L-3/T-2/ME Date: 07/08/2016

# BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA

L-3/T-2 B. Sc. Engineering Examinations 2014-2015

Sub: IPE 331 (Production Processes)

Full Marks: 280

Time: 3 Hours

USE SEPARATE SCRIPTS FOR EACH SECTION

The figures in the margin indicate full marks.

# SECTION – A

There are FOUR questions in this section. Answer any THREE.

1.	(a) Briefly describe the properties that determine the quality of a sand mold for sand	
	casting. What is the difference between a pattern and a core in sand molding?	(12)
	(b) With the help of suitable diagrams, describe the following:	(24)
	(i) Centrifugal casting	
	(ii) Gating system	
	(iii) Gravity die casting	
	(c) Name various defects in castings with suitable diagrams. Why is it important to	
	remove dross or slag during the pouring of molten metal into the mold? Explain	
	briefly.	$(10\frac{1}{3})$
2.	(a) Show by simple diagram, the shear angle associated with machining ductile metal.	
	How is the value of that shear angle affected by tool rake angle and chip thickness in a	
	given machining condition?	(12)
	(b) Prove that the maximum main cutting force (Pz) in an orthogonal cutting is	
	$2\tau_s S_0 \operatorname{tcot}\beta \text{ if } 2\beta + \eta - \gamma = \pi/2$ .	(12)
	(c) A mild steel rod of 150 mm diameter is turned on a lathe at a speed of 340 rpm,	
	feed of 0.24 mm/rev and 2.5 mm depth of cut by a tool having tool rake angle 20° and	
	principal cutting edge angle 60°. It is found by the dynamometer that the main cutting	
	force = 800 N and feed force = 400 N. The value of chip reduction coefficient is 3.5.	`
	Calculate the coefficient of friction, shear plane angle, chip velocity and dynamic yield	v
	shear strength.	(12)
	(d) What conditions of machining and cutting tool indicate that a cutting tool has	***
	failed? Explain briefly. What properties should a cutting tool material essentially	
	posses and why?	$(10\frac{\%}{3})$
3.	(a) Sketch the various weld joints and welds used in making a joint. Describe the	
	shielded metal arc welding process.	(12)
		4
	Contd P/2	. *

# **IPE 331 (ME)**

#### Contd... Q. No. 3

important features.

(b) With the help of suitable diagrams, describe the following: Submersed arc welding (ii) Resistance seam welding (iii) Resistance projection welding (c) Describe the features of a weld nugget. Explain the similarities and differences  $(10\frac{2}{3})$ between electron beam and laser beam welding. Given typical application for each. 4. (a) Explain why a casting may have a slightly different shape than the pattern used to make the mold. Explain the difference in the importance of drafts in green sand casting versus die mold casting. (12)(b) What are the standard angles of cutting tool? Explain them with suitable diagram. Why do the chip and tool-tip become very hot during machining metal? (12).(c) State the purpose of determining the magnitude and other characteristics of the cutting forces that develop during various kinds of machining work. Why can blind risers be smaller than open risers? (12)(d) Distortion is a serious problem in fusion welding, particularly arc welding. What measures can be taken to reduce the incidence and extent of distortion? Explain briefly.  $(10\frac{1}{3})$ SECTION - B There are FOUR questions in this section. Answer any THREE. 5. (a) What are the different operations that can be performed on a lathe? Explain any five in detail. (12)(b) With the help of neat sketch, describe the method of taper turning by offsetting the tailstock in a lathe machine. (10)(c) Briefly describe the parameters, which influence the performance of a grinding wheel. (18)(d) Write short note on spade drill and gun drill.  $(6\frac{2}{3})$ 6. (a) Discuss the gear cutting process in milling machine. Also discuss the necessity of change gear box in gear cutting.  $(16\frac{1}{3})$ (b) With neat sketches, show the constructional features of a twist drill and label the

Contd ..... P/3

(13)

RIZ.

# <u>IPE 331 (ME)</u>

# **Contd... Q. No. 6**

	(c) Describe the quick return motion mechanism of hydraune snaper with necessary	
	sketches.	(10)
	(d) Differentiate between up-milling and down-milling.	(7)
7.	(a) Discuss commonly observed forging defects.	(12 ½)
	<ul><li>(b) Explain thread rolling process and ring rolling process with suitable diagram.</li><li>(c) How roll force can be reduced in flat rolling? What measures can be taken to avoid</li></ul>	(12)
	the bending of rolls in flat rolling?	(12)
	(d) Describe steel ball production process with neat sketches.	(10)
8.	(a) Derive the expression for optimum cutting speed to minimize unit production cost	
	in turning operation.	$(12\frac{1}{3})$
	(b) Discuss the relative advantages and disadvantages of direct extrusion and indirect	
	extrusion process with necessary sketches.	(10)
	(c) With the help of suitable diagrams, discuss different sheet metal bending	
	operations.	(12)
	(d) How will you manufacture an aluminum beverage can using metal forming	
	processes? Explain each process with neat sketches.	(12)

L-3/T-2/MME Date: 17/07/2016

# BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA L-3/T-2 B. Sc. Engineering Examinations 2014-2015

Sub: MME 345 (Foundry Engineering)

Full Marks: 280

Time: 3 Hours

USE SEPARATE SCRIPTS FOR EACH SECTION

The figures in the margin indicate full marks.

# SECTION - A

There are **FOUR** questions in this section. Answer **Q. No. 1** and any **TWO** from the rest. Question #1 is Compulsory.

- 1. A foundry received an initial order of 10,000 pieces of castings made of A356 aluminium alloy of dimensions shown in Fig. 1 with a possibility of repeat order.
  - (a) It was decided to use greensand moulding system and, for that, to produce a master pattern made of aluminium from which steel working patterns were to be cast and machined. Using necessary allowances, determine the dimensions of the master pattern and its core prints.

    (10+10=20)
  - (b) Using modulus method, design a suitable feeding system for the casting. Indicate clearly the type of placement of feeder in the gating system. (15+5=20)
  - (c) Design a suitable gating system for the casting using a naturally pressurized gating system with a gating ratio of 1.0: 1.2: 1.4. Assume reasonable values for missing data. Indicate all basis and assumptions you used during the design. (15+5=20)
- (a) List the resistances to heat flow from the interior of the casting during solidification.
   Analyse the suitability of using chill and fin to enhance the transfer of heat from the liquid metal.

  (3+15=18)
  - (b) Using neat sketches discuss how columnar, equiaxed and other grain structures are developed during cooling of a pure metal ingot. (10)
  - (c) Why do you prefer fine-grained equiaxed structure in castings and ingots? How an ingot structure consists entirely of fine-grained equiaxed crystals can be developed. (2+10=12)
- (a) Explain the concept of undercooling. Deduce expressions indicating the relations between undercooling and critical radius and critical Gibbs free energy change during formation of a spherical nucleus inside a liquid metal. (5+15=20)
  - (b) Explain the term fluidity of liquid metal in casting. Examine how mode of solidification and solidification time control fluidity of liquid metal. (5+15=20)
- 4. (a) Classify casting alloys based on their solidification behaviour. Which one of them requires feeding most? What happens to a poorly fed casting? (3+2+15=20)
  - (b) What are gating systems? Analyse the functions of a good gating system. (2+10=12)
  - (c) Explain how surface tension of liquid metal controls filling of thin-sectioned mould. (8)

# <u>MME 345/MME</u>

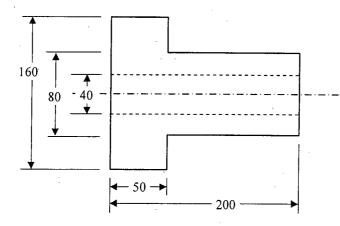
# $\underline{SECTION-B}$

There are FOUR questions in this section. Answer any THREE.

5.	(a) Discuss the casting rules that are followed to obtain good quality castings.	(15)
	(b) Compare sand casting, investment casting and permanent mould casting processes.	(15)
	(c) Different organic and inorganic materials are added to impart certain properties of	
	green sand mould. Write the name of the materials to be added in the green sand to	
	obtain the following properties:	(12)
	(i) increased collapsibility, (ii) reduced expansion problems, (iii) increased dry	
	strength, (iv) increased hot strength (v) improved surface finish.	
	(d) What factors affect the graphitization process in cast iron besides chemical	
	composition?	(4%)
6.	(a) Classify the cast irons and terms of microstructure and chemical composition (C and	
	Si%)	(15)
	(b) What is inoculation? How are inoculants added in gray iron to modify the structure	
	and properties?	(10)
	(c) Mention the factors that control the graphite shape in nodular cast iron.	(6%)
	(d) Write down the chemical reactions occur in a cupola furnace. What are effects of	
	temperature on the change of chemical composition of cast iron during melting?	(15)
7.	(a) Write down the green sand control properties with their resulting problems if they	
	are not properly maintained.	(15)
	(b) What type of die casting method you will choose for low melting point metal	
	casting? Briefly explain the process sequence of the method.	(10)
	(c) List the steps of precision casting method.	(6)
	(d) Discuss the melting and moulding practices of aluminium alloys.	$(15\frac{2}{3})$
8.	(a) Explain how surface films incorporate into the bulk liquid.	(20)
	(b) What is the effect of casting defects on yield strength?	(6%)
	(c) List the defects in casting that are produced due to the absorption of gas. Discuss the	
	preventive measures of the defects due to absorption of gas.	(12)
	(d) Explain the design concepts that are applied to obtain sound casting.	(8)

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Fig. 1 and other Data for Q. #1



Material composition:

A356 (Al-7Si-0.3Mg)

Density:

Moulding system: Pouring temperature: Critical gate velocity: Solidification shrinkage:

Greensand 700 °C 0.25 m/s

2.70 g/cc

Coeff. of discharge:

7.0 vol. % 0.80

(All dimensions are in mm)

# DATA SHEET FOR PATTERN AND CORE PRINT DESIGN

Density data: Steel = 7.8, Aluminium = 2.7, Core sand = 1.6 g/cm<sup>3</sup>

Compressive strength of core sand = 2.0 kg/cm<sup>2</sup>; Factor of safety = 5

Data for contraction allowances:

Contraction rule	Materials used and place of use
+8/1000	Cast iron in general, part of thin cast iron
+9/1000	Cast iron products of high shrinkage, part of thin cast steel
+10/1000	Same as above, and aluminium
+12/1000	Aluminium alloys, bronze, cast steel (thickness 5-7 mm)
+14/1000	High tension brass, cast steel
+16/1000	Cast steel (thickness over 10 mm in general)
+20/1000	Large cast steel
+25/1000	Large cast iron

#### Data for general machining allowances:

Type of metal and alloys	Machining allowance (mm)
Cast irons	
(i) Large size castings (>1000 mm)	10.0
(ii) Medium size castings (<150 mm)	3.0
Cast steels	
(i) Large size castings (>1000 mm)	12.0
(ii) Medium size castings (<150 mm)	4.3
Non-ferrous materials	
(i) Large size castings (>1000 mm)	5.0
(ii) Medium size castings (<150 mm)	1.5

#### Data for approximate taper allowances:

		Sand moulding						
Height of pattern	Shell Moulding	Metal	Wood					
mm		Machine drawn	Manual drawn	Machine drawn				
Up to 20	0° 45'	1° 30'	3°	3°				
20 to 50	0° 30'	1°	1° 30'	1° 30'				
:	:	:	:	:				
100 to 200	0° 20'	0° 30'	0° 45'	0° 45'				

# BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA

L-3/T-2 B. Sc. Engineering Examinations 2014-2015

Sub: IPE 381 (Measurement and Quality Control)

Full Marks: 210

usual meaning.

