 28 ＇v | 19288 | ¢ $\mathrm{BL}^{\prime}$＇日Z | EEL $0 t$ | GL6 6 b | ¢ $\angle 8.08$ | 90 | $\varepsilon 0$ | $1{ }^{\prime} 0$ |  |  |
| GLI 8 L | 49\％$\downarrow$ 2 | cas bz | E¢G＇ 98 | $92 \angle \mathrm{PE}$ | GEL＇日Z | 40 | z＇0 | 10 |  |  |
| 549 Z | L9toz | cotoz | ELE 乙¢ | ¢LS＇ze | SL9 ZV | a＇0 | 10 | 10 | $t$ | 切 |
| ［1］5 | ［ह］S | ［z］s | ［1］s | 1 dsiogl | －0．314 | EM | Z．th | LAM | W | $\perp$ |


| T | M | W1 | W2 | W3 | SPTfEDO | EDDISPT | S[1] | S[2] | \$[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 4 | 0.1 | 01 | 08 | 24.992 | 23108 | 10450 | 22600 | 22.883 | 24.992 |
|  |  | 0.1 | 02 | 07 | 30.092 | 25808 | 13.050 | 25300 | 25883 | 30092 |
|  |  | 01 | 03 | 06 | 35192 | 28508 | 15.650 | 28006 | 28.883 | 35192 |
|  |  | 01 | 0.4 | 05 | 40292 | 31208 | 18. 250 | 30705 | 31883 | 40.292 |
|  |  | 01 | 05 | 0.4 | 45392 | 33.908 | 20850 | 33.400 | 34883 | 45.392 |
|  |  | 01 | 06 | 0.3 | 5D 492 | 36.608 | 23450 | 36100 | 37883 | 50.492 |
|  |  | 01 | 07 | 02 | 55592 | 35308 | 26050 | 38800 | 40.883 | 55592 |
|  |  | 01 | 08 | 0.1 | 60692 | 42008 | 28650 | 41.50 ${ }^{\text {c }}$ | 43883 | 60692 |
|  |  | 02 | 0.1 | 07 | 28 883 | 27.517 | 15300 | 25500 | 26767 | 28883 |
|  |  | 0.2 | 02 | 06 | 33.983 | 30217 | 17.900 | 29200 | 29.767 | 33983 |
|  |  | 02 | 03 | 05 | 39083 | 32917 | 20500 | 31.906 | 32.767 | 39083 |
|  |  | 02 | 0.4 | 04 | 44183 | 35.617 | 23100 | 34.600 | 35767 | 44.183 |
|  |  | 02 | 05 | © 3 | 49283 | 38317 | 25700 | 37.30 Fb | 38767 | 49283 |
|  |  | 02 | 0.6 | 02 | 54383 | 41017 | 28300 | 40005 | 41767 | 54.383 |
|  |  | 02 | 07 | B1 | 59493 | 43717 | 30900 | $42.70{ }^{4}$ | 44767 | 59483 |
|  |  | 03 | 01 | 06 | 32775 | 31.925 | 20150 | 30.400 | 30650 | 32.775 |
|  |  | 03 | D2 | 05 | 37875 | 34625 | 22,750 | 33.100 | 33.650 | 37875 |
|  |  | 03 | 03 | D 4 | 42.975 | 37325 | 25.350 | 35.800 | 36650 | 42975 |
|  |  | 0.3 | 0.4 | 03 | 48.075 | 40.025 | 27950 | 38.500 | 39650 | 48.075 |
|  |  | 0.3 | 05 | 02 | 53.175 | 42725 | 30550 | 41.200 | 42.650 | 53175 |
|  |  | 0.3 | 06 | 0.1 | 58275 | 45425 | 33150 | 4390 | 45650 | 58.275 |
|  |  | 0.4 | 01 | 05 | 36.667 | 36333 | 26000 | 37.360 | 34.533 | 36667 |
|  |  | 04 | 02 | 04 | 41.767 | 39033 | 27.600 | 37.060 | 37.533 | 41767 |
|  |  | 04 | 03 | 03 | 46867 | 41.733 | 30206 | 39700 | 40533 | 46867 |
|  |  | 04 | 04 | 02 | 51.967 | 44,433 | 32800 | 42.400 | 43533 | 51.967 |
|  |  | 04 | 05 | 01 | 57.067 | 47133 | 35400 | 45100 | 46533 | 57.067 |
|  |  | 0.5 | 01 | 04 | 40.558 | 40742 | 29850 | 38200 | 38417 | 40558 |
|  |  | 05 | 02 | 03 | 45658 | 43442 | 32450 | 40200 | 41417 | 45 ¢5\% |
|  |  | 05 | 03 | 02 | 50.758 | 46142 | 35.050 | 43680 | 44.417 | 50758 |
|  |  | 0.5 | 04 | 0.1 | 55858 | 48842 | 37650 | 46300 | 47.417 | 55858 |
|  |  | 06 | 0.1 | 03 | 44.450 | 45.150 | 34.700 | 42100 | 42.300 | 44450 |
|  |  | 0.6 | 0.2 | 02 | 49.550 | 47.850 | 37.300 | 44880 | 45.300 | 49550 |
|  |  | 06 | 03 | 0.1 | 54650 | 50.550 | 39.900 | 47500 | 48300 | 54650 |
|  |  | 07 | 01 | 0.2 | 48342 | 49.558 | 39.550 | 46000 | 46183 | 48.342 |
|  |  | 0.7 | 0.2 | 0.1 | 53442 | 52258 | 42.150 | 48700 | 49.183 | 53442 |
|  |  | 08 | 0.1 | 0.1 | 52233 | 53.967 | 44400 | 49900 | 50.067 | 52233 |
| Sum |  |  |  |  | 1555 ¢0 | 142900 | 1002.00 | 136800 | 140200 | 165500 |


| T | M | W1 | W2 | W3 | SPTPED | EDDISPT | S[1] | S[2] | S[3] | $5[4]$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 5 | 0.1 | 0.1 | 08 | 25433 | 23.667 | 10875 | 23142 | 23225 | 25433 |
|  |  | 0.1 | 02 | 0.7 | 30.833 | 26.767 | 13.775 | 26242 | 26.425 | 36833 |
|  |  | 0.1 | 03 | 0.6 | 36233 | 29867 | 16.675 | 29.342 | 29625 | 36233 |
|  |  | 0.1 | 04 | 0.5 | 41.633 | 32.967 | 19.575 | 32.442 | 32825 | 41.653 |
|  |  | 01 | 05 | 04 | 47.033 | 36.067 | 22475 | 35542 | 36025 | 47033 |
|  |  | 0.1 | 06 | 03 | 52.433 | 39167 | 25.375 | 38642 | 39225 | 52433 |
|  |  | 0.1 | 07 | 02 | 57.833 | 42.267 | 28 275 | 41742 | 42.425 | 57833 |
|  |  | 0.1 | 08 | 0.1 | 63.233 | 45.367 | 31.175 | $44 \mathrm{B42}$ | 45.625 | 63233 |
|  |  | 0.2 | 01 | 07 | 29487 | 28.233 | 15.850 | 27.183 | 27250 | 29467 |
|  |  | 02 | 02 | 06 | 34.867 | 31.333 | 18.750 | 30.283 | 30450 | 34867 |
|  |  | 02 | 03 | 05 | 40.267 | 34.433 | 21.650 | 33383 | 33650 | 40267 |
|  |  | 02 | 04 | 0.4 | 45.667 | 37.533 | 24.550 | 36483 | 36.850 | 45667 |
|  |  | 02 | 0.5 | 03 | 51.067 | 40633 | 27.450 | 39583 | 40.050 | 51.067 |
|  |  | 0.2 | 0.6 | 02 | 56467 | 43.733 | 30.350 | 42683 | 43.250 | 56467 |
|  |  | 02 | 0.7 | 0.1 | 61.867 | 45833 | 33.250 | 45783 | 46.450 | 61867 |
|  |  | 0.3 | 0.1 | 0.6 | 33500 | 32800 | 20.825 | 31.225 | 31275 | 33500 |
|  |  | 0.3 | 02 | 0.5 | 38.900 | 35900 | 23.725 | 34.325 | 34475 | 38900 |
|  |  | 0.3 | 03 | 0.4 | 44.300 | 39000 | 25625 | 37425 | 37.675 | 44300 |
|  |  | 03 | 0.4 | 0.3 | 49.700 | 42.100 | 29.525 | 40525 | 40.875 | 49700 |
|  |  | 0.3 | 0.5 | 02 | 55100 | 45.200 | 32.425 | 43625 | 44075 | 55100 |
|  |  | 03 | 06 | 01 | 60500 | 48300 | 35.325 | 46725 | 47.275 | 60.500 |
|  |  | 04 | 01 | 0.5 | 37.533 | 37.367 | 25850 | 35267 | 35300 | 37533 |
|  |  | 04 | 02 | 04 | 42933 | 40467 | 28700 | 38367 | 38.500 | 42.933 |
|  |  | 0.4 | 03 | 03 | 48333 | 43567 | 31.600 | 41.467 | 41700 | 48.333 |
|  |  | 04 | 04 | 02 | 53.733 | 46667 | 34500 | 44.567 | 44900 | 53.733 |
|  |  | 04 | 0.5 | 01 | 59133 | 49.767 | 37.400 | 47.667 | 48100 | 59.133 |
|  |  | 05 | 0.1 | 04 | 41567 | 41.933 | 30775 | 39308 | 39325 | 41567 |
|  |  | 05 | 02 | 0.3 | 46967 | 45033 | 33675 | 42408 | 42.525 | 46.967 |
|  |  | 05 | 03 | 02 | 52.367 | 48133 | 36.575 | 45508 | 45725 | 52.367 |
|  |  | 0.5 | 0.4 | 01 | 57.767 | 54.233 | 39475 | 48608 | 48925 | 57767 |
|  |  | 0.6 | 0.1 | 0.3 | 45600 | 46.506 | 35750 | 43.350 | 43350 | 45600 |
|  |  | 06 | 02 | 02 | 51000 | 49.600 | 38.650 | 46.450 | 46550 | 51.000 |
|  |  | 06 | 0.3 | 01 | 56400 | 52.700 | 41550 | 49.550 | 49.750 | 56.400 |
|  |  | 07 | 0.1 | 02 | 49633 | 51.067 | 40725 | 47.392 | 47.375 | 49633 |
|  |  | 07 | 02 | 0.1 | 5503.3 | 54167 | 43625 | 50492 | 50575 | 55033 |
|  |  | 08 | 01 | 0.1 | 53667 | 55633 | 45.700 | 51433 | 51.400 | 53667 |
|  |  | Súm |  |  | 1708.00 | 149600 | 1053.00 | 143300 | 144300 | 170800 |


| $T$ | M | W1 | W2 | W／3 | SPTJEDD | EDDISPT | S［1］ | \＄［2］ | S［3］ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 6 | 0.1 | 01 | 0.8 | 25.875 | 24225 | 11300 | 23.683 | 23.667 | 25875 |
|  |  | 01 | 02 | 07 | 31.575 | 27.725 | 14500 | 27.183 | 27.167 | 31575 |
|  |  | 01 | 03 | 06 | 37275 | 31.225 | 17700 | 30683 | 30.667 | 37275 |
|  |  | 01 | 0.4 | 05 | 42.975 | 34725 | 20.900 | 34183 | 34167 | 42975 |
|  |  | 01 | 05 | 0.4 | 48675 | 38225 | 24.100 | 37.683 | 37667 | 48.675 |
|  |  | 01 | 06 | 03 | 54375 | 41.725 | 27305 | 41183 | 41.167 | 54.375 |
|  |  | 01 | 0.7 | D 2 | 60075 | 45225 | 30500 | 44683 | 44667 | 60075 |
|  |  | ［1 | 08 | 01 | 65.775 | 48725 | 33.700 | 48183 | 48167 | 65.775 |
|  |  | 02 | 01 | 07 | 30.050 | 28950 | 16．40以 | 27.867 | 27833 | 30.050 |
|  |  | 02 | 02 | 06 | 35.750 | 32.450 | 19．60b | 31367 | \＄1 333 | 35.750 |
|  |  | 62 | 0.3 | 05 | 41459 | 35.950 | $22.80 \square$ | 34867 | 34833 | 41450 |
|  |  | 02 | 04 | ［4 | 47.150 | 39450 | 26000 | 36367 | 38333 | 47．1．50 |
|  |  | 02 | 05 | 03 | 52.850 | 42950 | 29200 | 41.867 | 41 B33 | 52850 |
|  |  | 02 | 06 | 0.2 | 58550 | 46450 | 32400 | 45367 | 45.333 | 5 E 550 |
|  |  | 0.2 | 07 | B1 | 64250 | 49950 | 35600 | 48867 | 48833 | 64250 |
|  |  | 0.3 | 01 | 『6 | 34225 | 33675 | 21500 | 32.050 | 32 DOO | 34225 |
|  |  | 03 | § 2 | 05 | 39.925 | 37175 | 24700 | 35550 | 35500 | 39.925 |
|  |  | 63 | 03 | 04 | 45625 | 40 675 | 27.900 | 39.050 | 39000 | 45.625 |
|  |  | 03 | 04 | 03 | 51.325 | 44175 | 31.100 | 42.550 | 42500 | 51.325 |
|  |  | 03 | 》 5 | 0.2 | 57025 | 47.675 | 34.300 | 46.050 | 46000 | 57.025 |
|  |  | 03 | 06 | 01 | 62.725 | 51175 | 37500 | 49550 | 49500 | 62.725 |
|  |  | 04 | 01 | D 5 | 3 B 400 | 38400 | 26601 | 36233 | 36.167 | 38400 |
|  |  | D 4 | 02 | 04 | 44.100 | 41.900 | 29800 | 39733 | 39667 | 44．103 |
|  |  | 04 | 03 | Q3 | 49.800 | 45400 | 33000 | 43233 | 43167 | 49.800 |
|  |  | 04 | 0.4 | 02 | 55500 | 48.900 | 36200 | $4{ }^{4} 733$ | 46.667 | 55500 |
|  |  | 04 | 0.5 | 01 | 61200 | 52.400 | 39400 | 50.233 | 50.167 | 61200 |
|  |  | 05 | 01 | 04 | 42575 | 43125 | 31.700 | 40417 | 40333 | 42575 |
|  |  | 0.5 | 02 | 03 | 48275 | 46.625 | 34900 | 43.917 | 43.833 | 48.275 |
|  |  | 05 | 03 | 02 | 53.97 .5 | 50125 | 38100 | 47.417 | 47333 | 53975 |
|  |  | 05 | 0.4 | 0.1 | 59675 | 53625 | 41.300 | 50.917 | 50.833 | 59675 |
|  |  | 0.6 | 01 | 03 | 46750 | 47．850 | 36800 | 44600 | 44．500 | 46.750 |
|  |  | 06 | 02 | 02 | 52，450 | 51350 | 40000 | 48100 | 48000 | 52450 |
|  |  | 06 | 03 | 0.1 | 58150 | 54850 | 43.200 | 51600 | 51500 | 50.150 |
|  |  | 07 | 01 | 0.2 | 50925 | 52575 | 41.500 | 46783 | 48567 | 50925 |
|  |  | 07 | 02 | 0.1 | 56625 | 56075 | 45.100 | $522 \mathrm{B3}$ | 52167 | 56625 |
|  |  | 08 | 0.1 | 01 | 55． 100 | 57300 | 47000 | 52967 | 52 B 33 | 55100 |
| SUM |  |  |  |  | 1761.00 | 155300 | 1104.00 | 1498，00 | 149600 | 1761.00 |


| T | M | प＋1 | W2 | W13 | SPTHEDD | EDDISPT | S［1］ | S［2］ | S［3］ | S［4］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 7 | 01 | 0.1 | 0.8 | 26317 | 24783 | 11.725 | 24.225 | 24208 | 26.317 |
|  |  | 01 | 0.2 | 07 | 32317 | 28． 683 | 15.225 | 28.125 | 28108 | 32.317 |
|  |  | ［0． 1 | 03 | 0.6 | 38317 | 32583 | 18725 | 32，025 | 32008 | 38．317 |
|  |  | 01 | 04 | 0.5 | 44．317 | 36483 | 22225 | 35925 | 35908 | 44317 |
|  |  | 01 | 0.5 | 0.4 | 50317 | 46383 | 25725 | 39825 | 39808 | 50317 |
|  |  | 01 | 0.6 | 0.3 | 56317 | 44283 | 29225 | 43725 | 43708 | 56317 |
|  |  | 01 | 07 | 02 | 62.317 | 48163 | 32725 | 47.625 | 47608 | 62317 |
|  |  | 01 | 08 | 01 | 68317 | 52.083 | 36225 | 51.525 | 51508 | 68.317 |
|  |  | 02 | 01 | 0.7 | 30533 | 29667 | 16950 | 28550 | 28517 | 30633 |
|  |  | 0.2 | 02 | 06 | 36.633 | 33567 | 20．450 | 32.450 | 32417 | 36.633 |
|  |  | 02 | 03 | 05 | 42.633 | 37467 | 23.950 | 35350 | 36317 | 42633 |
|  |  | 02 | 04 | 0.4 | 48.633 | 41367 | 27450 | 40.250 | 40217 | 48633 |
|  |  | 02 | 05 | 03 | 54.633 | 45267 | 30950 | 44.150 | 44.117 | 54633 |
|  |  | 02 | 06 | 02 | 60.633 | 49167 | 34450 | 48.050 | 48.017 | 60633 |
|  |  | 02 | 07 | 01 | 66633 | 53.067 | 37950 | 51950 | 51.917 | 66.633 |
|  |  | 0.3 | 01 | 06 | 34950 | 34.550 | 22.175 | 32875 | 32.825 | 34.950 |
|  |  | 03 | 02 | 05 | 40950 | 38.450 | 25.675 | 36775 | 36.725 | 40.950 |
|  |  | 03 | 0.3 | 04 | 46950 | 42.350 | 29175 | 40675 | 40.625 | 46．950 |
|  |  | 0.3 | 0.4 | 0.3 | 52950 | 46.250 | 32675 | 44575 | 44.525 | 52．950 |
|  |  | 0.3 | 0.5 | 02 | 59950 | 50150 | 36175 | 48475 | 48425 | 58950 |
|  |  | ¢ 3 | 06 | 01 | 64950 | 54050 | 39.675 | b2 375 | 52.325 | 64950 |
|  |  | 0.4 | 0.1 | 05 | 39.267 | 39 433 | 27400 | 37200 | 37.133 | 39267 |
|  |  | 04 | 02 | 04 | 45267 | 43.333 | 30900 | 41100 | 41033 | 45.267 |
|  |  | 04 | 03 | 03 | 51，267 | 47233 | 34400 | 45.000 | 44933 | 51267 |
|  |  | 04 | 04 | ¢ 2 | 57267 | 51133 | 37.900 | 48900 | 48.833 | 57267 |
|  |  | 04 | 05 | 01 | 63267 | 55.033 | 41400 | 52809 | 52.733 | 63267 |
|  |  | 05 | 01 | 04 | 43583 | 44.317 | 32625 | 41525 | 41.442 | 43.583 |
|  |  | 05 | 02 | 03 | 49583 | 48.217 | 36125 | 45425 | 45342 | 49.683 |
|  |  | 05 | 03 | 02 | 55583 | 52.117 | 39625 | 49325 | 49242 | 55.583 |
|  |  | 05 | 04 | 0.1 | 61583 | 56017 | 43125 | 53.225 | 53142 | 61583 |
|  |  | 06 | 01 | 0.3 | 47900 | 49200 | 37850 | 45650 | 45750 | 47900 |
|  |  | 06 | 02 | 0.2 | 53900 | 53100 | 41350 | 49750 | 49650 | 53900 |
|  |  | 06 | 03 | 0.1 | 59900 | 57000 | 44 B50 | 53.650 | 53550 | 59900 |
|  |  | 07 | 01 | 0.2 | 52217 | 54083 | 43.075 | 50.175 | 50058 | 52217 |
|  |  | 0.7 | 02 | 01 | 58217 | 57983 | 46.575 | 54075 | 53958 | 58.217 |
|  |  | 08 | 01 | 01 | 56533 | 58.967 | 48300 | 54500 | 54367 | 55.533 |
| SUM |  |  |  |  | 181400 | 163000 | 1155.00 | 156300 | 156100 | 181400 |