Time: 3 Hours

The figures in the margin indicate full marks.

USE SEPARATE SCRIPTS FOR EACH SECTION

#### SECTION - A

There are FOUR questions in this Section. Answer any THREE.

1. (a) Why is the trace obtained of the surface profile by any stylus probe instrument distorted?

**(5)** 

(b) For the *constant chord* method, show that  $W = \frac{\pi M}{2} \cos^2 \psi$ . All symbols have their

(10)

(c) Calculate the chordal addendum and chordal thickness of a gear having base circle diameter to pitch circle diameter ratio of 0.906, base pitch of 15.71 mm and a blank diameter of 143.50 mm.

(10)

(d) How can you turn a transparent glass into a smoked glass? Write down the functions of the following components found in a *Tomlinson* surface meter:

(10)

(5)

- (i) Coil spring and leaf spring (ii) Cross roller (iii) Fixed rollers
- 2. (a) Discuss the tradeoff between Type I and Type II errors.

(6+9=15)

(c) *King's Landing*, the royal capital of *Westeros*, is expected to go through an economic recession. All the gold mines it owns are currently empty. Money for *King's Landing* is supplied from two sources during an economic recession period. The sources are the *Iron Bank of Braavos* (Source *A*) and the House *Tyrell of Highgarden* (Source *B*). Data reveals that during the recessioni period, the probability that the supply from Source *A* will be below normal is 0.30; the corresponding probability for Source *B* is 0.15. However, if

(b) Write down the axioms of probability. Explain the theorem of total probability.

Source A is below normal, the probability that Source B will also be below normal during

the same recession period is increased to 0.30.

The probability of money shortage in *King's Landing* will obviously depend on the supplies from the two sources. In particular, if only Source *A* is below normal supply, the probability of money shortage is 0.20, whereas if only Source *B* is below normal the corresponding probability of shortage is 0.25. Obviously, if none of the sources are below normal, there would be no chance of shortage, whereas if both sources are below normal during the recession period, the probability of money shortage in the capital would be 0.80.

What is the probability of money shortage in King's Landing during the expected recession period?

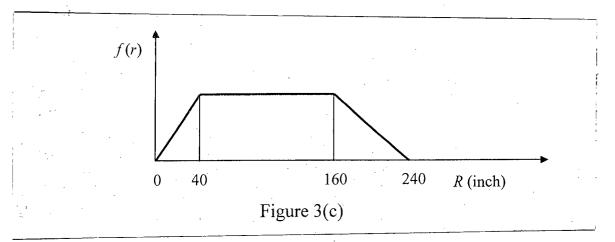
(15)

# **IPE 381**

- 3. (a) If a random variable is uniformly distributed on the interval [A, B], show that its mean,  $\mu = \frac{A+B}{2}$  and variance,  $\sigma^2 = \frac{(B-A)^2}{12}$ . (10)
  - (b) Consider a cantilever beam of span L m with a uniform load of W kg/m. The maximum shear force (S) and the maximum bending moment (M) at the fixed end are WL and  $\frac{WL^2}{2}$ , respectively. Consider L to be a constant and W to be a random variable with a

mean of  $\mu_W$  and a standard deviation of  $\sigma_W$ . (10)

- (i) Calculate Cov(S, M).
- (ii) Show that the correlation coefficient  $\rho_{S, M} = 1$ .
- (iii) Using the results obtained in parts (i) and (ii), are S and M perfectly correlated?
- (c) The PDF of the annual snowfall, R, of Winterfell is shown in Figure 3(c). (5+2+8=15)



- (i) Define the PDF of R properly.
- (ii) What is the mode?
- (iii) Find the coefficient of variation of R.
- 4. (a) List the properties of a binomial process.

(5)

(b) "Temperature in *Kelvin* scale is a ratio level variable and temperature in *Fahrenheit* scale is an interval level variable" – explain.

(5)

(15)

(c) If f(y|x) does not depend on x, then prove that f(y|x) = h(y) and f(x,y) = g(x) h(y) where the symbols have their usual meaning. (10)

(d) The marks obtained in IPE 381 by the students of ME batch 2012 are of interest. Ten scripts are randomly selected and tested, and the following results are obtained:

t of 210)
138
163
159

179

 $\frac{106}{165}$ 

# **IPE 381**

## Contd ... Q. No. 4(d)

- (i) We would like to demonstrate that the mean marks obtained exceed 160. Set up appropriate hyprotheses for investigating this claim.
- (ii) Test these hypotheses using a level of significance of 0.01. What are your conclusions?
- (iii) Construct a 99 percent confidence interval on the mean marks.

# **SECTION – B**

There are FOUR questions in this Section. Answer any THREE.

- (a) Discuss how to measure the effective diameter of a screw thread using three wire method using necessary illustrations. Also derive the equations for effective dia for Whitworth thread and Metric thread in this method.
  (20)
  (b) Shafts of 80 ± 0.5 mm diameter are to be checked by the help of a Go and a Not-Go
  - snap gauge. Design the gauges, sketch it and show its Go size and a Not-Go size dimensions. Assume normal wear allowance and gauge maker's tolerance. (15)
- 6. (a) Discuss the variations in control chart. (5)
  - (b) Discuss ultrasonic inspection technique with necessary figures. (10)
  - (c) A company and its customer agreed to follow a double sampling plan. For a lot of size 2000, the first sample size has to be 30 and the second sample size has to be 60. The acceptable number of defects for the first sample is 3 and for the second sample is 5. If the fraction nonconforming is 0.02, then calculate the total probability of acceptance for that lot.
- 7. (a) Discuss different aspects of quality that customers may value. (20)
  - (b) Following data shows the actual demand of a certain product for 7 consecutive months.

 Month
 1
 2
 3
 4
 5
 6
 7

 Demand
 76
 80
 83
 90
 95
 86
 98

Mind the forecasted demand for month 8 and month 9 using linear regression technique.

- (c) Discuss the differences between precision and accuracy.
- 8. (a) What are the types of uncertainty? Explain with examples. (5)
  - (b) Unoccupied seats on flights cause airlines to lose revenue. A large airline wanted to estimate its average number of unoccupied seats per flight. Based on a random sample of flights, the 95% confidence interval for mean number of unoccupied seats per flight was

Contd ..... P/4

(20)

(10)

**(5)** 

# **IPE 381**

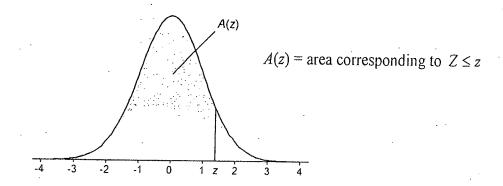
# Contd ... Q. No. 8(b)

given as: (7.5, 9.5). Answer the following questions. Do not perform any calculation for parts (ii) to (v).

- (10)
- (i) What was the mean number of unoccupied seats per flight for the sample of flights?
- (ii) Based on the 95% confidence interval, what would be the decision for testing  $H_0: \mu = 7$  versus  $H_1: \mu \neq 7$  at the 5% significance level?
- (iii) What would be the decision for testing  $H_0$ :  $\mu = 7$  verses  $H_1$ :  $\mu \neq 7$  at the 10% significance level?
- (iv) Based on the 95% confidence interval, what would be the decision for testing  $H_0: \mu = 9$  verses  $H_1: \mu \neq 9$  at the 5% significance level?
- (v) What would be the decision for testing  $H_0$ :  $\mu = 9$  verses  $H_1$ :  $\mu \neq 9$  at the 1% significance level?
- (c) The northbound bus traffic (going to *Dhaka North City Corporation* from *Dhaka South City Corporation*) at *New-market* bus station between 7 and 8 a.m. on a typical workday is studied. Busses are supposed to arrive every 5 minutes. Collected data indicate that buses generally arrive at the station with an average delay of 1 minute and a variance of 2.0 min<sup>2</sup>. Assume that the delay of each bus is statistically independent and log-normally distributed, and if a bus arrives within 30 seconds of the scheduled time it is not considered to be late.
  - (i) What is the probability that a bus will arrive late at this station?
  - (ii) What is the probability that the first bus to arrive on time will be the third bus?
  - (iii) What is the probability that no bus will arrive at the station on time during the 1 hour of peak traffic?
  - (iv) If a bus is late, what is the probability that it will arrive within 1 minute of the scheduled time?

(20)

# **Cumulative Standard Normal Distribution**



z	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09
0.0	0.5000	0.5040	0.5080	0.5120	0.5160	0.5199	0.5239	0.5279	0.5319	0.5359
0.1	0.5398	0.5438	0.5478	0.5517	0.5557	0.5596	0.5636	0.5675	0.5714	0.5753
0.2	0.5793	0.5832	0.5871	0.5910	0.5948	0.5987	0.6026	0.6064	0.6103	0.6141
0.3	0.6179	0.6217	0.6255	0.6293	0.6331	0.6368	0.6406	0.6443	0.6480	0.6517
0.4	0.6554	0.6591	0.6628	0.6664	0.6700	0.6736	0.6772	0.6808	0.6844	0.6879
0.5	0.6915		0.6985	0.7019	0.7054	0.7088	0.7123	0.7157	0.7190	0.7224
0.6	0.7257	0.7291	.0.7324	0.7357	0.7389	0.7422	0.7454	0.7486	0.7517	0.7549
0.7	0.7580	0.7611	0.7642	0.7673	0:7704	0,7734	0.7764	0.7794	0.7823	0.7852
8.0	0.7881	0.7910	0.7939	0.7967	0.7995	0.8023	0.8051	0.8078	0.8106	0.8133
0.9	0.8159	0.8186	0.8212	0.8238	0.8264	0.8289	0.8315	0.8340	0.8365	0.8389
1.0	0.8413	0.8438	0.8461	0.8485	0.8508	0.8531	0.8554	0.8577	0.8599	0.8621
1.1	0.8643	0.8665	0.8686	0.8708	0.8729	0.8749	0.8770	0.8790	0.8810	0.8621
1.2	0.8849	0.8869	0.8888	0.8907	0.8925	0.8944	0.8962	0.8980	0.8997	0.9015
1.3	0.9032	0.9049	0.9066	0.9082	0.9099	0.9115	0.9131	0.0300	0.9162	0.9177
1.4	0.9192	0.9207	0.9222	0.9236	0.9251	0.9265	0.9279	0.9292	0.9306	0.9177
1.5	0.9332	0.9345	0.9357	0.9370	0.9382	0.9394	0.9406	0.9418	0.9429	0.9319
I.G	0.9452	0.9463	0.9474	0.9484	0.9495	0.9505	0.9515	0.9525	0.9429	0.9441
1.7	0.9554	. 0.9564	0.9573	0.9582	0.9591	0.9599	0.9608	0.9525	0.9625	
1.8	0.9641	0.9649	0.9656	0.9664	0.9671	0.9678	0.9686	0.9693	0.9623	0.9633
1.9	0.9713	0.9719	0.9726	0.9732	0.9738	0.9744	0.9750	0.9055	0.9099	0.9706
2.0	0.9772	0.9778	0.9783	0.9788	0.9793	0.9798	0.9803	0.9736	0.9812	0.9767
2.1	0.9821	0.9826	0.9830	0.9834	0.9838	0.9842	0.2846	0.9850	0.9812	0.9817
2.2	0.9861	0.9864	0.9868	0.9871	0.9875	0.9878	0.9881			0.9857
2.3	0.9893	0.9896	0.9898	0.9901	0.9904	0.9906	0.9861	0.9884 0.9911	0.9887	0.9890
2.4	0.9918	0.9920	0.9922	0.9925	0.9927	0.9929	0.9931		0.9913	0.9916
2.5	0.9938	0.9940	0.9941	0.9943	0.9945	0.9946	0.9931	0.9932	0.9934	0.9936
2.6	0.9953	0.9955	0.9956	0.9957	0.9959	0.9960		0.9949	0.9951	0.9952
2.7	0.9965	0.9966	0.9967	0.9968	0.9969	0.9900	0.9961	0.9962	0.9963	0.9964
2.8	0.9974	0.9975	0.9976	0.9977	0.9977	0.9978	0.997]	0.9972	0.9973	0.9974
2.9	0.9981	0.9982	-0.9982	0.9983	0.9977	0.9978	0.9979	0.9979	0.9980	0.9981
.0	0.9987	0.9987	0.9987	0.9988	0.9988	0.9989	0.9985	0.9985	0.9986	0.9986
.1	0.9990	0.9991	0.9991	0.9991	0.9992	0.9999	0.9989	0.9989	0.9990	0.9990
.2	0.9993	0.9993	0.9994	0.9991	0.9992	0.9992	0.9992	0.9992	0.9993	0.9993
.3	0.9995	0.9995	0.9995	0.9994	0.9994		0.9994 -	0.9995	0.9995	0.9995
.4	0.9997	0.9997	0.9997	0.9997	0.9990	.0.9996	0.9996	0.9996	0.9996	0.9997
3.5	0.9998	0.9998	0.9998	0.9998	0.9997	0.9997	0.9997	0.9997	0.9997	0.9998
3.6	0.9998	0.9998	0.9999	0.9998	บ.ชุงชุ	0.9998	0.9998	0.9998	0.9998	0.9998

# Student's t Distribution

			Confidence	e Intervals,	С				
	80%	90%	95%	98%	99%	99.9%			
•		Level of	Significance for One-Tailed Test, $\alpha$						
df	0.10	0.05	0.025	0.01	0.005	0.0005			
•		Level of	Significanc	e for Two-Ta	ailed Test, $\alpha$				
	0.20	0.10	0.05	0.02	0.01	0.001			
1	3.078	6.314	12.706	31.821	63.657	636.619			
2	1.886.	2.920	4.303	6.965	9.925	31.599			
3	1.638	2.353	3.182	4.541	5.841	12.924			
4	1.533	2.132	2.776	3.747	4.604	8.610			
5	1.476	2.015	2.571	3.365	4.032	6.869			
6	1.440	1.943	2.447	3.143	3.707	5.959			
7	1,415	1.895	2.365	2.998	3,499	5.408			
8	1.397	1.860	2.306	2.896	3.355	5.041			
. 9	1.383	1.833	2.262	2.821	3.250	4.781			
10	1.372	1,812	2.228	2.764	3.169	4,587			
11	1.363	1.796	2.201	2.718	3.106	4.437			
12	1.356	1.782	2.179	2.681	3.055	4.318			
13	1.350	1.771	2.160	2,650	3.012	4.221			
14	1.345	1.761	2.145	2.624	2.977	4.140			
15	1.341	1.753	2.131	2.602	2.947	4.073			
16	1.337	1.746	2.120	2.583	2.921	4.015			
17	1.333	1.740	2.110	2.567	2,898	3.965			
18	1.330	1.734	2.101	2.552	2.878	3.922			
19	1 328	1.729	2.093	2.539	2.861	3.883			
20	1.325	1.725	2.086	2.528.	2.845	3.850			

L-3/T-2/ME Date: 23/07/2016

# BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA

L-3/T-2 B. Sc. Engineering Examinations 2014-2015

Sub: ME 343 (Machine Design II)

Full Marks: 210

Time: 3 Hours

USE SEPARATE SCRIPTS FOR EACH SECTION

The figures in the margin indicate full marks.

Assume reasonable values of any missing data.

'Shigley's Mechanical Engineering Design' Text Book will be supplied.

# SECTION - A

There are FOUR questions in this section. Answer any THREE.

(a) A 02 series single row deep groove ball bearing is to be designed for an application
with 3 kN axial load and 7 kN radial load. The outer ring will rotate at 500 rpm. The
design reliability is 96% for a life of 30 khr.

(20)

Find:

- (i) The equivalent radial load on the bearing.
- (ii) Minimum basic load rating  $C_{10}$  required.
- (b) A 02-30 mm bore angular contact ball bearing which was subjected to 200,000 revolutions with a radial load of 18 kN, is to be used under a changed radial load of 30 kN condition. Estimate the expected life in revolution under this new loading condition. Assume other conditions remain unchanged.

(15)

(a) A 32 mm × 32 mm sleeve bearing with 3.2 kN load rotates at 3600 rpm. SAE 10 lubricating oil is used with an average film temperature of 70°C. Estimate the radial clearance necessary to run the bearing in a minimum friction condition.

(20)

(b) Estimate the speed (rpm) at which a spur gear can be run to transmit 4 kW power with a design factor of safety 3 using Lewis's bending stress equation. The gear has 16 teeth with 3 mm module, 40 mm face width and 20° pressure angle. Use gear material yield strength as 250 MPa.

(15)

3. (a) Briefly explain the advantages and drawbacks of journal and rolling contact bearings in consideration of their applications.

(10)

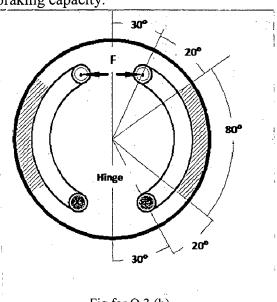
(b) Figure 3(b) shows an internal expanding type drum brake with hinges located as shown. The actuating forces on both shoes are F = 5 kN. The frition lining on the shoes are located centrally leaving a gap of  $20^{\circ}$  on both ends of the shoe. The mean coefficient of friction is 0.28. The inner diameter of drum is 300 mm, face width of the shoes are 50 mm, and radial distance of hinge pin from drum center is 120 mm. Assume the drum is rotating clockwise.

(25)

#### Contd... Q. No. 3(b)

Find:

- (i) Maximum pressure on the brake liner. Which shoe will be subjected to this maximum pressure?
- (ii) Estimate the total braking capacity.



- Fig for Q 3.(b)
- 4. A helical gear set has been selected to transmit input power of 3.5 kW. The pinion has 16 teeth with 20° normal pitch angle and 25° helix angle. The pinion rotates at 1500 rpm meshing with a 50 tooth helical gear. The normal module is 5 mm, face width is 50 mm, the gears have a quality number of 7. The pinion and gear material hardnesses are 240 HB and 200 HB respectively. Transmission is uniform. Assume pinion life of 10<sup>7</sup> cycles and reliability of 90%. Both gears are made with grade 2 through hardened steel.
- (35)
- (i) Calculate the factors of safety for the bending and wear of the pinion only.
- (ii) Based on the factors of safety which mode of failure is most likely to occurs first?

#### SECTION – B

There are FOUR questions in this section. Answer any THREE.

- (a) A single rope of designation 20 mm 6 × 19 IPS, regular lay, is used to lift a load of 1400 kg by a skip from a depth of 300 m. Self-weight of the skip is 900 kg.
   Take: D = 68d, E<sub>r</sub> = 83 GPa, maximum acceleration during lifting the load is 2 m/s². Determine,
- (17)

- (i) static safety factor considering bending effect.
- (ii) the life of rope if the fatigue safety factor considering bending effect is 2.
- (iii) the maximum elongation.
- (b) The smaller pulley (d = 200 mm) of a V-belt drive is directly connected to a 8 kW motor running at 1450 rpm. Multiple B3000 belts are to be selected with  $K_s = 1.4$  and  $n_d = 1.1$ , D = 300 mm. Determine-
- (18)

- (i) Number of belts required.
- (ii) Fatigue safety factor.
- (iii) Initial tension.
- (iv) Belt life in khr.

Take,  $k_b = 65.1 \text{ N.m}$ 

6. An electric motor (H = 2.5 hp, 1450 rpm) is directly coupled to a <u>double</u> threaded worm (material: High-test C.I.). The worm drives a 50 tooth gear (material: sand-cast bronze) that in turn runs a machine.

(35)

Given:  $\phi_n = 25^\circ$ ,  $m_t = \frac{1}{5}$  inch,  $d_w = 2$  inch,  $F_e = 1.5$  inch, load application factor = 1.25, design factor = 1, 1 hp = 33000  $\frac{ft - lb}{min}$ , lateral area of gear case = twice the minimum

lateral area recommended by AGMA. Determine: (i) gear rpm (ii) separating force between gear and worm (iii) efficiency of the drive (iv) safety factors by AGMA equation and also by Buckingham wear load equation (v) temperature rise of sump oil if a cooling fan is on.

7. (a) A pair of straight bevel gears (material: steel, grade 2, BHN = 200) have following data: driver pinion ( $N_p = 50$ ) runs at 400 rpm and transmits 8 kW to the gear ( $N_g = 100$ ), m = 15 mm at large end, b = 80 mm,  $\phi_n = 20^\circ$ , R = 95%,  $n_L$  (pinion) = 8 × 10<sup>3</sup> cycles,  $Q_v = 6$ , temperature = 70°C, both gears have smooth and uniform motion, they have uncrowned teeth and they are not straddle mounted. Find safety factor guarding against surface failure.