| T | 0 | W1 | W22 | Wiv | \$PTIEDD | EDDSPT | S]1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 8 | 0.1 | 02 | 0.7 | \$3 058 | 29.642 | 15950 | 29067 | 29.050 | 33058 |
|  |  | 0.1 | 03 | 66 | 39.358 | 33.942 | 19750 | 33367 | 33350 | 39358 |
|  |  | 0.1 | 04 | 0.5 | 45.658 | 38.242 | 23550 | 37667 | 37.650 | 45658 |
|  |  | 01 | 05 | 0.4 | 51.958 | 42,5-42 | 27.350 | 41967 | 41.950 | 51.958 |
|  |  | 01 | 06 | 0.3 | 58258 | 46842 | 31.150 | 46267 | 46250 | 58.258 |
|  |  | 01 | 0.7 | 02 | 64.559 | 51142 | 3*950 | 50567 | 50.550 | 64.558 |
|  |  | 0.1 | 08 | 01 | 70.858 | 55442 | 38750 | 54.867 | 54.850 | 70858 |
|  |  | 02 | 0.1 | 0.7 | 31217 | 30.383 | 17500 | 29233 | 29.200 | 31217 |
|  |  | 02 | 0.2 | 06 | 37517 | 34683 | 21.300 | 33533 | 33500 | 37517 |
|  |  | 02 | 0.3 | 05 | 43817 | 38983 | 25.100 | 37833 | 37.800 | 43817 |
|  |  | 02 | 0.4 | 04 | 50117 | 43283 | 28.900 | 42.133 | 42.100 | 50117 |
|  |  | 02 | 05 | 0.3 | 56417 | 47.583 | 32700 | 48433 | 46400 | 56.417 |
|  |  | 0.2 | 06 | 02 | 62717 | 51883 | 36500 | 50.733 | 50700 | 62.717 |
|  |  | 0.2 | 0.7 | W1 | 69.017 | 56183 | 40.300 | 55033 | 55000 | 69.017 |
|  |  | 0.3 | 01 | 06 | 35.675 | 35425 | 22,850 | 33.700 | 33650 | 35 的5 |
|  |  | 0.3 | 0.2 | 05 | 41.975 | 39725 | 26.650 | 38.090 | 37.950 | 41975 |
|  |  | 0.3 | 03 | 04 | 48.275 | 44025 | 30.450 | 42.390 | 42.250 | 48275 |
|  |  | 03 | 04 | 0.3 | 54575 | 48325 | 34250 | 46600 | 46550 | 54.575 |
|  |  | 03 | 05 | 02 | 60875 | 52625 | 3 O 050 | 50800 | 50850 | 60875 |
|  |  | 03 | 06 | 01 | 67.175 | 56925 | 41.850 | 55200 | 55.150 | 67175 |
|  |  | 04 | 01 | 05 | 40133 | 40467 | 28200 | 38167 | 38100 | 40133 |
|  |  | 0.4 | 02 | 04 | 46433 | 44.767 | 32.000 | 42467 | 42400 | 46.433 |
|  |  | 0.4 | 03 | 03 | 52.733 | 49067 | 35800 | 46.767 | 46700 | 52.733 |
|  |  | 0.4 | 04 | 02 | 59.033 | 53367 | 39600 | 51.067 | 51000 | 59.033 |
|  |  | 0.4 | 05 | 01 | 65.333 | 57.667 | 43400 | 55.367 | 55300 | 65.333 |
|  |  | 0.5 | 0.1 | 04 | 44.592 | 45.508 | 33.550 | 42633 | 42550 | 44.592 |
|  |  | 05 | 0.2 | 03 | 50892 | 49.808 | 37.350 | 46933 | 46850 | 50.892 |
|  |  | 05 | 0.3 | 02 | 57.192 | 54.108 | 41.150 44.950 | 51233 55533 | 51.150 55.450 | 57.992 63.492 |
|  |  | 05 | 0.4 | 0.1 | 63492 | 58.40 B 50.550 | 44.950 38900 | 47100 | 57.450 47.000 | 63.492 49.050 |
|  |  | 0.6 06 | -1 | 03 02 | 49050 55350 | 50.550 54950 | 38900 42.700 | 51.400 | 47.000 51300 | 55.350 |
|  |  | 06 | 03 | 01 | 61650 | 59.150 | 46.500 | 55.700 | 55600 | 61.650 |
|  |  | 07 | 01 | 02 | 53508 | 55.592 | 44250 | 51567 | 51450 | 53508 |
|  |  | 07 | 02 | 01 | 59808 | 59892 | 40050 | 55 Bb 7 | 55750 | 59808 |
|  |  | 08 | 01 | 01 | 57967 | 60633 | 49600 | 56.033 | 55900 | 57.967 |
| SUM |  |  |  |  | 189700 | 169700 | 120600 | 162800 | 152600 | 186700 |


| T | H | W1 | W2 | W3 | SPTJEDD | EDDISPT | S 11 | S[2] | \$[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 26 | 4 | 01 | 01 | 08 | 28633 | 13267 | 13275 | 26.342 | 26425 | 28633 |
|  |  | 01 | 02 | 07 | 33633 | 15.867 | 158.75 | 29.042 | 29225 | 33633 |
|  |  | 01 | 03 | 06 | 38633 | 18.467 | 18475 | 31.742 | 32025 | 38633 |
|  |  | 01 | 04 | 05 | 43633 | 21067 | 21075 | 34442 | 34825 | 43633 |
|  |  | 01 | 05 | 04 | 48633 | 23.667 | 23675 | 37142 | 37625 | 40633 |
|  |  | 01 | 06 | 03 | 53633 | 26.267 | 26275 | 39.842 | 40425 | 53.633 |
|  |  | 01 | 07 | 02 | 58.633 | 28 BE7 | 28.875 | 42542 | 43225 | 58633 |
|  |  | 01 | 09 | 01 | 63633 | 31.457 | 31475 | 45.242 | 46.025 | 63.633 |
|  |  | 02 | 01 | 07 | 32267 | 17.933 | 17950 | 29983 | 30.050 | 32267 |
|  |  | 02 | 02 | 06 | 37267 | 20533 | 20550 | 32693 | 32.850 | 37.267 |
|  |  | 02 | 03 | 05 | 42.267 | 23133 | 23150 | 35383 | 35.650 | 42.267 |
|  |  | 02 | 04 | 04 | 47267 | 25.733 | 29750 | 38083 | 38.450 | 47267 |
|  |  | 02 | 05 | 03 | 52267 | 28.333 | 28350 | 40.783 | 41.250 | 52.267 |
|  |  | 02 | 06 | 02 | 57267 | 30933 | 30.950 | 43483 | 44050 | 53267 |
|  |  | 0.2 | 07 | 01 | 62267 | 33533 | 33550 | 46183 | 46850 | 62.267 |
|  |  | 0.3 | 01 | 06 | 35.900 | 22600 | 22.625 | 33625 | 33675 | 35900 |
|  |  | 03 | 02 | 0.5 | 40900 | 25.200 | 25.225 | 36.325 | 36.475 | 40900 |
|  |  | 03 | 0.3 | 04 | 45900 | 27.800 | 27325 | 39025 | 39.275 | 45900 |
|  |  | 0.3 | 0.4 | 4 | 50900 | 30400 | 30425 | 41.725 | 42.075 | 50.900 |
|  |  | 0.3 | 0.5 | 02 | 55900 | 33.000 | 33025 | 44.425 | 44.875 | 55900 |
|  |  | 0.3 | 06 | 01 | 60900 | 35600 | 35.625 | 47.125 | 47.675 | 60.900 |
|  |  | 04 | 0.1 | 05 | 39533 | 27.267 | 27300 | 37.267 | 37300 | 39533 |
|  |  | 04 | 02 | 0.4 | 44533 | 29.867 | 29900 | 39.967 | 40.100 | 44533 |
|  |  | 04 | 03 | 0.3 | 49533 | 32467 | 32.500 | 42.667 | 42.900 | 49533 |
|  |  | 04 | 14 | 02 | 54533 | 35067 | 35.100 | 45.367 | 45.700 | 54533 |
|  |  | 04 | 05 | D1 | 59.533 | 37667 | 37.700 | 48.067 | 48500 | 59533 |
|  |  | 05 | 01 | 04 | 43.167 | 31.933 | 31.975 | 40.908 | 49.925 | 43167 |
|  |  | 05 | 02 | 03 | 48.167 | 34.533 | 34575 | 43608 | 43.725 | 48167 |
|  |  | 05 | 03 | 0.2 | 53.167 | 37.133 | 37.175 | 45309 | 46525 | 53.167 |
|  |  | 05 | 04 | D. 1 | 58.167 | 39733 | 39775 | 49008 | 49.325 | 58167 |
|  |  | 06 | 01 | 0.3 | 46800 | 36.600 | 36650 | 44.550 | 44550 | 46.800 |
|  |  | 06 | 02 | 02 | 51.800 | 39200 | 39.250 | 47.250 | 47350 | 51.800 |
|  |  | 06 | 03 | 01 | 56800 | 41800 | 41.850 | 49.950 | 50150 | 56.800 |
|  |  | 07 | 0.1 | - 2 | 50433 | 41.267 | 41.325 | 48.192 | 48175 | 50.433 |
|  |  | 07 | 0.2 | 01 | 55433 | 43.667 | 43925 | 50.692 | 50.975 | 55.433 |
|  |  | \$, 8 | 01 | 01 | 54.067 | 45933 | 46.000 | 51833 | 51.800 | 54067 |
| SUM |  |  |  |  | 175600 | 108800 | 108500 | 1481.00 | 149100 | 175600 |


| 002981 | 006095 | OW゙しL．96 | 00 LЕしト | 000614 | 002981 | Whs |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| を86＇95 | L9L゙ちら | 006 Hg | 009 ${ }^{2}$ | EES $8 t$ | ¢ ¢ 699 | 10 | 10 | 80 |  |  |
| 21989 | BGEt5 | GLt $\mathrm{p}_{5}$ | 988＇9t | 14日 96 | 21985 | 10 | $z 0$ | $\angle 0$ |  |  |
| LLOEG | B98 65 | 9460 | GL9 ¢ | L19¢t | L6＇\＆9 | 20 | 10 | L0 |  |  |
| 00809 | 056 Es | 090＇09 | OGb st | 0069\％ | 00¢ 09 | 10 | $\varepsilon 0$ | 90 |  |  |
| O0205 | OGtog | oss 05 | 056 | 006.16 | cotbs | で0 | CO | 90 |  |  |
| 0026 | 096＇9b | 0co 2 t | OSL 8 E | 00188 | 00165 | $\varepsilon 0$ | 10 | 90 |  |  |
| E86 19 | 209＇s | G29 ¢¢ | cztep | EBE EO | ¢66．19 | 10 | $\pm 0$ | 90 |  |  |
| ¢SC＇g | Z N$) \mathrm{OS}$ | Szt．09 | gzz＇00 | celot | EBC9 9 | 20 | \％0 | 90 |  |  |
| ¢82＇0G | てゆら9t | 9zg＇sp | ¢̧0＇2E | E869E | c8L 09 | 80 | 20 | G0 |  |  |
| ๕81＇Gp | Z CO ¢ t | SZtet | G28＇E® | EALEE | Est 9b | Fo | 1＇0 | 90 |  |  |
| 29989 | E¢L £ | 002 ¢ | 002 しb | 299 L｜ | ［99＇¢9 | 1.0 | 50 | $\checkmark 0$ |  |  |
| $\angle 9089$ | عe9 6t | 00260 | OOS 日E | 29t 88 | 49085 | 20 | ¢0 | $\checkmark 6$ |  |  |
| L9t 29 | EEL．9t | 00290 | $00 ¢ \mathrm{Sc}$ | L92 58 | 29\％＇29 | E＇0 | ¢0 | $\checkmark 6$ |  |  |
| 4989 | とくgで | 002 zb | DO1 CE | L90 こ¢ | 298＇90 | $\dagger 0$ | z0 | $\square 0$ |  |  |
| く92 した | と¢168 | OOZ 68 | 00682 | 49888 | 298＇しb | 90 | 10 | $\checkmark 5$ |  |  |
| 0¢E cg | szezs | GLLCS | G $\angle 668$ | 05688 | 05c． 59 | 10 | 90 | $\varepsilon 0$ |  |  |
| OGL 69 | szz 6 t | $9_{L L} 60$ | GLL 98 | 05298 | 0926 6 | 20 | 90 | $\varepsilon 0$ |  |  |
| OSl ts | GZL ¢t | 9 26 gb | GL9 EE | OSS EE | 0＇tios | $8 \cdot 0$ | $\bigcirc 0$ | $\varepsilon 0$ |  |  |
| 0 GGP | szz てt | gLz＇zo | GLE 0E | OSE OE | 0¢98\％ | ＋0 | $8 \cdot 0$ | ¢0 |  |  |
| 056 てt | GzL ${ }^{\text {为 }}$ | GLEaE | SLLEZ | 091 22 | 0s6＇z | 50 | 20 | 80 |  |  |
|  | 922 Sc | GLZ＇GE | ct6ez | 09618 | DGE LE | 90 | 10 | ¢0 |  |  |
| EEO＇L9 | LLEZS | OSEZg | Dgz＇ec | E\＆Z 8 C | ع¢0 19 | 10 | 10 | 20 |  |  |
| cet 19 | 46\％ | 0 S 8 8 | OSO SE | ¢ ¢cose | E¢D 19 | 20 | 90 | 20 |  |  |
| eca＇cs | LLESt | OSç\％ | Dsa＇Le | ¢ 8818 | ¢ع8 95 | 80 | G＇0 | 20 |  |  |
| CEZ 05 | く18゙t\％ | $0 ¢ 817$ | 059 昩 | E¢9 87 | E¢COG | $t 0$ | $\checkmark 0$ | 20 |  |  |
| EE9＇\％ | LIE 8E | 0sc\％e | Ost＇g\％ | £ ¢ $\dagger$＇GZ | ces tb | 90 | 80 | 20 |  |  |
| cea＇6e | 218 $\downarrow$ ¢ | OSE $\dagger ¢$ | OSでてz | £¢Z てZ | Ec0 6 E | 90 | 20 | 20 |  |  |
| EEt＇¢E | 21818 | OSE LE | 050＇61 | E¢O6し | ¢¢っ ¢ | 40 | 1＇0 | $2{ }^{\prime}$ |  |  |
| ［1／29 | 806 LS | SZ6＇19 | ¢zs $x$ | LLS 96 | LLC 89 | 10 | 80 | 10 |  |  |
| くんて＇と9 | 80t 8 t | Sで $3 \downarrow$ | ¢ZE ¢¢ | LLE EE | 24.69 | 20 | 10 | 10 |  |  |
| 219＇29 | 806 | 926 | GZ1 0¢ | Lい0を | －16．4c | ¢＇0 | 90 | 10 |  |  |
| 46 LG | 80t し | gzrit | 9Z692 | LL69\％ | 4L6＇LS | ¢0 | 50 | 10 |  |  |
| Lに＇9y | 80628 | St6 4 ¢ | ¢zL \＆z | 2l⿺尢 | LLE90 | 9.0 | b0 | 10 |  |  |
| 41200 | 80ヶ $\downarrow$ ¢ | Sてb $\downarrow \mathrm{E}$ | ¢Zs OZ | 2LGOZ | LLL 4 | 90 | $\varepsilon 0$ | 10 |  |  |
| U1＇ge | 80608 | 9Zb OE | GZE 16 | くしどこし | LH 98 | 40 | 20 | 10 |  |  |
| 41962 | 80t $2 乙$ | GEFL | g 21 | しい | LLF6\％ | 80 | 10 | 10 | 9 | 92 |
| ［b］ | ［c］s | ［2］s | ［i］s | 1dsfage | 00．jlds | EM | zM | 1 M | H | 1 |