(18)

(b) A <u>double</u> stranded ANSI 160 roller chain is selected to transmit a nominal power of 50 kW at 300 rpm with  $K_s = 1.4$  and  $n_d = 1.5$  in a rough environment.

**(17)** 

Given:  $\frac{C}{p} = 25$ ,  $N_1 = 17$ ,  $N_2 = 51$ . Determine (i) speed ratio,  $\frac{\Delta V}{V}$  (ii) fatigue safety factor (iii) bending force on the driving shaft based on the design power (iv) required lubrication type.

8. (a) Design data of a helical compression spring are as follows:

(20)

ends: squared and ground

material: 302 stainless steel (peened),  $\gamma = 82 \times 10^{-6} \frac{N}{mm^3}$ .

wire dia: 6 mm, spring index: 10, free length: 315 mm.

The spring deflects by 77.29 mm under a dead weight (F<sub>m</sub>) of 400 N. Next, a fluctuating load (F<sub>a</sub>) of 300 N is applied to it.

Determine (i) spring constant, number of active turns and solid height (ii) chance of collapse/buckling (iii) fatigue safety factor by Sine's criterion. Use Zimmerli's data. (iv) the spring's response, if frequency of F<sub>a</sub> is 53.92 Hz.

(b) An automobile leaf spring carrier a total vertical load of 8 kN, so that half of this load acts on each tip (eye). The spring has 10 leaves, each leaf has a width of 80 mm and a thickness of 10 mm. Total span of the main leaf is 500 mm. Take, E = 200 GPa.

(15)

- (i) With a free hand sketch show the dimensions of a triangular flat spring that is equivalent to half of the leaf spring.
- (ii) Find energy absorbed by the leaf spring because of the 8 kN load.

1

L-3/T-2/MEDate: 27/07/2016

# BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA

L-3/T-2 B. Sc. Engineering Examinations 2014-2015

Sub: ME 303 (Convection, Boiling, Condensation and Mass Transfer)

Full Marks: 210

Time: 3 Hours

#### USE SEPARATE SCRIPTS FOR EACH SECTION

The figures in the margin indicate full marks.

Assume reasonable values for missing data. All symbols have their usual meaning.

SECTION – A There are **FOUR** questions in this section. Answer any **THREE**. 1. (a) Define Grashof number, Prandtl number and Nusselt number. Using dimensional analysis, show that for natural convection heat transfer over a flat plate, Nu = f(Gr, Pr).(17)(b) Oil flow in a journal bearing can be treated as parallel flow between two large isothermal plates with one plate moving at a constant velocity of 12 m/s and the other stationary. Consider such a flow with a uniform spacing of 0.7 mm between the plates. The temperature of the upper and lower plates are 40°C an 15°C, respectively. By simplifying and solving the continuity, momentum and energy equations, determine (i) the velocity and temperature distributions in the oil, and (ii) the maximum temperature and where it occurs. (18)2. (a) A 1.0-kW heater is constructed of a glass plate with an electrically conducting film which produces a constant heat flux. The plate is 60 by 60 cm and placed in an airstream at 27°C, 1 atm with  $u_{\alpha} = 5$  m/s. Calculate the average temperature difference along the plate and the temperature difference at the trailing edge. (20)(b) Air at 27°C and 1 atm flows over a 20-cm square flat plate at a free-stream speed of 20 m/s. The last half of the plate is heated to a constant temperature of 350 K. Calculate the heat lost by the plate. (15)3. (a) How is the thermal entry length defined for flow in a tube? In what region is the flow in a tube fully developed? **(5)** (b) Draw the temperature profiles of the developing and the fully developed thermal boundary layers inside a circular pipe when (i) the pipe wall is subjected to a constant (10)heat flux and (ii) the pipe wall is maintained at the constant temperature. (c) In a parabolic trough concentrator, solar energy is collected by placing a tube at the focal line of the collector and passing fluid through the tube. The arrangement resulting in a uniform heat flux of 2000 W/m<sup>2</sup> along the axis of the tube of diameter 60 mm.

Calculate (i) the length of the tube required to heat water from 20°C to 80°C, which

flows at the rate of 0.01 kg/s and (ii) the surface temperature at the outlet of the tube.

Contd ..... P/2

(20)

4. (a) A 28-cm-high, 18-cm-long, and 18-cm-wide rectangular container suspended in a room at 24°C is initially filled with cold water at 2°C. The surface temperature of the container is observed to be nearly the same as the water temperature inside. The emissivity of the container surface is 0.8, and the temperature of the surrounding surfaces is about the same as the air temperature. Determine the water temperature in the container after 3 h, and the average rate of heat transfer to the water. Assume the heat transfer coefficient on the top and bottom surfaces to be the same as that on the side surfaces.

**(20)** 

(b) A horizontal pipe 0.30 m in diameter is maintained at a temperature of 250°C in a room where the ambient air is at 15°C. Calculate the heat transfer coefficient and the free convection heat loss per unit meter of length.

(15)

## SECTION - B

There are FOUR questions in this section. Answer any THREE.

5. (a) Write down the mechanism of condensation heat transfer over a vertical tube and discuss.

**(7)** 

(b) What are the differences between film-wise and dropwise condensation? In which case you will expect more heat flux and why?

(8)

(c) Calculate the average heat transfer coefficient for film-wise condensation of pure water-vapor at atmospheric pressure for the following cases:

(20)

: 4

- (i) a vertical plate of 1 meter in length.
- (ii) the outside-surface of a vertical cylinder of 1.5 cm OD and 1 meter in length.
- (iii) the outside surface of a horizontal cylinder 1.5 cm OD and 1 meter length.
- (iv) Discuss your findings that you have obtained in the above cases.

In all cases, assume that the surface temperature is constant at 35°C below the saturation temperature. The following properties of the condensate may be assumed:  $k_e = 0.65 \text{ W/m}^{\circ}\text{C}$ ,  $\rho_e = 998 \text{ kg/m}^{3}$ ,  $h_{fg} = 2400 \text{ kJ/kg}$ ,  $\mu_e = 0.562 \times 10^{-3} \text{ kg/m-sec}$ .

6. (a) Give a sketch of a typical pool boiling curve for a surface in a pool of water at atmospheric pressure. Describe the influence of relevant factors affecting the nucleate boiling heat transfer.

(15)

(b) What are the differences between nucleate and film boiling heat transfer? Explain the importance of radiation on film boiling heat transfer.

(10)

(c) Describe the methods of enhancing flow boiling heat transfer.

(10)

(a) A wet garment is hung on a wall for drying. Write down the one dimensional mass 7. transfer equation with appropriate initial and boundary conditions and discuss. (10)(b) In order to avoid over pressurization as well as maintain a pressure close to one atm, an industrial pipe-line containing ammonia gas is vented to ambient air. Ventag is achieved by tapping the pipe line and inserting 3 mm diameter tube, which extends upto 15 mm into the atmosphere. With the entire system operating at 25°C, calculate (15)the mass rate of contamination of the atmospheric air with ammonia in kg/hr. (i) (ii) the mass rate of air diffused with ammonia in the pipe Assume mass diffusivity of ammonia in air =  $0.29 \times 10^{-4}$  m<sup>2</sup>/sec, molecular weight of ammonia 17 kg/kmol, molecular weight of air 29 kg/kmol and  $R = 8.3 \times 10^{-2}$  m<sup>3</sup> atm/kmol K. (c) Discuss the relation Sh = f(Re, Sc), where the symbols have their usual meanings. (10)(a) A heat exchanger is to be designed to cool 8.7 kg/sec an ethyl alcohol solution 8.  $(c_p = 3800 \text{ J/kg}^{\circ}\text{C})$  from  $80^{\circ}\text{C}$  to  $50^{\circ}\text{C}$  with cooling water  $(c_p = 4200 \text{ J/kg}^{\circ}\text{C})$  entering the tube side at 15°C at a rate of 9.8 kg/sec. The overall heat transfer coefficient based on the outer tube surface is 510 W/m<sup>2</sup> °C. Calculate the heat transfer area for each of the following flow arrangements: (20)parallel flow, shell and tube. (i) counter flow, shell and tube. (ii) one shell pass two tube passes. (iv) cross-flow both fluids unmixed. discuss the results that you have obtained. (b) Describe the importance of  $\varepsilon$ -NTU methods of heat exchanger analysis. **(6)** (c) Write short notes on the following: **(9)** (i) Fouling of heat exchanger. Compact heat exchanger. (ii) Regenerative heat exchanger.

Temp. <i>T</i> , °C	Density ho, kg/m <sup>3</sup>	Specific Heat c <sub>p</sub> , J/kg·K	Thermal Conductivity k, W/m·K	Thermal Diffusivity æ, m²/s	Dynamic Viscosity µ, kg/m·s	Kinematic Viscosity v, m <sup>2</sup> /s	Prandtl Number Pr	Volume Expansion Coeff. $\beta$ , 1/K
				Engine Oil	(unused)			
0	899.0	1797	0.1469	9.097 × 10 <sup>-8</sup>	3.814	$4.242 \times 10^{-3}$	46,636	0.00070
20	888.1	1881	0.1450	$8.680 \times 10^{-8}$	0.8374	$9.429 \times 10^{-4}$	10,863	0.00070
40	876.0	1964	0.1444	$8.391 \times 10^{-8}$	0.2177	$2.485 \times 10^{-4}$	2,962	0.00070
60	863.9	2048	0.1404	$7.934 \times 10^{-8}$	0.07399	$8.565 \times 10^{-6}$	1,080	0.00070
80	852.0	2132	0.1380	$7.599 \times 10^{-8}$	0.03232	$3.794 \times 10^{-5}$	499.3	0.00070
100	840.0	2220	0.1367	$7.330 \times 10^{-8}$	0.01718	$2.046 \times 10^{-5}$	279.1	0.00070
120	828.9	2308	0.1347	$7.042 \times 10^{-8}$	0.01029	$1.241 \times 10^{-5}$	176.3	0.0007.0
140	816.8	2395	0.1330	$6.798 \times 10^{-8}$	0,006558	$8.029 \times 10^{-6}$	118.1	0.00070
150	810.3	2441	0.1327	$6.708 \times 10^{-8}$	0.005344	6.595 × 10 <sup>-6</sup>	98.31	0.00070

	Sui		orced Convection Flow over Flat I lated at Film temperature	Plates				
Tumo	Restrictions	Fluid Flow	Heat Transfer					
Type	Restrictions	1101011011	Isothermal $(T_w = constant)$	Isoflux $(q_w = constant)$				
	Laminar:	$C_{f,x} = 0.664 Re_x^{-1/2}$	$Nu_{x} = 0.332 Re_{x}^{1/2} Pr^{1/3}$	$Nu_x = 0.453 Re_x^{1/2} Pr^{1/3}$				
Local	$Re_x < 5 \times 10^5$ 0.6 < Pr < 50	<i>y</i> ,x	x x					
	Laminar:	1/2	$Nu_L = 0.664 Re_L^{1/2} Pr^{1/3}$	$Nu_L = 0.680 Re_L^{1/2} Pr^{1/3}$				
Average	$Re_L < 5 \times 10^5$	$C_f = 1.328 Re_L^{-1/2}$	$Na_L = 0.004 Re_L$ 11	$\int \mathbf{T} \mathbf{u}_L = 0.000 \mathbf{T} \mathbf{u}_L \mathbf{T}$				
	0.6 < Pr < 50							
	Turbulent:	$C_{f,x} = 0.059 Re_x^{-1/5}$	$Nu_r = 0.0296 Re_r^{4/5} Pr^{1/3}$	$Nu_x = 0.0308 Re_x^{4/5} Pr^{1/3}$				
Local	$5 \times 10^5 \le \text{Re}_{x} \le 10^7$	<i>y</i> , <i>x</i>						
	$0.6 \le \Pr \le 60$	1/5		4/5p 1/3				
	Turbulent: $5 \times 10^5 \le \text{Re}_L \le 10^7$	$C_f = 0.074 Re_L^{-1/5}$	$Nu_L = 0.037 Re_L^{4/5} Pr^{1/3}$	$Nu_L = 0.037 Re_L^{4/5} Pr^{1/3}$				
Average	$0.6 \le \Pr \le 60$		_					
<del></del>	0.0 211 200							
	ξ = unheat	ed starting length	,	p+1				
Average	Laminar: R	$e_L < 5 \times 10^5$ ; p = 2	$\operatorname{Nu}_{L} = \operatorname{Nu}_{L(\operatorname{for}\xi=0)} \left( \frac{L}{L-\xi} \right) \left[ 1 - \left( \frac{\xi}{L} \right)^{\frac{p+1}{p+2}} \right]^{\frac{p}{p+1}}$					
Average	Turbulent: 5 ×	$10^5 \le \text{Re}_{\text{L}} \le 10^7$ ; p = 8						
			_	~				