| 006081 | 00 あら！ | D0＇9pgl | 00＇0ヵしい | 006815 | 00＇6081 | WIS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 005 gS | ¢¢Z＇¢ | 298 | 008 くt | 8¢でLD | OOS ¢S | 10 | 10 |  |  |  |
| 92026 | 29575 | c89 25 | 008 ct | でだらも | 920 LS | 10 | 20 | $\angle 0$ |  |  |
| 92Lits | 29t 6 ¢ | E8G 64 | 00s＇zt | でゅで | gZL＇L言 | 20 | 10 | $\leq 0$ |  |  |
| Osc＇ss | 006 IS | 00025 | 00¢＇ct | 09t ¢ t | OGG 89 | $1 \cdot 0$ | $\varepsilon 0$ | 90 |  |  |
| O¢\％¢¢ | 0088 | 006 旳 | 009＇00 | OSG Dt | 092 cis | z＇0 | zo | 90 |  |  |
| 0S6 4 | 00290 | 008 ct | $0022 \angle$ | 09928 | 05627 | $\varepsilon 0$ | L＇0 | 90 |  |  |
| 92009 | EEC LG | LELG | $0091 \downarrow$ | 899 5 | 920＇09 | 10 | $\bigcirc 0$ | 90 |  |  |
| GLL＇pG | ECl ${ }^{\text {b }}$ | L32 8\％ | 001．88 | 89985 | GLL＇p9 | 20 | E0 | 50 |  |  |
| SLt 6 b | E¢OGO | 215 5 | 00815 | 8GL GE | SLt 6t | $\varepsilon \cdot 0$ | Z＇0 | 50 |  |  |
| Sさん $\ddagger$ | E¢G］ | 210 己t | 006 乙 | 898＇ze | GLL tot | $\pm 0$ | L＇0 | G＇0 |  |  |
| 0096 | 49908 | ces DS | 002 $6 ¢$ | 49968 | 00919 | 10 | 9.0 | to |  |  |
| OLE 95 | 190＇20 | EqG Lb | 00 98 | 492＇98 | 00895 | 20 | $\forall 0$ | ＋0 |  |  |
| 00075 | 498＇0 | と¢t ${ }^{\text {¢ }}$ | $006 \varepsilon \varepsilon$ | 499＇¢¢ | 00015 | E 0 | $\varepsilon 0$ | 50 |  |  |
| 00L9 | L9z＇L5 | と¢Eしゃ | 00018 | Lag Of | 0025t | ＋0 | z＇0 | $\downarrow 0$ |  |  |
| OOS＇0t | 29185 | E¢Z BE | 001＇82 | 49082 | － | 90 | 10 | $\checkmark 0$ |  |  |
| Gzl ¢9 | 0066 | DS6＇6t | $008 \angle 8$ | 9LL＇2¢ | GZ1 E9 | 10 | 90 | $\varepsilon^{\prime} 0$ |  |  |
| Sz8＊9 | 008＇90 | 0989 | 006 ヶ¢ | GLE 吃 | S28 29 | z＇0 | s＇0 | $\varepsilon \square$ |  |  |
| Sくg てg | 00280 | OSLE | 000 ZE | 926 18 | gze＇zs | $8 \cdot 0$ | 0 | $\varepsilon 0$ |  |  |
| 9とでし | 0090 | 0590 | 00l＇6z | SL0 62 | çでくt | $\bigcirc 0$ | ¢0 | $\varepsilon 0$ |  |  |
| ¢でった | OOG 2 E | oss＇ce | 00292 | SLl 9Z | ¢て6＇しb | 95 | z 0 | $\varepsilon 0$ |  |  |
| 58950 | OOt te | DSt 7 | $00 \chi^{\prime}$ ¢ | SLZ CZ | 929＇98 | 90 | 10 | $\varepsilon 0$ |  |  |
| 05979 | ¢ $¢ 66$ | 292 bt | 00695 | ¢咟 $5 ¢$ | 099＇9 | 10 | $\angle 0$ | 20 |  |  |
| OGE GG | をEL90 | 49197 | 000 琯 | ¢86 己¢ | OSE 65 | 20 | 90 | 20 |  |  |
| $050 \pm 9$ | EEOEt | L90＇Et | 001 0¢ | ع80＇0¢ | 090 ¢c | $\varepsilon 6$ | 9.0 | 20 |  |  |
| OSL＇St | EE6 68 | L96＇68 | 002 $2 z$ | £b1＇z | OSL Bb | $\bigcirc 0$ | $\checkmark 0$ | 20 |  |  |
| ostet | ¢¢8 9E | L98＇98 | OOE 㲸 | ESZ $\downarrow$ C | Octict | 50 | \＆0 | 20 |  |  |
| OG1＇ 8 c | EELCE | 292 | 000 L2 | E8E L | 091＇88 | 90 | 20 | 20 |  |  |
| 0 gez | ES9 08 | 2990\％ | 00581 | E80 81 | DG8 乙 | 40 | 10 | z＇0 |  |  |
| 92l＇99 | 2958 | Eş＇sp | 000 汉 | Z65＇£ | GL1 99 | 10 | 80 | 10 |  |  |
| GLP 09 | 19t 9b | £8t cb | $001 \%$ | て60＇L | 52869 | 20 | 10 | 10 |  |  |
| SLS S9 | 298＇20 | c8E で | 00で的 | 261 BZ | 5LG＇gs | $\varepsilon 0$ | 90 | 10 |  |  |
| glz 09 | 29268 | cse 68 | 00¢＇cz | 26Z 52 | ¢LZ＇OS | $\downarrow 0$ | 50 | 10 |  |  |
| SL6 tt | 29198 | E8b 9E | 000 zZ | 26E z2 | 9L6＇by | co | $\downarrow 0$ | 10 |  |  |
| 9 2968 | 290 EE | ced $2 ¢$ | OOS 61 | 26ガあ！ | GL9 6E | 90 | ¢0 | 10 |  |  |
| 9LE＇t¢ | 49662 | ces＇6z | 00991 | 269＇91 | GLE $\dagger$ ¢ | 40 | $2 \prime 0$ | 10 |  |  |
| 9L0 62 | 29892 | 889 9\％ | 00 2 ¢1 | 269＇81 | 92062 | 80 | 10 | 10 | G | 92 |
| ［ t$]$ S | InIs | ［z］s | ［1］ | 1d5／093 | 00310 | EM | LM | LM | W | 1 |


| T | H | W1 | W2 | W3 | SPT/EDD | EDDISPT | S[1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 26 | 7 | 01 | 0.1 | 0.8 | 29958 | 14.542 | 14550 | 27.967 | 27950 | 29.958 |
|  |  | 0.1 | 02 | 0.7 | 35858 | 18042 | 18 0.50 | 31.867 | 31.850 | 35858 |
|  |  | 0.1 | 03 | 06 | 41.758 | 21.542 | 21550 | 35767 | 35.750 | 41.758 |
|  |  | 0.1 | 04 | 05 | 47.65B | 25.042 | 25.050 | 39667 | 39.650 | 47.658 |
|  |  | 0.1 | 05 | 04 | 53.558 | 28.542 | 28.550 | 43.567 | 43.550 | 53.558 |
|  |  | 0.1 | 0.6 | 03 | 59458 | 32042 | 32050 | 47467 | 47450 | 59458 |
|  |  | 01 | 07 | 02 | 65358 | 35542 | 35.550 | 51.367 | 51.350 | 65.358 |
|  |  | 01 | 08 | 01 | 71.258 | 39.042 | 39.050 | 55267 | 55.250 | 71258 |
|  |  | 0.2 | 01 | 0.7 | 34017 | 19583 | 19600 | 32033 | 32.040 | 34.017 |
|  |  | 02 | 02 | 0.6 | 39917 | 23 D83 | 23.100 | 35.933 | 35900 | 39917 |
|  |  | 02 | 0.3 | 0.5 | 45817 | 26.583 | 26.600 | 39833 | 39.800 | 45817 |
|  |  | 02 | 0.4 | 0.4 | 51.717 | 30.063 | 30.100 | 43733 | 43.700 | 51717 |
|  |  | 02 | 0.5 | 03 | 57.617 | 33.663 | 33.600 | 47633 | 47600 | 57617 |
|  |  | 02 | 0.6 | 02 | 63517 | 37.083 | 37.100 | 51.533 | 51500 | 63517 |
|  |  | 02 | 07 | 0.1 | 69417 | 40583 | 40600 | 55433 | 55.400 | 69417 |
|  |  | 03 | 01 | 06 | 38075 | 24625 | 24650 | 36.100 | 36.050 | 38.075 |
|  |  | 03 | 02 | 05 | 43975 | 28125 | 28150 | 40.100 | 39.950 | 43.975 |
|  |  | 0.3 | 03 | 0.4 | 49.875 | 31.625 | 31.650 | 43900 | 43850 | 49.875 |
|  |  | 03 | 0.4 | 0.3 | 55775 | 35.125 | 35150 | 47800 | 47750 | 55775 |
|  |  | 03 | 05 | 0.2 | 61.675 | 38.625 | 38.550 | 51700 | 51650 | 61.675 |
|  |  | 03 | 06 | 0.1 | 67.575 | 42.125 | 42.150 | 55600 | 55.550 | 67.575 |
|  |  | 04 | 01 | 05 | 42.133 | 29667 | 29.700 | 40167 | 40100 | 42.133 |
|  |  | 04 | 02 | 04 | 48033 | 33167 | 33200 | 44067 | 44,000 | 48033 |
|  |  | 0.4 | 03 | 03 | 53933 | 36667 | 36700 | 47.967 | 47.900 | 53933 |
|  |  | 0.4 | 04 | 02 | 59833 | 40.167 | 40.200 | 51867 | 51809 | 59833 |
|  |  | 04 | 05 | 01 | 65733 | 43.667 | 43700 | 55767 | 55.700 | 65733 |
|  |  | 05 | 0.1 | 04 | 46.192 | 34708 | 34750 | 44233 | 44150 | 46.192 |
|  |  | 05 | 0.2 | 03 | 52.092 | 38.208 | 38250 | 48133 | 48.050 | 52.092 |
|  |  | 05 | 0.3 | 0.2 | 57.992 | 41.708 | 41750 | 52033 | 51950 | 57.992 |
|  |  | 05 | 0.4 | 0.1 | 63892 | 45.208 | 45250 | 55.933 | 55850 | 63.892 |
|  |  | 06 | 0.1 | 03 | 50.250 | 39.750 | 39800 | 48.300 | 48200 | 50250 |
|  |  | 06 | 02 | 02 | 56150 | 43.250 | 43.300 | 52.200 | 52100 | 56,150 |
|  |  | 06 | 03 | 61 | 62050 | 46750 | 46.800 | 56100 | 56000 | 62050 |
|  |  | 07 | 01 | 0.2 | 54308 | 44792 | 44850 | 52367 | 52250 | 54.308 |
|  |  | 07 | 02 | 01 | 60208 | 48292 | 48350 | 56.267 | 56150 | 60.208 |
|  |  | 08 01 0.1 |  |  | 58367 | 49833 | 49900 | 56433 | 56300 | 52367 |
| SUM |  |  |  |  | 121500 |  | 124200 | 1676.00 | 167400 | 191500 |
|  |  |  |  |  | SPTIEDD |  |  | 1 5]2] |  |  |
| $T$ | M | W1 | W2 | W3 |  | ERODISPT | S[1] |  | S[3] | S[4] |
| 26 | 8 | 01 | 01 | 08 | 30400 | 14967 | 14975 | 28508 | $\begin{aligned} & 28492 \\ & 27005 \end{aligned}$ |  |
|  |  | 0.1 | 02 | 0.7 | 36600 | 18767 | 18775 | 32.808 |  |  |
|  |  | 0.1 | 03 | 0.6 | 42 BDO | 22567 | 22.575 | 37108 | $\begin{aligned} & 32.792 \\ & 37.092 \end{aligned}$ | 36800 42.800 |
|  |  | 01 | 0.4 | 05 | 49,900 | 26.367 | 26375 | 41408 | 41.392 | 49.000 |
|  |  | 01 | 05 | 04 | 55.200 | 30167 | 30175 | 45708 | 45692 | 55.200 |
|  |  | 01 | 06 | 03 | 61400 | \$3 967 | 33.975 | 5000 B | 49992 | 61.40067600 |
|  |  | 0.1 | 07 | 02 | 67600 | 37767 | 37775 | 54.308 | 54292 |  |
|  |  | 01 | 08 | 0.1 | 73800 | 41567 | 41575 | 58608 | 58592 | 7380034600 |
|  |  | 02 | 0.1 | 0.7 | 34.500 | 20133 | 20150 | 32.717 | 32683 |  |
|  |  | 0.2 | 02 | 06 | 40800 | 23.933 | 23950 | 37017 | 36.983 | 40.80047.000 |
|  |  | 02 | 03 | 0.5 | 47000 | 27733 | 27.750 | 41317 | 41283 |  |
|  |  | 02 | 04 | 0.4 | 53200 | 31533 | 31.550 | 45617 | 45.583 | $\begin{aligned} & 47.000 \\ & 53200 \end{aligned}$ |
|  |  | 02 | 0.5 | 03 | 59400 | 35333 | 35350 | 49.917 | 49883 | 59400 |
|  |  | 02 | 0.6 | © 2 | 65600 | 39.133 | 39.150 | 54.217 | 54183 | 65.600 |
|  |  | 0.2 | 0.7 | D 1 | 71.806 | 42.933 | 42.950 | 58.517 | 58.483 | 71.800 |
|  |  | 0.3 | 01 | D. 6 | 38800 | 25.300 | 25.325 | 36.925 | 36875 | 3880045000 |
|  |  | 0.3 | 0.2 | 05 | 45000 | 29100 | 29125 | 41.225 | 41175 |  |
|  |  | 03 | 03 | 0.4 | 51.200 | 32900 | 32925 | 45.525 | 45475 | $\begin{aligned} & 45000 \\ & 51,200 \end{aligned}$ |
|  |  | 0.3 | 04 | 0.3 | 57.400 | 36.700 | 36725 | 49.825 | 49775 | 57.40063600 |
|  |  | 03 | 0.5 | 0.2 | 63600 | 40500 | 40525 | 54,125 | 54075 |  |
|  |  | 03 | 06 | 01 | 69800 | 44.300 | 44325 | 58425 | 58375 | 63600 69800 |
|  |  | 04 | 01 | 05 | 43000 | 30467 | 30.500 | 41133 | 41067 | $\begin{aligned} & 43000 \\ & 49200 \end{aligned}$ |
|  |  | 04 | 02 | 04 | 49200 | 34257 | 34300 | 45433 | 45367 |  |
|  |  | 0.4 | 03 | 03 | 55400 | 39.067 | 38100 | 49.733 | 49.667 | 5540 g |
|  |  | 04 | 04 | 02 | 61600 | 41867 | 41.900 | 54033 | 53967 | 61. 600 |
|  |  | 04 | 0.5 | 01 | 67.800 | 45667 | 45700 | 58333 | 58.257 | 6780047200 |
|  |  | 05 | 01 | 04 | 47200 | 35.6す3 | 35675 | 45342 | 45.258 |  |
|  |  | 05 | G2 | 0.3 | 53406 | 39,433 | 39475 | 49642 | 49.658 | $\begin{aligned} & 47200 \\ & 53400 \end{aligned}$ |
|  |  | 05 | 03 | 0.2 | 59600 | 43233 | 43275 | 53942 | 53858 | $59600$ |
|  |  | D. 5 | 04 | 01 | 65.80 C | 47.033 | 47.075 | 58242 | 58.158 | 65800 |
|  |  | 06 | 0.1 | 03 | 51400 | 40800 | 40850 | 49550 | 494.50 | 51400 |
|  |  | 0.6 | 02 | 02 | 57600 | 44600 | 44650 | 53850 | 53750 | 57600 |
|  |  | 06 | 0.3 | 01 | 63.800 | 48.400 | 48450 | 58150 | 58050 | $\begin{aligned} & 63 \mathrm{BOO} \\ & 55600 \end{aligned}$ |
|  |  | 07 | 0.1 | 02 | 55.600 | 45967 | 46025 | 53.758 | 53642 |  |
|  |  | 07 | 0.2 | 0.1 | 61,800 | 49.767 | 49825 | 58058 | 57.942 | $\begin{aligned} & 55600 \\ & 61.806 \end{aligned}$ |
|  |  | 48 | 0.1 | 01 | 59800 | 51133 | 51,200 | 57.967 | 57833 | 59800 |
|  |  | SUM |  |  | 196800 | 1292.00 | 129300 | 174100 | 173900 | 196800 |


| T | M | W1 | W2 | W/3 | SPTJEDD | EDDISPT | S[1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 27 | 4 | 01 | 01 | $0 \cdot 1$ | 18517 | 16.092 | 16109 | 16942 | 17625 | 18517 |
|  |  | 0.1 | 02 | 07 | 23.517 | 18692 | 18700 | 20142 | 21725 | 23517 |
|  |  | 0.1 | 0.3 | 06 | 28517 | 21.292 | 21.300 | 23.442 | 25.825 | 28 517 |
|  |  | 0.1 | 04 | 05 | 33517 | 23892 | 23900 | 26742 | 29.925 | 33517 |
|  |  | 01 | 05 | 04 | 38517 | 26492 | 26500 | 30042 | 34025 | 38. 517 |
|  |  | 0.1 | 06 | 03 | 43517 | 29.092 | 29.100 | 33342 | 38.125 | 43517 |
|  |  | 01 | 0.7 | 02 | 48.517 | 31.692 | 31700 | 36642 | 42225 | 18517 |
|  |  | 01 | 08 | 0.1 | 53.517 | 34292 | 34300 | 39542 | 46325 | 53517 |
|  |  | 02 | 01 | 07 | 23033 | 20.583 | 20.600 | 213 B 3 | 22.150 | 23033 |
|  |  | 02 | 02 | 06 | 28033 | 23183 | 23200 | 24.683 | 26250 | 28033 |
|  |  | 02 | 03 | 0.5 | 33033 | 25793 | 25800 | 27983 | 30350 | 33033 |
|  |  | D 2 | 04 | 0.4 | 34033 | 28393 | 28400 | 31283 | 34450 | 38033 |
|  |  | 02 | 05 | 03 | 43033 | 30983 | 31000 | 34583 | 38.550 | 43033 |
|  |  | 02 | 06 | 02 | 48033 | 33583 | 33600 | 37883 | 42.650 | 48033 |
|  |  | 02 | 07 | 0.1 | 53033 | 36183 | $5620 ¢$ | 41.183 | 46750 | 53033 |
|  |  | 03 | 01 | 06 | 27 556 | 25.075 | 25100 | 25925 | 26675 | 27550 |
|  |  | 03 | 02 | 05 | 32550 | 27.675 | 27700 | 29225 | 30775 | 32550 |
|  |  | 03 | 03 | 04 | 37.550 | 30275 | 30300 | 32525 | 34875 | 37.550 |
|  |  | 03 | [4 | 03 | 42550 | 32875 | 32.900 | 35825 | 38975 | 42550 |
|  |  | 03 | [5 | 02 | 47.550 | 35475 | 35.500 | 39125 | 43075 | 47550 |
|  |  | 03 | 66 | 01 | 52550 | 38075 | 38100 | 42425 | 47175 | 52550 |
|  |  | 04 | 01 | 05 | 32.067 | 29567 | 29.600 | 30.467 | 31200 | 32.067 |
|  |  | 0.4 | 02 | [ 4 | 37067 | 32167 | 32200 | 33767 | 35300 | 37067 |
|  |  | 04 | 03 | ¢ 3 | 42063 | 34.767 | 34800 | 37.067 | 39.400 | 42067 |
|  |  | D 4 | 04 | 0.2 | 47067 | 37367 | 37.400 | 40.367 | 43500 | 47067 |
|  |  | D 4 | 05 | 01 | 52.067 | 39967 | 40.000 | 43.657 | 47600 | 62.067 |
|  |  | 05 | 01 | C 4 | 35583 | 340.58 | 34100 | 35008 | 35725 | 35583 |
|  |  | 05 | 02 | 03 | 41583 | 36.658 | 35704 | 38308 | $39 \mathrm{B25}$ | 41.583 |
|  |  | 0.5 | 03 | 02 | 46583 | 39.258 | 39300 | 41.608 | 43925 | 46.583 |
|  |  | 0.5 | 04 | 01 | 51583 | 41.858 | 41900 | 44.908 | 48025 | 51.583 |
|  |  | 06 | 01 | 03 | 4150 | 38.550 | 38600 | 39550 | 40250 | 41.100 |
|  |  | 06 | 02 | 0.2 | 46100 | 41150 | 41.200 | 42.850 | 44350 | 46.100 |
|  |  | 06 | 0.3 | 01 | 51100 | 43750 | 43800 | 46.150 | 48450 | 51100 |
|  |  | 0.7 | 01 | 92 | 45617 | 43.042 | 43100 | 44092 | 44775 | 45617 |
|  |  | 0.7 | 0.2 | 0.1 | 50.617 | 45642 | 45700 | 47.392 | 48875 | 50.617 |
|  |  | 0.8 | 01 | 01 | 50.133 | 47533 | 47600 | 48633 | 49300 | 5013.3 |
| SUM |  |  |  |  | 146600 | 1175.00 | 117600 | 126500 | 135900 | 146600 |