Table A-5 | Properties of air at atmospheric pressure.†

Table A-5   Properties of air at atmospheric pressure.		1					ļ						<u> </u>		
The visues of $\mu_{c}$ $k_{c}$ $p_{c}$ and may be used over a farly wide range of pressures    The visual may be used over a farly wide range of pressures	Table /	-5   Proper	ties of air at au	mospheric pi	ressure.†				Table	A-9 Propert	lies of water (s	aturated li	quid).†		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		and may be used over a fairly wide range of pressures									(4802cm)	r <sup>3</sup> Δ <i>T</i>	The second of th	्राक्षिक रहा है। प्रतिस्कृतिक से स	
100						k W/m⋅°C	α x 10 <sup>4</sup> in <sup>2</sup> /s	Pr ·				0	u.		
100	100	3.6010	1.0266	0.6924	1.923				j.			***	100 A 100 A	100 Yes	7.5° <b>n</b> = 3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	150	2.3675	1.0099	1.0283	4.343	0.013735	0.05745		, °F	, °C	kJ/kg °C	kg/m	Kg/m ⋅s	wm C	1166
1.4128			1.0061	1.3289	7.490	0.01809									
1,1774   1,0057   1,8462   15,69   0,02624   0,22160   0,708   40   4.44   4,208   999.8   1,55   0.575   11,35     300   0,9980   1,0090   2,075   20,76   0,03003   0,2983   0,697   50   10   4,195   999.2   1,31   0,585   9,40     400   0,8826   1,0140   2,286   25,90   0,03365   0,3760   0,689   60   15,56   4,186   998.6   1,12   0,595   7,88     450   0,7833   1,0207   2,484   31,71   0,03797   0,4222   0,683   70   21,11   4,179   997.4   9,88,10 <sup>-1</sup>   0,604   6,78     500   0,7048   1,0295   2,671   37,90   0,04038   0,5564   0,680   0,6532   0,680   0,6632   1,0392   2,848   44,34   0,04360   0,6532   0,680   80   26,67   4,179   995.8   8,6   0,614   5,85     550   0,6423   1,0392   2,848   44,34   0,04360   0,6532   0,680   90   32,22   4,174   994.9   7,65   0,623   5,12     6600   0,5879   1,0551   3,018   51,34   0,04569   0,7512   0,680   90   32,22   4,174   994.9   7,65   0,623   5,12     6600   0,5879   1,0551   3,018   51,34   0,04559   0,8778   0,682   100   37,78   4,174   994.9   6,82   0,630   4,53     700   0,5030   1,0752   3,332   66,25   0,05330   0,9672   0,684   10   43,33   4,174   998.6   5,62   0,664   3,64     750   0,4709   1,0856   3,481   73,91   0,05509   1,0774   0,686   120   48,89   4,174   988.8   5,62   0,644   3,64     800   0,4405   1,0978   3,625   82,29   0,05779   1,1951   0,689   130   54,44   4,179   985.7   5,13   0,649   3,30     850   0,4149   1,1095   3,765   90,75   0,06028   1,3007   0,692   1,400   4,400   1,400   4,400			1.0053	1.5990							1	i			
1.00		1.1774	- 1.0057	1.8462	15.69				40	4,44	4.208		1		
100	350	0.9980	1.0090	2.075	20.76				50	10	4.195	999.2			
450         0.7833         1.0207         2.484         31.71         0.03707         0.4222         0.680         80         26.67         4.179         997.4         9.8×10 <sup>3</sup> 0.0604         5.85           500         0.7048         1.0295         2.671         37.90         0.04038         0.5564         0.680         80         26.67         4.179         995.8         8.6         0.614         5.85           550         0.623         1.0392         2.848         44.34         0.04369         0.6532         0.680         90         32.22         4.174         994.9         7.65         0.630         5.12           660         0.5879         1.0551         3.018         51.34         0.04953         0.8578         0.682         100         37.78         4.174         999.0         6.82         0.630         4.53           700         0.5030         1.0752         3.332         66.25         0.05230         0.9672         0.684         110         43.33         4.174         990.6         6.16         0.637         4.04           750         0.4709         1.0856         3.481         73.91         0.05509         1.0774         0.688         130         <		0.8826	1.0140	2.286	25.90				60	15.56	4.186	998.6	1.12	0.595	
500         0.7048         1.0295         2.671         37.90         0.04038         0.5564         0.680         80         26.67         4.179         995.8         8.6         0.614         5.85           550         0.6423         1.0392         2.848         44.34         0.04639         0.6532         0.680         80         32.22         4.174         994.9         7.65         0.630         5.12           650         0.5879         1.0551         3.018         51.34         0.04659         0.7512         0.680         100         37.78         4.174         999.0         6.82         0.630         4.53           700         0.5030         1.0752         3.332         66.25         0.05320         0.9672         0.684         110         43.33         4.174         990.0         6.16         0.637         4.04           750         0.4709         1.0856         3.481         73.91         0.05509         1.0774         0.686         120         48.89         4.174         988.8         5.62         0.644         3.64           800         0.4169         1.1095         3.625         82.29         0.05779         1.1951         0.689         130         54.		0.7833	1.0207	2.484	31.71	0.03707		}	70	21.11	4.179	997.4	9.8×10 <sup>4</sup>	0,604	6.78
550         0.6423         1.0392         2.848         44.34         0.04360         0.6532         0.680         90         32.22         4.174         994.9         7.65         0.623         5.12           600         0.5879         1.0551         3.018         51.34         0.04659         0.7512         0.680         90         32.22         4.174         993.0         6.82         0.630         4.53           700         0.5330         1.06525         3.177         58.51         0.04953         0.8678         0.682         100         37.78         4.174         990.6         6.16         0.637         4.04           700         0.5030         1.0752         3.332         66.25         0.05230         0.9672         0.684         110         43.33         4.174         990.6         6.16         0.637         4.04           800         0.4091         1.08856         3.481         73.91         0.05250         1.0774         0.686         120         48.89         4.174         988.8         5.62         0.644         3.64           800         0.4192         1.1095         3.765         90.75         0.06028         1.3007         0.692         140		r I	1.0295	2.671	37.90	0.04038	0.5564	ſ		Į.	1	905.8	8.6	0.614	5,85
600 0.5879 1.0551 3.018 51.34 0.04659 0.7512 0.680 90 37.78 4.174 993.0 6.82 0.630 4.53 6.50 0.5430 1.0635 3.177 58.51 0.04953 0.8578 0.682 10.0 37.78 4.174 990.6 6.16 0.637 4.04 0.050 0.5030 1.0752 3.332 66.25 0.05230 0.9672 0.684 110 43.33 4.174 990.6 6.16 0.637 4.04 0.04953 0.8578 0.682 1.051 0.05230 0.9672 0.684 110 43.33 4.174 990.6 6.16 0.637 4.04 0.04953 0.04953 0.0579 0.0579 0.04709 1.0856 3.481 73.91 0.05509 1.0774 0.686 120 48.89 4.174 988.8 5.62 0.644 3.64 0.04953 0.04953 0.0579 0.05779 1.1951 0.689 130 54.44 4.179 985.7 5.13 0.649 3.30 0.0579 0.3925 1.1212 3.899 99.3 0.06279 1.4271 0.696 150 65.55 4.183 980.3 4.71 0.654 3.01 0.050 0.3925 1.1212 3.899 99.3 0.06279 1.4271 0.696 150 65.55 4.183 980.3 4.3 0.659 2.73 0.050 0.3716 1.1321 4.023 108.2 0.06525 1.5510 0.699 160 71.11 4.186 977.3 4.01 0.665 2.53 1000 0.3524 1.1417 4.152 117.8 0.06752 1.6779 0.702 170 76.67 4.191 973.7 3.72 0.668 2.33 1000 0.3204 1.160 4.44 138.6 0.0732 1.969 0.704 180 82.22 4.195 970.2 3.47 0.673 2.16 1100 0.3204 1.160 4.44 138.6 0.0732 1.969 0.704 180 82.22 4.195 970.2 3.47 0.673 2.16 1100 0.2515 1.214 5.17 205.5 0.0891 2.920 0.705 220 93.33 4.204 963.2 3.06 0.678 1.90 1.000 0.2515 1.214 5.17 205.5 0.0891 2.920 0.705 220 93.33 4.204 963.2 3.06 0.678 1.90 1.000 0.2515 1.214 5.17 205.5 0.0891 2.920 0.705 220 104.4 4.216 955.1 2.67 0.684 1.66 0.684 1.66 0.051 1.000 0.1858 1.309 6.29 338.5 0.117 4.811 0.704 4.819 0.704 4.209 918.0 1.86 0.684 1.17 9000 0.1858 1.309 6.29 338.5 0.117 4.811 0.704 4.819 0.704 4.209 918.0 1.86 0.684 1.17 9000 0.1858 1.309 6.29 338.5 0.117 4.811 0.704 4.819 0.704 4.44 1.38 6.50 3.69 0.124 5.260 0.702 2.00 1.48.9 4.296 918.0 1.86 0.684 1.17 9000 0.1858 1.309 6.29 338.5 0.117 4.811 0.704 4.004 0.044 4.467 8.594 1.59 0.685 1.24 0.065 1.00 0.1662 1.372 6.72 3.99.6 0.131 5.715 0.700 400 0.204 4.467 8.594 1.57 0.6675 1.00 0.666 0.85 0.100 0.1682 1.372 6.72 3.99.6 0.131 5.715 0.700 400 0.204 4.467 8.594 1.59 0.665 1.00 0.666 0.85 0.100 0.1658 1.574 7.35 504.0 0.161 7.020 0.718 550 0.877 5.50 4.77 3.55 504.0 0.				2.848	44.34	0.04360	0.6532		,, ,		1	1	1	i	5.12
650         0.5430         1.0635         3.177         58.51         0.04953         0.6878         0.682         100         37.78         4.174         990.6         6.16         0.637         4.04           700         0.5030         1.0752         3.332         66.25         0.05230         0.9672         0.684         110         43.333         4.174         988.8         5.62         0.644         3.64           750         0.4709         1.0856         3.481         73.91         0.05509         1.0774         0.686         120         48.89         4.174         988.8         5.62         0.644         3.64           800         0.4405         1.0978         3.625         82.29         0.05779         1.1951         0.689         130         54.44         4.179         983.3         4.71         0.654         3.01           900         0.3925         1.1212         3.899         99.3         0.06729         1.4271         0.696         150         65.55         4.183         980.3         4.3         0.669         2.73           950         0.3716         1.1321         4.023         108.2         0.06525         1.5510         0.699         160         7				3.018	51.34	0.04659	0.7512	0.680			ļ			i	1
700         0.5030         1.0752         3.332         66.25         0.05230         0.9672         0.684         110         43.33         4.174         990.0         0.16         0.037           750         0.4709         1.0856         3.481         73.91         0.05509         1.0774         0.686         120         48.89         4.174         985.8         5.62         0.649         3.30           800         0.4405         1.0978         3.625         82.29         0.05779         1.1951         0.689         130         54.44         4.179         985.7         5.13         0.649         3.30           900         0.3925         1.1212         3.899         99.3         0.06279         1.4271         0.696         150         65.55         4.183         980.3         4.3         0.659         2.73           950         0.3716         1.1321         4.023         108.2         0.06525         1.5710         0.699         160         71.11         4.186         977.3         4.01         0.668         2.33           1100         0.3204         1.160         4.44         138.6         0.0732         1.969         0.704         180         82.22         4.19				3,177	58.51	0.04953	0.8578	0.682			1	1		1	1
750 0.4709 1.0856 3.481 73.91 0.05509 1.0774 0.686 120 48.89 4.174 988.8 5.02 0.04408 800 0.4405 1.0978 3.625 82.29 0.05779 1.1951 0.689 130 54.44 4.179 985.7 5.13 0.649 3.30 8350 0.4149 1.1095 3.765 90.75 0.06028 1.3977 0.696 150 65.55 4.183 980.3 4.71 0.654 3.01 900 0.3925 1.1212 3.899 99.3 0.06279 1.4271 0.696 150 65.55 4.183 980.3 4.3 0.659 2.73 950 0.3716 1.1321 4.023 108.2 0.06525 1.5510 0.699 160 71.11 4.186 977.3 4.01 0.665 2.53 1000 0.3524 1.1417 4.152 117.8 0.06752 1.6779 0.702 170 76.67 4.191 973.7 3.72 0.668 2.33 1100 0.3204 1.160 4.44 138.6 0.0732 1.969 0.704 180 82.22 4.195 970.2 3.47 0.673 2.16 1200 0.2947 1.179 4.99 159.1 0.0782 2.251 0.707 190 87.78 4.199 966.7 3.27 0.6675 2.03 1300 0.2707 1.197 4.93 182.1 0.0837 2.583 0.705 200 93.33 4.204 963.2 3.06 0.678 1.90 1300 0.2515 1.214 5.17 205.5 0.0891 2.920 0.705 200 93.33 4.204 963.2 3.06 0.678 1.90 1500 0.2255 1.230 5.40 229.1 0.0946 3.262 0.705 240 115.6 4.229 946.7 2.44 0.685 1.51 1500 0.2205 1.284 5.63 254.5 0.100 3.609 0.705 240 115.6 4.229 946.7 2.44 0.685 1.51 1500 0.2082 1.267 5.85 280.5 0.105 3.977 0.705 260 126.7 4.250 937.2 2.19 0.685 1.36 1500 0.1702 1.287 6.07 308.1 0.111 4.379 0.704 280 137.8 4.271 928.1 1.98 0.685 1.24 1800 0.1970 1.287 6.07 308.1 0.111 4.379 0.704 280 137.8 4.271 928.1 1.98 0.685 1.24 1800 0.1970 1.287 6.07 308.1 0.111 4.379 0.704 280 137.8 4.271 928.1 1.98 0.685 1.24 1800 0.1970 1.287 6.07 308.1 0.111 4.379 0.704 400 204.4 4.466 918.0 1.57 0.667 1.02 2000 0.1682 1.332 6.72 399.6 0.134 5.715 0.700 400 204.4 4.467 859.4 1.36 0.666 0.666 0.85 2400 0.1488 1.574 7.35 504.0 0.169 6.500 0.18 500 0.718 550 287.7 5.024 733.5 9.51 × 10 -5 2400 0.1488 1.574 7.35 504.0 0.169 7.020 0.718 550 287.7 5.024 733.5 9.51 × 10 -5 2400 0.1488 1.574 7.35 504.0 0.169 7.020 0.718 550 287.7 5.024 733.5 9.51 × 10 -5 2400 0.1488 1.574 7.35 504.0 0.169 7.020 0.718 550 287.7 5.024 733.5 9.51 × 10 -5 2400 0.1488 1.574 7.35 504.0 0.169 7.020 0.718 550 287.7 5.024 733.5 9.51 × 10 -5 2400 0.1488 1.574 7.35 504.0 0.169 7.020 0.718 550 287.7 5.024 7					66.25	0.05230	0.9672	0.684			Į.	1	1		
800 0.4405 1.0978 3.625 82.29 0.05779 1.1951 0.689 130 54.44 4.179 985.7 5.13 0.649 3.30 5.04 1419 1.1095 3.765 90.75 0.06028 1.3097 0.692 140 60 4.179 983.3 4.71 0.654 3.01 900 0.3925 1.1212 3.899 99.3 0.06279 1.4271 0.696 150 65.55 4.183 980.3 4.3 0.659 2.73 950 0.3716 1.1321 4.023 108.2 0.06525 1.5510 0.699 160 71.11 4.186 977.3 4.01 0.665 2.53 1000 0.3524 1.1417 4.152 117.8 0.06752 1.6779 0.702 170 76.67 4.191 973.7 3.72 0.668 2.33 1100 0.3204 1.160 4.44 138.6 0.0732 1.969 0.704 180 82.22 4.195 970.2 3.47 0.673 2.116 1200 0.2947 1.179 4.09 159.1 0.0782 2.251 0.707 190 87.78 4.199 966.7 3.27 0.675 2.03 1300 0.2707 1.197 4.93 182.1 0.0837 2.583 0.705 200 93.33 4.204 963.2 3.06 0.678 1.90 1400 0.2515 1.214 5.17 205.5 0.0891 2.920 0.705 200 93.33 4.204 963.2 3.06 0.678 1.90 1400 0.2515 1.214 5.17 205.5 0.0891 2.920 0.705 240 115.6 4.229 946.7 2.44 0.665 1.51 1.00 0.2211 1.248 5.63 254.5 0.100 3.609 0.705 240 115.6 4.229 946.7 2.44 0.665 1.51 1600 0.2211 1.248 5.63 254.5 0.100 3.609 0.705 240 115.6 4.229 940.7 2.44 0.665 1.51 1600 0.2211 1.248 5.63 254.5 0.100 3.609 0.705 240 115.6 4.229 940.7 2.44 0.665 1.51 1600 0.1858 1.309 6.29 338.5 0.117 4.811 0.704 300 148.9 4.296 918.0 1.86 0.684 1.17 1.190 0.1858 1.309 6.29 338.5 0.117 4.811 0.704 300 148.9 4.296 918.0 1.86 0.684 1.17 0.0677 1.02 0.1682 1.372 6.72 399.6 0.131 5.715 0.700 400 204.4 4.467 859.4 1.36 0.685 1.24 0.685 1.24 0.158 1.372 6.72 399.6 0.131 5.715 0.700 400 204.4 4.467 859.4 1.36 0.666 0.85 2.200 0.1682 1.372 6.72 399.6 0.131 5.715 0.700 400 204.4 4.467 859.4 1.36 0.666 0.85 2.200 0.1602 1.419 6.93 432.6 0.139 6.120 0.707 500 260 4.731 785.2 1.07 0.616 0.83 2400 0.1488 1.574 7.35 504.0 0.149 6.540 0.710 500 260 4.731 785.2 1.07 0.616 0.83 2400 0.1488 1.574 7.35 504.0 0.166 7.020 0.718 550 287.7 5.024 735.5 9.51 × 10-5 0.0616 0.83 2400 0.1488 1.574 7.35 504.0 0.166 7.020 0.718 550 287.7 5.024 735.5 9.51 × 10-5 0.0616 0.83 2400 0.1488 1.574 7.35 504.0 0.166 7.020 0.718 550 287.7 5.024 735.5 9.51 × 10-5 0.0616 0.83 2400 0.1488 1.574 7.35 504.0 0.166					73.91	0.05509	1.0774	0.686		1	į.	1	,	1	!
850         0.4149         1.1095         3.765         90.75         0.06028         1.3097         0.692         140         60         4.179         983.3         4.71         0.654         3.01           900         0.3925         1.1212         3.899         99.3         0.06279         1.4271         0.696         150         65.55         4.183         980.3         4.3         0.665         2.73           950         0.3716         1.1321         4.023         108.2         0.06525         1.5510         0.699         160         71.11         4.186         977.3         4.01         0.665         2.53           1100         0.3224         1.1417         4.152         117.8         0.06752         1.6779         0.702         170         76.67         4.191         973.7         3.72         0.668         2.33           1100         0.3204         1.160         4.44         138.6         0.0732         1.969         0.704         180         82.22         4.195         970.2         3.47         0.673         2.16           1200         0.2947         1.179         4.09         159.1         0.0837         2.583         0.705         200         93.33		1			82.29	0.05779	1.1951	0.689	130	54.44	4.179	1	1		1
900 0.3925 1.1212 3.899 99.3 0.06279 1.4271 0.696 150 65.55 4.183 980.3 4.3 0.659 2.73 950 0.3716 1.1321 4.023 108.2 0.06525 1.5510 0.699 160 71.11 4.186 977.3 4.01 0.665 2.53 1000 0.3524 1.1417 4.152 117.8 0.06752 1.6779 0.702 170 76.67 4.191 973.7 3.72 0.668 2.33 1100 0.3204 1.160 4.44 138.6 0.0732 1.969 0.704 180 82.22 4.195 970.2 3.47 0.673 2.16 1200 0.2947 1.179 4.69 159.1 0.0782 2.251 0.707 190 87.78 4.199 966.7 3.27 0.675 2.03 1300 0.2707 1.197 4.93 182.1 0.0837 2.583 0.705 190 87.78 4.199 966.7 3.27 0.675 2.03 1400 0.2515 1.214 5.17 205.5 0.0891 2.920 0.705 200 93.33 4.204 963.2 3.06 0.678 1.90 1400 0.2515 1.214 5.17 205.5 0.0891 2.920 0.705 220 104.4 4.216 955.1 2.67 0.684 1.66 1500 0.2355 1.230 5.40 229.1 0.0946 3.262 0.705 240 115.6 4.229 946.7 2.44 0.685 1.51 1700 0.2082 1.267 5.85 280.5 0.105 3.977 0.705 260 126.7 4.250 937.2 2.19 0.685 1.36 1700 0.2082 1.267 5.85 280.5 0.105 3.977 0.705 260 126.7 4.250 937.2 2.19 0.685 1.24 1.90 0.1970 1.287 6.07 308.1 0.111 4.379 0.704 280 137.8 4.271 928.1 1.98 0.685 1.24 1.99 0.1858 1.309 6.29 338.5 0.117 4.811 0.704 300 148.9 4.296 918.0 1.866 0.684 1.17 0.697 1.02 0.1682 1.372 6.72 399.6 0.131 5.715 0.700 400 204.4 4.467 859.4 1.36 0.665 1.00 0.1682 1.372 6.72 399.6 0.131 5.715 0.700 400 204.4 4.467 859.4 1.36 0.665 1.00 0.1538 1.482 7.14 464.0 0.149 6.540 0.710 500 260 4.731 785.2 1.07 0.616 0.83 2400 0.1458 1.574 7.35 504.0 0.161 7.020 0.718 550 287.7 5.024 735.5 9.51 × 10 - 5					90.75	0.06028	1.3097	0.692	140	60	4.179	983.3	4.71		l
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-				99.3	0.06279	1.4271	0.696	150	65.55	4.183	980.3	4.3	0.659	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					108.2	0.06525	1.5510	0.699	160	71.11	4.186	977.3	4.01	0.665	2.53
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						0.06752	1.6779	0.702			1	973.7	3.72	0.668	2.33
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					138.6	0.0732	1.969	0.704		1	1			0.673	2.16
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					159.1	0.0782	2.251	0.707						0.675	2.03
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				!	182.1	0.0837	2,583	0.705			1	1		Į.	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					205.5	0.0891									
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		•			229.1	0.0946	3.262				1	1		1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			t :	1	254.5	0.100	3.609				1				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				5.85	280.5 ′	0.105	3.977	0.705			1				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				6.07	308.1	0.111								i .	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		1	1		338.5	0.117	4.811	0.704			1			1	
2100 0.1682 1.372 6.72 399.6 0.131 5.715 0.700 400 204.4 4.467 859.4 1.30 0.063 1.00 2200 0.1602 1.419 6.93 432.6 0.139 6.120 0.707 450 232.2 4.585 825.7 1.20 0.646 0.85 2300 0.1538 1.482 7.14 464.0 0.149 6.540 0.710 500 260 4.731 785.2 1.07 0.616 0.83 2400 0.1458 1.574 7.35 504.0 0.161 7.020 0.718 550 287.7 5.024 735.5 9.51×10 <sup>-5</sup>				<b>}</b>	369.0	0.124	5.260				1	1			
2200 0.1602 1.419 6.93 432.6 0.139 6.120 0.707 450 232.2 4.585 825.7 1.20 0.646 0.63 2300 0.1538 1.482 7.14 464.0 0.149 6.540 0.710 500 260 4.731 785.2 1.07 0.616 0.83 2400 0.1458 1.574 7.35 504.0 0.161 7.020 0.718 550 287.7 5.024 735.5 9.51×10 <sup>-5</sup>							5.715	0.700				1			
2300 0.1538 1.482 7.14 464.0 0.149 6.540 0.710 500 260 4.731 785.2 1.07 0.616 0.83 2400 0.1458 1.574 7.35 504.0 0.161 7.020 0.718 550 287.7 5.024 735.5 9.51×10 <sup>-5</sup>							6.120	0.707							
2400 0.1458 1.574 7.35 504.0 0.161 7.020 0.718 550 287.7 5.024 735.5 9.51×10 <sup>-3</sup>							6.540	0.710		l .	1	4		0.616	0,8,5
2400 0.143.0 1.57 5.703 678.7 8.68		3					7.020	0.718	550	287.7	1			İ	
	2500	0.1394	1.688	7.57	543.5	0.175	7.441	0.730	600	315.6	5.703	678.7	8.68		