| T | M | W1 | W2 | W3 | SPTIED | EDDISPT | S 11 | S[2] | \$[3] | S(4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 27 | 5 | 01 | 01 | 60 | 18.842 | 16517 | 16525 | 17.167 | 17.950 | 78842 |
|  |  | 01 | 02 | 07 | 24042 | 19.417 | 19425 | 20.667 | 22.250 | 24042 |
|  |  | 01 | 0.3 | 06 | 29242 | 22.317 | 22.325 | 24167 | 26550 | 29.242 |
|  |  | 01 | 04 | 0.5 | 34442 | 25217 | 25225 | 27667 | 30.850 | 34442 |
|  |  | 01 | 05 | 04 | 39642 | 28117 | 28125 | 31.167 | 35.15D | 39642 |
|  |  | 01 | 06 | 03 | 44 642 | 31017 | 39.025 | 34667 | 39.450 | $44 \mathrm{EA2}$ |
|  |  | 01 | 07 | 0.2 | 50.042 | 33917 | 33925 | 38. 167 | 43750 | 50042 |
|  |  | 01 | D8 | 0.1 | 55242 | 36.817 | 36825 | 41667 | 48050 | 55.242 |
|  |  | 02 | 07 | 07 | 23343 | 21133 | 21150 | 21.833 | 22600 | 23483 |
|  |  | 02 | 0.2 | 0.6 | 28683 | 24,033 | 24050 | 25333 | 26.900 | 28.583 |
|  |  | 02 | 03 | 05 | 33883 | 26.933 | 26950 | 28833 | 31205 | 33883 |
|  |  | 02 | 04 | 0.4 | 39043 | 29833 | 29850 | 32333 | 35500 | 39 ¢83 |
|  |  | 02 | 05 | 0.3 | 44.283 | 32.733 | 32.750 | 35833 | 39800 | 44.283 |
|  |  | 0.2 | 0.6 | 02 | 49463 | 35633 | 35650 | 39333 | 44100 | 49483 |
|  |  | 02 | 07 | 0.1 | 54683 | 38.533 | 36550 | 42833 | 48400 | 54.683 |
|  |  | 03 | 01 | 06 | 28.125 | 25750 | 25775 | 26500 | 27250 | 28125 |
|  |  | 03 | 02 | 05 | 33325 | 28.650 | 28675 | 30.000 | 31550 | 33325 |
|  |  | [ 3 | D3 | 04 | 38525 | 31.550 | 31.575 | 33500 | 35.850 | 38525 |
|  |  | 03 | D 4 | D 3 | 43725 | 34450 | 34.475 | 37000 | 40.150 | 43725 |
|  |  | 03 | ¢5 | D 2 | 48925 | 37.350 | 37.375 | 40500 | 44.450 | 48.925 |
|  |  | 03 | D6 | 01 | 54, 125 | 40250 | 40.275 | 44000 | 48.750 | 54.125 |
|  |  | 04 | 01 | 0.5 | 32.767 | 30.367 | 30.400 | 31.167 | 31900 | 32.767 |
|  |  | 04 | 02 | D 4 | 37967 | 33287 | 33300 | 34667 | 36200 | 37.957 |
|  |  | 04 | 03 | 0.3 | 43.167 | 36.167 | 36205 | 38.167 | 40.500 | 43.167 |
|  |  | 04 | 0.4 | 02 | 48367 | 39067 | 39100 | 41667 | 44800 | 48367 |
|  |  | 04 | 05 | 01 | 53567 | 41.967 | 42.000 | 45167 | 49.100 | 53567 |
|  |  | 05 | 01 | 04 | 37.408 | 34.983 | 35025 | 35.833 | 36550 | 37.408 |
|  |  | 05 | 02 | 0.3 | 42.60日 | 37883 | 37.925 | 39333 | 40850 | 42.608 |
|  |  | 05 | 0.3 | 02 | 47.808 | 40783 | 40825 | 42 E 33 | 45150 | 47.808 |
|  |  | 05 | 04 | 01 | 53.008 | 43683 | 43725 | 46.333 | 49450 | 53008 |
|  |  | 06 | 01 | 0.3 | 42.050 | 39600 | 39650 | 40.500 | 41200 | 42.050 |
|  |  | 06 | 02 | 02 | 47250 | 42.500 | 42550 | 44.900 | 45.500 | 47250 |
|  |  | 0.6 | 03 | 01 | 52450 | 45.400 | 45.450 | 47.500 | 49800 | 52.450 |
|  |  | 07 | 0.1 | 0.2 | 46692 | 44217 | 44275 | 45.167 | 45850 | 46692 |
|  |  | 07 | 02 | 0.1 | 51,892 | 47117 | 47175 | 48667 | 50150 | 51892 |
|  |  | 08 | 01 | 01 | 51.333 | 49833 | 48 SOO | 49833 | 50500 | 51.333 |
|  |  | SUM |  |  | 150500 | 1226 b0 | 1227.00 | 1304.00 | 139800 | 1505.00 |


| 00＇E85 1 | 00－92\％！ | 00 ZSEL | 00 BZEL | 008282 | DOECgi | WITS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\underline{E} L E S$ | 006 | ¢EZZG | 00515 | Cど 15 | ELCLEG | 10 | ＇0 | 80 |  |  |
| てが比 | 002 29 | HでG | çi＇0s | 290 OS | てttros | 10 | 20 | $\angle 0$ |  |  |
| で8 时 | 00025 |  | cze 9t | 4 Cg ＇9p | 2⿰⿺乚一匕⿱㇒日勺十 8 | と＇0 | 10 | $\angle 0$ |  |  |
| OSL 55 | OOG ZG | 00208 | 0S 28 b | 00L＇Et | 091．${ }^{\text {ch }}$ | 10 | 80 | 90 |  |  |
| OGG 6b | 008\％ | $008^{\circ} 9$ | OSZ ¢t | 002 ct | OSS | 20 | 20 | 90 |  |  |
| 056 Et |  | 00t＇zo | OS2け | 002＇t | 096＇sb | ¢0 | 1.0 | 90 |  |  |
| 898 cc | 00EZ9 | 8816\％ | GLE $2 t$ | ¢ce $2 t$ | 898＇ç | 10 | 30 | $¢ 0$ |  |  |
| 89\％＇09 | 009\％\％ | caz 5 | GLeqt | Ecest | 8SZ 09 | 20 | E＇0 | G0 |  |  |
| 899＇t | 0062 | E8¢ | gic＇ot | Eetot | 859 tt | \＆＇0 | 20 | 9.0 |  |  |
| 850 EE | OOZ8E | 86t2c | 928＇98 | E¢\％ 9 C | 39068 | $\checkmark 0$ | 10 | 50 |  |  |
| L4599 | 00125 | L91＇80 | 00056 | 1969t | 299＇99 | 10 | 50 | 50 |  |  |
| 29605 | 00t 21 | く9で物 | 0045 | 190で | 290＇09 | 200 | P0 | $\$ 0$ |  |  |
| 1965 | 002＇20 | 49800 | 00066 | 2968E | 298 9b | co | 80 | $\square 0$ |  |  |
| 49268 | 00088 | $\angle 90^{\circ} \mathrm{Sc}$ | 00c 98 | $29 力 \mathrm{SE}$ | 29164 | $\pm 0$ | 20 | $\pm 0$ |  |  |
| L91比 | 008 5 | LgS 28 | 000＇z¢ | 29618 | 29150 | 90 | 10 | $\vdash 0$ |  |  |
| SL2 29 | 006 ls | OSt 20 | cz9 ${ }^{\text {¢ }}$ | 0091 | $512<5$ | 10 | 90 | $\Sigma 0$ |  |  |
| Gta＇LG | 002 Lt | －¢ | 9で＇じ | 00115 | gL9＇Lg | 20 | g＇0 | $\varepsilon 0$ |  |  |
| ¢ $20.9 p$ | OOS 2 t | 098゙80 | Gz9 28 | 009＇28 | SLO 9\％ | ع＇0 | ¢0 | 80 |  |  |
| 5to 0 | 00日 28 | O¢力 ¢E | 5でもく | 0018 | ¢ぐ0 | $\bigcirc 0$ | ¢0 | $\varepsilon$＇0 |  |  |
| G28＇0E | 00l $\frac{1}{}$ ¢ | OGc＇te | ces＇0¢ | 00908 | 928 y | 90 | で0 | E 0 |  |  |
| GLZ 62 | O0\％ 82 | 0592 L | 9 c | 001 LZ | GLZ 6Z | 90 | 10 | E0 |  |  |
| E86 25 | O0L＇ 19 | ECL 9b | OGZ Et | عEZ＇を | E86 LS | 10 | $\angle 0$ | 20 |  |  |
| £8¢＇z | O0\％ 2 C | EEZ P | 092 68 | EELEE | ¢8E 25 | \％ 0 | 90 | 20 |  |  |
| ESL 95 | 00¢ zo | ¢EE ๕E | OSZ＇98 |  | cgl 96 | 80 | 90 | 20 |  |  |
|  | 009\％2 | ¢¢ャワを | 092＇乙§ | ¢ $¢ \perp$ て | と日じ | ¢0 | $\pm 0$ | 20 |  |  |
| 枸G＇GE | 006て¢ | ¢cg oc | OGZ EL | EEL 62 | ¢ ¢ ¢ ¢ | 50 | E0 | 20 |  |  |
| ¢ 8662 | OOZ 82 | Ecg gz | OGL Gz | £ ¢ L＇gz | 89662 | 90 | 20 | 70 |  |  |
| ¢ac＇tz | $005 \%$ | \＆eLzz | osz＇zz | £とZ てひ | と日c゙って | 40 | 10 | z0 |  |  |
| 26989 |  | くいらす | ¢28け | ＜98＇1t | Z69\％9 | 10 | 80 | 10 |  |  |
| 260 ¢9 | 0089 | 2゙くしか | SLE\％ | 2968 8 | $260{ }^{-89}$ | 20 | 40 | 10 |  |  |
| 26\％ 26 | $0012 \%$ | L1E LE | S1att | 298 吃 | 26tit | ¢0 | 90 | 10 |  |  |
| 268\％ | OOD 28 | くも゙く | SLE゙1E | 29816 | 268゙け | $\pm 0$ | 90 | 10 |  |  |
| Z 6298 | 002 28 | LLE 62 | 9LSLZ | 29812 | 26898 | 50 | $\square^{\prime} 0$ | 10 |  |  |
| てE908 | 000 BC | L19 9z | GLE＇tz | $298 \downarrow$ ¢ | 269 0E | 90 | E 0 | 10 |  |  |
| 26092 | 008 ¢ | 2以して | GL80Z | L9802 | 260 gz | 10 | 20 | 10 |  |  |
| て6t 61 | 00918 | 218゙く | 5LE11 | 69826 | て6trot | 80 | 10 | 10 | $L$ | $L Z$ |
| ［t］S | ［غ］s | ［2］ | ［1］S | 1dSioce | Ggarlds | EM | 2．4 | LM | W | 1 |


| 00 やすら | 00＇Leti | 00 Etel | 00 －123 | 002ん2上 | 00＇VbGI | Wns |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EES＇ZG | 002＇19 | EEO IS | ODZ 09 | E¢ト＇OG | £ç＇z9 | 10 | 1＇0 | 80 |  |  |
| L9185 | get is | 20660 | 099＇8b | 265 时 | 291 EG | L＇0 | 20 | 10 |  |  |
| 29120 | 52695 | でて 9\％ | OSt St | 26E 5b | 492．2\％ | 20 | 10 | $\angle 0$ |  |  |
| 008＇g | ¢¢1．29 | Ocs 8 | OOL 2 | 090＇L | 008 \＆ 9 | 10 | ¢0 | 90 |  |  |
| 00サ＇8\％ | 0s9\％9t | OSt 5 | 0065 | 058 ¢ | 00\％${ }^{\circ}$ | $2 \cdot 0$ | 20 | $9{ }^{\prime} 0$ |  |  |
| 000＇¢ | 05： 20 | OSt し | O020 | 09900 | 000 Eb | $\varepsilon 0$ | 10 | $9{ }^{\prime} 0$ |  |  |
| cob＇vs | ge8 0 ¢ | 85 2 Lb | OGg ¢b | cos＇sp | Ect po | 10 | $\bigcirc 0$ | G 0 |  |  |
| ๕co bt | GLE 90 | 850 pt | OGE Zt | 80E＇Z | ع60 50 | 20 | co | G0 |  |  |
| £ ¢ ¢ ¢ | G 28 ip | $8 S^{\circ} \mathrm{C}$ | OSl 68 | 801 6E | ¢ ¢ ¢ ¢ | ع00 | 20 | 50 |  |  |
| £ ¢ ¢ $¢$ | G $£ \varepsilon 18$ | 89998 | OSE＇s¢ | 89698 | EEZ 3E | $\checkmark 0$ | 10 | to |  |  |
| $\angle 90 \cdot 9$ | 00909 | 2995 | 000 ${ }^{\circ}$ | 4968 | 49099 | t＇0 | 50 | $\checkmark 0$ |  |  |
| 1986 | 00198 | 496 てt | 0080t | 4920t | 29960 | 20 | P0 | $\pm 0$ |  |  |
| 292 tb | 0091\％ | 29268 | 009 LE | ＜9G2 2 | L9\％to | $\varepsilon 0$ | ¢0 | $\checkmark 0$ |  |  |
| 29888 | Dol＇28 | 295 | ORT 比 | 498 比 | 298 ac | $\pm 0$ | 20 | $\pm 0$ |  |  |
| 19\％ $\mathrm{E}^{\circ} \mathrm{E}$ | 009 己 | 49818 | 002 18 | 191＇L6 | 29\％E¢ | 90 | 10 | $\pm 0$ |  |  |
| 0025s | 9Z¢＇0G | S＜s 9b | O5t で | GZt $\downarrow t$ | 00LGs | 10 | 90 | $\varepsilon 0$ |  |  |
| 00¢09 | ¢て8＇ct | SLE＇V | BGZ 68 | GZZ 6E | 00805 | 20 | Gor | $\varepsilon 0$ |  |  |
| 006 | GZE し | 92688 | OGO 9E | 520＇9 | DO6＇tr | $\varepsilon 6$ | ＇0 | ¢0 |  |  |
| 00568 | 9Z898 | Gくtトた | OS＇ 28 | cz8 て¢ | 00568 | ＋＇0 | ¢ 0 | \＆ 0 |  |  |
| 001＇ve | gzéze | SLL OE | DS9 6z | 9Z9 6z | 001 加 | 9.0 | 20 | $8 \cdot 0$ |  |  |
| 002＇62 | Sziz2 | S $\angle 0 \angle Z$ | OSt 92 | çt 9\％ | 002 82 | 90 | 10 | ¢0 |  |  |
| EEE 99 | 05009 | cat $\dagger$ | 00605 | ¢880t | Ece＇gc | 10 | 10 | 20 |  |  |
| Ec6 09 | OSc\％ | C8L Op | 002 28 | $\varepsilon 8928$ | CE6 OG | 20 | 90 | z＇0 |  |  |
| ¢¢G ¢t | 050＇L | ceo LE | $00 \mathrm{~S} \downarrow \mathrm{E}$ | ¢8ャ $\downarrow$ ¢ | EEG ¢ | 80 | 50 | で0 |  |  |
| ¢EL Ot | OfS 98 |  | O0¢ 18 | ¢日C 18 | EELOt | $\checkmark 0$ | 50 | 20 |  |  |
| とEL゙ゆ¢ | Ofoze | £89 6Z | 00182 | c80＇sz |  | 50 | $\varepsilon 0$ | 20 |  |  |
| とEč6z | OSS 12 | E86 cz | 00672 | ¢8日 $\dagger 2$ | ¢¢E 6Z | 90 | 20 | 20 |  |  |
| ¢ ¢ ¢ ¢ | DSOEZ | £gZ $<2$ | 00642 | 88912 | ¢ع6 ¢Z | 20 | 10 | 20 |  |  |
| 2969s | 5LL＇tb | 26E $\mathrm{E}^{\circ}$ | 05c．6¢ | でど6e | 29699 | 10 | 80 | 10 |  |  |
| L9＇5G | ¢ $\angle$ て＇Gb | 26968 | 65698 | でじ9¢ | 295＇19 | 20 80 |  | 10 |  |  |
| $294^{\prime} 9$ | SLLOD | 26658 | 056て¢ | で6でく | 29695 | 80 $\square 0$ | 90 |  |  |  |
| 1920 | ¢LŻ＇98 | 26己 てE | 加 68 | で2 62 | $2920 \%$ | 8 | $\bigcirc$ | 10 |  |  |
| L9E58 | GLIIE | 26 c 8 8 | OGG 9Z | Zヤ¢9Z | 20\％5\％ | 90 | 80 | 10 |  |  |
| 49662 | GLでしZ | Z68 t | 0¢c¢\％ | でと＇¢z | 296.62 | 90 | 8 | 10 |  |  |
| 499＇pz | GLE＇Z | 261して | OSLOZ | てカレ＇0z | 29572 | 20 | 10 | 10 10 10 | 9 | $\angle 2$ |
| 2916 | Gtで81 | 26p 21 | 0 GG 5 | Zヤ696 | $\underline{49161}$ | 80 | 2M |  | N | － |
| ［t］s | ［¢］$]$ | ［z］s | ［l］5 | 1dSt00 | 003lds | E．h | cm | m | N | 1 |


| 7 | M | W1 | W2 | W3 | SPTIEDD | EDDISPT | S[1] | S[2] | S[3] | $5[4]$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 27 | 8 | 0.1 | 0.1 | 0.8 | 19.817 | 17.792 | 17800 | 18142 | 18925 | 19817 |
|  |  | 0.1 | 02 | 0.7 | 25617 | 21.592 | 21600 | 22242 | 23825 | 25617 |
|  |  | 0.1 | 03 | 0.6 | 31.417 | 25392 | 25400 | 26342 | 28725 | 31417 |
|  |  | 0.1 | 0.4 | 0.5 | 37217 | 29192 | 29200 | 30442 | 33.625 | 37.217 |
|  |  | 01 | 0.5 | 04 | 43017 | 32992 | 33.000 | 34.542 | 38525 | 43017 |
|  |  | 01 | 06 | 03 | 48.817 | 36792 | 36800 | 38.642 | 43425 | 48.817 |
|  |  | 0.1 | 07 | 0.2 | 54617 | 40592 | 40.600 | 42.742 | 48325 | 54617 |
|  |  | 01 | 08 | 01 | 60417 | 44.392 | 44.400 | 46842 | 53.225 | 60417 |
|  |  | 02 | 01 | 07 | 24833 | 22.783 | 22.800 | 23183 | 23950 | 24833 |
|  |  | 02 | 02 | 06 | 30633 | 26.583 | 26.600 | 27283 | 28.850 | 30.633 |
|  |  | 02 | 03 | 05 | 36433 | 30383 | 30,400 | 31383 | 33.750 | 36433 |
|  |  | 02 | 04 | 04 | 42.233 | 34183 | 34200 | 35483 | 38650 | 42.233 |
|  |  | 02 | 0.5 | 03 | 48.033 | 37.983 | 38.000 | 39583 | 43550 | 44.033 |
|  |  | 02 | 06 | 02 | 53833 | 41.783 | 41800 | 43.683 | 48450 | $53 \mathrm{B33}$ |
|  |  | 0.2 | 07 | 0.1 | 59633 | 45583 | 45600 | 47.783 | 53350 | 59633 |
|  |  | 0.3 | 01 | 0.6 | 29850 | 27775 | 27.800 | 28225 | 28975 | 29850 |
|  |  | 03 | 02 | 0.5 | 35650 | 31575 | 31,600 | 32.325 | $33 \mathrm{B75}$ | 35650 |
|  |  | 0.3 | 03 | 0.4 | 41.450 | 35375 | 35400 | 36425 | 38775 | 41450 |
|  |  | 03 | 04 | 03 | 47.250 | 39.175 | 39200 | 40525 | 43675 | 47250 |
|  |  | 03 | 05 | 0.2 | 53050 | 42.975 | 43000 | 44625 | 48575 | 53050 |
|  |  | 03 | 06 | 0.1 | 56850 | 46.775 | 46.800 | 48725 | 53475 | 58850 |
|  |  | 0.4 | 0.1 | 0.5 | 34867 | 32767 | 32800 | 33.267 | 34.000 | 34.867 |
|  |  | 0.4 | 0.2 | 04 | 40.667 | 36567 | 36600 | 37367 | 38.900 | 40667 |
|  |  | 04 | 0.3 | 03 | 46467 | 40367 | 40400 | 41467 | 43800 | 46467 |
|  |  | 04 | 0.4 | 02 | 52267 | 44.167 | 44200 | 45567 | 48700 | 52.267 |
|  |  | 04 | 05 | 01 | 58067 | 47957 | 48.000 | 49667 | 53600 | 58.067 |
|  |  | 05 | 01 | $0 \cdot 4$ | 39883 | 37758 | 37.800 | 38.308 | 39025 | 39883 |
|  |  | 05 | 02 | 03 | 45683 | 41558 | 41600 | 42.408 | 43.925 | 45683 |
|  |  | 05 | 03 | 02 | 51.483 | 45.358 | 45400 | 46508 | 48826 | 51483 |
|  |  | 0.5 | 04 | 01 | 57283 | 49150 | 49200 | 50608 | 53.725 | 57.293 |
|  |  | 06 | 01 | 0.3 | 44900 | 42750 | 42.800 | 43350 | 44.050 | 44900 |
|  |  | 06 | 0.2 | 02 | 50.700 | 46550 | 46600 | 47.450 | 48950 | 50700 |
|  |  | 06 | 03 | 01 | 56.500 | 50350 | 50400 | 51,650 | 53850 | 56500 |
|  |  | 07 | 01 | 02 | 4997 | 47742 | 47.800 | 48392 | 49075 | 49917 |
|  |  | 07 | 02 | 0.1 | 55717 | 51542 | 51.600 | 52.492 | 53975 | 55717 |
|  |  | 0.8 | 01 | 01 | 54933 | 52.733 | 52800 | 53.433 | 54.100 | 54933 |
|  |  | SUM |  |  | 1622.00 | 1379.00 | 138000 | 142100 | 151500 | 1622:00 |


| T | M | W1 | W2 | W3 | SPTIEDD | EDDISPT | S[] | \$[2] | 5[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 28 | 4 | 0.1 | 01 | 08 | 21242 | 18.917 | 18925 | 19567 | 20.350 | 21242 |
|  |  | 01 | 02 | 07 | 26142 | 21.517 | 21525 | 22767 | 24.350 | 25142 |
|  |  | 0.1 | 03 | 0.6 | 31.042 | 24.117 | 24.125 | 25967 | 28.350 | 31042 |
|  |  | 01 | 04 | 0.5 | 35.942 | 26717 | 25.725 | 29167 | 32.350 | 35.942 |
|  |  | 01 | 05 | 04 | 40842 | 29.317 | 29325 | 32.367 | 36350 | 40842 |
|  |  | 01 | 05 | [3 | 45742 | 31.917 | 31.925 | 35567 | 40350 | 45.742 |
|  |  | 01 | 0.7 | 02 | 50642 | 34.517 | 34.525 | 36767 | 44350 | 60.642 |
|  |  | 0.1 | 03 | 01 | 55.542 | 37.117 | 37125 | 41967 | 48.350 | 55542 |
|  |  | 02 | 01 | 07 | 25583 | 23.233 | 23.250 | 23.933 | 74.700 | 25583 |
|  |  | 02 | 02 | 06 | 30.483 | 25833 | 25.850 | 27133 | 28.700 | 30.483 |
|  |  | 0.2 | 03 | 05 | 35383 | 28433 | 28450 | 30.333 | 32.700 | 35383 |
|  |  | 0.2 | 04 | 0.4 | 40283 | 31033 | 31.050 | 33.533 | 36.700 | 40283 |
|  |  | 02 | 0.5 | 0.3 | 45.183 | 33633 | 33650 | 36733 | 40700 | 45.183 |
|  |  | 02 | 06 | 02 | 50.083 | 36233 | 36.250 | 39933 | 44700 | 50.063 |
|  |  | 02 | 07 | 01 | 54983 | $38 \mathrm{B33}$ | 38.850 | 43133 | 46700 | 54.983 |
|  |  | 03 | 01 | 06 | 29925 | 27550 | 27.575 | 28.300 | 29050 | 29925 |
|  |  | 03 | 0.2 | 05 | 34825 | 30150 | 30.175 | 31.590 | 33050 | 34.825 |
|  |  | 03 | 0.3 | 04 | 39.725 | 32750 | 32.775 | 34.700 | 37050 | 39725 |
|  |  | 03 | 04 | 03 | 44.625 | 35350 | 35.375 | 37.900 | 41050 | 44.625 |
|  |  | 0.3 | 05 | 02 | 49525 | 37.950 | 37975 | 41.100 | 45050 | 49525 |
|  |  | 0 | 06 | 0.1 | 54425 | 40550 | 40575 | 44.300 | 49.050 | 54425 |
|  |  | 04 | 0.1 | 05 | 34267 | 31867 | 31,900 | 32667 | 33400 | 34.267 |
|  |  | 0.4 | 02 | 0.4 | 39167 | 34467 | 34500 | 35867 | 37.400 | 39.167 |
|  |  | 04 | 03 | 03 | 44067 | 37067 | 37.100 | 39067 | 41400 | 44.067 |
|  |  | 04 | 0.4 | 02 | 48967 | 39667 | 39.700 | 42.267 | 45400 | 48.867 |
|  |  | 04 | 05 | 01 | 53867 | 42267 | 42.300 | 45467 | 49400 | 53.867 |
|  |  | 05 | 01 | 04 | 38.608 | 38.183 | 36.225 | 37033 | 37750 | 38.608 |
|  |  | 05 | 02 | 03 | 43.508 | 38.783 | 38.825 | 40.233 | 41750 | 43508 |
|  |  | 05 | 03 | 0.2 | 406408 | 41.383 | 41.425 | 43.433 | 45750 | 48408 |
|  |  | 0.5 | 04 | 0.1 | 53308 | 43983 | 44.025 | 46633 | 49.750 | 53308 |
|  |  | 06 | 01 | 0.3 | 42950 | 40500 | 40550 | 41400 | 42.100 | 42950 |
|  |  | 06 | 02 | 02 | 47850 | 43100 | 43150 | 44600 | 46.100 | 47.250 |
|  |  | 06 | 03 | 01 | 52750 | 45700 | 45.750 | 47800 | 50.100 | 52750 |
|  |  | 07 | 01 | 5.2 | 47292 | 44.817 | 44875 | 45767 | 46450 | 47292 |
|  |  | 07 | 02 | 01 | 52.192 | 47417 | 47,475 | 48967 | 50450 | 52.192 |
|  |  | 08 | 01 | 01 | 51,633 | 49133 | 49200 | 50133 | 50800 | 51.633 |
|  |  | SUM |  |  | 1541.00 | 126200 | 1263.00 | 1340.00 | 143400 | 1541.00 |


| 00＇6191 | 00 こ151 | 00日しって | 00 ¢9¢． | 00＇6981 | 00619 | WกS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EEOtS | 902ES | EtS＇Z9 | 008 IS | EEL＇19 | CEO＇tS | 10 | 10 | 80 |  |  |
| でも $\downarrow$ ¢ | 000 ES | LLG＇G | Sてtos | L9E 09 | でじけS | 10 | 20 | 10 |  |  |
| でぢ6\％ | 0096 | 216\％ | ¢で2\％ | 291\％ | 2to60 | z＇0 | 10 | 10 |  |  |
| O5\％＇gs | 009＇Z9 | 00505 | 0¢の＇60 | 0006 | OSt GS | 1＇0 | $\varepsilon 0$ | 90 |  |  |
| Ostos | 00t 8 b | 0069 | 0985 | D085 | OSt 09 | 20 | 20 | 90 |  |  |
| $0 ¢ 8 \pm$ | 000 to | OES Et | OGS 27 | Dos CV | 098＇p\％ | $\varepsilon 0$ | 10 | 90 |  |  |
| QG1 9G | 009 てS | ¢8\％ 0 | SLS 26 | E¢S ${ }^{\text {co }}$ | 85195 | 10 | $\nabla^{\circ} \mathrm{O}$ | 50 |  |  |
| 89808 | 002 8\％ | 86850 | SLt pt | ¢c0＇to | 859 DS | て0 | 80 | G0 |  |  |
| B9950 | 000＇ど | EBZ Cb | らしてしか | £と己 しt | 8G9 5t | E＇0 | C0 | 90 |  |  |
| 892＇0\％ | 0016 6E | E89 8¢ | G10 9 | ECO 88 | 8sZ＇0t | $\geqslant 0$ | 10 | 40 |  |  |
| 19895 | 00679 | 29力＇日V | 00 Eb | 49790 | 29999 | 10 | 50 | $\nabla^{\prime} 0$ |  |  |
| L9915 | 000＇86 | $\angle 98$ tb | 001．8p | $1908 \%$ | L9G L | て＇0 | $\bullet 0$ | $\geqslant 0$ |  |  |
| 4929 | 009 ct | L92 16 | 006.68 | 198＇68 | 292 9t | E0 | 50 | $\geqslant 0$ |  |  |
| 1960 | 002 68 | 29918 | 001 䗆 | 499＇98 | 290 0 | \％ 0 | 20 | ＊0 |  |  |
| 4995 | $000{ }^{\circ} \mathrm{D}$ | 190㠶 | OOS＇EE | 19\％ع 5 | 199 5 | 50 | 10 | 10 |  |  |
| g $25 \angle 5$ | $00 \mathrm{O}^{\prime} \mathrm{ZS}$ | 0ct 20 | ¢26 0 | 006＇㠸 | GLG 25 | 10 | 90 | $¢ 0$ |  |  |
| GLZ Z9 | 908 Lt | 098＇\％ | çıbt | 00に1t | Gıて 29 | 2゙0 | 50 | ¢0 |  |  |
| 9169 9 | の0\％をt | OSZ＇00 | GZG 8E | 0058 C | 94697 | 80 | $\rightarrow 0$ | $\varepsilon 0$ |  |  |
| 919＇1t | 90060 | 0 cs＇9\％ | GCE G¢ | OOE SE | 929.17 | 70 | 80 | \％0 |  |  |
| GLE 9E | 9 OSOE | 捾の＇に家 | GZL 2 E | 001 乙E | GLE 9\％ | co | 20 | 50 |  |  |
| SLOEE | 00208 | OGt＇6Z | SZ5 82 | 006＇92 | GLOIE | 90 | 10 | E0 |  |  |
| E8Z 89 | 000125 | をどもの | 095 をt |  | を日C 89 | 10 | 10 | 20 |  |  |
| と的を枵 | 009 Lt | こと8で | 加どロt | EEE Ot | ¢06 己9 | 20 | 90 | 20 |  |  |
| ¢39 $4 t$ | 002 EV | EEZ＇68 | OGV $\angle E$ | を比tを | C日g | 50 | 50 | 20 |  |  |
| と的を | 0088 E | Ec9 5s | O¢6＇E | EE6 ¢¢ | CBE Z | $\nabla 0$ | 50 | Z0 |  |  |
| 880 $\angle 5$ | なったもく | ERO＇Z | O51 OE | ECL OE | 800＇28 | 50 | 80 | 20 |  |  |
| E8L5 | 00008 | ECt BZ | 0¢G＇LZ | EEG $2 乙$ | ¢8LLE | 90 | 20 | 20 |  |  |
|  | 00958 | ESE゙ちZ | OGE＇tz | EEE $\dagger Z$ | ¢8t9\％ | $\angle 0$ | 10 | ＜0 |  |  |
| 266 89 | 008＇19 | LltG\％ | GLL Zt | 49トで | Z66 89 | 10 | 80 | 10 |  |  |
| 269 E9 | $000 \cdot 20$ | 218し\％ | SL6 8E | 498＇日 | Z69 ES | Z0 | $\leq 0$ | 10 |  |  |
| 26E＇8 | 000\％ | 2lて＇会 | 914．GE | 29158 | Z6E 8\％ | ع＇0 | 90 | 10 |  |  |
| 260 ct | 0098 | $419+8$ | SLS $Z E$ | 195 乙8 | 260 \＆\％ | － 0 | 90 | 10 |  |  |
| 262t5 | 90で比 | く10＇レ8 | SLE 6Z | 19¢＇62 | Z62 28 | 90 | 00 | 10 |  |  |
| て6t＇で | 00662 | Lbt $\angle C$ | GLL 92 | 19192 | こ6も こ¢ | 90 | EO | 10 |  |  |
| Z61 LZ | 00\％ 92 | 118Eて | 5L6＇も己 | 196 ZZ | て6し＇ご | $\leq 0$ | C0 | 10 |  |  |
| て6日 して | 00012 | $\triangle 1 Z O Z$ | SL261 | 49261 | 26日 6 | $8 \cdot 0$ | 10 | 10 | 9 | 2？ |
| ［is | tels | ［て］${ }^{\text {c }}$ | ［म］ | Ldsicas | －03／idS | EM | ZMh | 6／h | W | 1. |


| 00＇0691 | $00 \varepsilon \angle \square 1$ | 00\％ 28. | 00－0181 | 00 ＇zLEL | 000851 | WกT |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| £Ea＇ZG | 000 ZS | ¢E¢＇LG | OOS DS | Eとb＇OS | £E\％乙S | 10 | 10 | 80 |  |  |
| t9t Es | gesis | 2b2 Of | 0568 | 26885 | 29t cs | 10 | 20 | $\angle 0$ |  |  |
| 29E 8b | gzcilt | で¢ 9 ${ }^{\text {¢ }}$ | 090＇9b | 2665t | 498＇6 ${ }^{\text {d }}$ | ¢0 | 10 | 20 |  |  |
| DOL | OG\％ 19 | OSt 69 | 00b＇Lb | OSE $2 ⿰ ㇒ ⿻ 土 一 ⿱ 一 𫝀$ | 001＇vg | 10 | ¢0 | 90 |  |  |
| 000＇6 | OSでしt | OSL 94 | OLS＇to | OSt ${ }^{\text {ot }}$ | 000＇6t | 20 | Z0 | 90 |  |  |
| 00618 | OGOEt | OSどで「 | 009 しt | $0 ¢ 9$＇$\downarrow$ | 006 Eb | $\varepsilon 0$ | ＇0 | 90 |  |  |
| EEL 9 ¢ | 926 | 850 旳 | OGE Gb | 80日 5 | ¢ 2.7 bc | 10 | $\checkmark 0$ | 90 |  |  |
| Ec9 6b | 926＇9b | 899 | 096＇z | 806 Zt | Ec9＇6 | て 0 | E O | G＇0 |  |  |
| EES ${ }^{\text {b }}$ | 9LLCV | BGZ Lis | 090＇0\％ | 800 Dt | を¢¢\％ | $\varepsilon 0$ | Z | 9.0 |  |  |
| ¢¢t＇6を | GLEs 8 E | 698＇2¢ | OSL 2 E | 801．28 | ¢Et $6 \Sigma$ | V＇0 | 10 | G 0 |  |  |
| 290 59 | 00609 | 296＇9\％ | OOE $\dagger \square$ | 49z＇por | t9E cs | 10 | 90 | $\bigcirc 0$ |  |  |
| t92 05 | 00496 | 299 Ef | 00t しt | 49E14 | 49209 | Z0 | V0 | $\square 0$ |  |  |
| 2915t | OECOL | L910\％ | 00¢＇s¢ | 29088 | L91．gb | ¢0 | E0 | to |  |  |
| 29000 | ODE 大 | 29298 | 00998 | L95 58 | 290 Ot | $\nabla 0$ | 20 | $\square 0$ |  |  |
| 296 $\dagger$ ¢ | 00t $0 \times$ | L9EEC | 0042\％ | 29928 | L9S＇0 | 50 | 10 | t＇0 |  |  |
| 000 gs | g 2909 | 5185 | OGL＇Z $\downarrow$ | SZL | 00099 | 10 | 90 | $\varepsilon 0$ |  |  |
| 006＇09 | Sで96 | Sくでで | OGE6E | gz8＇68 | 00605 | でロ | G 0 | E0 |  |  |
| 008 c ¢ | sてzても | GIO＇6E | 09698 | 926 98 | 0085 | ¢0 | $\pm 0$ | $\varepsilon \square$ |  |  |
| 00206 | Szo 8 ¢ | G29 ce | 050 pc | $920 \downarrow$ 切 | 002．00 | $\square_{0}$ | E0 | $8 \cdot 0$ |  |  |
| 00958 | ¢ze＇c¢ | cız 28 | Os卜＇t\％ | SZ1 18 | 009 Gc | 50 | でO | E0 |  |  |
| 00soc | sza 6\％ | G 28 BL | 0sz＇8z | szz 82 | OOG OE | 90 | 10 | ¢0 |  |  |
| ¢69 99 | Ofe 09 | ç2＇tb | 002 － | çl 10 | E¢9＇9\％ | 10 | 10 | 20 |  |  |
|  | 0 cc 9 | cee＇to | ODE 8 E | c8\％ 88 | Etc＇rg | द0 | 90 | 20 |  |  |
| c¢t 95 | OS6 L | ع 26 LE | 00t 58 | ¢8¢ ¢¢ | とEャ $9 t$ | $\varepsilon{ }^{\prime} 0$ | ¢ 0 | 20 |  |  |
| EEE！${ }^{\text {ct }}$ | 05L2L | E8s | 005 己 | ¢ ¢ $\dagger$ C $¢$ | ¢とE しt | 10 | 0 | 20 |  |  |
| ¢¢己 9E | Oct 6 ct | ¢81 LE | 00962 | Eas 62 | ¢¢己 9¢ | 50 | ¢ 0 | 20 |  |  |
| £ど＇に | O5E 62 | CRLLZ | 00598 | 899 gz | と¢1＇に | 90 | 20 | Z0 |  |  |
| E00 g\％ | OGl gz | 888＇vz | 008 Ez | ¢ $8<\varepsilon Z$ | £ 2092 | 40 | 10 | 20 |  |  |
| 49Z 29 | G 2005 | Z69＇§ | 0G9 6E | 26968 | 29Z＇L9 | 10 | 80 | 10 |  |  |
| 291－z9 | $9 \angle 8 \mathrm{~Gb}$ | C6Z＇0ヶ | OGL 98 | 20298 | 29129 | 20 | $\angle 0$ | 10 |  |  |
| 2902\％ | GLa＇L | 268 9 | OGB E $\varepsilon$ | 2 LE ¢ | 1904 | ¢0 | 90 | 10 |  |  |
| 296\％ | ¢ $\angle \square \pm E$ | ことザ¢气 | 0560 0 | 20600 | 29614 | $\pm 0$ | 50 | 10 |  |  |
| 29898 | GEZEE | CSO＇0\％ | OSb 82 | 20082 | 29898 | G0 | $\checkmark 0$ | 10 |  |  |
| 290＇18 | St0 62 | Z69＇9Z | 091 9z | ztl sz | 29E1E | 90 | $\varepsilon$ | 10 |  |  |
| 19992 | 528 比 | Z62 82 | OGでてz | でて て | 19992 | 40 | 20 | 10 |  |  |
| 499＇Lを | 52902 | 26861 | 09865． | でぐぐく | 19512 | 60 | 10 | 10 | 9 | 㫜 |
| ［0］s | ［E］s | ［žs | ［1］ | IdSidoz | 0031近S | 2M | ZM | LM | W | 1 |