Geometry	Correlation(s)	Restrictions	Evaluation of Fluid Properties	Thermal condition
Vertical Plate	McAdams: $Nu_L = 0.59 Ra_L^{1/4}$	$10^4 < Ra_L < 10^9$		
	McAdams: Nu, = 0.10Ra <sup>1/3</sup>	$10^9 < Ra_L < 10^{13}$		Isothermal
	Churchill and Chu: Nu <sub>L</sub> = 0.68 + $\frac{0.670 Ra_L^{1/4}}{\left[1 + (0.492 / Pr)^{9/16}\right]^{4/9}}$	$10^{-1} < Ra_L < 10^9$	$T_f = (T_s + T_{\varpi})/2$	
	Churchill and Chu: Nu <sub>L</sub> = $\left\{0.825 + \frac{0.387 Ra_L^{1/6}}{\left[1 + (0.492 / Pr)^{9/16}\right]^{8/27}}\right\}^2$	$10^{-1} < Ra_L < 10^{12}$		
	27 0 (0(0 * P.)) <sup>1/5</sup>	$10^5 < Gr_s^* Pr < 10^{11}$		Isoflux
	$Nu_x = 0.60 \left( Gr_x^* Pr \right)^{1/5}$ $Nu_L = 1.25 \left[ Nu_x \right]_{x=L}$	$Gr_s^* = \frac{g\beta q_w x^4}{kv^2}$	$T_f = (T_s + T_{\infty})/2$ , $T_s$ is average surface	
	$Nu_{x} = 0.17 (Gr_{3} Pr)^{1/4}$	$2 \times 10^{13} < Gr_r^* Pr < 10^{16}$	temperature	
	$Nu_L = 1.136 \left[ Nu_x \right]_{x=L}$	200 700,77 700		
Horizontal Cylinder	$Nu_D = 0.53 (Gr_D Pr)^{1/4}$	$P_{\rm r} > 0.5,$ $10^3 < Gr_D < 10^9$		Isothermal
	$Nu_D = 0.53 (Gr_D Pr^2)^{1/4}$	Liquid metals, $10^3 < Gr_D < 10^9$		
	Churchill and Chu: $Nu_D = 0.36 + \frac{0.518 Ra_D^{1/4}}{\left[1 + (0.559 / Pr)^{9/16}\right]^{4/9}}$	$10^{-6} < Ra_D < 10^9$	$T_f = (T_s + T_{\infty})/2$ , for gases $\beta = 1/T_f$	
	Churchill and Chu: Nu <sub>D</sub> = $\left\{0.60 + \frac{0.387 \ Ra_D^{1/6}}{\left[1 + (0.559 / Pr)^{9/16}\right]^{8/27}}\right\}^2$	$10^{-5} < Ra_D < 10^{12}$		

TABLE 8.4	Summary of	convection	correla	tions for I	now in a	circular	tune
	Oummary v.					1145	

Correlation		Conditions
$f = 64/Re_D$	(8.19)	Laminar, fully developed
$Nu_D = 4.36$	(8.53)	Laminar, fully developed, uniform $q_s''$
$Nu_D = 3.66$	(8.55)	Laminar, fully developed, uniform $T_s$
$\overline{Nu}_D = 3.66 + \frac{0.0668  Gz_D}{1 + 0.04  Gz_D^{2/3}}$	(8.57)	Laminar, thermal entry (or combined entry with $Pr \ge 5$ ), uniform $T_s$ , $Gz_D = (D/x) Re_D Pr$
$\overline{Nu_D} = \frac{\frac{3.66}{\tanh[2.264 \ Gz_D^{-1/3} + 1.7 \ Gz_D^{-2/3}]} + 0.0499 \ Gz_D \tanh(Gz_D^{-1})}{\tanh(2.432 \ Pr^{1/6} \ Gz_D^{-1/6})}$	(8.58)	Laminar, combined entry, $Pr \ge 0.1$ , uniform $T_s$ , $Gz_D = (D/x) Re_D Pr$
$tanh(2.432 PT^{**}G_{tb}^{**})$		
$\frac{1}{\sqrt{f}} = -2.0 \log \left[ \frac{elD}{3.7} + \frac{2.51}{Re_D \sqrt{f}} \right]$	(8.20)°	Turbulent, fully developed
$f = (0.790 \ln Re_D - 1.64)^{-2}$	(8.21) <sup>c</sup>	Turbulent, fully developed, smooth walls, $3000 \lesssim Re_D \lesssim 5 \times 10^6$
$Nu_D = 0.023  Re_D^{4/5}  Pr^{\alpha}$	(8.60) <sup>d</sup>	Turbulent, fully developed, $0.6 \lesssim Pr \lesssim 160$ , $Re_D \gtrsim 10,000$ , $(L/D) \gtrsim 10$ , $n = 0.4$ for $T_s > T_m$ and $n = 0.3$ for $T_s < T_m$
$Nu_D = 0.027 Re_D^{4/5} Pr^{1/3} \left(\frac{\mu}{\mu_s}\right)^{0.14}$	$(8.61)^d$	Turbulent, fully developed, $0.7 \lesssim Pr \lesssim 16,700$ , $Re_D \gtrsim 10,000$ , $L/D \gtrsim 10$
$Nu_D = \frac{(f/8)(Re_D - 1000) Pr}{1 + 12.7(f/8)^{1/2}(Pr^{2/3} - 1)}$	$(8.62)^d$	Turbulent, fully developed, $0.5 \lesssim Pr \lesssim 2000$ , $3000 \lesssim Re_D \lesssim 5 \times 10^6$ , $(L/D) \gtrsim 10$