| T | M | W1 | W/2 | W/3 | SPT/EOD | EDDISPT | S[1] | S[2] | S[3] | S 141 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 28 | 7 | 01 | 01 | 08 | 22217 | 20.192 | 20200 | 20542 | 21325 | 22217 |
|  |  | 01 | 0.2 | 07 | 27.717 | 23.692 | 23700 | 24342 | 25925 | 27.717 |
|  |  | 01 | 0.3 | 06 | 33217 | 27.192 | 27200 | 28142 | 30525 | 33217 |
|  |  | 01 | 04 | 05 | 38717 | 30692 | 30.700 | 31942 | 35125 | 38717 |
|  |  | 0.1 | 05 | 0.4 | 44217 | 34192 | 34200 | 35.742 | 39.725 | 44217 |
|  |  | 01 | 0.6 | 03 | 49.717 | 37692 | 37700 | 39542 | 44.325 | 49717 |
|  |  | 01 | 0.7 | 02 | 5.5217 | 41.192 | 41200 | 43342 | 48.925 | 55.217 |
|  |  | 01 | 08 | 01 | 60717 | 44,692 | 44.700 | 47142 | 53.525 | 60717 |
|  |  | 0.2 | 01 | 0.7 | 26.933 | 24883 | 24.900 | 25.283 | 26050 | 26.933 |
|  |  | 0.2 | 02 | 0.6 | 32433 | 28383 | 28.400 | 29.083 | 30650 | 32433 |
|  |  | 0.2 | 03 | 0.5 | 37933 | 31883 | 31.900 | 32.883 | 35250 | 37933 |
|  |  | 0.2 | 04 | 04 | 43433 | 35383 | 36.400 | 36683 | 39850 | 43433 |
|  |  | 02 | 05 | 03 | 48933 | 38.883 | 38900 | 40.483 | 44.450 | 48933 |
|  |  | 02 | 0.6 | 02 | 54.433 | 42383 | 42400 | 44.283 | 49,050 | 54.433 |
|  |  | 02 | 0.7 | 01 | 59.933 | 45883 | 45900 | 48083 | 53.650 | 59.933 |
|  |  | 03 | 0 | 06 | 31650 | 29575 | 29600 | 30025 | 30.775 | 31650 |
|  |  | 03 | Q 2 | 0.5 | 37.150 | 33075 | 33.100 | 33.825 | 35375 | 37.150 |
|  |  | 03 | 03 | 0.4 | 42650 | 36575 | 36600 | 37.625 | 39975 | 42.650 |
|  |  | 03 | 0.4 | 03 | 48150 | 40075 | 40.100 | 41.425 | 44.575 | 48.150 |
|  |  | 0.3 | 0.5 | 02 | 53650 | 43575 | 43.600 | 45225 | 49.175 | 53.650 |
|  |  | 0.3 | 06 | 0.1 | 59.150 | 47.075 | 47.100 | 49 625 | 53775 | 59.150 |
|  |  | 04 | 0.1 | 05 | 36.367 | 34.267 | 34.300 | 34767 | 35500 | 36.367 |
|  |  | 04 | 0.2 | 04 | 41.867 | 37.767 | 37800 | 38567 | 40106 | 41.867 |
|  |  | 0.4 | 0.3 | 0.3 | 47.367 | 41.267 | 41.300 | 42367 | 44700 | 47,367 |
|  |  | 04 | 04 | 02 | 52.857 | 44767 | 44800 | 46.167 | 49300 | 52867 |
|  |  | 04 | 05 | 01 | 58.367 | 48267 | 48300 | 49967 | 53.900 | 58367 |
|  |  | 05 | 01 | 04 | 41.083 | 38.958 | 39600 | 39508 | 40225 | 41 DB3 |
|  |  | 05 | 0.2 | 03 | 46.583 | 42458 | 42500 | 43.308 | 44825 | 46583 |
|  |  | 05 | 0.3 | 02 | 52.083 | 45958 | 46,000 | 47.108 | 49.425 | 52083 |
|  |  | 05 | 04 | 01 | 57583 | 49458 | 49.500 | 50909 | 54.025 | 57.583 |
|  |  | 0.6 | 01 | 03 | 45 EDO | 43.650 | 43700 | 44250 | 44.950 | 45 B00 |
|  |  | 0.6 | 0.2 | 02 | 51.300 | 47.150 | 47200 | 48050 | 49550 | 51300 |
|  |  | 06 | 0.3 | 01 | 56.800 | 50.650 | 50700 | 51850 | 54150 | 56800 |
|  |  | 0.7 | 0.1 | 02 | 50.517 | 48342 | 48400 | 48.992 | 49675 | 50.517 |
|  |  | 07 | 0.2 | 01 | 56.017 | 51 B42 | 51900 | 52.792 | 54275 | 56017 |
|  |  | 0.8 | 0.1 | 0.1 | 55.233 | 53.033 | 53100 | 53.733 | 54400 | 55233 |
| SUM |  |  |  |  | 165800 | 1415.00 | 141600 | 145700 | 155100 | 165¢.00 |


| T | M | W1 | W2 | W3 | SPTIEDO | EDDISPT | S $[1]$ | $\mathbf{S}[2]$ | S[3] | \$[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 28 | 8 | 01 | 0.1 | 08 | 22.542 | 20617 | 20625 | 20867 | 21650 | 22,542 |
|  |  | 01 | 0.2 | 07 | 28.242 | 24417 | 24425 | 24867 | 26450 | 28242 |
|  |  | 01 | 03 | 0.6 | 33942 | 28217 | 28.225 | 28867 | 31250 | 33942 |
|  |  | 0.1 | 04 | 05 | 39642 | 32017 | 32025 | 32,867 | 36050 | 39642 |
|  |  | 01 | 0.5 | 04 | 45.342 | 35817 | 35825 | 36.867 | 40850 | 45.342 |
|  |  | 01 | 0.6 | 03 | 51042 | 35617 | 39625 | 40867 | 45650 | 51.042 |
|  |  | 0.1 | 07 | 0.2 | 55.742 | 43417 | 43.425 | 44867 | 50450 | 56.742 |
|  |  | 0.1 | 08 | 01 | 62.442 | 47.217 | 47.225 | 48.867 | 55250 | 62442 |
|  |  | 02 | 01 | 0.7 | 27.383 | 25433 | 25450 | 25.733 | 26500 | 27.383 |
|  |  | 02 | 02 | 06 | 33.083 | 29.233 | 29250 | 29.733 | 31.300 | 33083 |
|  |  | 0.2 | 0.3 | 05 | 38783 | 33033 | 33050 | 33733 | 36.100 | 38783 |
|  |  | 02 | 04 | 0.4 | 44483 | 36833 | 36850 | 37733 | 40.900 | 44.483 |
|  |  | 02 | 05 | 03 | 50.183 | 40633 | 40650 | 41.733 | 45.703 | 50.183 |
|  |  | 0.2 | 06 | 0.2 | 55883 | 44433 | 44450 | 45739 | 50.500 | 55883 |
|  |  | 02 | 0.7 | 0.1 | 51.583 | 48233 | 48250 | 49733 | 55.300 | 61.583 |
|  |  | 03 | 0.1 | 06 | 32225 | 30.250 | 30275 | 30.600 | 31.350 | 32225 |
|  |  | 03 | 02 | 05 | 37.925 | 34050 | 34.075 | 34600 | 36.150 | 37925 |
|  |  | 03 | 03 | 04 | 43625 | 37850 | 37875 | 38.600 | 40.950 | 43625 |
|  |  | 0.3 | 0.4 | 03 | 49325 | 41650 | 41675 | 42.600 | 45.750 | 49.325 |
|  |  | 0.3 | 0.5 | 02 | 55025 | 45450 | 45475 | 46.600 | 50.550 | 55.025 |
|  |  | 03 | 0.6 | 01 | 60.725 | 49250 | 49275 | 50600 | 55350 | 60.725 |
|  |  | 04 | 0.1 | 05 | 37067 | 35067 | 35.100 | 35.467 | 36.200 | 37067 |
|  |  | 04 | 02 | 0.4 | 42767 | 38.867 | 38.900 | 39.467 | 41.000 | 42767 |
|  |  | 04 | 03 | 0.3 | 48467 | 42.667 | 42700 | 43467 | 45800 | 48467 |
|  |  | 0.4 | 04 | 02 | 54167 | 46.467 | 46500 | 47.467 | 50,600 | 54.967 |
|  |  | 04 | 05 | 0.1 | 59867 | 50.267 | 50300 | 51.467 | 55400 | 59867 |
|  |  | 05 | 01 | 04 | 41908 | 39883 | 39.925 | 40333 | 41.050 | 41908 |
|  |  | 05 | 02 | 03 | 47.508 | 43683 | 43725 | 44333 | 45850 | 47.608 |
|  |  | 05 | 03 | 02 | 53308 | 47.483 | 47.525 | 48333 | 50.650 | 53.30 B |
|  |  | 05 | 04 | 01 | 59008 | 51.293 | 51,325 | 52.333 | 55450 | 59008 |
|  |  | 06 | 01 | D3 | 46.750 | 44.700 | 44750 | 45200 | 45900 | 46750 |
|  |  | 06 | 0.2 | 0.2 | 52450 | 48500 | 42550 | 49.200 | 50.700 | 52.460 |
|  |  | 06 | 03 | 0.1 | 58150 | 52.300 | 52350 | 53200 | 55500 | 58150 |
|  |  | 07 | 01 | 02 | 59592 | 49517 | 49.575 | 50067 | 50.750 | 51592 |
|  |  | 07 | 02 | 01 | 57.292 | 53317 | 53.375 | 54.067 | 55550 | 57.292 |
|  |  | 08 | 0.1 | 01 | 56.433 | 54333 | 54400 | 54.933 | 55600 | 56433 |
|  |  | SUM |  |  | 1697.00 | 1465.00 | 146700 | 1496.00 | 159000 | 1697 D0 |


| 00 çs | 0087c！ | 00 ¢らtb | 00．1001 | 0000．0． | 005595 | W 1 S |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Eee $\dagger$ ¢ | 009 Eg | ¢¢8＇Zg | 00125 | Eco ${ }^{\circ}$ | EとEV気 | 1.0 | 10 | 80 |  |  |
| 2PDG9 | 00e＇§s | L18＇19 | 52106 | 49965 | 2togs | $1{ }^{\prime} 0$ | 20 | 10 |  |  |
| 2500s | 002 6t | $\angle 150$ | $928<6$ | 2920 20 | 2 bOOS | 20 | 10 | 10 |  |  |
| OSLSg | OOL ES | 00809 | OSE＇6\％ | 008＇6 ${ }^{\text {b }}$ | OSLS 5 | 10 | E＇0 | 90 |  |  |
| OStos | 000＇6p | $00 c^{\circ} \mathrm{L}$ | OSt $\mathrm{gr}^{\text {b }}$ | 00\％ 9 | OSLOS | 20 | 2 D | 90 |  |  |
| c5 35 | 006＇t | 00でか | DSG Et | 009＇cp | OGL＇Gb | $\varepsilon 0$ | 10 | 90 |  |  |
| B5t 98 | 006＇z9 | ¢ 816 b | ct6 $2 t$ | Ec6 $\mathrm{L}^{\circ}$ | 89t 95 | 10 | $\square 0$ | 90 |  |  |
| 85\％し¢ | 008＇8 ${ }^{\text {d }}$ | ¢Bt 9\％ | St0 5b |  |  | 20 | E0 | 90 |  |  |
| 89t\％ | 002 $\ddagger$ | EBL Et | 54t Cb | Ecl＇zo | 8St 9 b | E0 | 20 | 90 |  |  |
| BSt it | 0090 t | ¢68 68 | GL2 68 | $\varepsilon \varepsilon 268$ | 85t $\downarrow$ | $\forall 0$ | L＇0 | 90 |  |  |
| 29145 | 00428 | 292\％ | 009 gb | 49590 | 491．4s | 10 | $G 0$ | $\checkmark 0$ |  |  |
| L91＇2G | 00985 | 29\％ 5 ¢ | 002 E\％ | 2包包 | 291．2s | zo | $\pm 0$ | ¢0 |  |  |
| 29314 | 009 tt | 191＇zo | 00800 | 2920p | 4914 | \＆＇0 | $\varepsilon 0$ | $\square^{0}$ |  |  |
| 2912\％ | 00v＇0t | 19885 | 006 LE | 49828 | 291＇2\％ | $\bigcirc 0$ | z0 | $\checkmark 0$ |  |  |
| 29128 | 00E 98 | L9598 | 000 98 | 296＇s¢ | 29128 | 50 | 10 | $\pm 0$ |  |  |
| 54825 | 009 己s | 052\％ | czz sb | 00256 | SLB LS | 10 | 90 | $8 \cdot 0$ |  |  |
| ct8 $¢ 5$ | 00t 8 t | OStoto | çe zi | 00E て $\dagger$ | 528 Z | z＇0 | ¢0 | 80 |  |  |
| ç8 $2 ⿰$ | 00E $\dagger t$ | OG5＇レ\％ | çt＇6¢ | 00t ¢ ¢ | S 28 Lt | 80 | $\forall 0$ | \＆＇0 |  |  |
| G28 Z | 00 Ot | $098{ }^{\circ} \mathrm{LE}$ | SCs＇98 | 00G 98 | S 28 Z | $\pm 0$ | $\varepsilon \cdot 0$ | 80 |  |  |
| GLa 2 E | 001．98 | OS5゙ビ |  | 009 EE | GL8 28 | 90 | 20 | 80 |  |  |
| GL8＇z8 | 000 乙 | osでィ | 52208 | 0020 | GL8 2 E | 90 | 10 | $8 \%$ |  |  |
| ¢69＇89 | 00 ZS | EEC． 97 | 0捾＇も | ¢ ¢＇¢ | ¢ \％\％ | 10 | $\angle$－ | 20 |  |  |
| ERS 的 | 00\％＇6\％ | cebst | OG6 06 | عc6 6 ¢ | E8s＇¢5 | 2＇0 | 90 | 20 |  |  |
| Egs 8 | 001 \＄ | cel Ob | OGO EE | ع¢0 8 㫜 | Esc＇or | $8 \cdot 0$ | c＇0 | 20 |  |  |
| EGS ¢ 6 | 000＇00 | cers 98 | QSI SE | CE！SE | Ess＇Er | 50 | $\checkmark 0$ | 20 |  |  |
| EB5 疑 | OOG＇GE | $\varepsilon \varepsilon G \varepsilon \varepsilon$ | OCZ ZE | とこどてく | ERG 8 E | 50 | $\varepsilon 0$ | 20 |  |  |
| $\varepsilon \in 9^{\circ} \mathrm{E}$ ¢ | 00818 | $\varepsilon \subset Z 0 ¢$ | OSE 62 | £ce＇6z | CSS EE | 90 | 20 | z0 |  |  |
| 885 87 | D0， 22 | ¢E6 9Z | 65t9\％ | CEv＇9z | E8G 82 | $\angle 0$ | 10 | 20 |  |  |
| Z62 69 | D01 29 | 21290 | GLt 2 p | $29 t 2 t$ | 262 65 | ＋0 | 80 | 10 |  |  |
| 262 kG | 000 旪 | くけで | GLG 6E | 29568 | 262 b | 20 | 10 | 10 |  |  |
| Z6Z 68 | 0068 | くLV6 | S 299 S | 299 ge | と放60 | $\varepsilon 6$ | 90 | 10 |  |  |
| て6Z 㖇 | 008＇ts | Lt89 | GLLEE | 1928 E | てEz | ¢0 | 50 | 10 |  |  |
| Z62 6E | 00258 | L19 Z | G28 0e | 19806 | 26Z＇68 | 90 | $\bigcirc 0$ | 10 |  |  |
| て6でにく | 00915 | ぐで6Z | 9L6 2 C | 19612 | こ6で切 | 90 | $\varepsilon 0$ | 10 |  |  |
| て6で 62 | OOSLZ | 41658 | 9LO 9z | 290 cz | Z62＇62 | 10 | 20 | 10 |  |  |
| 26Z +2 | DOF＇¢ | 119 zz | Sくlでて | 19187 | 26でもて | 80 | 10 | 1.0 | ¢ | 62 |
| ［t］ | ［ह］S | ［2］s | ［l］s | 1 dSTO | 00．jids | SM | 2M | LA | W | 1 |


| 00 9691 | 00\％6051 | $00 ¢ \underline{y c}$ | 000581 | 00＇6さを4 | 0096191． | WnS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 00829 | ¢ ¢ ${ }^{\text {cis }}$ | 00808 | ¢ELOG | EEL ¢ ${ }^{\text {c }}$ | 10 | ＇0 | 80 |  |  |
| 492．Es | GZOZS | 2ts $0 ¢$ | OSで的 | Z6L 6 | L9185 | 10 | 20 | 20 |  |  |
| 496．60 | g2t 9b | てtt 20 | 099 9p | 26G 9b | 2968 | 20 | ＇0 | $\angle 0$ |  |  |
| 00t oc | 05t5 | 0\％\％＇大 | 002 $2 t$ | 059 t | 00009 | L＇0 | EO | 90 |  |  |
| 00965 | 058 Lb | OSc＇9t | 0015 | OGO 5 | 009＇6力 | 20 | C0 | 90 |  |  |
| 008 \＄ | 056 | OSZ Et | 005 Zt | OGVても | 008 to | E0 | 10 | 90 |  |  |
| ¢ \％O＇S | GLtic | BSE $\square^{\text {b }}$ | 0st＇9b | 801 9b | EEOSg | \％ | $\checkmark$ | G 0 |  |  |
| £ C＇ $0 ¢$ | SLC＇Lb | 8SZ 5＊ | OSG＇ t ¢ | $8058 t$ | Ece $\mathrm{DF}^{\text {c }}$ | 2＇0 | ¢0 | 50 |  |  |
| ¢¢t ¢b | G 19 ¢ ¢ | 651で | 09600 | 806.06 | \＆とb＇sb | E 0 | zo | 90 |  |  |
| ¢c9 0 | GLCE 6 | Ect 68 | OSE 88 |  | Ecgot | $\rightarrow 0$ | 10 | g＇0 |  |  |
| 499 cc | 002\％ | 29220 | $009 \%$ | L99 pt | 499＇cg | 1.0 | 50 | V＇0 |  |  |
| 498＇09 | 00c：2t | L9！tr | 000＇で | 296 し | $\angle 9809$ | 20 | $\checkmark 0$ | $\square D^{\circ}$ |  |  |
| L90＇9\％ | 00\％$¢ t$ | 290 lb | 001＇6E | 49868 | 2909\％ | 8＇0 | 80 | $\square 0$ |  |  |
| 492 it | 00 S 6 | 296＇LE | 00898 | L92＇9s | 29216 | $\pm 0$ | 20 | ＋0 |  |  |
| LSt゙9s | 009 GE | 19806 | 002＇VE | L91 08 | 49b＇9§ | G0 | 10 | $\pm$－0 |  |  |
| DOE 95 | S7609 | GLI 9b | 0so＇sp | czo et | 00 e 9 | 1＇0 | 90 | E0 |  |  |
| 00915 | 92002 | GL0 ¢b | OSt or | 9Zt＇ob | 00915 | 20 | 90 | E® |  |  |
| 002＇90 | çl $\square^{\text {b }}$ | SL6＇60 | 098＇28 | gzg 28 | 002＇90 | 80 | $\checkmark 0$ | $\varepsilon 0$ |  |  |
| OOC＇L | scze6E | 9 289 | OGZ $¢ ¢$ | cze se | 006＇L | ¢ D | 80 | 80 |  |  |
| 00128 | GZEsE | GLL＇E¢ | 059 Ze | 宛g＇tE | 001 28 | 90 | z＇0 | $\varepsilon \cdot 0$ |  |  |
| 008 z\％ | ço＇te | SL9 0E | DCODO | czo 0e | 00¢＇z | 90 | 10 | E0 |  |  |
| ¢¢6． 99 | 0g9 09 | EROGO | 005 26 | と号じ | ¢ ¢ $9 ¢$ | 10 | 20 | 20 |  |  |
| Eとt＇zs | 0SL 9t | CEG＇LO | 006 㫙 | cese ${ }^{\text {es }}$ | £ $¢ 1$ Z¢ | 20 | 9.0 | 2＇0 |  |  |
| Ece $2 \square$ | 098 で | ¢68 88 | 00 Ec | $\varepsilon 8298$ | ¢¢¢ $\angle$ | 80 | 90 | 20 |  |  |
| Ecg z | 0568 | cetcs | 002 Ec | £89＇¢E | E¢S ${ }^{\text {¢ }}$ | $\pm 0$ | $\square{ }^{\circ}$ | 20 |  |  |
| ¢ 2 L $2 ¢$ | OSO SE | C89＇Z8 | 001 LE | E80＇LE | ECLLE | 90 | 80 | zo |  |  |
| とこどて¢ | OGLIE | ¢8962 | OOS 8 E | Cspor | E¢G 78 | 90 | z＇0 | 20 |  |  |
| をとし＇的 | OGZ 2 L | Cut 97 | 006 sz | E88 9z | ¢¢1 $\mathrm{EZ}^{\text {c }}$ | 20 | ${ }^{\prime} 0$ | 20 |  |  |
| L9G 29 | SLéOS | 266\％ | 056＇5E | てセ6 6E | 299＇25 | 10 | 80 | 10 |  |  |
| 494． 29 | SLt 96 | 2680 | DSE LE | 2ヵ¢2E | L926 6 | $2 \cdot 0$ | 40 | 10 |  |  |
| L96＇Lt | GLG Z t | 乙 62.2 C | OGLtE | でで吠 | 49625 | ¢0 | 90 | 10 |  |  |
| L91Et | \＄2968 | 269\％ | OGI＇RE | でI てe | 4948 | 70 | 50 | 1.0 |  |  |
| L9E明 |  | Z65＊ | 09962 | 2t5 6\％ | L9888 | 50 | $\pm 0$ | 10 |  |  |
| L9S $8 ¢$ | 92808 | 26t88 | 0\％6＇92 | 2ち69\％ | 499＇8t | 90 | E0 | 10 |  |  |
| 29282 |  | 乙be gl | 0sc＇oz | でさ ちて | 294＇82 | 20 | 20 | 10 |  |  |
| $\underline{4968}$ | G 20 Cl | Z6Z ZZ | OFL＇LZ | こせさして | 296＇zz | 80 | 10 | 10 | $\dagger$ | 62 |
| tis | ［ $¢$ ］ | ［ 7 ］． | ［L］ | 1dS／403 | GOJj1dS | EM | ZM | LM | w | 1 |


| T | M ${ }^{\text {l }}$ | W1 | W2 | W3 | SPTIEDD | EDDJSPT | S[1] | S[2] | S[3] | ST4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 29 | 6 | 01 | 0.1 | 0.8 | 24.617 | 22.592 | 22.600 | 22.542 | 23725 | 24617 |
|  |  | 0.1 | 0.2 | 07 | 29817 | 25.792 | 25.806 | 26442 | 28.025 | 25.817 |
|  |  | 0.1 | 03 | 06 | 35017 | 28.992 | 29000 | 29942 | 32325 | 35017 |
|  |  | 0.1 | 04 | 0.5 | 40217 | 32.192 | 32.200 | 33442 | 36625 | 40217 |
|  |  | 0.1 | 0.5 | 0.4 | 45.417 | 35392 | 35400 | 36942 | 40925 | 45417 |
|  |  | 01 | 06 | 0.3 | 50617 | 38.592 | 36600 | 40.442 | 45225 | 50.617 |
|  |  | 0.1 | 07 | 0.2 | 55817 | 41.792 | 41.800 | 43942 | 49.525 | 55817 |
|  |  | 0.1 | 08 | 01 | 61017 | 44.902 | 45000 | 47.442 | 53825 | 69017 |
|  |  | 0.2 | 0.1 | 07 | 29.033 | 26.983 | 27 E00 | 27.363 | 28150 | 29.033 |
|  |  | 02 | 0.2 | 0.6 | 34.233 | 30183 | 30200 | 30883 | 32.450 | 34233 |
|  |  | 02 | 03 | 0.5 | 39433 | 33383 | 33400 | 34.383 | 36750 | 39433 |
|  |  | 0.2 | 04 | 0.4 | 44633 | 36.583 | 36800 | 37.883 | 41050 | 44.633 |
|  |  | 0.2 | 0.5 | 03 | 49833 | 39.783 | 39800 | 41383 | 45350 | 49833 |
|  |  | 0.2 | 0.6 | 02 | 55033 | 42983 | 43.000 | 44883 | 49650 | 55.033 |
|  |  | 0.2 | 07 | 01 | 60.233 | 46.183 | 46.260 | 48.363 | 53950 | 60233 |
|  |  | 03 | 01 | 06 | 33.450 | 31.375 | 31.400 | 31.825 | 32575 | 33450 |
|  |  | 03 | 02 | 0.5 | 38.550 | 34.575 | 34.600 | 35325 | 36875 | 38650 |
|  |  | 03 | 0.3 | 0.5 | 43.850 | 37.775 | 37.800 | 38825 | 41.175 | 43.850 |
|  |  | 03 | 04 | 03 | 49.050 | 40.975 | 41.000 | 42.325 | 45475 | 49050 |
|  |  | 03 | 06 | 02 | 54250 | 44.175 | 44200 | 45.825 | 49775 | 54.250 |
|  |  | 03 | 06 | 0.1 | 59450 | 47375 | 47.400 | 49325 | 54.075 | 59.450 |
|  |  | 04 | 01 | 0.5 | 37.867 | 35767 | 35800 | 36267 | 37.000 | 37.867 |
|  |  | 04 | 02 | 04 | 43.067 | 38.967 | 39.000 | 39767 | 41.300 | 43.067 |
|  |  | 0.4 | 03 | ¢3 | 48.267 | 42.167 | 42200 | 43267 | 45800 | 48267 |
|  |  | 04 | 0.4 | $\bigcirc 2$ | 53467 | 45367 | 45400 | 46.767 | 49900 | 53.467 |
|  |  | 04 | 05 | 0.1 | 58.667 | 48567 | 48.600 | 50267 | 54.200 | 58.667 |
|  |  | 0.5 | 01 | 04 | 42.283 | 4 1 158 | 40200 | 40,708 | 41425 | 42.283 |
|  |  | 0.5 | 02 | 03 | 47.493 | 43358 | 43.400 | 44.208 | 45725 | 47.483 |
|  |  | 0.5 | 03 | 02 | 52683 | 46558 | 46600 | 47.708 | 50025 | 52.683 |
|  |  | 0.5 | 04 | 01 | 57883 | 49758 | 49800 | 51.208 | 54325 | 57.883 |
|  |  | 0.6 | 01 | 03 | 46700 | 44550 | 44600 | 45.150 | 45850 | 46700 |
|  |  | 06 | 62 | 0.2 | 51900 | 47750 | 47.800 | 48650 | 50150 | 51.900 |
|  |  | 06 | 0.3 | 01 | 57100 | 50.950 | 51000 | 52150 | 54.450 | 57.100 |
|  |  | 0.7 | 0.1 | 02 | 51117 | 48942 | 49000 | 49.592 | 50275 | 51.117 |
|  |  | 0.7 | 62 | 0.1 | 56.317 | 52142 | 52.200 | 53092 | 54575 | 56.317 |
|  |  | 08 | 01 | 0.1 | 55533 | 53333 | 53.400 | 54.933 | 54700 | 55.533 |
| इण़M |  |  |  |  | 169400 | 1451.00 | 145200 | 149300 | 1597.00 | 1694 \% |


| 1 | M | W1 | W2 | W3 | SPTJED | EDDISPT | S[1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 29 | 7 | 0.1 | 0.1 | 08 | 24942 | 23017 | 23025 | 23.267 | 24050 | 24.942 |
|  |  | 01 | 0.2 | 0.7 | 30342 | 26517 | 26.525 | 26.967 | 28550 | 30342 |
|  |  | 01 | 03 | 0.6 | 35.742 | 30.017 | 30025 | 30667 | 33050 | 35742 |
|  |  | 0.1 | 04 | 05 | 41142 | 33.517 | 33525 | 34367 | 37.550 | 41142 |
|  |  | 0.1 | 0.5 | 04 | 46542 | 37.017 | 37.025 | 38.067 | 42050 | 46.542 |
|  |  | 0.1 | 06 | 03 | 51942 | 40.517 | 40.625 | 41.767 | 46550 | 51.942 |
|  |  | 0.1 | 0.7 | 02 | 57342 | 44.017 | 44.025 | 45.467 | 51050 | 57.342 |
|  |  | 01 | 08 | 01 | 62.742 | 47.517 | 47525 | 49.167 | 55550 | 62742 |
|  |  | 0.2 | 01 | 07 | 29483 | 27.533 | 27550 | 27.433 | 28600 | 29.483 |
|  |  | 02 | 02 | 06 | 34.883 | 31.033 | 31050 | 31.533 | 33100 | 34883 |
|  |  | 02 | 03 | 05 | 40283 | 34.533 | 34550 | 35.233 | 37600 | 40.283 |
|  |  | 02 | 04 | 04 | 45.683 | 38033 | 38050 | 38.933 | 42.100 | 45683 |
|  |  | 0.2 | 0.5 | 03 | 51.883 | 41.533 | 41 550 | 42633 | 46600 | 51.083 |
|  |  | 02 | 0.6 | 0.2 | 56483 | 45.033 | 45 CSO | 46333 | 51.100 | 56483 |
|  |  | 0.2 | 0.7 | 0.1 | \$1.883 | 48533 | 48550 | 50.033 | 55600 | 61883 |
|  |  | 0.3 | 0.1 | $00 \cdot$ | 34.025 | 32050 | 32075 | 32.400 | 33150 | 34 D 25 |
|  |  | 0.3 | 0.2 | 05 | 39.425 | 35550 | 35575 | 36500 | 37.650 | 39425 |
|  |  | 03 | 03 | 0.4 | 44825 | 39050 | 39075 | 39800 | 42.150 | 44825 |
|  |  | 03 | 04 | D 3 | 50225 | 42.550 | 42575 | 43500 | 45650 | 50.225 |
|  |  | 03 | 05 | 02 | 55.625 | 46.050 | 46075 | 47200 | 51.150 | 55.625 |
|  |  | 03 | 06 | 0.1 | 61.025 | 49.550 | 49575 | 50900 | 55.650 | 61.025 |
|  |  | 0.4 | 01 | 0.5 | 38567 | 36567 | 36600 | 36967 | 37.700 | 38.567 |
|  |  | 0.4 | 02 | 0.4 | 43967 | 40067 | 40100 | 40.667 | 42.200 | 43967 |
|  |  | 04 | 03 | 0.3 | 49367 | 43567 | 43.600 | 44367 | 46.700 | 49.367 |
|  |  | 04 | 04 | 0.2 | 54.767 | 47067 | 47100 | 48.067 | 51.200 | 54767 |
|  |  | 04 | 0.5 | 0.1 | 60.167 | 50567 | 50.600 | 51767 | 55.700 | 60167 |
|  |  | 05 | 0.1 | 0.4 | 43108 | 41.083 | 41125 | 41533 | 42250 | 43.108 |
|  |  | 0.5 | 02 | 0.3 | 48.508 | 44.583 | 44625 | 45233 | 41950 | 48508 |
|  |  | 05 | 0.3 | 02 | 53.908 | 48083 | 48125 | 48.933 | 51.250 | 53908 |
|  |  | 0.5 | 04 | 0.1 | 59.308 | 51583 | 51625 | 52.633 | 55750 | 59308 |
|  |  | 06 | 0.1 | 0.3 | 47650 | 45600 | 45650 | 45100 | 46800 | 47650 |
|  |  | 06 | 0.2 | 0.2 | 53050 | 49100 | 49.150 | 49800 | 51.300 | 53.050 |
|  |  | 0.6 | 0.3 | 0.1 | 58450 | 52600 | 52.650 | 53500 | 55.8 .90 | 58450 |
|  |  | 0.7 | 0.1 | 02 | 52.192 | 50117 | 50175 | 50667 | 51.350 | 521192 |
|  |  | 0.7 | D 2 | 0.1 | 57.592 | 53617 | 53675 | 54367 | 55850 | 57.592 |
|  |  | 08 | 01 | 01 | 56.733 | 54633 | 54.700 | 55233 | 55.900 | 56.733 |
| SUM |  |  |  |  | 173300 | 1502.00 | 150300 | 1532.00 | 1626.00 | 173300 |


| T | M | W/1 | W2 | W3 | SPTPEDO | EDDISPT | S[1] | S[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 29 | 8 | 0.1 | 01 | 08 | 25.267 | 23442 | 23.450 | 23.592 | 24375 | 25.267 |
|  |  | 0.1 | 02 | 07 | 30.869 | 27242 | 27.250 | 27.492 | 29.075 | 30867 |
|  |  | 01 | 0.3 | 06 | 36.467 | 31.042 | 31.050 | 31392 | 33.775 | 36467 |
|  |  | 01 | 0.4 | 0.5 | 42.067 | 34.842 | 34.850 | 35.292 | 38.475 | 42067 |
|  |  | 01 | 0.5 | 0.4 | 47,667 | 38.642 | 36650 | 39.192 | 43175 | 47.667 |
|  |  | 01 | 06 | 0.3 | 53.267 | 42.442 | 42.450 | 43.092 | 47875 | 53.267 |
|  |  | 0.1 | 07 | 0.2 | 58867 | 46.242 | 46.250 | 46992 | 52.575 | 58867 |
|  |  | 01 | 08 | 01 | 54467 | 50042 | 50050 | 50892 | 57.275 | 64467 |
|  |  | 0.2 | 01 | 07 | 29.933 | 28.083 | 28.190 | 28.288 | 29050 | 29933 |
|  |  | 02 | 02 | 06 | 35533 | 31.883 | 31.900 | 32183 | 33750 | 35533 |
|  |  | 02 | 03 | 0.5 | 41,133 | 35683 | 35700 | 36.083 | 38.450 | 41.133 |
|  |  | 02 | 04 | 04 | 46733 | 39483 | 39500 | 39.983 | 43150 | 46733 |
|  |  | 02 | 05 | 0.3 | 52333 | 43.283 | 43300 | 43883 | 47850 | 52.333 |
|  |  | 02 | 06 | 02 | 57.933 | 47.083 | 47.100 | 47783 | 52550 | 57.933 |
|  |  | 02 | 07 | 01 | 63.593 | 50.883 | 50.900 | 51683 | \$7.250 | 63533 |
|  |  | 0.3 | 0.1 | 06 | 34.600 | 32.725 | 32.750 | 32975 | 33.725 | 34.600 |
|  |  | 03 | 02 | 05 | 40200 | 36.525 | 36.550 | 36875 | 38425 | 40200 |
|  |  | 03 | 03 | 0.4 | 45800 | 40.325 | 40.350 | 40.775 | 43125 | 45.801 |
|  |  | 0.3 | 04 | 03 | 51.400 | 44.125 | 44.150 | 44.675 | 47825 | 51.400 |
|  |  | 0.3 | 0.5 | 02 | 57000 | 47.925 | 47.950 | 48575 | 52.525 | 57.000 |
|  |  | 0.3 | 0.6 | 01 | 62.600 | 51.725 | 51.750 | 52475 | 57.225 | 62600 |
|  |  | 0.4 | 0.1 | 05 | 39.267 | 37.367 | 37.400 | 37667 | 38.400 | 39.267 |
|  |  | 04 | 0.2 | 04 | 44.867 | 41.167 | 41.200 | 41567 | 43100 | 44867 |
|  |  | 0.4 | 03 | 03 | 50.467 | 44.967 | 45000 | 45467 | 47.800 | 50467 |
|  |  | 0.4 | 04 | 0.2 | 56.067 | 48.767 | 48800 | 49367 | 52.500 | 56.067 |
|  |  | 04 | 05 | 0.1 | 61.667 | 52567 | 52600 | 53.267 | 57200 | 61.667 |
|  |  | 0.5 | 0.1 | 04 | 43933 | 4200 H | 42.050 | 42.358 | 43075 | 43933 |
|  |  | 05 | 02 | 03 | 49.533 | 45808 | 45850 | 46258 | 47.775 | 49533 |
|  |  | 05 | 03 | 02 | 55133 | 49608 | 49650 | 50.158 | 52475 | 55133 |
|  |  | 05 | 04 | 01 | 60733 | 53408 | 53.450 | 54058 | 57175 | 60.733 |
|  |  | 06 | D 1 | 03 | 48.600 | 46650 | 46700 | 47.050 | 47750 | 48.600 |
|  |  | 06 | D 2 | 02 | 5-4.200 | 50450 | 50500 | 50950 | 52450 | 54.200 |
|  |  | 06 | D 3 | 01 | 59800 | 54259 | 54300 | 54.850 | 57150 | 59800 |
|  |  | 07 | 01 | 02 | 53.267 | 51292 | 51350 | 51.742 | 52425 | 53267 |
|  |  | 07 | 02 | 01 | 58367 | 55.092 | 55150 | 55642 | 57.125 | 58867 |
|  |  | 08 | 01 | 0.1 | 57.933 | 55.933 | 56000 | 56433 | 57100 | 57933 |
| SUW |  |  |  |  | 177206 | 1553.00 | 155400 | 1571 D0 | 168500 | 177200 |