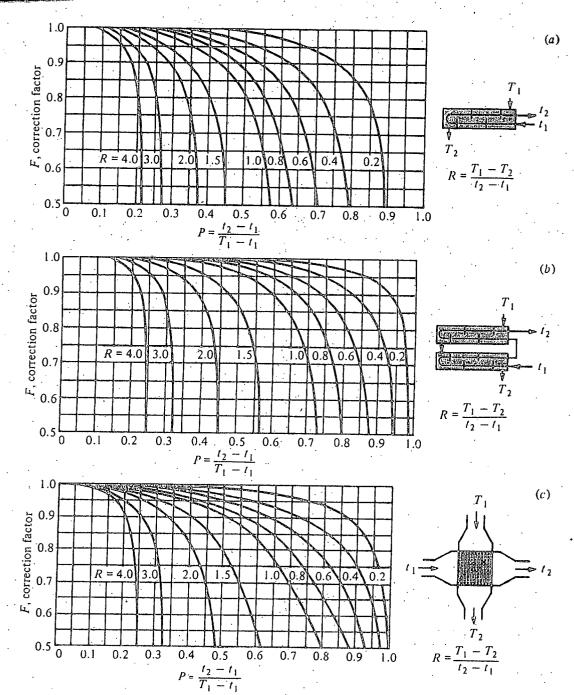


Figure 11-16 Correction factor F for computing  $\Delta T_{\rm corrected}$  for multipass and cross-flow exchangers. (a) One shell pass and two tube pass or multiple of two tube pass; (b) two shell pass and four tube pass or multiple of four tube pass; (c) single-pass, cross-flow, both fluids unmixed. (From Bowman, Mueller, and Nagle [45].)

$$h_m = 0.943 \left[ \frac{g\rho_l(\rho_l - \rho_v)h_{fg}k_l^3}{\mu_l(T_v - T_w)L} \right]^{1/4}$$

$$h_m = 0.725 \left[ \frac{g\rho_l(\rho_l - \rho_v)h_{fg}k_l^3}{\mu_l(T_v - T_w)D} \right]^{1/4}$$

L-3/T-2/ME

# BANGLADESH UNIVERSITY OF ENGINEERING AND TECHNOLOGY, DHAKA

L-3/T-2 B. Sc. Engineering Examinations 2014-2015

Sub: ME 323 (Fluid Mechanics II)

Full Marks: 210

Time: 3 Hours

Date: 01/08/2016

(20)

(10)

USE SEPARATE SCRIPTS FOR EACH SECTION

# **SECTION - A**

There are FOUR questions in this section. Answer any THREE.

The figures in the margin indicate full marks.

Moody diagram and Isentropic Flow Table are attached.

- 1. (a) Distinguish between Couette flow and Poiseuille flow. (5)
  - (b) Derive the velocity distribution in a laminar flow between two parallel plates, with the upper plate moving with velocity U. List all assumptions used in the derivation. (15)
  - (c) Derive the expressions for pressure drop and friction factor as functions of average velocity in a laminar flow between two parallel stationary plates. (15)
- 2. (a) Explain the terms (i) apparent shear stress and (ii) eddy viscosity in a turbulent flow. (8)
  - (b) What is minor loss? Determine the flow rate through the pipe shown in Fig. Q2b. Loss coefficients are: Square edge entrance = 0.5, standard 4cm screwed elbow = 0.95.
  - (c) What is hydraulic radius? Water at 20°C is transported at 0.01 m/s velocity through a smooth horizontal conduit of 2 cm × 4 cm cross section. Determine the hydraulic radius and the Reynolds number for this flow. (7)
- 3. (a) Discuss the mechanism, conditions and adverse effects of flow separation. How can the flow separation be avoided? (10)
  - (b) Write short notes on: (i) Kármán vortex street and (ii) Stall condition of an airfoil. (10)
  - (c) Show that for an isentropic flow through a nozzle, the relationship between flow area and velocity depends on the Mach number of the flow. (15)
- 4. (a) What is shock wave? Show that the Mach numbers upstream and downstream of a normal shock wave are linked as (25)

$$M_2^2 = \frac{M_1^2 + \frac{2}{k-1}}{\frac{2k}{k-1}M_1^2 - 1}$$

Then establish the relations of upstream and downstream Mach numbers, pressures and temperatures across a normal shock wave if the fluid is air.

(b) A converging-diverging nozzle, with an exit area of  $40 \text{ cm}^2$  and a throat area of  $10 \text{ cm}^2$ , is attached to a reservoir with  $T = 20^{\circ}\text{C}$  and p = 400 kPa absolute. Determine the two exit pressures that result in M = 1 at the throat for an isentropic flow. Also, determine the associated exit temperatures and velocities and flow rates.

# SECTION - B

There are FOUR questions in this section. Answer any THREE.

The questions are of equal value. Assume reasonable data if necessary.

- 5. (a) With the help of diagrams explain the different types of similarities which may exist between a model and its prototype.
  - (b) A pipe of diameter 1.25 m is required to transport oil of specific gravity 0.85 and viscosity 3 Ns/m<sup>2</sup> at the rate of 2900 l/s. In order to model this flow, water is allowed to flow through a 150 mm diameter pipe having viscosity 1.1 Ns/m<sup>2</sup>. Find the velocity and rate of flow in the model pipe.
- 6. (a) Discuss the Reynolds number, Froude number and Euler number giving illustrations of their significance. Explain Buckingham  $\pi$ -theorem for dimensional analysis.
  - (b) The power P supplied by a centrifugal pump depends on volume flow rate of water Q, specific weight of water  $\gamma$  and head H. Using Buckingham  $\pi$ -theorem show that  $P = f(Q, \gamma, H)$ .
- 7. (a) What are the conditions of maximum velocity and maximum discharge through a circular open channel? Prove these conditions.
  - (b) Water is flowing through a trapezoidal open channel having side slope of 1 horizontal to 2 vertical and the bed slope is 1 in 1600. The area of flow is 45 m<sup>2</sup>. Find the dimensions of the channel and also the discharge if it is most economical. Take Chezy's constant C = 60.
- 8. (a) Explain boundary layer thickness. Derive the equations of displacement thickness and momentum thickness.
  - (b) What is flowing at the rate of  $0.20 \text{ m}^3/\text{s}$  through a circular open channel of 0.7 m diameter. Calculate the slope of the bed of the channel considering maximum velocity of flow. Take Chezy's constant C = 65.

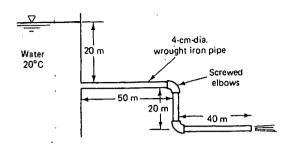


Figure for Q2b

Table 1: Isentropic Flow of a Perfect Gas, & = 1.4

M	$p/p_0$	$T/T_0$	AĴA*	M	$p/p_0$	<i>T/T</i> <sub>0</sub>	NA⁴
0.00	1,0000	1.0000	₩	2.10	0.1094	0.5313	1.8369
0.00	0.9930	0.9980	5.8218	2.20	0.0935	0.5081	2.0050
0.20	0.9725	0.9921	2.9635	2.30	0.0800	0.4859	2.1931
0.30	0.9395	0.9823	2.0351	2.40	0.0684	0.4647	2.4031
0.40	0.8956	0.9690	1.5901	2.50	0.0585	0.4444	2.6367
0.50	0.8430	0.9524	1,3398	2.60	0.0501	0.4252	2.8960
0,60	0.7840	0.9328	1.1882	2.70	0.0430	0.4068	3.1830
0.70	0.7209	0.9107	1.0944	2,80	0.0368	0.3894	3.5001
0.80	0.6560	0.8865	1.0382	2.90	0.0317	0.3729	3.8498
0,90	0.5913	0.8606	1,0089	3.00	0.0272	0.3571	4.2346
1.00	0.5283	0.8333	1.0000	3.10	0.0234	0.3422	4.6573
1.10	0.4684	0.8032	1,0079	3.20	0.0202	0.3281	5.1210
1,20	0.4124	0.7764	1.0304	3.30	0.0175	0.3147	5.6286
1,30	0.3609	0.7474	1,0663	23.40	0.0151	0.3019	6.1837
1.40	0.3142	Ö.7184	1.1149	3.50	0.0131	0.2899	6.7896
	0.2724	0.6897	1.1762	3.60	0.0114	0.2784	7.4501
1.50	0.2353	0.6614	1.2502	3.70	0.0099	0.2675	8.1691
1.60		0.6337	1.3376	3.80	0.0086	0.2572	8.9506
1.70	0.2026 0.1740	0.6068	1.4390	3.90	0.0075	0.2474	9.7990
1.80	0.1740	0.5807	1.5553	4.00	0.0066	0.2381	10.7188
1.90 2.00	0.1492	0.5556	1.6875	1.00			

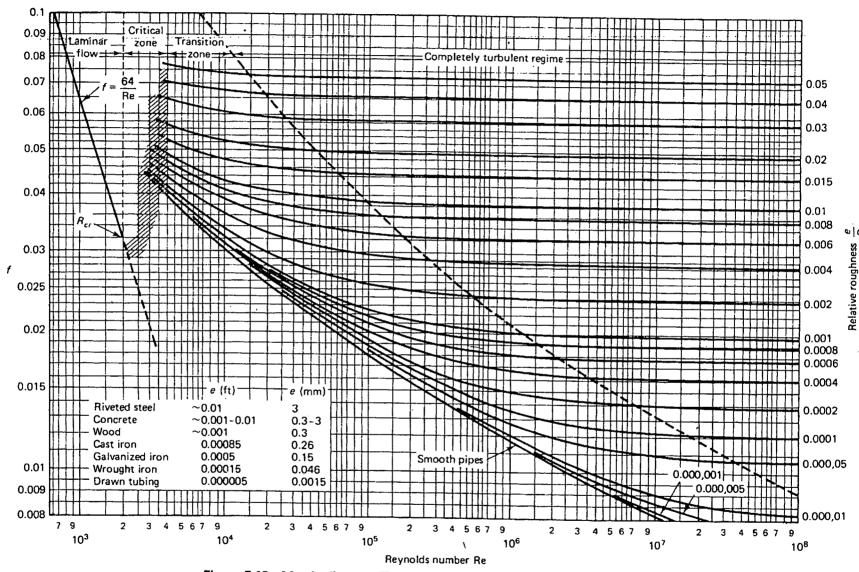


Figure 7.13 Moody diagram. (From L. F. Moody, Trans. ASME, Vol. 66, 1944.)