| T | H | W1 | W2 | W3 | SPTIEDD | EDPISPT | S[1] | S[2] | \$[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 30 | 4 | 01 | 01 | 08 | 25392 | 12.983 | 12975 | 12.942 | 24.500 | 25392 |
|  |  | W $\downarrow$ | 02 | 0.7 | 29292 | 15283 | 15475 | 15442 | 27500 | 29292 |
|  |  | W1 | 03 | 0.6 | 33192 | 17583 | 17.975 | 17.942 | 30500 | 33.192 |
|  |  | 01 | 0.4 | 0.5 | 37092 | 19883 | 20.475 | 20.442 | 33500 | 37.092 |
|  |  | 01 | 95 | 다 4 | 40992 | 22183 | 22975 | 22.942 | 36500 | 40.992 |
|  |  | 01 | 46 | 03 | 44.892 | 24483 | 25475 | 25442 | 39500 | 44892 |
|  |  | 01 | 6.7 | 안 | 48.792 | 26783 | 27975 | 27.942 | 42500 | 48792 |
|  |  | 01 | 08 | 0.1 | 52.692 | 29083 | 30475 | 30442 | 45500 | 52692 |
|  |  | 0.2 | 0.1 | 07 | 28883 | 17.667 | 17.450 | 17.383 | 28000 | 28883 |
|  |  | 02 | 0.2 | 0.6 | 32783 | 19967 | 19.950 | 19883 | 31000 | 32.783 |
|  |  | 0.2 | 0.3 | 0.5 | 36683 | 22 267 | 22.450 | 22.383 | 34000 | 36.663 |
|  |  | 02 | 04 | 0.4 | 40583 | 24567 | 24950 | 24883 | 37000 | 40583 |
|  |  | 62 | 05 | 0.3 | 44483 | 26867 | 27450 | 27.383 | 40600 | 44483 |
|  |  | 02 | 0.6 | 0.2 | 48383 | 29167 | 29.950 | 29883 | 43.0100 | 48383 |
|  |  | 0.2 | 07 | 01 | 52283 | 31.467 | 32.450 | 32383 | 46.000 | 52.2 BP |
|  |  | 03 | 01 | 06 | 32375 | 22.350 | 21925 | 21825 | 31.500 | 32.375 |
|  |  | 03 | 02 | 0.5 | \$6 275 | 24650 | 24425 | 24.325 | 34.500 | 36275 |
|  |  | 0.3 | 0.3 | 04 | 40.175 | 26.950 | 26.925 | 26825 | 37.500 | 40.175 |
|  |  | 03 | 0.4 | 03 | 44075 | 29.250 | 29425 | 29325 | 40500 | 44075 |
|  |  | 03 | 0.5 | 0.2 | 47975 | 31550 | 31.925 | 31.825 | 43500 | 47975 |
|  |  | 0.3 | 0.6 | 01 | 51 B75 | 33.850 | 34425 | 34325 | 46500 | 51.875 |
|  |  | 0.4 | 01 | 05 | 35867 | 27.033 | 26.400 | 26267 | 35000 | 35867 |
|  |  | 04 | 02 | 04 | 39.767 | 29333 | 28900 | 28.767 | 38000 | 39767 |
|  |  | 0.4 | 03 | 03 | 43.6施 | 31633 | 31400 | 31.267 | 41.000 | 43667 |
|  |  | 04 | 04 | 0.2 | 47.567 | 33933 | 33900 | 33.767 | 44.000 | 47567 |
|  |  | 04 | 05 | 01 | 51.467 | 36233 | 36400 | 36.267 | 47.000 | 51467 |
|  |  | 0.5 | 01 | 04 | 39359 | 31.717 | 30.875 | 30708 | 38500 | 39358 |
|  |  | 05 | 0.2 | 0.3 | 43258 | 34017 | 33.375 | 33208 | 41.500 | 43.258 |
|  |  | 05 | 0.3 | 0.2 | 47158 | 36317 | 35.875 | 35.708 | 44.500 | 47.158 |
|  |  | ¢ 5 | 0.4 | 0.1 | 51.058 | 38617 | 38 375 | 38208 | 47500 | 51.058 |
|  |  | 0.6 | 01 | 03 | 42850 | 36400 | 35350 | 35150 | 42.000 | 42850 |
|  |  | 66 | 02 | 0.2 | 46750 | 38700 | 37.850 | 37.650 | 45000 | 46.750 |
|  |  | 06 | 0.3 | 0.1 | 56650 | 41000 | 40.350 | 40.150 | 48000 | 50.650 |
|  |  | 0.7 | 01 | 02 | 46342 | 41.003 | 39825 | 39592 | 45500 | 46342 |
|  |  | 0.7 | 02 | 01 | 50.242 | 43363 | 42325 | 42.092 | 48500 | 50242 |
|  |  | 0.8 | 01 | 01 | 49833 | 45767 | 44300 | 44033 | 49000 | 49833 |
| SUM |  |  |  |  | 1535.00 | 105400 | 1053.00 | 1949.06 | 1428 00 | 1535.00 |


| T | 中 10 | W1 | W2 | W3 | SPT/EDO | EDDISPT | S[1] | S[2] | S[3] | 5[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 30 | 5 | 01 | 01 | 08 | 25700 | 13.392 | 13275 | 13.242 | 24808 | 2.5.700 |
|  |  | 01 | 0.2 | 0.7 | 29800 | 15.992 | 15.975 | 15942 | 28008 | 29800 |
|  |  | 01 | 0.3 | 06 | 33.960 | 18592 | 18.675 | 18642 | 31208 | 33900 |
|  |  | D 1 | D 4 | 05 | 38000 | 21192 | 21375 | 21.342 | 34.408 | 38.000 |
|  |  | 01 | 0.5 | D 4 | 42100 | 23792 | 24075 | 24.042 | 37608 | 42.100 |
|  |  | 0.1 | 06 | 03 | 45200 | 26.392 | 26775 | 26742 | 40808 | 46.200 |
|  |  | 0.1 | 07 | 02 | 50300 | 28992 | 29475 | 29442 | 44.008 | 50.300 |
|  |  | 01 | 08 | 0.1 | 54400 | 31592 | 32175 | 32.142 | 47.208 | 54400 |
|  |  | 02 | 01 | 07 | 29.300 | 18.183 | 17850 | 17783 | 28417 | 29.300 |
|  |  | 02 | 02 | 06 | 3.3 .400 | 20.783 | 20550 | 20483 | 31.617 | 33400 |
|  |  | 02 | 0.3 | 05 | 37500 | 23383 | 23250 | 23.183 | 34.817 | 37500 |
|  |  | 02 | 04 | 04 | 41600 | 25983 | 25.950 | 25883 | 38017 | 41600 |
|  |  | 02 | 05 | 03 | 45.700 | 28583 | 28650 | 28583 | 41217 | 45.700 |
|  |  | 02 | 06 | 0.2 | 49.800 | 31183 | 31.350 | 31283 | 44.417 | 49800 |
|  |  | 02 | 0.7 | 01 | 53960 | 33783 | 34050 | 33983 | 47.617 | 53900 |
|  |  | 03 | 0.1 | 06 | 32900 | 22975 | 22425 | 22.325 | 32025 | 32.900 |
|  |  | 03 | 02 | 0.5 | 37050 | 25.575 | 25125 | 25.025 | 35.225 | 37.000 |
|  |  | 03 | 03 | 04 | 41.100 | 28.175 | 27.825 | 27.725 | 38.425 | 41.100 |
|  |  | 03 | 0.4 | 03 | 45200 | 30.775 | 30.525 | 30425 | 41.625 | 45200 |
|  |  | 03 | 05 | 0.2 | 49300 | 33.375 | 33225 | 33125 | 44825 | 49.300 |
|  |  | 0.3 | D6 | 0.1 | 53400 | 35975 | 35.925 | 35825 | 48025 | 53406 |
|  |  | 04 | D 1 | 05 | 36.505 | 27.767 | 27.000 | 26867 | 35.633 | 36500 |
| - |  | 04 | 02 | 04 | 40606 | 30367 | 29700 | 29567 | 38.833 | 40600 |
|  |  | 04 | 03 | 03 | 44700 | 32967 | 32400 | 32.267 | 42.033 | 44700 |
|  |  | 04 | 04 | b 2 | 48800 | 35567 | 35100 | 34,967 | 45233 | 48800 |
|  |  | 04 | 05 | 01 | 52.900 | 38167 | 37800 | 37667 | 48433 | 52900 |
|  |  | 0.5 | 01 | 0.4 | 40100 | 32558 | 31575 | 31408 | 39.242 | 40.100 |
|  |  | 05 | 02 | 03 | 44200 | 35.158 | 34.275 | 34108 | 42.442 | 44200 |
|  |  | 05 | 03 | 0.2 | 48300 | 37756 | 36975 | 36808 | 45642 | 48300 |
|  |  | 0.5 | 04 | 0.1 | 52400 | 40358 | 39675 | 39508 | 48842 | 52.400 |
|  |  | 06 | 01 | 0.3 | 43700 | 37350 | 36150 | 35950 | 42850 | 43700 |
|  |  | 06 | 02 | 02 | 47 BOO | 39950 | 38850 | 38.650 | 46050 | 47.800 |
|  |  | 06 | 03 | 01 | 51900 | 42550 | 41550 | 41350 | 49250 | 51900 |
|  |  | 07 | 01 | 02 | 47.300 | 42.142 | 40725 | 40492 | 46458 | 47300 |
|  |  | 07 | 02 | 01 | 51.400 | 44,742 | 43125 | 43192 | 49658 | 51.400 |
|  |  | 08 | 01 | 0.1 | 50900 | 46.933 | 45300 | 45.033 | 50067 | 50900 |
| SUM |  |  |  |  | 1572.00 | 110300 | 1089.00 | 108500 | 146500 | 157200 |


| T | 市 | W\% | W2 | W/3 ${ }^{-1}$ | SPTJEDD | EDDJSPT | S[4] | 5[2] | S[3] | S[4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 30 | 6 | 01 | 01 | 03 | 26008 | 13800 | 13575 | 13542 | 25117 | 26008 |
|  |  | 01 | 0.2 | 07 | 30308 | 16700 | 16475 | 16442 | 23517 | 30.309 |
|  |  | 01 | 03 | 06 | 34608 | 19600 | 19.375 | 19342 | $31 \$ 17$ | 34608 |
|  |  | 01 | 04 | 0.5 | 38.908 | 22.500 | 22.275 | 22242 | 35317 | 38908 |
|  |  | 01 | 05 | 04 | 43208 | 25400 | 25175 | 25.142 | 38717 | 43208 |
|  |  | 01 | 06 | 03 | 47508 | 28300 | 28075 | 28042 | 42117 | 47508 |
|  |  | 01 | 0.7 | 02 | 51808 | 31200 | 30.975 | 30942 | 45.517 | 51.808 |
|  |  | 0.1 | 08 | 01 | 56,108 | 34100 | 33875 | 33842 | 48917 | 56108 |
|  |  | 02 | 01 | 07 | 29717 | 18700 | 18250 | 18.183 | 28833 | 29717 |
|  |  | 02 | 02 | 06 | 34017 | 21600 | 21150 | 21083 | 32233 | 34017 |
|  |  | 02 | © 3 | 05 | 38317 | 24500 | 24050 | 23983 | 35633 | 38317 |
|  |  | 02 | 04 | 04 | 42617 | 27.400 | 26950 | 26883 | 39033 | 42.617 |
|  |  | 02 | 05 | 03 | 46.917 | 30300 | 29850 | 29.783 | 42.433 | 46917 |
|  |  | 02 | 06 | 02 | 51.217 | 33200 | 32.750 | 32683 | 45833 | 51217 |
|  |  | 02 | 07 | 01 | $55 \$ 17$ | 36100 | 35650 | 35.583 | 49233 | \$5 517 |
|  |  | 03 | 01 | 06 | 33425 | 23600 | 22925 | 22.825 | 32550 | 33425 |
|  |  | 03 | 02 | 45 | 37725 | 26500 | 25825 | 25.725 | 35950 | 37725 |
|  |  | $\square 3$ | 03 | 0.4 | 42.025 | 29.400 | 28.72 .5 | 28.525 | 39350 | 42.025 |
|  |  | 03 | 04 | 03 | 46325 | 32300 | 31625 | 31525 | 42750 | 46.325 |
|  |  | 03 | 05 | 02 | 50625 | 35200 | 34525 | 34.425 | 46150 | 50525 |
|  |  | 03 | 06 | ¢ 1 | \$4.925 | 38.100 | 37.425 | \$7.325 | $49 \$ 50$ | 54.925 |
|  |  | 04 | 01 | 05 | 37133 | 28500 | 27600 | 27467 | 36267 | 37133 |
|  |  | 04 | 02 | 04 | 41433 | 31400 | 30500 | 30367 | 39667 | 41433 |
|  |  | 04 | 0.3 | 03 | 45733 | 34300 | 33400 | 33267 | 43067 | 45733 |
|  |  | 04 | 04 | 02 | 50033 | 37200 | 36300 | 36167 | 45467 | 50033 |
|  |  | 04 | 05 | 01 | 54333 | 40.100 | 39200 | 39.067 | 49.867 | 54.333 |
|  |  | 05 | 01 | 04 | 40842 | 33400 | 32275 | 32.108 | 39.983 | 40842 |
|  |  | 0.5 | 0.2 | 0.3 | 45142 | 36350 | 35175 | 35008 | 43383 | 45142 |
|  |  | 05 | 03 | 02 | 49442 | 39200 | 38075 | 37.908 | 46.783 | 49.442 |
|  |  | 05 | 04 | 01 | 53742 | 42.100 | 40975 | 40,808 | 50.183 | 53.742 |
|  |  | 06 | 01 | 03 | 44550 | 38300 | 36950 | 36750 | 43700 | 4455 D |
|  |  | 06 | 02 | 02 | 48850 | 41200 | 39850 | 39650 | 47100 | 48850 |
|  |  | 06 | 03 | 0.1 | 53150 | 44100 | 42750 | 42550 | 50500 | 53150 |
|  |  | 07 | 01 | 0.2 | 48.258 | 43200 | 41.625 | 41.392 | 47.417 | 48.258 |
|  |  | 07 | 02 | 01 | 52558 | 46100 | 44525 | 44292 | 50.817 | 5255 B |
|  |  | 08 | 01 | 01 | 51967 | 48100 | 46300 | 46033 | 51133 | 51967 |
|  |  | SUM |  |  | 160900 | 115200 | 112500 | 7121.00 | 150200 | 160900 |


| （k） 889 | 00925 | 00＇LIZL |  | 0160971 | 008891 | 1403 |  |  |  |  |
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| OSZ 58 | 19ヶ¢ 8 | c89＇Z2 | 0GL＇Zも | とぐとこ | 0¢Z ¢ ¢ | 90 | ＜0 | 20 |  |  |
| DSG DE | 49962 | ERI 6L | 0SC＇6l | EEL＇6L | OGG＇0E | 2.0 | 10 | 20 |  |  |
| GEG＇69 | EEEGS | Zロ官88 | \＄29＇的 | くりト它 | 52965 | 10 | 80 | 10 |  |  |
| SZ8 15 | EEc\％\％ | てbe SE | GLE＇GE | LIg＇SE | 9て8＇Vi | こ＇0 | 20 | 10 |  |  |
| çi 99 | ¢CL $\dagger \square$ | でぐ1E | G18＇L | L17E | ¢くし OS | \％ 0 | 90 | 10 |  |  |
| cこt＇Gb | を边0t | でを\％8 | SLE 日Z | く19白己 | らでらけ | $t 0$ | 90 | 10 |  |  |
| GLL QF | をとし 2 | でロ゙ャZ | S 18 ヤC | LlIGZ | G240\％ | 90 | ＋0 | 10 |  |  |
| S6098 | £EE EE | こだにく | GLEして | L19＊V | G20＇9E | 90 | C－0 | $1 \cdot 0$ |  |  |
| GRE＇LE | E¢S＇6U | て切くも | SL8＇2l | さいじ8． | GくE＇I\＆ | 40 | 20 | 10 |  |  |
| 979 ¢Z | c¢ 1 ç | でE $\ddagger 1$ | SLE゙も1 | 119゙っ！ | 92992 | 80 | 10 | $1 \cdot 0$ | 它 | tr |
| ［b］5 | ［を］S | ［z］S | ไj］ | EdS／003 | －0．311 15 | C．MA | CM | Wh | W | 1 |


| 00 9t9 | 006851 | 00\％6915 | 00＇¢ ¢ | Do＇LOZ | 009091 | Wก15 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| عEO＇¢S | 00でてS | CELく | 0075 | 492 68 | ceots | 10 | 10 | $\mathrm{a}^{\prime} 0$ |  |  |
| LLE¢S | 966＇19 | 265\％${ }^{\text {\％}}$ | 928 gr | 89t $2 \boldsymbol{P}$ | LL／EG | 10 | 20 | 20 |  |  |
| LLC 6b | GLe＇eb |  | ¢zg＇z | 6sで比 | 4LC 6 | 20 | 10 | 40 |  |  |
| OOt ES | DGLIG | OG0＇b | OGZ＇t | OGS＇g | 00\％ 6 | 10 | ¢0 | 90 |  |  |
| 0066 | OS1 8t | 0Gษ゙Dt | $0901 \%$ | Ostiz | $006{ }^{\circ} 6$ | zo | 20 | 90 |  |  |
| 00ヶ5 5 | DSS bt | 05928 | 958．28 | $0 ¢ 0 ゙ 68$ | 00\％9\％ | $\varepsilon 0$ | 5 | 90 |  |  |
| ¢80 cs | GZG＇LG | 80G＇で | 929\％ | 2re ¢t | ¢00 95 | 10 | $\bigcirc 0$ | 50 |  |  |
| ¢ $8 \mathrm{C}^{\prime} 05$ | gz6＇2b | $808.6 \varepsilon$ | 92060 | 2109 $0 t$ | ces 05 | 20 | EO | 50 |  |  |
| c60＇9b | gzitb | 801＇98 | 9LZ 9¢ | でも $2 ¢$ | ¢00 96 | ¢0 | 20 | 90 |  |  |
| Ess＇し＞ | getob | 806.78 | 940 EE | でで坞 | \＆\％¢ 1 | ¢0 | 10 | 50 |  |  |
| 292＇gs | 00¢19 | 2960 P | 001 15 | ع¢0 で | ＜9259 | 10 | Sb | $\square 0$ |  |  |
| 292＇Lg | 002\％ | 29L2 2 | 006 LE |  | 202 Ls | 20 | $\square 0$ | $\pm 0$ |  |  |
| 2949p | OOL tot | 295゙比 | D02 tE | EE9 SE | 29290 | $\varepsilon 0$ | $\varepsilon 0$ | $\checkmark 0$ |  |  |
| 292＇zr | OOS Ot | 29\％ 12 | DOS LE | と¢っても | L9Z $2 t$ | $\pm 0$ | 20 | $\pm 0$ |  |  |
| 292\％ | 00698 | 4918 L | ODE 日C | EEZ 6Z | L9E2E | 50 | 10 | $\square 0$ |  |  |
| Osios | 910＇LS | 9 $\mathrm{SV}^{-68}$ | 9ZS 6e | 9ZZ Ot | OSt ${ }^{\text {cos }}$ | 10 | 90 | 80 |  |  |
| oss ${ }^{\circ}$ | ctrit | $\mathrm{Gz2} 9 \mathrm{E}$ | ¢ZE＇¢ | S $2012 \varepsilon$ | OG5＇19 | \％ 0 | 90 | \％0 |  |  |
| 0ctit | 928Et | Szo ce | szlec | SZ8 \＆ | Ost2t | $\varepsilon 0$ | $\checkmark 0$ | E0 |  |  |
| 0967 | S $\angle Z Z^{\circ} 0 \times$ | 978 6z | 9z66z | 9Z90¢ | 096 Zt | $\% 0$ | E\％O | co |  |  |
| OSb 8 ¢ | S 29.98 | cza＇9z | GZE＇92 | $9 Z 0^{\circ} \mathrm{Cz}$ | $0 \mathrm{~Gb} \mathrm{~B}^{\text {c }}$ | G＇0 | 20 | E＇0 |  |  |
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| とELB | 0sget | EBt Le | DSS に | く10 ze | を¢1时 | ¢0 | so | 20 |  |  |
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| Ect 0 | 09\％ $\mathrm{s}_{2}$ | ¢89\％ | OGL Bt | LIZ 6b | Ect 0e | 40 | 10 | 20 |  |  |
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| LE＇Eg | G20：\％ | Zbles | GLL E¢ | 80ャ E E | LIEES | z0 | 10 | 10 |  |  |
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| 41968 | sczige | でG ¢ | SLG ¢z | 20\％\＆ | 4 18 ＇ 6 ¢ | g＇0 | $\square^{\circ}$ | 10 |  |  |
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[^0]:    * Ihe best schedule with the minimum weighted function

[^1]:    * The best schedule with the ninimum weighted function

